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General Electric Company
Albany, New York

Final (100%) Design Report for the OSD Remedy

Volume I of III

Fletcher's Paint Works and Storage Facility
Superfund Site - Operable Unit 1
Milford, New Hampshire

November 21, 2012

SDMS Doc ID 529093

DRAFT

FOR EPA REVIEW

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Fletcher's Paint Works and Storage Facility Superfund Site – Operable Unit 1
Milford, New Hampshire

Prepared for:
General Electric Company
Albany, New York

Prepared by:
ARCADIS of New York, Inc.
6723 Towpath Road
Syracuse
New York 13214-0066
Tel 315.446.9120
Fax 315.449.0017

Our Ref.:
B0020895

Date:
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Table of Contents

Abbreviations **i**

1. Introduction **1**

1.1 Background 1

1.2 Previous Remedial Design Activities 2

1.3 Purpose and Scope of Final Design Report for the OSD Soil Remedy 6

1.4 Site History and Description 7

1.4.1 Elm Street Area 8

1.4.2 Mill Street Area 9

1.4.3 Drainage Ditch/Culvert System 10

1.4.4 Summary of Site Characteristics 10

1.5 Description of AROD Remedy and Cleanup Standards 12

1.5.1 EPA's Description of the AROD Remedy 13

1.5.2 Performance Standards 16

1.5.2.1 Soil Cleanup Levels 16

1.5.2.2 Interim Cleanup Levels for Groundwater 20

1.6 Format of Document 22

1.7 Other Related Documents 24

1.8 Disclaimer 27

2. Site Investigation Activities and Results **28**

2.1 Introduction 28

2.2 Remedial Investigation 28

2.3 Pre-Design Investigation 29

2.4 Supplemental Design and Data Collection Activities 30

2.5 Physical Setting 36

2.5.1 Regional Geology 37

2.5.2 Site Topography 37

2.5.3 Subsurface Conditions – Elm Street Area 37

2.5.4 Subsurface Conditions – Mill Street Area 38

2.6 Development of Limits of Excavation 39

2.6.1 Methodology for Developing the Limits of Excavation 39

2.6.2 Boundary Conditions and Risk Management Decisions Impacting the Development of the Limits of Excavation 41

2.6.3 Estimates of the Volume of Material Subject to Excavation 45

3. Site Preparation Activities 48

3.1 Overview 48

3.2 Performance of Accelerated Remedial Action Items 49

3.3 Remedial Action Contractor Procurement 52

3.4 Site Controls, Site Access, and Alternate Residential Access 53

3.4.1 Elm Street Area 55

3.4.2 Keyes Park 56

3.4.3 Mill Street Area 57

3.5 Substantive Requirements of Regulations Imposing Permitting Requirements 58

3.6 Identification and Establishment of Exclusion Zones, Contaminant Reduction Zones, and Support Zones 58

3.6.1 Exclusion Zones 58

3.6.2 Contaminant Reduction Zones 59

3.6.3 Support Zone 60

3.6.4 Establishment of Zones and Management of Access 60

3.7 Utility Services 61

3.7.1 Relocation of Overhead Utilities 62

3.7.2 Replacement Storm Sewer Utility 63

3.8 Erosion and Sedimentation Controls 66

3.9 Site Clearing Activities 67

3.10 Protection/Decommissioning of Groundwater Monitoring Wells, Pumping Wells, and Temporary Piezometers 68

3.11 Clean Materials/Equipment Staging Area 70

3.12 Temporary Staging/Vehicle Loading Areas for Excavated Soils 70

3.13 Decontamination Area(s) 72

3.14 Traffic Control 73

4. Implementation of Remedial Action 76

4.1 Overview 76

4.2 Installation of Engineering Controls 76

4.2.1 Elm Street Area Excavations 78

4.2.2 Mill Street Area Excavations 80

4.3 Relocation of Sand Cap at the Elm Street Area 83

4.4 Design of Mill Street Area Excavation Dewatering Systems 83

4.4.1 Dewatering of SPTC Cells 84

4.4.2 Dewatering of Shallow Water Table Excavations 85

4.5 Design Overview and Staging/Construction of Temporary Water Treatment System and Ancillary Equipment 86

4.5.1 Objective of Temporary Water Treatment System 87

4.5.2 Influent Characteristics 87

4.5.3 Design Overview of Temporary Water Treatment System 89

4.5.4 Staging/Construction of Temporary Water Treatment System and Ancillary Equipment 93

4.6 Temporary Water Treatment System Performance Testing 93

4.7 Performance/Sequencing of the Remedial Action 94

4.7.1 Full-Scale Operation of Temporary Water Treatment System 96

4.7.2 Full-Scale Dewatering Activities at the Mill Street Area 97

4.7.3 Excavation of Phase 1 Impacted Materials at the Elm and Mill Street Areas 98

4.7.3.1 Phase 1 Excavation - Elm Street Area 98

4.7.3.2 Phase 1 Excavation - Mill Street Area 101

4.7.4 Excavation of Phase 2 Impacted Materials at the Elm and Mill Street Areas 102

4.7.4.1 Phase 2 Excavation - Elm Street Area 102

4.7.4.2 Phase 2 Excavation - Mill Street Area 103

4.7.5 Management of Temporary Staging/Material Handling Areas 104

4.7.6 Loading of Vehicles for Transportation of Excavated Materials to Off-Site Disposal Facilities 105

4.7.7 Verification of Limits of Excavation 106

4.8 Waste Management and Off-Site Disposal of Excavated Materials, Process Residuals and Other Miscellaneous Materials 107

4.8.1 Management of Excavated Materials and Other Project-Related Waste 107

4.8.2 Waste Characterization, Transportation, and Disposition of Residuals 109

5. Site Restoration 112

5.1 Overview 112

5.2 Backfilling of Excavations 112

5.3 Protection and Restoration of Utilities 114

5.4 Restoration of Final Surfaces 116

5.5 Groundwater Monitoring Well Replacement/New Well Installation 119

5.6 Equipment/Materials Cleaning and Demobilization 121

5.7 Post-Construction Monitoring Activities and Site Control 121

6. Groundwater Monitoring Zone 124

7. Evaluation of Applicable or Relevant and Appropriate Requirements (ARARs) 125

8. Technical Drawings and Specifications 126

8.1 Technical Drawings 126

8.2 Technical Specifications 131

9. Remedy Implementation Construction Cost Estimate and Schedule 134

9.1 Remedy Implementation Construction Cost 134

9.2 Remedy Implementation Construction Schedule 134

10. Future Activities and Schedule 135

10.1 Future Remedial Design Activities and Schedule 135

10.2 Future Remedial Action Activities and Schedule 135

Tables

1 Historic PCB Soil Sample Data

2 Summary of PDI PCB Sample Data – Elm Street Area Surface Soils

3 Summary of PDI PCB Sample Data – Elm Street Area Subsurface Soils

4 Summary of PDI PCB Sample Data – Mill Street Area Surface Soils

5 Summary of PDI PCB Sample Data – Mill Street Area Subsurface Soils

6 Summary of Pre-Construction Verification PCB Soil Sample Data – Elm Street Area

7 Summary of Soil Characterization Sample Data

8 Elm Street Area Exceedances of 1 mg/kg Surface SCL Not Addressed by Limits of Soil Removal

9 Mill Street Area Exceedances of 1 mg/kg SCLs Not Fully Addressed When Using Backhoe for Guide Walls of SPTC Wall and Focused Excavation Performed North of SPTC Wall, or Otherwise Already Approved by USEPA

10 Estimated Volume of Material Subject to Remedial Action to Achieve Non-Corridor SCLs

11 Additional Soil Removal Required for Replacement Storm Sewer, Cover System, Storm Water Retention Area, and Gabion Wall

12 Estimated Total Volume of Material Subject to Remedial Action

13 Groundwater Elevation Monitoring Data

14 UST Characterization Data – Wastewater

15 UST Characterization Data – Non-Wastewater

16 Summary of Existing Well Construction

17 Chemical-specific ARARs

18 Action-specific ARARs

19 Location-specific ARARs

Figures

1 Site Location Map

2 Elm Street Area – Existing Utilities and Historic Sampling Locations

3 Mill Street Area – Existing Utilities and Historic Sampling Locations

4 Elm Street Area – Soil Sampling Locations and Surface Soil PCB Sample Data

5 Elm Street Area – Subsurface Soil PCB Sample Data

6 Mill Street Area – Soil Sampling Locations and Surface Soil PCB Sample Data

7 Mill Street Area – Subsurface Soil PCB Sample Data

8 Elm Street Area – Utility Corridor Locations

9 Elm Street Area – Soil Removal Limits to Achieve Non-Corridor SCLs

10 Elm Street Area – Additional Soil Removal Required for Replacement Storm Sewer, Cover System, Storm Water Retention Area, and Gabion Wall

11 Elm Street Area – Combined Limits of Excavation

12 Mill Street Area – Excavation Limits and SPTC Wall Configuration

13 Mill Street Area – Focused Excavation Details

14 Elm Street Area – Monitoring Wells Subject to Decommissioning/Protection/Installation/Replacement

15 Mill Street Area – Monitoring Wells Subject to Decommissioning/Installation/Replacement

Appendices

A Verification Sampling Plan

B Technical Drawings

C Technical Specifications

D OSD Staging Scenario

E Truck Route and Traffic Analysis Report

F Design Calculations

G Project Construction Schedule

H Construction Quality Assurance Plan

I Contingency Plan

Abbreviations

AMSL	Above mean sea level
ARAI	Accelerated Remedial Action item
ARAR	Applicable or relevant and appropriate requirement
AROD	Amended Record of Decision
bgs	Below ground surface
CERCLA	Comprehensive Environmental Response, Compensation, and Liability Act
CLP	Contract Laboratory Program
COCs	Constituents of concern
CP	Contingency Plan
CQAP	Construction Quality Assurance Plan
CRSP	Community Relations Support Plan
CRZ	Contaminant reduction zone
CSM	Conceptual site model
cy	Cubic yards
DNAPL	Dense non-aqueous phase liquid
EMP	Environmental Monitoring Plan
EPA	United States Environmental Protection Agency
ESD	Explanation of Significant Differences

EZ	Exclusion zone
Final Design Report: Final (100%) Design Report for the OSD Remedy	
FSP	Field Sampling Plan
GAC	Granular activated carbon
GE	General Electric Company
GMZ	Groundwater Management Zone
gpm	Gallons per minute
Guilford	Guilford Transportation Industries, Inc.
HASP	Site Health and Safety Plan
HDPE	High-density polyethylene
IC/AR Plan	Institutional Controls/Access Restrictions Plan
ICL	Interim cleanup level
Intermediate LTTD Design Report: Intermediate (60%) Design Report for the LTTD Remedy	
Intermediate OSD Design Report: Intermediate (60%) Design Report for the OSD Remedy	
LMP	Long-term Maintenance Plan
LTTD	Low temperature thermal desorption
mg/kg:	Milligrams per kilogram (parts per million [ppm])
mg/L	Milligrams per liter (ppm)
µg/L	Micrograms per liter (ppb)

MMF	Multi-media filter
NHDES	New Hampshire Department of Environmental Services
NHDHHS	New Hampshire Department of Health and Human Services
O&M Plan	Operation and Maintenance Plan
OSD	Off-site disposal
OSHA	Occupational Safety and Health Administration
OU-1	Operable Unit 1
OU-2	Operable Unit 2
OWS	Oil/water separator
PAHs	Polycyclic aromatic hydrocarbons
PCBs	Polychlorinated biphenyls
PDI	Pre-Design Investigation
PD Report	Pre-Design Report
PD Work Plan	Pre-Design Work Plan
POP	Project Operations Plan
ppb	Parts per billion
PPE	Personal protective equipment
ppm	Parts per million
PQL	Practical quantification limit

Preliminary Design Report: Preliminary (30%) Design Report for the LTTD Remedy

Preliminary Traffic Report: Truck Route and Traffic Analysis Preliminary Report	
QAPP	Quality Assurance Project Plan
RAWP	Remedial Action Work Plan
RCRA	Resource Conservation and Recovery Act
RD/RA	Remedial design/remedial action
RD Work Plan	Remedial Design Work Plan
RI	Remedial investigation
RI Report	Final Remedial Investigation for the Fletcher's Paint Site
ROD	Record of Decision
SAP	Sampling and Analysis Plan
SCL	Soil cleanup level
SDDC	Supplemental design data collection
Site	Fletcher's Paint Works and Storage Facility Superfund Site
SMP	Site Management Plan
SOW	RD/RA Statement of Work
SPTC	Soldier pile tremie concrete
SVOCs	Semi-volatile organic compounds
SZ	Support zone
Town	Town of Milford
TR/TA Report	Truck Route and Traffic Analysis Report

TSCA	Toxic Substances Control Act
TSOW	Technical Scope of Work
TSS	Total Suspended Solids
UAO	Unilateral Administrative Order
UFPO	Underground Facilities Protection Organization
URS	URS Consultants
USACE	United States Army Corps of Engineers
UST	Underground storage tank
VOCs	Volatile organic compounds
VSP	Verification Sampling Plan
WMP	Surface Water and Groundwater Monitoring Plan (also known as the Water Monitoring Plan)
WMR	Water Monitoring Report
WMI	Waste Management, Inc.

1. Introduction

1.1 Background

On December 31, 2007, the General Electric Company (GE) submitted to the United States Environmental Protection Agency (EPA) a *Final (100%) Design Report for the OSD Remedy* (Final Design Report) for Operable Unit 1 (OU-1) of the Fletcher's Paint Works and Storage Facility Superfund Site (Site) located in Milford, New Hampshire. That document was submitted pursuant to a Unilateral Administrative Order (UAO) issued by the United State Environmental Protection Agency (EPA) to GE on July 16, 2001, as modified by the EPA on August 15, 2001. That UAO required GE to conduct pre-design, remedial design, and remedial action activities (collectively referred to herein as "RD/RA activities") necessary to implement EPA's selected remedy for the Site, as described in EPA's: (1) Record of Decision (ROD) for OU-1 dated September 30, 1998; (2) Explanation of Significant Differences (ESD) dated March 14, 2001; and (3) the RD/RA Statement of Work (SOW) for OU-1 (which is Attachment C to the UAO, as modified). That UAO also governed the performance of such RD/RA activities to address polychlorinated biphenyls (PCBs) and other hazardous substances found by the EPA in soil, sediment, groundwater, and/or surface water at OU-1. The Final Design Report was also submitted in accordance with EPA's November 1, 2007 letter that provided comments on GE's June 4, 2007 *Intermediate (60%) Design Report for the LTTD Remedy* (Intermediate [60%] LTTD Design Report) and GE's June 12, 2007 *Intermediate (60%) Design Report for the OSD Remedy* (Intermediate [60%] OSD Design Report).

Subsequent to submittal of the December 2007 Final Design Report, EPA issued a *Proposed Plan* on June 3, 2008 for changing the source control component of the OU-1 soils remedy from Low Temperature Thermal Desorption (LTTD) to Off-Site Disposal (OSD). Much of the information provided in EPA's Proposed Plan was based on information provided in GE's June 12, 2007 *Remedy Comparison Document* (as revised on September 21, 2007). A public information meeting was held on June 17, 2008 and a public hearing was held on July 8, 2008 to present EPA's Proposed Plan to the public and to receive public comments on that plan. GE provided comments on EPA's Proposed Plan during the public comment period in a letter to EPA dated August 18, 2008. EPA subsequently prepared and released an Amended Record of Decision (AROD) on June 15, 2009 changing the previous LTTD remedy specified in the 1998 ROD to an OSD remedy. On June 11, 2010, EPA issued the *Second Modification to Administrative Order and Statement of Work* (Second UAO Modification) incorporating the change in site remedy. Finally, EPA issued a second ESD related to Interim Cleanup Levels (ICLs) for Site groundwater on September 30, 2010.

As further documented in Section 1.2, GE made several design-related submittals subsequent to the submittal of the December 2007 Final Design Report. EPA provided approval with modifications to the December 2007 Final Design Report (as amended) in a letter to GE dated September 30, 2011. As requested in that letter, representatives of EPA, the United States Army Corps of Engineers (USACE), New Hampshire Department of Environmental Services (NHDES) and GE met on November 8, 2011 to discuss EPA's September 30, 2011 letter and other topics related to revising/resubmitting the Final Design Report and the initiation of the Remedial Action phase of the OSD remedy. During that meeting, it was agreed that GE would provide: (1) a listing of certain elements of the Remedial Design that could be performed prior to the full-scale implementation of the OSD remedy; a work plan to address data gaps identified in the draft Constructability Review Report; and (3) an updated Remedial Design Schedule for OU-1. GE submitted each of these items to EPA on December 22, 2011. Additional details regarding each of these submittals (including applicable revisions) are provided in subsequent sections of this report. This revised *Final (100%) Design Report for the OSD Remedy* (revised Final Design Report) was prepared in response to EPA's September 30, 2011 comments on the December 31, 2007 Final Design Report and incorporates the various Remedial Design submittals provided since submittal of that report, as well as the results of the supplemental design data collection (SDDC) activities performed at the Site between May and October 2012.

GE notified the EPA by letter dated August 27, 2001, that it would perform pre-design, remedial design, and related activities at the Site in accordance with the UAO (as modified), and GE reserved its rights with respect to all other aspects of the UAO. In accordance with EPA's November 1, 2007 letter, GE is submitting this revised Final Design Report. However, in so doing, GE does not waive or modify in any way the reservation of rights set forth in its August 27, 2001 letter, or GE's assertions in its July 30, 2007 correspondence responding to EPA's June 20, 2007 "approval with modifications" letter.

1.2 Previous Remedial Design Activities

This revised Final Design Report is based on the results of prior investigations at the Site, specifically the remedial investigation (RI) performed by EPA between 1992 and 1994, the pre-design investigation (PDI) and supplemental investigations performed during the remedial design phase of the project by GE under the UAO. EPA's RI is documented in the *Final Remedial Investigation for the Fletcher's Paint Site* (RI Report) (A.D. Little, 1994). GE's PDI is documented in the revised *Pre-Design Report* (PD Report) submitted to the EPA on January 14, 2005. The PD Report was approved by the EPA, with modifications, in a letter dated March 31, 2005. (As requested in a subsequent letter from EPA dated April 14, 2005, GE submitted a red-line/strike-out version of a revised PD Report on May 23,

2005 which incorporated EPA's modifications. EPA provided comments on the re-line/strike-out version of the PD Report in a letter to GE dated March 11, 2009. GE submitted a revised Pre-Design Report addressing EPA's comments (as well as making certain other corrections) on April 2, 2009.

Pursuant to the UAO, GE also submitted a *Remedial Design Work Plan* (RD Work Plan) to the EPA on April 28, 2005. The RD Work Plan, which was approved (in part) with modifications by the EPA in a letter dated August 18, 2005, described the major tasks and deliverables associated with the remedial design for the OU-1 remedy.

On November 30, 2005, GE submitted the Preliminary Design Report, as specified by the EPA in its ROD for OU-1. On March 27, 2006, the EPA issued a disapproval letter for the Preliminary Design Report, and provided comments on several aspects of the Preliminary Design Report. In response to that letter, GE made several subsequent submittals for the preliminary design, most of which were in response to EPA and Town comments on the Preliminary Design Report and/or based on discussions with EPA regarding certain aspects of the preliminary design, including:

- *Preliminary (30%) Design Report Addendum No. 1* (Addendum No. 1) submitted to the EPA on May 11, 2006;
- A letter from GE to the EPA dated June 1, 2006 regarding the engineered cover system for the Elm Street Area (this is described in Sections 5.2 and 5.4);
- A letter from GE to the EPA dated August 17, 2006 regarding confirmation sampling and the cover system for the Elm Street Area;
- A letter from GE to the EPA dated November 2, 2006 regarding revisions to two figures and one table associated with the Preliminary Design Report;
- A letter from GE to the EPA dated December 22, 2006 regarding revisions to two figures associated with the engineered cover system for the Elm Street Area;
- A letter from GE to the EPA dated January 12, 2007 regarding revisions to two figures associated with the limits of excavation presented for the Elm Street Area in the Preliminary Design Report (as amended);
- A letter from GE to the EPA dated January 26, 2007 regarding the engineered cover system for the Elm Street Area, in partial response to comments provided in a Town letter dated January 4, 2007;

- A letter from GE to the EPA dated January 30, 2007 regarding the utility corridors for the Elm Street Area, in partial response to comments provided in a Town letter dated January 4, 2007;

- A letter from GE to the EPA dated February 28, 2007 regarding the engineered cover system, utility corridors and tree planting corridors for the Elm Street Area;

- A letter from GE to the EPA dated March 27, 2007 regarding revisions to four figures associated with the cover system, utility corridors and tree planting corridors for the Elm Street Area;

- A letter from GE to the EPA dated March 30, 2007 regarding the excavation limits for the Mill Street Area (this is described in Section 2.6);

- A letter from GE to the EPA dated April 19, 2007 regarding modification of the ESD;

- A letter from GE to the EPA dated May 2, 2007 regarding the cover system, utility corridors and tree planting corridors for the Elm Street Area;

- A letter from GE to the EPA dated May 10, 2007 regarding the excavation limits for the Mill Street Area; and,

- A letter from GE to the EPA dated May 18, 2007 regarding the engineered cover system, utility corridors and other site restoration issues associated with the Elm Street Area, in response to comments provided in a Town letter dated March 30, 2007.

EPA provided approval with modifications for certain of the above-listed submittals in two letters to GE. Specifically, a February 13, 2007 letter to GE provided approval with modifications for the confirmation sampling included in the Preliminary Design Report, as modified by GE's August 17, 2006 submittal. That letter also provided comments related to the excavation limits at and near the Mill Street Area. A February 27, 2007 letter to GE provided approval with modifications for the cover system and utility corridors at the Elm Street Area included in the Preliminary Design Report, as modified by GE's August 17 and December 22, 2006 submittals.

In an April 5, 2007 letter, the EPA subsequently provided approval with modifications for the entire Preliminary Design Report, as modified by Addendum No. 1 "and the numerous design components which have been further modified through recent submissions relative to the cap/cover, utility plans and confirmation sampling". In its letter, EPA directed GE to

proceed with preparation of the 60% design submittals described in Section 1.1. Since that time, GE has made the following submittals associated with the Remedial Design:

- Intermediate (60%) LTTD Design Report;
- Intermediate (60%) OSD Design Report;
- Remedy Comparison Document;
- Final (100%) Design Report for the OSD Remedy;
- A letter from GE to the EPA dated October 14, 2008 providing alternate access/parking area design details for Keyes Park;
- A letter from GE to the EPA dated October 30, 2008 identifying the former Milford Police Department property as the primary truck staging area and providing revised elements of the Truck Route and Traffic Analysis (TR/TA) Report (Appendix E of the Final Design Report);
- A letter from GE to the EPA dated June 22, 2009 providing additional revisions to the TR/TA Report;
- A letter from GE to the EPA dated August 13, 2009 providing additional revisions to the TR/TA Report;
- A letter from GE to the EPA dated November 2, 2009 providing alternate access design details for Tax Parcel 25-11;
- A letter from GE to the EPA dated April 21, 2010 providing alternate access design details for certain residential properties adjacent to the Mill Street Area;
- A letter from GE to the EPA dated September 13, 2010 providing a revision to the seasonal low water table elevation for a portion of the Elm Street Area;
- A letter from GE to the EPA dated October 21, 2010 providing revised elements of the gabion wall design for the Elm Street Area;
- A letter from GE to the EPA dated October 28, 2010 regarding the Town of Milford's revised plans for the restoration of the Elm Street Area;

- A letter from GE to the EPA dated October 29, 2010 providing modifications to the support of excavation design associated with the replacement storm sewer at the Elm Street Area;

- A letter from GE to the EPA dated November 18, 2010 providing design details for the relocation of the overhead utilities along Mill Street and Keyes Drive;

- A letter from GE to the EPA dated December 2, 2010 providing revised alternate access design details for certain residential properties adjacent to the Mill Street Area;

- A letter from GE to the EPA dated January 19, 2011 providing several revised elements of the Final Design Report associated with the revision to the seasonal low water table in the vicinity of Excavation Cell V (now Excavation Cell W) at the Elm Street Area;

- Electronic mails from GE to the EPA dated May 2, 2011 providing revised hybrid cover system and utility corridor figures for the Elm Street Area;

- A Remedial Design schedule and associated table for OU-1 submitted to EPA on December 22, 2011, as revised in a letter from GE to EPA dated May 2, 2012;

- *Technical Scope of Work – Accelerated Remedial Action Items* (TSOW), July 12, 2012; and

- A letter from GE to the EPA dated August 27, 2012 providing responses to EPA Comments on the July 2012 TSOW.

As further described in Section 2.4, supplemental design investigation activities were performed between May and October 2012 to address data gaps identified in the draft Constructability Review Report on the December 2007 Final Design Report. The results of those investigations have also been incorporated into this revised Final Design Report.

1.3 Purpose and Scope of Final Design Report for the OSD Soil Remedy

The purpose of the Final Design Report is to describe the engineering design and approach for implementing the OSD soil remedy, which specifies the excavation and off-site disposal of impacted soils containing certain constituents of concern (COCs) at concentrations greater than the soil cleanup levels (SCLs) specified in the AROD. This revised Final Design Report has also been prepared to assist with competitively bidding the project and the selection of a Remedial Action Contractor to implement the remediation activities. The Remedial Action Contractor would implement the construction phase of the OU-1 soil

remedy after a Remedial Action Work Plan (RAWP) has been submitted to and approved by EPA.

1.4 Site History and Description

The Site is located within a mixed-use area consisting of residential and light commercial/industrial properties immediately west of the center of Milford, as shown on Figure 1. Since the 1800s, the Site has had many agricultural, commercial, and industrial uses, including serving as the Milford town dump for more than 20 years, from 1921 to 1947. From 1948 until 1991, Fletcher's Paint Works (also known as the Milford Paint Works) operated at the Site. Fletcher's Paint Works operations included the manufacture, storage, and distribution of water-based latex paints and organic-based solvent paints, with an annual production volume ranging between 25,000 to 35,000 gallons. Also, Fletcher's Paint Works purchased and resold industrial chemicals and other materials to other entities. Spills, leaks, manufacturing operations, and dust suppression activities led to the current contamination of the soils at the Site. As a result, PCBs and other contaminants were released to the environment and are found at concentrations in Site soils, sediments, and groundwater at levels that pose an unacceptable risk to human health and the environment. Additional details on the Site history and the characterization of the contamination at the Site can be found in the 1998 ROD and the 2009 PD Report.

According to the EPA, the areas that comprise OU-1 were identified based on a number of considerations, including geographic location, prior regulatory definition and status, scope and timing of response actions, current and reasonably foreseeable land use, and nature and extent of the affected media. OU-1 includes the Elm Street Area and Mill Street Area (now both owned by the Town) and private property in the vicinity of those parcels. The Souhegan River and Keyes Field (also known as Keyes Park) are part of Operable Unit 2 (OU-2), which is not subject to the RD/RA activities required by the UAO, as modified.

As discussed in Section 1.1, the EPA issued a UAO for the Site on July 16, 2001, as modified on August 15, 2001 and June 11, 2010, directing GE to conduct an RD/RA program associated with the ROD remedy to address PCBs and other hazardous substances detected by the EPA in soil, sediment, groundwater, and/or surface water during its RI. Excluding the area of impacted groundwater, OU-1 measures approximately 2 acres in size and generally consists of the following three areas:

- The former Fletcher's Paint Works site at 39 Elm Street, referred to herein as the Elm Street Area;

- The former Fletcher's Paint Works storage facility, on the north side of Mill Street, referred to herein as the Mill Street Area; and,

- A drainage ditch/culvert system that traverses in a northerly direction from the Mill Street Pond, past the Mill Street Area and through the Elm Street Area to the Souhegan River.

Additional information regarding each of these areas is provided in the following sections.

1.4.1 Elm Street Area

The Elm Street Area is approximately 1.6 acres and is located along the southern bank of the Souhegan River. This property is where Fletcher's Paint Works formerly conducted manufacturing and retail distribution activities in the Elm Street Area. As shown on Figure 2, the Elm Street Area is bounded by the Souhegan River to the north (a portion of the Elm Street Area is located within the 100-year floodplain), a Revolutionary War-era cemetery to the east, Elm Street (State Route 101A) to the south, and an access road for Keyes Field to the west.

Since the 1800s, when the Elm Street Area was reportedly used as agricultural farmland, all uses of the Elm Street Area have been commercial or industrial, including as hide storage for a tannery, a blacksmith and carriage painting shop, an armory, the town dump, and an automotive dealership. Most recently, after Fletcher's Paint Works ceased operation, a retail consignment shop was operated in a portion of the building formerly used by Fletcher's Paint Works. The consignment shop was closed in 2000 prior to demolition and removal of the building (as further discussed below).

Until recently, the structures at the Elm Street Area included a one-story brick and concrete block building (referenced above) with an approximate footprint of 24,500 square feet, a small parking area adjacent to Elm Street, and five underground storage tanks (USTs). Other structures present at the Elm Street Area include five discharge pipes extending from the southern riverbank, which are/were used to discharge storm water runoff from the town drainage system and/or from the former Fletcher Paint Works manufacturing facility.

Since 1998, four removal actions have been completed at the Elm Street Area, three by the EPA, and one by GE. The first removal action at the Elm Street Area occurred between May and October 1988, when the EPA staged 863 drums for subsequent waste characterization sampling and off-site disposal. The EPA also placed a cap (consisting of geotextile fabric and clean soil) over a portion of the Elm Street Area. The second removal action at the Elm Street Area was performed by the EPA between November and

December 1991, and consisted of removing laboratory containers in the building followed by the installation of a fence around the property. In 1993, the EPA performed a third removal action to characterize and dispose of several hundred containers of miscellaneous materials associated with the former Fletcher's Paint Works manufacturing activities at the Site. The cap at the Elm Street Area was also repaired and re-graded at that time. During the summer of 1996, GE voluntarily performed a fourth removal action, which consisted of excavation and off-site disposal of soils containing low levels of PCBs in the vicinity of the current Korean War Memorial (adjacent to the east side of the former one-story building and immediately south of the cemetery) (see Figure 2).

Between December 2000 and January 2001, EPA demolished and removed the one-story building at the Elm Street Area and removed the two USTs located under the sidewalk in front of the former building. The building slab was also broken up and disposed off-site. The granite block foundation of the building was left in place to help support the adjacent cemetery.

1.4.2 Mill Street Area

The Mill Street Area is approximately 0.25 acres and is located approximately 700 feet south of the Elm Street Area. The Mill Street Area is bounded to the north by an active railroad line (which includes a main line (i.e., the north line) and a siding (i.e., the south line which connects to the main line both east and west of the Mill Street Area), to the east by Cottage Street, to the south by Mill Street, and to the west by the former Draper Fuel Company (Draper) coal yard (Figure 3). A small storage shed and a building that housed a gristmill were formerly located at the Mill Street Area.

Historic operations at the Mill Street Area included grain storage in elevators and a gristmill. After these operations ceased, Fletcher's Paint Works used the buildings to store paint components.

Concurrent with several of the removal actions performed at the Elm Street Area (described in Section 1.4.1), removal actions were also performed at the Mill Street Area. During the 1988 removal action, the EPA placed a geotextile and clean soil cap at the Mill Street Area and removed bags of asbestos from a small storage shed formerly located at the Mill Street Area. During EPA's 1993 removal action, waste materials stored inside the Mill Street building were characterized and disposed off-site, the building was demolished, and the building demolition debris was characterized and sent off-site for disposal. During this removal action, the EPA also repaired the cap that was installed in 1988, installed additional cap materials over the footprint of the former storage building, and hydroseeded the property. In the summer of 1995, GE conducted an EPA-ordered removal action consisting

of the removal and off-site disposal of PCB-containing soils from three residential properties located south of the Mill Street Area. GE also installed a 10-foot wide paved apron along Mill Street to prevent degradation and wear of the cap, and graded and paved Mill Street to facilitate storm water runoff away from the residences and onto the Mill Street Area.

In addition to the removal actions specified above, GE performed some remedial activities associated with a small coal transfer building located on the Draper parcel adjacent to the Mill Street Area. That building was destroyed by fire in October 2001. In February 2002, the property owner removed the fire-related debris. Following this work, GE performed additional remedial work at the Site, including placement of a liner within the former truck-scale pit and backfilling the pit to surface grade with clean backfill, sampling and subsequent removal for off-site disposal of approximately 230 tons of surplus coal, and placement of a liner and a 1-foot thick clean soil cover over the former building footprint. This work was completed in February 2002.

1.4.3 Drainage Ditch/Culvert System

Beginning at the Mill Street Pond and traversing in a northerly direction to the Souhegan River is a drainage ditch/culvert system that is also considered part of the OU-1 portion of the Site. Seasonal and storm water flows are carried by the drainage ditch beneath Mill Street, past the Mill Street Area and the Draper coal yard, then along the eastern side of Hampshire Paper Company to a stone culvert located behind (i.e., immediately south of) the Snack Corner Mobil station. The culvert then carries the flow beneath Cottage and Elm Streets, then underneath the eastern portion of the Elm Street Area where it subsequently discharges into the Souhegan River.

1.4.4 Summary of Site Characteristics

The RI performed by the EPA identified impacts to soil, sediment, surface water, and groundwater resulting from historic operations at the Site. Based on the results of that RI and EPA's subsequent baseline human health risk assessment, the ROD established SCLs for certain constituents detected in OU-1 soils and ICLs for certain constituents in OU-1 groundwater, as further discussed in Section 1.5 below. The AROD remedy, as modified by the 1st ESD, requires soil removal to achieve the specified SCLs. For OU-1 groundwater, the AROD, as modified by the 2nd ESD, requires monitored natural attenuation following source control (i.e., the OU-1 soil remedy) until achievement of the specified ICLs for groundwater.

As a result, the PDI performed by GE under the UAO focused largely on the collection of additional soil sample data to provide sufficient information to design the OU-1 soil remedy.

As described in Section 2.3, this involved the collection of several hundred surface and subsurface soil samples from locations at or near the Elm and Mill Street Areas, which were collected mainly for the purpose of determining the presence and extent of soils containing PCBs in excess of the SCLs. Section 4 of the PD Report provided detailed discussions of the performance and the results of the soil sampling activities performed under the PDI. Section 2.4 of this report provides a description of the supplemental design data collection activities performed by GE subsequent to the performance of the PDI.

The results of the PDI and supplemental soil investigations have provided sufficient detail to design the OU-1 soil remedy. The PDI and supplemental soil sample data collected by GE were generally consistent with the levels observed by EPA during the RI. The incorporation of these data into the remedial design resulted in a slight increase (i.e., approximately 4.4%) in the volume of soil removal required to achieve the ROD-specified SCLs (approximately 30,175 cubic yards [cy] versus the 28,900 cy estimated in the ROD). In addition, approximately 4,100 cy of additional materials will require excavation. These materials, which are not subject to off-site disposal and will be used as on-site backfill, are associated with sloping of excavations to safely implement the Remedial Action and to install an engineered soil cover, replacement storm sewer, storm water retention area, and gabion retailing wall at the Elm Street Area. Therefore, the total volume of soil excavation contemplated by this revised Final Design Report is approximately 36,306 cy, or about 26% more than estimated by EPA in the ROD.

Although not the primary focus of the remedial design, the PDI included the installation of several additional groundwater monitoring wells at the Elm and Mill Street Areas. The PDI also included the performance of a comprehensive round of groundwater sampling in February 2004. As directed by EPA in a June 20, 2007 letter, GE submitted a revised *Surface Water and Groundwater Monitoring Plan* (also known as the Water Monitoring Plan [WMP]) to EPA on July 30, 2007. A revised version of the WMP was submitted to EPA on April 14, 2008. The WMP specifies the groundwater monitoring activities to be performed during the pre-design and remedial design phases of the project. (GE also submitted an *Environmental Monitoring Plan* [EMP] to EPA on July 30, 2007, as revised through GE's response on December 31, 2007 to EPA's groundwater-related comments dated November 1, 2007 and revised a second time on April 14, 2008. That document proposes the groundwater monitoring activities to be performed during the post-construction phase of the project.) Section 2.5 of the revised WMP (and also the EMP) provides a discussion of the groundwater data collected at the Site prior to the submittal date of those documents.

As also directed by EPA in its June 20, 2007 letter, groundwater monitoring under the revised WMP was initiated at the Site in July 2007. The scope of the groundwater monitoring activities during each quarterly monitoring event includes the collection of

groundwater elevation monitoring data, groundwater quality sampling, and, for certain events, the monitoring for the potential presence of dense non-aqueous phase liquids (DNAPL) in certain bedrock wells at the Mill Street Area. The results of the first quarterly monitoring event were presented in the *Water Monitoring Report* (WMR) that was submitted to EPA on October 16, 2007. To date, GE has performed 22 quarterly monitoring events under the WMP. The data for these events are provided in WMRs that are submitted to EPA approximately 90 days after the completion of each quarterly monitoring event. Each WMR provides a summary of the groundwater quality data from the previous investigation activities performed at the Site, as well as the data from the most recent monitoring event. Finally, as further described in Section 2.4, supplemental hydraulic testing activities (which included: the installation of temporary piezometers and monitoring wells; water level monitoring; pump testing; groundwater quality sampling; and the collection of DNAPL samples for chemical and physical analyses) were performed at the Site between May and July 2012. The data from those investigations were evaluated to determine the need for any revisions to the design of the OSD soil remedy. As such, those data have been incorporated into the design revisions presented herein, as appropriate; however, the detailed discussion of the supplemental hydraulic testing activities and the associated data will be provided in the forthcoming report on the SDDC activities that will be submitted subsequently to this revised Final Design Report.

In general, the groundwater elevation monitoring data collected to date support the seasonal low water table elevation identified in the December 2007 Final Design Report, as modified by: (1) GE's September 13, 2010 and January 19, 2011 letters to EPA; and (2) the July/August 2012 Water Monitoring Report. The groundwater data collected to date at the Site also support EPA's conclusion in the AROD that certain constituents are present in groundwater at the Site at levels above the specified ICLs. Finally, as further described in Section 2.4, the hydraulic testing activities performed at the Mill Street Area between May and July 2012 resulted in the observation of DNAPL in certain wells at the Mill Street Area and the collection of samples for physical and chemical analyses.

1.5 Description of AROD Remedy and Cleanup Standards

This section of the Final Design Report provides a brief summary of the remedial action selected in the AROD for OU-1, identifies the SCLs established by EPA for the Elm and Mill Street Areas, as modified by the 1st ESD, and also identifies the ICLs established by the EPA for OU-1 groundwater, as modified by the 2nd ESD. Additional details regarding the OU-1 remedy are provided in EPA's AROD, the 1st and 2nd ESD, and also the UAO and attached SOW (as modified).

1.5.1 EPA's Description of the AROD Remedy

The AROD and the Second Modification to the UAO include a description of the remedial action selected by the EPA for OU-1. In general, the EPA-specified remedy addresses the following media:

1. Surface (0- to 1-foot deep) soils at the Elm and Mill Street Areas;

2. Subsurface (greater than 1-foot deep) soils at the Elm and Mill Street Areas; and

3. Groundwater.

Restating from the AROD, the Second Modification to the UAO provides a summary of the OU-1 remedy. Applicable excerpts from those paragraphs are quoted below (in italics).

Paragraph 52 of the Second Modification to the UAO specifies the following for the Mill Street Area soils:

> *Excavation of surface soils (0 to 1 foot) at the Mill Street Area to a depth of 1 foot, wherever PCB concentrations are greater than 1 mg/kg PCB.*

Paragraph 53 of the Second Modification to the UAO also specifies the following for the Mill Street Area soils:

To address the future risks associated with ingestion of contaminated groundwater at the Mill Street Area as a result of leaching, the activities include:

a. Excavation of subsurface soils at the Mill Street area (1 foot to 20 feet [bedrock] below surface), wherever PCB concentrations remain that exceed 1 mg/kg PCB.

b. Water collected from the dewatering of the excavated soils and water collected as a result of lowering of the water table to conduct the excavation would be either treated on-site in a mobile unit and appropriately discharged to the Souhegan River or sent off-site to a treatment facility.

c. Backfilling of clean materials into the excavated areas to restore the property consistent with the anticipated future use of the Site. A portion of the Mill Street area would be paved, physically re-aligning Mill Street. The pavement would reduce infiltration of precipitation, control erosion, and promote drainage away residential properties.

d. *Off-site treatment/disposal of all excavated soil and debris. All contaminated soil and debris will be treated and/or disposed of in appropriate facilities/landfills in accordance with RCRA and TSCA disposal regulations.*

e. *Re-grading and repair of the storm drainage ditch system, as necessary, to promote surface water flow away from the Site. Erosion control measures shall be incorporated into the final drainage system to prevent erosion or debris from restricting future storm water flow from the Mill Street Area or filling in of the drainage ditch.*

Paragraph 54 of the UAO specifies the following for the Elm Street Area soils:

a. *Excavation of surface soils at the Elm Street Area to a depth of 1 foot, wherever PCB concentrations are greater than 1 mg/kg PCB.*

b. *Excavation of subsurface soils, within the utility corridor(s), at the Elm Street Area, wherever PCB concentrations are greater than 25 mg/kg PCB. Final location of the utility corridor(s) within the Elm Street Area will be determined during design.*

Additional language pertaining to the utility corridor(s) at the Elm Street Area is contained on page 14, Section III.B.5 of the SOW (as modified), which states:

> *At the Elm Street Area, the storm drainage system currently under the Fletcher's Paint Works building, is not accessible by town personnel since the system lies, in some places, 17 feet below the surface, and below areas of heavily contaminated soil. The drainage system channels contaminated groundwater directly to the Souhegan River during periods of high elevation of the groundwater. The Respondent shall decommission the old, existing drainage system and re-route a new drainage system within a utility corridor to be designed and constructed as part of the Work.*

Paragraph 55 of the UAO also specifies the following for the Elm Street Area soils:

To address the future risks associated with ingestion of contaminated groundwater at the Elm Street Area as a result of leaching, the activities include:

a. *Excavation of remaining subsurface soils to the seasonally low water table, wherever PCBs remain that exceed 100 mg/kg, including the excavation and off-site treatment and/or disposal in an appropriate facility or landfill of the "hot spot," a semi-solid stain (polyamide or polyurethane) material.*

b. *Removal and disposal of the three underground storage tanks located at the Fletcher's Elm Street Area.*

c. *Off-site treatment/disposal of all excavated soil and debris. All contaminated soil and debris will be treated and/or disposed of in appropriate facilities/landfills in accordance with RCRA and TSCA disposal regulations.*

d. *Final consolidation of site soils, backfilling with clean fill, grading, construction of an engineered, low permeability soil cover, restoration, and landscaping of the Site. The final cover would promote drainage, and further minimize infiltration through the residual contamination at the Site and be part of the final restoration and landscaping design. Erosion control measures will be incorporated into the final grading to prevent erosion of the cover materials off-site and into the Souhegan River.*

e. *Institutional controls would be implemented to prevent unauthorized access into the subsurface. Deed restrictions and/or notices would also have to be issued to restrict future use of the Site, or the modification of the cover or surface drainage structures in ways inconsistent with this remedy or the anticipated use of the Site.*

Paragraph 56 of the UAO specifies the following remedial action for OU-1 groundwater:

a. *Establish a Groundwater Management Zone (GMZ) under NH's Comprehensive Groundwater Policy. The GMZ sets plume boundaries within which groundwater will be monitored over time to ensure that the contaminate concentrations are decreasing; to ensure that the remaining contamination has not migrated beyond the established plume boundaries or impacted the Souhegan River; and that the remedial action cleanup is working and remaining effective over time. Institutional controls would have to be implemented to restrict the use of the groundwater within the GMZ, while contaminant concentrations are in excess of drinking water standards. Further action may be necessary consistent with the NH Comprehensive Groundwater Policy.*

b. *Intermediate Groundwater Cleanup Levels must be achieved within the GMZ and maintained for a period of three consecutive years. A risk assessment will be performed on residual groundwater contamination to determine protectiveness of the remedy. If EPA determines the remedy is not protective, the remedial action shall continue until protective levels are achieved and not exceeded for three years or until the remedy is deemed protective or is modified.*

A more complete description of the remedy is found in the ROD, ESD, AROD, and in the Statement of Work, as modified and attached hereto.

1.5.2 Performance Standards

The EPA has established performance standards for the OU-1 remedy, including SCLs and groundwater ICLs. Those SCLs and groundwater ICLs are summarized below.

1.5.2.1 Soil Cleanup Levels

EPA established SCLs for the OU-1 remedy in the ROD, as amended. Those SCLs are referenced in the table below:

EPA's Selected Soil Cleanup Levels

Area	SCLs (mg/kg)
SCLs for the Protection of Human Health from Dermal Contact and Accidental Ingestion	
Surface Soils: 0 to 1 Foot at Elm and Mill Street Areas:	
Benzo[a]anthracene	2.1[1]
Benzo[a]pyrene	0.2[1]
Benzo[b]fluoranthene[2]	2.0[1]
Total PCBs	1.0[3]
Arsenic	0.9[1]
Subsurface Soils: 1 to 10 Feet at Elm Street Area Utility Corridor(s):	
Total PCBs	25
Subsurface SCLs for the Prevention of Leaching to the Groundwater for the Protection of Human Health	
Elm Street Area: Total PCBs	100
Mill Street: Total PCBs	1[3]

Notes:

1. Excavation of surface soils containing concentrations of these constituents above the corresponding SCLs will occur only where co-located with soils containing total PCBs above the applicable SCL.
2. EPA's AROD and the Second Modification to the SOW identify benzo[a]fluoranthene as a soil cleanup constituent. No such compound exists. It has been assumed that this is a typographical error and that the intended constituent is benzo[b]fluoranthene.
3. As stated in EPA's March 31, 2005, April 19, 2005 and February 13, 2007 letters, certain areas with low-levels of total PCBs may not require excavation. Refer to Section 2.6 for additional details.
4. mg/kg = milligrams per kilogram (parts per million [ppm]).

Following issuance of the ROD, EPA made three clarifications to the SCLs specified therein. The first clarification related to the SCLs for non-PCB constituents in surface soils at the Elm and Mill Street Areas. GE previously expressed concern to the EPA regarding the SCLs for arsenic (which appeared to be lower than the established background level in New Hampshire) and benzo(a)pyrene (which was lower than the corresponding laboratory practical quantitation limit [PQL]). As a result, the EPA issued an ESD on March 14, 2001 allowing potential modifications to the SCLs for arsenic and other constituents in surface soils with "very low cleanup levels, such as…benzo(a)pyrene." Specifically, the ESD included the following language:

> *"If a cleanup value described in the ROD, is not capable of being detected with good precision and accuracy or is below background values, then either the practical quantification limit (PQL) or a background value will be used, as appropriate, for the soil cleanup level."*

GE's concern regarding the ROD-specified SCLs for arsenic and certain polycyclic aromatic hydrocarbons (PAHs) was recognized in the 1st ESD, with further clarification provided in a May 7, 2002 conference call between GE and EPA representatives. In addition, the EPA submitted a letter to the New Hampshire Department of Heath and Human Services (NHDHHS) on June 4, 2002 requesting a modification to the SCL for arsenic to 11 mg/kg based on state-wide background concentrations. The 1st ESD and May 7, 2002 conference call were referenced in EPA's May 1, 2003 comment letter, in which the EPA recognized that surface soils containing PAHs that exceed the specified SCLs would not require excavation once the total PCB concentrations meet the 1 mg/kg SCL in surface soils. The EPA further clarified this statement in a May 13, 2003 conference call, where the agency stated that excavation of surface soils containing arsenic which exceed the specified SCLs would not require excavation once the total PCB concentrations meet the specified SCL of 1 mg/kg in surface soils. GE submitted a letter to EPA on April 19, 2007 which requested that EPA modify the 1st ESD to reflect its intent with respect to the cleanup of PAHs and arsenic in surface soils. Specifically, that letter requested that the EPA modify the 1st ESD to reflect its intent that excavation to address arsenic, benzo(a)pyrene, benzo(a)anthracene, and benzo(b)fluoranthene in surface soils would only be required where excavation was required to achieve the surface soil SCL of 1 mg/kg for total PCBs.

In Comment #7 of the September 30, 2011 letter providing comments on the December 2007 Final Design Report, EPA indicated that an ESD is not required "to address GE's concerns that the arsenic and PAHs in surface soils would need to be addressed beyond areas where PCBs exceed 1 mg/kg." EPA based this determination on certain language provided in the 2009 AROD and AROD Responsiveness Summary. However, the UAO (as modified) purports to require GE to certify the achievement of all of the Performance

Standards and SCLs specified in the ROD, as amended. There is no exemption to this requirement for surface soils containing arsenic and PAHs at concentrations exceeding the applicable SCLs that are not co-located with surface soils containing PCBs at concentrations exceeding the applicable SCL. Specifically, Section IX.C, Paragraph 99 of the UAO (as modified) requires that GE provide certification "…that the Performance Standards and cleanup levels for Site soils ha[ve] been met in full satisfaction of the requirements of this Order." Paragraph VI.J.3 of the SOW (as modified) also requires that the Final Remedial Construction Report include "[d]ocumentation that the Performance Standards have been met for the Site soils including, but not limited to: sampling locations and procedures to confirm excavation of all soils contaminated above cleanup levels". As a result, GE maintains their request that EPA modify the UAO/SOW or ESD to be consistent with EPA's intention to eliminate the requirement to address surface soils containing arsenic and PAHs at concentrations above the applicable SCLs that are not co-located with PCBs greater than the applicable SCL of 1 mg/kg.

The second clarification related to observed total PCB concentrations in subsurface soils located west of Keyes Drive. Specifically, EPA's March 31, 2004 conditional approval letter for GE's March 17, 2004 supplemental sampling proposal required GE to collect subsurface soil samples at location ESSB-H03 west of Keyes Drive (adjacent to the Elm Street Area) and compare the results of those samples to a subsurface SCL of 1 mg/kg. GE's April 12, 2004 response to comment letter requested clarification regarding the subsurface SCL in the vicinity of the Elm Street Area. At the April 15, 2004 weekly status meeting (held during the pre-design investigation), the EPA clarified its comment by indicating that soils west of Keyes Drive are not considered part of the Elm Street Area and, therefore, the SCL of 1 mg/kg is applicable for subsurface soils west of Keyes Drive.

The third clarification to the SCLs specified in the ROD related to observed PCB concentrations in subsurface soils at sampling location MSSB-C01 at the Mill Street Area. Specifically, following performance of the PDI activities presented in the November 2003 *Pre-Design Work Plan* (PD Work Plan), GE submitted a document titled *Proposed Supplemental Pre-Design Delineation Soil Sampling Activities* on March 17, 2004. On March 25, 2004, representatives of the EPA, USACE, and GE met to review the scope of the supplemental soil investigation proposed by GE. Based on discussions during that meeting, subsequent correspondence between the EPA and GE, and as documented in EPA's March 31, 2005 approval letter for the PD Report, the EPA indicated that the observed concentrations of total PCBs at sampling location MSSB-C01 were consistent with the EPA's Spill Policy (40 CFR 761.125) for commercial areas and, therefore, that those soils would not be subject to the 1 mg/kg SCL specified for total PCBs in the surface and subsurface soils at the Mill Street Area.

GE and EPA have had extensive discussions regarding a fourth clarification to the subsurface SCLs for certain soils at the Mill Street Area. Specifically, Section 2.6 of the Preliminary Design Report indicated that risk management decisions similar to that made by EPA regarding sampling location MSSB-C01 would be appropriate, given sufficient technical justification, to certain other soil sampling locations at or near the Mill Street Area (e.g., in the vicinity of the railroad tracks immediately north of the Mill Street Area). To that end, EPA's February 13, 2007 approval with modifications letter for the confirmation sampling portion of the Preliminary Design Report (as modified by GE's August 17, 2006 submittal) concurred with the basis for the risk management decisions proposed by GE to not remove certain subsurface soil samples at sampling locations MSSB-B12, -B13, -B17, -C14, -C15, and -C17. GE made a subsequent submittal to EPA on March 30, 2007 providing technical justification in support of risk management decisions for these and other samples containing total PCBs in excess of the 1 mg/kg PCB SCLs for the Mill Street Area. GE supplemented its March 30, 2007 submittal in a May 10, 2007 letter.

Comment #14 of EPA's September 30, 2011 letter to GE providing comments on the December 2007 Final Design Report indicated that, with the exception of four specific sampling locations, EPA accepted the proposal as outlined in GE's March 30, 2007 letter to EPA. GE acknowledges the comment that "EPA can accept GE's proposal to not excavate the significant, additional volume of soil" that would be necessary to address soil known to contain PCB concentrations greater than the SCL that are outside the limits of soil removal specified herein. However, the very paragraphs of the UAO cited by EPA in support of this comment undermine EPA's intention. Specifically, Paragraph 96 of the UAO (as modified) states, that: "[n]othing in the Order, or in EPA's approval of the Statement of Work, or in the Remedial Design or Remedial Action Work Plans, or approval of any other submission, shall be deemed to constitute a warranty or representation of any kind by EPA that full performance of the Remedial Design or Remedial Action will achieve the Performance Standards set forth in the ROD, ESD and in Section IV (Performance Standards) of the Statement of Work. Respondent's compliance with such approved documents does not foreclose EPA from seeking additional Work to achieve the applicable performance standards."

Contrary to EPA's suggestion in Comment #14, the maximum contaminant level for PCBs in groundwater is not the only Performance Standard subject to this provision of the UAO (as modified). Removal of all "surface soils" at the Mill Street and Elm Street Areas and all "subsurface soils" at the Mill Street Area that contain PCBs at a concentration greater than the applicable Performance Standards or SCLs of 1 mg/kg, is also a requirement of the ROD (as amended) and UAO/SOW (as modified). (*See, e.g.,* AROD, pages 30-32 and 45 [Table 5]; the Second Modification to the UAO, pages 21 and 22, 25, and 32; and the Second Modification to the SOW, pages 4 - 8, 10 - 11, 19, and 23 – 26). Long before each

of these documents was last modified, EPA's March 31, 2005 and February 13, 2007 letters to GE approved limits of excavation that would not achieve the 1 mg/kg SCLs at certain sampling locations. As indicated in Comments #7 and #14, EPA provided those approvals because it recognized that completely achieving the SCLs "could decrease the short term effectiveness" of the remedy and "would increase the cost", "without changing or increasing the long term protectiveness or affecting the overall protectiveness of the remedy."

GE agrees with EPA's position. In fact, the design changes that would be necessary to certify completion of a remedy that would achieve these SCLs would result in a remedy that would certainly require a further amendment to the Record of Decision. As EPA recognizes in Comments #7 and #14, such design changes would result in a significantly greater excavation volume and area, with resulting increases in: the time to implement the remediation activities; cost; and disruption, including the need to completely interrupt rail service adjacent to the Mill Street Area (including the northern rail line). When GE raised this issue in a November 8, 2011 meeting with EPA, USACE, NHDES representatives, EPA acknowledged that Comment #14 did not sufficiently address this issue and indicated that it would provide a further response. No response has been received at the time of this submittal. GE suggests that EPA and GE discuss the specific locations in which the SCLs will not be achieved by the OU-1 Remedial Action specified herein, and the locations at which GE knows that certification of achievement of the SCLs will be impossible so that appropriate amendments or modifications can be made to ROD and/or UAO/SOW.

Additional details regarding the development of the limits of soil removal and the preceding clarifications are provided in Section 2.6.

1.5.2.2 Interim Cleanup Levels for Groundwater

In the ROD (as amended), EPA established interim groundwater performance standards for the OU-1 remedy. As indicated in Section 1.1, EPA issued a second ESD on September 30, 2010 establishing a new ICL for arsenic and increasing the ICL established in the ROD and AROD for manganese from 180 micrograms per liter (μg/L, or parts per billion [ppb]) to 300 μg/L. The interim performance standards are the groundwater ICLs presented in the AROD, the 2nd ESD and the UAO (as modified), as referenced in the following table:

EPA's Selected Interim Cleanup Levels for Groundwater

Constituent	Interim Cleanup Level (µg/L)
Carcinogenic COCs	
Volatiles:	
Benzene	5.0
1,2-Dichloroethane	5.0
Trichloroethylene	5.0
Pesticides/PCBs:	
Total PCBs	0.5
Non-Carcinogenic COCs	
Volatiles:	
Ethylbenzene	700
Toluene	1,000
Semi-Volatiles:	
1,2,4-Trichlorobenzene	70
PCBs	0.5
Metals:	
Manganese	300*
Arsenic	10

Note:

* The ambient groundwater quality standard is now 840 ug/L [see Table 600-1 at Env-Or 600.03(c)], substantially higher that the ICL set in the ROD.

On October 25, 2010, GE submitted a letter in response to EPA's 2nd ESD indicating that the modified ICL for manganese should be 840 µg/L, which is the Ambient Groundwater Quality Standard (AGQS) set by the NHDES [see Table 600-1 at Env-Or 603.03(c)]. That letter also indicated that ICL for arsenic should be eliminated on the basis that EPA's own observations that "currently, arsenic levels in groundwater are not in exceedance of the 10 µg/L drinking water standard." EPA has not yet responded to GE's October 25, 2010 letter.

As determined by the EPA in the ROD (as amended), and as set forth in the UAO (as modified), the Remedial Action for OU-1 groundwater is monitored natural attenuation until the groundwater ICLs specified above have been achieved for a period of three consecutive years. At that time, the EPA will re-assess the cumulative risk presented by the residual levels of constituents in groundwater, and if the risk is found to be acceptable, the protective residual levels will constitute the final cleanup levels for groundwater and the groundwater

remedy will be considered complete. The EPA has also stated that if the risk is found to be unacceptable, the EPA will establish modified groundwater cleanup levels, and monitored natural attenuation will continue until the modified groundwater cleanup levels have been achieved and it has been determined that the residual levels of constituents in groundwater do not pose an unacceptable risk.

As indicated in the ROD (as amended), EPA estimated that the time required to achieve the ICLs will be 25 years for volatile organic compounds (VOCs) in overburden groundwater, and 100 years or greater for total PCBs. That document went on to indicate that the restoration timeframe for VOCs in bedrock groundwater was expected to be greater than the 20 to 25 years estimated for the overburden and remain greater than the 100 years estimated for PCBs in the overburden. On July 30, 2007, GE submitted a letter to EPA providing a separate evaluation of the estimated groundwater cleanup timeframes. As noted therein, it was determined that it will take approximately 20 years and 81 years, respectively, to achieve the ICLs for trichloroethene and PCBs within the overburden aquifer. It was also estimated that the groundwater cleanup timeframe for PCBs in the bedrock at the Mill Street Area is approximately 154 years. These estimates were generally consistent with EPA's estimates presented in the ROD.

The times estimated by EPA to achieve the ICLs stated in the ROD (as amended) and 2nd ESD are for groundwater quality impacts related to the Elm and Mill Street Areas. However, there are other known sources of ICL constituents in groundwater that could affect the estimated cleanup timeframe for groundwater. In particular, one current and one former gasoline station that are known to have adversely impacted groundwater quality are located immediately upgradient of the Elm Street Area. Another gasoline station known to have adversely impacted groundwater quality is located about 1,000 feet west of the Elm Street Area, upgradient of Keyes Field. Finally, as previously indicated, EPA has revised the ICL of for manganese in groundwater to 300 μg/L (and GE has requested that EPA further revise that ICL to be equal to the AGQS of 840 μg/L). Based on the fact that manganese is a naturally occurring constituent, it may also affect the estimated cleanup timeframes for groundwater specified above.

1.6 Format of Document

The remainder of the Final Design Report is presented in nine sections. The title and a brief overview of the contents of each section are provided below:

- **Section 2 – Site Investigation Activities and Results,** provides an overview of the historical, pre-design, and supplemental investigations, the results of which were used in developing the final design.

- **Section 3 – Site Preparation Activities,** describes the activities to be completed to prepare the Site for the OU-1 soil remedy.

- **Section 4 – Implementation of Remedial Action,** summarizes the proposed remediation activities to be conducted at the Site for the OU-1 soil remedy.

- **Section 5 – Site Restoration,** describes the activities required to restore the Site along with a description of post-restoration site control and monitoring activities.

- **Section 6 – Groundwater Monitoring Zone (GMZ),** includes an overview of the post-construction groundwater monitoring to be performed for the OU-1 remedy, including the establishment of a GMZ within which use of groundwater will be restricted. This section references the EMP and Institutional Controls/Access Restrictions (IC/AR) Plan, both of which were submitted to EPA on July 30, 2007, as revised through GE's response on December 31, 2007 to EPA's groundwater-related comments dated November 1, 2007, and revised a second time on April 14, 2008. The EMP includes specific details regarding the long-term (i.e., post-construction) groundwater monitoring program and the IC/AR Plan provides specific details regarding the establishment of a GMZ.

- **Section 7 – Evaluation of Applicable or Relevant and Appropriate Requirements (ARARs),** identifies ARARs for the OU-1 remedy and provides preliminary information regarding how each will be met through the performance of the Remedial Action.

- **Section 8 – Technical Drawings and Specifications,** identifies the technical drawings accompanying this revised Final Design Report, a discussion of drawing components, and a listing of relevant Technical Specifications.

- **Section 9 – Estimated Construction Cost and Schedule,** provides the estimated cost and schedule to implement the OU-1 soil remedy.

- **Section 10 – Future Activities and Schedule,** identifies the scope and proposed schedule for future activities associated with implementation on the OSD soil remedy, including selection of a Remedial Action Contractor and preparation of a RAWP and associated documents.

Substantial supporting documentation was prepared in support of the Final Design Report. In addition to the tables and figures included in Volume I of this revised Final Design Report, Volumes II and III include several appendices providing information relevant to this final design. Specifically, the following information is provided in the appendices to this report: a

Verification Sampling Plan (VSP, Appendix A); Technical Drawings (Appendix B); Technical Specifications (Appendix C); OSD Staging Scenario (Appendix D); the TR/TA Report (Appendix E); Design Calculations (Appendix F); the revised Project Construction Schedule (Appendix G); a *Construction Quality Assurance Plan* (CQAP, Appendix H); and a *Contingency Plan* (CP, Appendix I).

Finally, Section 10 of the Intermediate OSD Design Report provided a list of the required elements of the Final Design Report. That list included a Constructability Review Report, a final bid package, reproducible mylars of drawings, and a correlation of the design plans and specifications. However, EPA's November 1, 2007 letter indicated that the Final Design Report should include the elements specified in Paragraph 84 of the UAO, which did not include the four above-listed items. GE requested clarification regarding the need to include these four items in the Final Design Report via electronic mail dated November 8, 2007, and recommended that these components of the Remedial Design could be submitted following completion of EPA's remedy selection process. EPA concurred with this recommendation via electronic mail dated November 14, 2007. As subsequently required by EPA's September 30, 2011 approval with modification letter for the December 2007 Final Design Report, the Constructability Review Report and final bid documents are included in this revised Final Design Report. In addition, EPA's September 30, 2011 letter indicated that the mylar drawings would not be required as an element of the revised Final Design Report. Finally, as agreed with EPA during the November 8, 2011 meeting, the correlation of design plans and specifications is not a required element of this revised Final Design Report.

1.7 Other Related Documents

The following documents will be prepared in support of the RD/RA activities. Some of these documents will be provided under separate cover from this revised Final Design Report, while others are provided as appendices herein.

- A revised *Project Operations Plan* (POP), which includes the *Site Management Plan* (SMP), *Sampling and Analysis Plan* (SAP), consisting of a *Field Sampling Plan* (FSP) and a *Quality Assurance Project Plan* (QAPP), and a *Community Relations Support Plan* (CRSP). Additional information regarding each of these documents is provided below:

    - A revised SMP, providing appropriate updates to the general site management procedures and measures (i.e., responsibilities and communications, site access controls, security, equipment cleaning and decontamination procedures, waste disposal procedures, ambient air monitoring procedures, data quality assessment

and management, and contingency procedures for emergencies) that will be implemented during the course of the OU-1 soil remedy.

- A revised FSP and QAPP, providing appropriate updates to the field sampling activities and procedures, laboratory analytical methods, sample handling and documentation procedures, and quality assurance/quality control procedures.

- A revised CRSP, providing appropriate updates to the procedures and activities that will be utilized to distribute project-related information and updates to the general community.

- A revised *Site Health and Safety Plan* (HASP), providing appropriate updates to the minimum health and safety requirements and procedures for all activities associated with implementation of the OU-1 soil remedy.

- A *Contingency Plan*, provided in Appendix I of this revised Final Design Report, which expands upon the emergency procedures identified in the HASP and SMP and identifies minimum procedures to minimize the potential risks to on-site workers and the general public resulting from the unplanned release of hazardous constituents or other emergencies.

- A *Constructability Review Report*, providing an objective third party evaluation of the implementation of the OU-1 soil remedy and its components in relation to the Site. GE has retained URS Corporation (URS) to prepare the Constructability Review Report. URS visited the Site on November 13, 2007 and subsequently completed much of its review of the OU-1 soil remedy. As indicated during the November 8, 2011 meeting, the draft Constructability Review Report identified certain data gaps in the draft remedial design. Those data gaps formed the basis for the supplemental design data collection activities described in Section 2.4. Thus, this revised Final Design Report incorporates several revisions resulting from the Constructability Review Report and the subsequent supplemental design data collection activities. The Constructability Review Report has also been updated to reflect the supplemental design data collection activities and the subsequent design revisions.

- A *Construction Quality Assurance Plan*, provided in Appendix H of this revised Final Design Report, which describes the various procedures and requirements that will be implemented during construction-related activities performed as part of the OU-1 soil remedy. Such activities are designed to assist the selected remedial contractor (i.e., the Remedial Action Contractor) with implementing the remedy such that it meets or

exceeds the design criteria, plans, and specifications, thus supporting the certification of the achievement of the applicable performance standards.

- A RAWP, which will include, methodologies, plans, and schedules for completion of at least the following (as specified in Paragraph 89 of the UAO, as modified):

  - A revised Project Operations Plan;

  - Implementation of the CQAP;

  - Development and submission of the air monitoring, Long-term Maintenance Plan and Environmental Monitoring Plan (note that the latter document was submitted to EPA on July 30, 2007, as revised on April 14, 2008);

  - Identification of and satisfactory compliance with applicable permitting requirements;

  - Implementation of the Operation and Maintenance Plan for the OU-1 soil remedy; and

  - Implementation of the Contingency Plan.

  Paragraph 89 of the UAO (as modified) indicates that the RAWP shall also include a schedule for implementing all Remedial Action tasks identified in the SOW (as modified).

- The *Environmental Monitoring Plan*, which sets forth the long-term groundwater monitoring activities for OU-1 following the completion of the OU-1 soil remedy. As previously indicated, this document was submitted to EPA on July 30, 2007, as revised on April 14, 2008.

- The IC/AR Plan, which provides details regarding the access requirements, access restrictions and institutional controls for the construction and post-construction phases of the OU-1 soil remedy. This includes information regarding the GMZ that will be established pursuant to the ROD (as amended). Similar to the EMP, the IC/AR Plan was submitted to EPA on July 30, 2007, revised through GE's response on December 31, 2007 to EPA's groundwater-related comments dated November 1, 2007, and revised a second time on April 14, 2008.on April 14, 2008.

- An *Operation and Maintenance Plan* (O&M Plan), providing an evaluation of the long-term operation, maintenance and monitoring (OM&M) of the various components of the OU-1 soil remedy, including descriptions of: typical OM&M activities; potential operational problems; routine process monitoring and analysis; contingency operation and monitoring; an operational safety plan; budget for annual OM&M activities; and record-keeping and reporting requirements. The O&M Plan will also discuss the roles and responsibilities of various parties in implementing the plan.

1.8 Disclaimer

This revised Final Design Report is intended to provide an appropriate level of detail for the implementation of the OU-1 soil remedy. The actual equipment selection and specific aspects of the implementation of the Remedial Action will be determined by the Remedial Action Contractor based on its experience and equipment availability, with certain exceptions (e.g., phasing, loading requirements, etc.). Further, once the Remedial Action Contractor has been selected, a RAWP must be prepared and submitted to EPA for review and approval.

2. Site Investigation Activities and Results

2.1 Introduction

The extensive investigation activities performed at the Site for OU-1 form the basis for the Remedial Design activities documented herein. Those investigation activities were performed in multiple phases, including: (1) EPA's RI performed between October 1991 and January 1994; (2) PDI activities performed by GE between May 2003 and August 2004; (3) supplemental investigation activities performed following the submittal of the January 2005 PD Report; and (4) supplemental design data collection activities performed by GE between May and October 2012. Sections 2.2 and 2.3 present an overview of soil investigation activities performed during the RI and PDI, respectively. Section 2.4 presents a summary of supplemental design data collection activities performed by GE since submittal of the January 2005 PD Report. Section 2.5 presents an overview of the physical setting of the Site, including geologic and hydrogeologic information for the Elm and Mill Street Areas. This information was utilized to assist with the design of the fixed excavation structural supports/groundwater flow cut-off barriers and groundwater dewatering systems. Finally, Section 2.6 presents an overview of the development of the limits of excavation. This overview includes: a discussion of revisions to the applicable portions of the conceptual site model (CSM) presented in the Intermediate LTTD and OSD Design Reports based on EPA comments and additional data collected since submittal of the Preliminary Design Report; modifications to the preliminary limits of excavation and preliminary estimates of the volume of excavated soil/material subject to the Remedial Action; and, identification and description of certain soil sampling locations within the Elm and Mill Street Areas that cannot be addressed during the performance of the Remedial Action based on physical constraints/boundaries and/or risk management decisions.

2.2 Remedial Investigation

Soil, sediment, groundwater, and/or surface water data were generated by EPA during Phase 1A and Phase 1B of the RI. As indicated in Section 4.2 of the PD Work Plan, only data generated in accordance with Contract Laboratory Program (CLP) methods were used in this Remedial Design. Soil screening data derived from the on-site field laboratory used by the EPA during performance of the RI were not considered for the Remedial Design.

As indicated in Section 1.5.2, excavation and treatment of surface soils containing non-PCB constituents at concentrations greater than the SCLs is only required for surface soils containing total PCBs in excess of the SCL of 1 mg/kg. Therefore, PCB data alone form the basis for the limits of excavation presented in this revised Final Design Report. Because only PCB soil sample data were considered in the limits of excavation presented herein,

and because the EPA's non-PCB soil sample data from its RI were presented in Table 2 of the PD Report, those data are not presented again in this report. The EPA's RI CLP laboratory PCB sample data are summarized in Table 1 and the corresponding soil sampling locations for the Elm and Mill Street Areas are presented on Figures 2 and 3, respectively.

2.3 Pre-Design Investigation

This section summarizes the PDI activities performed by GE between May 2003 and August 2004. Detailed descriptions of the scope of the pre-design activities and the results of that investigation are provided in Section 4 of the PD Report. A brief overview of the PDI activities is provided below.

As discussed in the PD Report, the pre-design activities were performed in two phases at the Site. Phase 1 of the PDI involved the performance of miscellaneous activities (i.e., site survey, geophysical survey, UST characterization, monitoring well survey, and groundwater elevation monitoring) to establish baseline conditions at the Site and assist with the design and implementation of certain Phase 2 activities. The Phase 1 investigation activities were initiated with a project kickoff meeting on May 16, 2003 and were performed in accordance with the June 2003 revised PD Work Plan (which incorporated EPA comments on the previous PD Work Plan). The Phase 1 investigation activities were essentially completed by August 15, 2003 and documented in the PD Work Plan submitted in November 2003.

Phase 2 of the PDI was completed to provide sufficient data to proceed with the design of the ROD-specified LTTD and OSD soil remedies. The majority of the Phase 2 investigation activities proposed in the revised PD Work Plan was completed between November 7, 2003 and February 26, 2004. However, supplemental delineation soil sampling activities were performed on several occasions between April 13 and August 26, 2004. In summary, the PDI for the Elm and Mill Street Areas involved an extensive soil sampling program designed to assist with the identification of soils containing constituents at concentrations greater than the applicable SCLs and the subsequent development of limits of excavation to address such soils. As indicated in Section 4.6.1 of the PD Report, the soil sampling activities at the Site involved the following:

- Collection of more than 200 surface and over 650 subsurface soil samples from more than 120 locations at and near the Elm Street Area.

- Collection of more than 100 surface and over 730 subsurface soil samples from more than 110 locations at and near the Mill Street Area.

Tables 2 through 5 present the surface and subsurface PCB soil sample data for the Elm and Mill Street Areas generated during the PDI. The RI and PDI soil sampling locations and surface soil sample data for the Elm Street Area are presented on Figure 4, while the subsurface soil sample data are presented on Figure 5. Similarly, the RI and PDI soil sampling locations and surface soil sample data for the Mill Street Area are presented on Figure 6, while the subsurface soil sample data are presented on Figure 7.

2.4 Supplemental Design and Data Collection Activities

Section 6 of the PD Report provided a discussion of actual and potential outstanding data needs following performance of the PDI. Some of the data needs did not require action or were completed prior to submittal of the Preliminary Design Report and documented therein, including: property lines/boundaries at the Elm Street Area; completion of the monthly groundwater elevation monitoring; collection of supplemental geotechnical data; and, performance of the soil column study that was proposed in the PD Work Plan.

Certain of the other actual/potential data needs identified in the PD Report were completed prior to submittal of the Intermediate LTTD and OSD Design Reports, including:

- Performance of a comprehensive traffic survey;
- Location and alignment of the future utility corridor(s) at/adjacent to the Elm Street Area; and
- Performance of additional soil sampling delineation activities.

As further described in Section 3.14, GE made several submittals to EPA during the Remedial Design phase of the project that were associated with the performance of the specified traffic survey and an analysis of the impact of performing both the LTTD and OSD soil remedies on pedestrian and vehicular traffic in the vicinity of the Site. Those initial submittals were the basis for the TR/TA Report presented in the December 2007 Final Design Report. That report presented the results of the traffic survey and traffic capacity analyses performed as part of the Remedial Design, provided additional details regarding the impacts to pedestrian and vehicular traffic in the vicinity of the Site resulting from implementation of the OU-1 soil remedy and provided an evaluation of the need for measures to mitigate the impacts to such traffic resulting from implementation of the OU-1 soil remedy. As indicated in Sections 1.2 and 3.14, that report was subsequently revised in several submittals to EPA dated October 30, 2008, June 22, 2009 and August 13, 2009. The TR/TA Report provided in Appendix E has been revised to incorporate these submittals.

Similarly (and as documented in Section 1.2), GE has made several submittals related to the location/alignment of the future utility corridors at the Elm Street Area, including: Addendum No.1 to the Preliminary Design Report, and letters to EPA dated January 30, February 28, March 27, May 2, and May 18, 2007. As indicated in the Intermediate LTTD and OSD Design Reports, the locations and depths of the utility corridors associated with the Town's future use of the Elm Street Area had been resolved with the submittal of those various documents. However, the Town of Milford notified EPA and GE via an electronic mail dated December 7, 2010 that the Town had elected to eliminate the proposed memorial park restoration design for the Elm Street Area in lieu of a design that proposed additional parking. This modification also resulted in the elimination of all of the utility corridors proposed in the December 2007 Final Design Report, except for the corridors associated with the replacement storm sewer line and the existing water line along Keyes Drive. GE, EPA, and the Town of Milford subsequently participated in several discussions and exchanged conceptual drawings associated with the design of a hybrid soil cover and parking area restoration design for the Elm Street Area and the associated utility corridors. As indicated in Section 1.2, GE provided revised drawings for design of the utility corridors and the restoration of the Elm Street Area to EPA via electronic mail dated May 2, 2012. GE has further revised the alignment of the replacement storm sewer line based on the results of the supplemental design data collection activities performed between May and July 2012. Figure 8 presents the locations and dimensions of the existing utility corridor and the proposed replacement storm sewer, while Sections 3.7 and 5.3 of this report provide additional information regarding these utility corridors.

Regarding supplemental delineation soil sampling, GE performed such activities at both the Elm and Mill Street Areas in late October 2005. These investigations were performed in an attempt to delineate the extent of soils containing PCBs in excess of the applicable SCLs at certain portions of the Elm and Mill Street Areas. Specifically, supplemental samples were collected for analysis of PCBs in the vicinity of sampling locations ESSB-L15E and -S11S at the Elm Street Area and sampling location MSSB-E05W at the Mill Street Area. The data were included in GE's August 17, 2006 letter to EPA regarding confirmation soil sampling. The data are also presented in Tables 3 and 5 and Figures 5 and 7 and have been incorporated into the soil removal limits presented in this revised Final Design Report.

In addition to the above-described supplemental investigation activities, GE performed certain supplemental survey activities to provide additional information associated with certain features at both the Elm and Mill Street Areas, including:

- Location of an oak tree in the vicinity of the cemetery adjacent to the Elm Street Area for which the Town requested GE implement protective measures during the performance of the OU-1 soil remedy.

- Additional survey associated with the portion of the drainage ditch/culvert system located within Cottage Street that is related to the rerouting/replacement of the storm drainage system that runs along the east side of the Elm Street Area.

- Supplemental survey activities to assist with the design of the Mill Street realignment and to confirm/provide additional detail regarding the topography at the Mill Street Area and the portion of the adjacent Draper property located west of the drainage ditch.

The data from these supplemental survey activities were incorporated into the applicable mapping, figures and technical drawings presented in this revised Final Design Report.

Following submittal of the December 2007 Final Design Report, GE performed several supplemental investigation activities for the purpose of providing data to address uncertainties associated with the Remedial Design. The first such uncertainty was a lack of geotechnical data in the vicinity of the riverbank or the Elm Street Area and along the cemetery east of the Elm Street Area. GE proposed supplemental geotechnical investigation activities in several letters to the EPA dated May 8, June 22, August 21, August 31, and September 28, 2009. Those supplemental geotechnical investigations involved the following activities:

- Advancement of five geotechnical borings within the Souhegan River to determine the depth to bedrock and to develop a better understanding of the lithology and physical properties of the soil/bedrock in the area of the sheetpile demarcation wall and gabion retaining wall;

- Advancement of one geotechnical boring to confirm the assumed absence of bedrock to the design depth of a particular excavation support near the base of the slope along the western boundary of the cemetery;

- Geotechnical analysis of 10 soil samples collected from the riverbank;

- Rock coring in certain borings and chemical analysis of bedrock groundwater samples collected during the drilling activities; and

- Collection of detailed topographical survey information within the riverbank/riverbed in the vicinity of the Elm Street Area.

The results of the supplemental geotechnical investigation activities were provided in a letter from GE to EPA dated December 28, 2009. The bedrock groundwater quality data provided therein indicated that one of the two bedrock groundwater samples collected from

the geotechnical borings advanced to bedrock along the riverbank contained trichloroethene at a concentration greater than the corresponding ICL and both samples contained PCBs at concentrations greater than the corresponding ICL. The geotechnical data resulting from these investigations were incorporated into the design modifications presented in GE's October 21 and 29, 2010 submittals to EPA and incorporated into this revised Final Design Report.

As previously indicated, EPA's September 30, 2011 letter to GE provided approval with modifications for the December 2007 Final Design Report (as amended). As requested in that letter, representatives of EPA, USACE, NHDES and GE met on November 8, 2011 to discuss EPA's approval with modifications letter and other topics related to revising/resubmitting the Final Design Report and the initiation of the Remedial Action phase of the OSD remedy. During that meeting, GE indicated that the draft Constructability Review Report had identified uncertainties associated with three elements of the Remedial Design, including: (1) the dewatering rate for the deeper excavation cells (i.e., within the soldier pile and tremie concrete [SPTC] walls at the Mill Street Area; (2) side-wall verification sampling on the passive sides of excavation supports at the Elm Street Area (as specified in the VSP provided in Appendix A of the December 2007 Final Design Report); and (3) soil characterization to assist with determining the appropriate off-site treatment and/or disposal of materials excavated during the OU-1 soil remedy.

As agreed during the November 8, 2011 meeting, GE submitted a *Work Plan for Additional Field Work Necessary to Address Constructability Issues Regarding the OU-1 Soil Remedy* (also known as the SDDC Work Plan) on December 22, 2011. EPA and USACE provided comments to that document in a letter to GE dated February 17, 2012. Additional comments were provided in conference calls (February 29 and March 7, 2012) and via electronic mails dated March 23, April 2, and April 4. The SDDC Work Plan was revised twice to address the EPA and USACE comments and resubmitted on April 6 and May 4, 2012. In addition, based on the results of the initial pre-construction verification soil sampling activities, GE proposed the collection of additional pre-construction verification soil samples under the SDDC Work Plan in an electronic mail to EPA dated July 18, 2012. EPA provided comments on GE's proposal in a letter to GE dated September 7, 2012. Several of EPA's comments were incorporated into the subsequent pre-construction verification soil sampling activities.

In summary, GE performed the following SDDC activities between May and October 2012:

- Hydraulic testing involving the following activities: redevelopment of 11 existing monitoring wells; installation and development of five new monitoring wells, two new pumping wells, and four temporary piezometers; installation of 42 pressure transducers

equipped with data loggers to establish pre- and post-hydraulic testing conditions and document the impacts of the hydraulic testing; performance of specific capacity, step-drawdown, and constant rate pumping tests; and performance of baseline and post-hydraulic water quality sampling events, followed by monitoring for the potential presence of DNAPL in select wells/piezometers;

- Collection of 101 (including four sample duplicates) pre-construction sidewall verification soil samples for analysis of PCBs; and

- Collection of 89 soil characterization samples for analysis various waste characterization analyses, including: VOCs, semi-volatile organic compounds (SVOCs), pesticides/herbicides, and/or metals using the toxicity leaching characteristic procedure (TCLP); corrosivity, ignitability, reactivity; and PCBs.

Although not identified as an uncertainty associated with the Remedial Design, the water generated by the various hydraulic testing activities was treated on-site utilizing a temporary water treatment system that included certain components that are similar to the temporary water treatment system design for the OU-1 soil remedy. By treating such water, GE was able to determine whether any modifications to the design of the temporary water treatment system design for the OU-1 soil remedy were appropriate.

The data from these supplemental investigations were reviewed to determine the potential need for revisions to applicable elements of the Remedial Design. Specifically, the hydraulic testing data was evaluated to determine the potential need for revision to the estimated dewatering rates for the deep excavations at the Mill Street Area. Similarly, the data from the pre-construction verification soil sampling were reviewed to determine the potential need for revisions to the support of excavation design and VSP for the Elm Street Area. The soil characterization data were reviewed to determine the potential presence of any hazardous waste regulated under the Resource Conservation and Recovery Act (RCRA, 40 CFR 261.24). Finally, the results of the treatment of the water from the hydraulic testing activities were reviewed to determine the potential need for any revisions to the design of the temporary water treatment system for the OU-1 soil remedy.

The results of the various data reviews are briefly summarized below along with conclusions, as appropriate:

- The groundwater flow model provided in the Preliminary Design Report identified an estimated maximum dewatering rate of 75 gpm for certain excavations at the Mill Street Area. The groundwater flow model was updated and recalibrated using the hydraulic testing data generated under the SDDC Work Plan. The updated, recalibrated model

indicates that the specified target dewatering elevations for each SPTC excavation cell at the Mill Street Area can be achieved within a 14-day period, with expected average dewatering rates of 21 to 50 gallons per minute (gpm). Section 2.10 of the SDDC Work Plan provided details regarding the evaluation of the hydraulic testing data. As described therein, ranges were identified within which modifications to the designs for the SPTC wall, dewatering system, or the temporary water treatment system would not be required. While the estimated 14-day average dewatering rates described above are less than the estimated dewatering rate presented in the Preliminary Design Report, they are not sufficiently low to warrant revisions to the designs of the SPTC wall, dewatering system, or the temporary water treatment system. Therefore, as a conservative measure, those elements of the Remedial Design were not revised based on the anticipated dewatering rates calculated using the updated, recalibrated groundwater model.

- As indicated above, the pre-construction verification soil sampling was performed in an iterative manner. The results of the initial sampling indicated that 14 of the initial 34 (including one sample duplicate) preconstruction verification soil samples contained PCBs at concentrations greater than the SCL of 100 mg/kg applicable to subsurface soils at the Elm Street Area. As a result, GE proposed additional preconstruction verification sampling in a July 18, 2012 electronic mail. EPA provided comments to that proposal in a September 7, 2012 letter and GE conducted two additional rounds of sampling. The results of that sampling indicated that only seven of the additional 67 pre-construction verification soil samples contained PCBs at concentrations greater than the SCL of 100 mg/kg. The pre-construction verification soil sample data collected under the SDDC Work Plan are provided in Table 6. These data were used to revise the limits of soil removal, the locations of the excavation supports at the Elm Street Area, and the VSP provided in Appendix A.

- The results of the soil characterization sampling indicated that only four of the 89 collected soil samples had constituent concentrations that would require management under RCRA disposal regulations. Specifically, three of the 39 samples collected from the Elm Street Area and submitted for TCLP analysis contained lead at concentrations greater than 5 milligrams per liter (mg/L) (i.e., concentrations ranging from 5.3 to 26.5 mg/L). In addition, one of the 50 samples collected at the Mill Street Area and submitted for TCLP analysis contained heptachlor at a concentration greater than 0.08 mg/L (i.e., 0.0094 mg/L). The results of the soil characterization sampling are provided in Table 7. This data and all other waste characterization data collected to date for the Site will be provided to the selected Remedial Action Contractor and will be utilized to develop a Waste Management Plan that will be included in the forthcoming RAWP.

In addition to the data evaluation activities described above, the performance of the temporary water treatment system used during the SDDC activities was evaluated. Accumulated waters from the hydraulic testing activities were stored in three influent tanks and treated through a temporary water treatment system that included an oil/water separator, an organo-clay filter, two 2,000 pound granular activated carbon vessels, and a dual chamber bag filter. Treated waters were stored in an effluent tank for sampling to demonstrate achievement of the discharge criteria specified in Table 3 of the SDDC Work Plan prior to discharge.

The initial batch of treated effluent did not meet the discharge criteria for PCBs. As a result, the treated water was pumped back to the influent tanks. A review of the water quality sample data collected from the pumping wells during the hydraulic testing indicated elevated concentrations of PCBs. Additionally, DNAPL was observed during the installation of the pumping wells and following performance of the hydraulic testing. Although the treatment system was equipped with an oil/water separator and an organo-clay filter, the effluent tank was cleaned and wipe-sampled to make sure no impacts resulted from the initial treatment. Concurrently with the effluent tank cleaning, influent waters were treated in 5,000 gallon batches, cycling the treated water back to the influent tanks. Samples of the treated effluent were collected during the batch treatment to demonstrate achievement of the discharge criteria. Also, the granular activated carbon and cartridges for the bag filter were exchanged, the bag filters were moved to the end of the treatment train, and sub-micron filters cartridges were installed. Once the effluent results for the batch treatment indicated achievement of the discharge criteria, the water in each influent tank was sequentially treated to the effluent tank, sampled to demonstrate compliance with the discharge criteria in Table 3 of the SDDC Work Plan, and ultimately discharged to the drainage ditch at the Mill Street Area in accordance with the SDDC Work Plan. Based on the results of these water treatment activities, certain modifications were made to the temporary water treatment system for the OU-1 soil remedy, as further described in Section 4.5.

Additional details regarding the performance of the SDDC activities and the evaluation of the data from those investigations will be provided in a forthcoming SDDC Report that will be submitted in January 2013. However, as previously indicated, the data from those supplemental investigation activities were incorporated into this revised Final Design Report, as appropriate.

2.5 Physical Setting

This section provides an overview of the physical setting of the Site, including geologic, topographic, and hydrogeologic information that was used in developing the Final Design

Report. Additional details regarding each of these topics are provided in the following sections. It should be noted that some of the information provided herein was presented in EPA's RI Report.

2.5.1 Regional Geology

The Site is located at the eastern end of the Milford-Souhegan glacial drift aquifer within the Souhegan River valley. The glacial drift aquifer is approximately 3 miles long, following the Souhegan River. This aquifer varies between 1,200 feet and 1.5 miles wide. The southern boundary of the aquifer is defined by the contact between the saturated and unsaturated stratified drift in the valley and the till covered uplands. The glacial deposits consist of Pleistocene glacial sediments, including poorly graded, dense till and well-sorted stratified drift. While some till is present at the top of bedrock within localized areas in the glacial aquifer, the majority of the till is in the upland areas. Stratified drift deposits, which make up the majority of the unconsolidated aquifer, were deposited by streams that existed in the present Souhegan River valley during glacial retreat. The depositional nature of the stratified drift created a heterogeneous mix of coarse sand and gravel in the western section of the aquifer, and coarse to fine sand with discontinuous silt lenses in the eastern section of the aquifer. The underlying bedrock is part of the Massabesic-Merrimack-Rye terrain, and is composed of Precambrian to Ordovician granite and gneiss.

2.5.2 Site Topography

The ground surface at the Elm Street Area slopes downward 20 feet (from approximately 255 feet above mean seal level [AMSL] to 235 feet AMSL) over a distance of approximately 40 feet along the northern site boundary. The Souhegan River is at the bottom of the steep northern slope, at an elevation of approximately 235 feet AMSL. The ground surface slopes from approximately 265 feet AMSL in the southeast corner of the Elm Street Area to approximately 255 feet AMSL at the top of the river bank in the northern portion of the Elm Street Area.

The majority of the Mill Street Area is at a relatively level elevation of approximately 260 feet AMSL. There is an elevated railroad bed on the northern edge of the Mill Street Area at approximately 265 feet AMSL. A drainage ditch with a bottom elevation of approximately 253 feet AMSL is situated along the western side of the Mill Street Area.

2.5.3 Subsurface Conditions – Elm Street Area

Approximately 14 to 26 feet of fill exists at the Elm Street Area. Along the Souhegan River, the bottom of fill is between 227 and 235 feet AMSL, which suggests that fill placement

started along the prior natural riverbank and continued into the upland area. The fill consists primarily of loose to medium dense silty sand with gravel zones and occasional layers of organic silt. In some areas, the borings suggest that the fill contains cobbles, boulders, and debris including wood, brick, coal, glass, metal, tires, slag, asphalt shingles, tree stumps, other materials associated with the former Town dump, and vegetative matter.

An approximately 12- to 28-foot thick outwash layer is present below the fill and over granite bedrock. The outwash unit consists primarily of medium dense to very dense, stratified sand and gravel with silty layers and occasional to frequent cobbles and boulders.

A discontinuous, transitional layer of weathered bedrock and/or glacial till was observed overlying competent bedrock. The bedrock surface beneath the Elm Street Area ranges in elevation from approximately 228 feet AMSL (32 feet below ground surface [bgs]) at the southeast corner of the Elm Street Area, to approximately 198 feet AMSL (50 feet bgs) at the northwest corner.

2.5.4 Subsurface Conditions – Mill Street Area

The fill at the Mill Street Area is approximately 6 to 10 feet thick, and consists primarily of loose to dense, poorly- to well-graded sand with variable amounts of silt and organic material. Gravel and cobble zones were occasionally encountered in the PDI test borings.

An approximately 10- to 16-foot thick outwash layer is present below the fill and above the bedrock. The outwash unit consists primarily of medium dense to very dense, stratified sand and gravel with silty layers and occasional to frequent cobbles and boulders, particularly in the lower half of the unit. Near the southwest corner of the Mill Street Area, auger refusal was frequently encountered at relatively shallow depths, which suggests a zone of potential subsurface obstructions (e.g., cobbles, boulders, debris) in this area.

The top of bedrock beneath the Mill Street Area ranges in elevation from approximately 244 feet AMSL (16 feet bgs) at the east side of the Mill Street Area to approximately 234 feet AMSL (24 feet bgs) at the west side. The bedrock surface gently undulates from east to west and contains approximately 2- to 6-foot high peaks and valleys.

Wells installed into the bedrock at and near the Mill Street Area encountered 0 to 10 feet of gneiss overlying granite. The gneiss was absent in most areas. However, where present, the gneiss was observed to be highly fractured with granite intrusions. The fractures typically ranged from horizontal to as steep as 80 degrees, although fracture dips of horizontal to 40 degrees predominated. The granite, which was encountered consistently in the bedrock boreholes, was observed to be slightly to moderately fractured, with decreasing

fracture prevalence at depth. The fractures in the granite are typically horizontal, although fracture dips up to 80 degrees were also observed. Secondary mineralization was observed along many fractures in both the granite and gneiss.

2.6 Development of Limits of Excavation

A general CSM for the Site was first presented in Section 4.2 of the PD Report. That CSM was revised to incorporate EPA comments and was presented in Section 4.2 of the revised PD Report. Additional revisions to the CSM were made in Section 2.6 of the Preliminary Design Report. The CSM was revised again for the Intermediate LTTD and OSD Design Reports to incorporate the supplemental PDI sampling data summarized in Section 2.4 and to reflect information provided in numerous submittals to EPA, as reviewed and commented upon by the EPA.

The remainder of this section presents an overview of the methodology used to develop the limits of excavation, the identification of boundary conditions and descriptions of certain soils not subject to the Remedial Action based on risk management decisions, and estimates of the volume of excavated soil/material subject to the Remedial Action. The limits of excavation presented in the December 2007 Final Design Report have been modified to incorporate the results of the supplemental investigation and design activities performed since submittal of that document.

2.6.1 Methodology for Developing the Limits of Excavation

The data included in the CSM were used to develop preliminary limits of excavation for both the Elm and Mill Street Areas. With some exceptions (further described below), the limits of excavation were developed using a next cleanest point methodology, which generally entails the following:

- At each soil sampling location, the deepest sample containing total PCBs in excess of the ROD-specified subsurface SCLs was identified.

- The depth of excavation at each sampling location was then established using the following criteria:

  - Maximum limits of excavation - The ROD specifies that the maximum depth of excavation at the Elm Street Area is the seasonal low water table. Similarly, the ROD indicates that bedrock represents the maximum depth of excavation at the Mill Street Area. Data collected during the PDI and the quarterly monitoring performed under the WMP was utilized to establish the depth of the seasonal low

water table at the Elm Street Area and the bedrock at the Mill Street Area. Where soil sampling data contained PCBs in excess of the subsurface SCLs down to these maximum limits of excavation, the depth of excavation extends the seasonal low water table or bedrock, as appropriate. Excavation Cell W on Technical Drawing G-10 represents an excavation to the seasonal low water table at the Elm Street Area, while Excavation Cells H and O on Technical Drawing G-15 represent excavations to the bedrock at the Mill Street Area.

- Soil sample data - Where not extended to the maximum limits of excavation, soil sampling data were used to establish the depth of excavation at each sampling location. Specifically, the depth of excavation was established as the bottom of the sample depth increment containing total PCBs in excess of the applicable subsurface SCL, where the next sample interval did not contain total PCBs in excess of that SCL. However, at a few locations such soil sampling data are not available. GE proposed to perform confirmatory soil sampling for these areas in the Preliminary Design Report. Based on subsequent feedback provided by EPA in its February 13, 2007 letter, a more extensive site-wide confirmation sampling program was developed and included in the Intermediate Design Reports. Additional details regarding the confirmation sampling activities that will be performed at the Site are provided in the revised VSP that is included in Appendix A to this revised Final Design Report.

- The horizontal limits of soil removal at each depth interval with an exceedance of the applicable SCL were established using an approach similar to that specified above for the vertical limits of soil removal, consisting of the following:

  - The first step involved the identification of the sample(s) containing total PCBs in excess of the applicable SCL at the greatest depth relative to existing grade at both the Elm and Mill Street Areas.

  - At each such location, the horizontal limits of soil removal were extended outward from the location(s) requiring excavation to adjacent sample locations containing total PCBs at concentrations less than the applicable SCL at the same depth interval.

  - This process was repeated proceeding from deep to shallow excavations until the horizontal limits of soil removal were established for each sample containing total PCBs in excess of the applicable SCLs.

- In addition to the aforementioned vertical limits of excavation, certain lateral physical barriers/boundaries have been identified for the OU-1 soil remedy. Specifically, the Souhegan River, the cemetery, and the southern (i.e., east-bound) lane of Elm Street all serve as horizontal physical boundaries for the Elm Street Area. At the Mill Street Area, the lateral physical boundaries consist of the northern rail line (which must remain in operation) and the residential properties south of Mill Street (which were previously remediated in 1995, as discussed in Section 1.4.2). Excavation will not be required beyond these horizontal physical barriers, as described in the following sections.

Use of this methodology represents a conservative approach to determining the limits of excavation where there are no physical barriers/boundaries. By expanding the horizontal limits of removal to the next cleanest point, it is conservatively assumed that all soil between the sample requiring excavation and the adjacent "clean" sampling location(s) contains total PCBs at a concentration above the applicable SCL. As a result, this approach likely results in the overestimation and, therefore, over-excavation, of material during the OU-1 soil remedy.

2.6.2 Boundary Conditions and Risk Management Decisions Impacting the Development of the Limits of Excavation

As previously indicated, the limits of excavation were modified in certain portions of the Elm and Mill Street Areas based on horizontal boundary conditions/physical constraints and/or risk management decisions. Additional details regarding such modifications to the horizontal limits of excavation at the Elm and Mill Street Areas are provided below.

The first such boundary condition/physical constraint is associated with the property boundary between the Elm Street Area and the cemetery. Specifically, the southwestern corner of the cemetery abutted two walls of the former Fletcher's Paint building. As illustrated on Figures 9 and 11, portions of the exterior wall of the former building, which were left in place by EPA following demolition of that building, function as a retaining wall for the cemetery, which has a ground surface elevation approximately seven feet higher than the adjacent portions of the Elm Street Area. As also illustrated on those figures, EPA installed a soil berm adjacent to the retaining wall following demolition of the building to provide additional structural support for the wall. The roof for the former building extended beyond the exterior walls and slightly into the cemetery. A small asphalt drainage swale was constructed in the cemetery to collect precipitation run-off from the structure. Limited sampling was performed in the vicinity of the drainage swale during the Pre-Design Investigation to document PCB concentrations in surface soils adjacent to the drainage swale. The results of that sampling indicated that two surface soil sampling locations

contained PCBs at concentrations greater than the applicable SCL of 1 mg/kg: ESSS-R18E (0.98 ppm, with a sample duplicate of 1.7 ppm) and ESSS-R20N (2.4 ppm). To avoid further disturbance, and as agreed with EPA, no further sampling was performed within the cemetery during the PDI.

With regard to the development of the limits of soil removal at the Elm Street Area, limited excavation activities are proposed within the cemetery. Specifically, cells requiring excavation to depths greater than 1 foot were terminated at the bottom of the slope for the cemetery or the retaining wall as shown for Excavation Cells JJ2, LL, and MM on Figure 11 and Technical Drawing G-12. As also shown on those Figure 11 and Technical Drawing G-12, the limits of excavation for Excavation Cell OO, which requires one foot of soil removal along the western boundary of the cemetery, do not extend beyond the top of the slope. Finally, the limits of Excavation Cell FF, which also requires one foot of soil removal, extend slightly into the cemetery to address soils associated with sampling locations ESSS-R18E and ESSS-R20N. These activities will also include removal of the small asphalt drainage swale and the cutting and capping and/or filling with grout of the drain lines that conveyed precipitation run-off from the roof. As indicated in Table 8, although the remediation activities proposed herein will include the removal of certain soils associated with these sampling locations (including the sampling locations themselves, as indicated on Figure 11), GE will not be able to certify achievement of the Performance Standards and SCLs for these two samples because no soil to the north of the sampling locations is proposed for excavation. Further, no verification soil sampling will be performed for this portion to Excavation Cell FF since excavation activities beyond those illustrated on Figure 11 or Technical Drawing G-12 will not be performed within the cemetery.

There were two other boundary conditions associated with Elm Street and the Souhegan River that impacted the development of the limits of soil removal for the Elm Street Area. First, the limits of Excavation Cells I and FF were terminated at the southern (i.e., east-bound) lane of Elm Street, as shown on Figure 11 and Technical Drawing G-12, so that a minimum of one lane of vehicular traffic could be maintained along this street throughout the performance of the Remedial Action. Also, the limits of soil removal were modified for the excavation cells along the riverbank of the Souhegan River. Specifically, the northern limits of excavation for each cell along the riverbank were determined by extending the base of the excavation to the riverbank until the excavation "daylights" at the appropriate elevation along the riverbank. No excavation cells were extended into the Souhegan River as the river is considered part of Operable Unit 2, for which EPA is currently preparing a Feasibility Study Report.

At the Mill Street Area, there are two boundary conditions that impacted the development of the limits of excavation. First, the residential properties south of Mill Street were previously

remediated by EPA in 1995. As a result, the limits of excavation for the Mill Street Area did not extend south of Mill Street. Second, prior to preparation of the Preliminary Design Report, it was expected that both rail lines immediately north of the Mill Street Area would remain operational during implementation of the OU-1 soil remedy. However, based on the data collected during the PDI, excavation to bedrock is necessary within Excavation Cells H and O (see Technical Drawing G-15). Therefore, the Preliminary Design Report proposed the removal of the southern rail line (which is not the main rail line, but a siding that is reportedly used to stage/rearrange rail cars) and excavation of the underlying impacted soils. The ROD (as amended) and the UAO (as modified) require that at least one rail line remain operational, so the Preliminary Design Report proposed to leave the northern rail line in place, with no excavation of underlying soils. Moreover, as documented in GE's May 10, 2007 submittal to EPA, Guilford Transportation Industries, Inc. (Guilford, the owner of the rail lines adjacent to the Mill Street Area) has indicated that excavation activities must not be initiated within one foot of the southern edge of the railroad ties of the northern rail line and that any such excavation must have a maximum slope extending away from the tracks of 1.5H:1V. This requirement was incorporated into the revised figures provided in GE's May 10, 2007 submittal, as well as the Interim Design Reports and the December 31, 2007 Final Design Report. Additional details regarding the relocation of the southern rail siding are provided in Section 3.2. The above-described boundary conditions were factored into the development of the limits of excavation and the risk-management decisions for the Mill Street Area.

As discussed in Section 1.4.2, the EPA indicated that the concentrations of PCBs at sample location MSSB-C01 (i.e., two samples containing total PCBs at concentrations of 4.4 mg/kg [11- to 13-feet depth interval] and 9.5 mg/kg [23- to 25-foot depth interval]) were consistent with the EPA's Spill Policy (40 CFR 761.125) for commercial areas. EPA determined that those soils are not subject to the 1 mg/kg subsurface SCL specified for the Mill Street Area. Therefore, the Remedial Design does not propose any soil removal in the vicinity of sampling location MSSB-C01.

Based on extensive discussions with EPA since submittal of the Preliminary Design Report, and as confirmed by EPA's February 13 and November 1, 2007 letters, risk-management decisions are also justified for certain other soil sampling locations at or near the Mill Street Area (e.g., in the vicinity of the railroad tracks immediately north of the Mill Street Area). As previously indicated the limits of excavation at the Mill Street Area can only proceed to within a certain distance of the northern rail line. Therefore, the Preliminary Design Report (as modified by GE's August 17, 2006 submittal) did not propose the excavation of subsurface soils at locations MSSB-B12, MSSB-B13, and MSSB-B17, which are located between the two rail lines (see Figure 12). These sampling locations contain sporadic, low-level exceedances of the subsurface SCL (i.e., a total of four samples containing total PCBs

at concentrations between 2.0 and 5.4 mg/kg, which is less than the maximum observed concentration of 9.5 mg/kg at sampling location MSSB-C01). To further minimize disturbance to the railroad, the Preliminary Design Report (as modified by GE's August 17, 2006 submittal) did not propose the excavation of subsurface soils at locations MSSB-C14, MSSB-C15, and MSSB-C17. Similar to locations MSSB-B12, MSSB-B13, and MSSB-B17, these sampling locations contain sporadic, low-level exceedances of the subsurface SCL (i.e., seven samples containing total PCBs at concentrations between 1.1 and 2.6 mg/kg). It should be noted, however, that some of the soils associated with these locations will be removed as part of the remediation activities proposed in this revised Final Design Report because the excavation approach in the vicinity of these sampling locations involves sloping the northern sidewall of Excavation Cell T, which is a deeper excavation located south of sampling locations MSSB-C14, MSSB-C15, and MSSB-C17 (see Figure 12). Finally, the majority of the surface soils associated with sampling locations MSSB-B13, MSSB-B17, MSSS-B13E (inclusive of the physical sampling locations) and a portion of the surface soils associated with sampling location MSSS-C18N will be removed as part of the excavation activities proposed for the Mill Street Area in this revised Final Design Report. However, due to the requirements to maintain: (1) at least one operational rail line throughout the performance of the OU-1 soil remedy; and (2) the structural integrity and safety of the northern rail line, expansion of the limits of excavation to the north to address all surface soils associated with the subject sampling locations is not possible, as indicated on Figure 12.

As requested by EPA, GE provided technical justification for not excavating certain soil samples with total PCBs above the 1 mg/kg SCL set by the EPA in the ROD for surface and subsurface soils at the Mill Street Area. Specifically, excluding the two subsurface soil samples at location MSSB-C01 that were already approved by EPA to be excluded from the OU-1 soil remedy, GE provided technical justification in a March 30, 2007 submittal to also exclude 41 soil samples at 23 locations (see Table 5 in the March 30, 2007 submittal). In a May 10, 2007 submittal, GE modified its March 30, 2007 submittal regarding the limits of excavation at and near the Mill Street Area. However, those modifications did not alter the number of soil samples or number of sampling locations proposed to be excluded from the OU-1 soil remedy.

As indicated in Section 1.5.2.1, EPA's February 13, 2007 approval with modifications letter for the confirmation sampling portion of the Preliminary Design Report (as modified by GE's August 17, 2006 submittal) concurred with the rationale for excluding certain additional subsurface soil samples at sampling locations MSSB-B12, MSSB-B13, MSSB-B17, MSSB-C14, MSSB-C15, and MSSB-C17 from the limits of excavation for the Mill Street Area. Eleven of the 41 soil samples presented in Table 5 of GE's March 30, 2007 submittal occur at these six locations. The remaining 30 soil samples occurred at 19 locations and were

presented in Table 6 of GE's March 30, 2007 submittal, reproduced as Table 9 in the Intermediate Design Reports and Table 9 in this revised Final Design Report. GE requested that EPA approval to also exclude these soil samples from the limits of excavation. EPA's November 1, 2007 letter did not include any comments on Table 9 of the Intermediate Design Reports, or on the figures that showed the limits of excavation for the Elm and Mill Street Areas.

As noted in Section 1.5.2, GE will not be able to provide certification of the achievement of the Performance Standards and SCLs for the areas/sampling locations described above at the Elm and Mill Street Area, as required in the AROD and UAO/SOW (as modified). GE maintains its request that EPA provide appropriate amendments or modifications to the AROD and/or UAO/SOW to address the certification requirement as it pertains to these specific sampling locations.

2.6.3 Estimates of the Volume of Material Subject to Excavation

The methodology, boundary conditions, and risk management decisions described in the preceding sections were used to develop the limits of excavation for the Elm and Mill Street Area presented in the revised Final Design Report. The limits of excavation required to achieve the surface and subsurface SCLs for the Elm Street Area are presented on Figure 9 and Technical Drawing G-10. As indicated in Table 10, the volume of soil removal required to achieve the SCLs at the Elm Street Area is approximately 21,220 cy. With respect to the Mill Street Area, the limits of excavation required to achieve the surface and subsurface SCLs are presented on Figures 12 and 13, as well as Technical Drawings G-15 and G-26. As shown in Table 10, the volume of soil removal required to achieve the SCLs at the Mill Street Areas is approximately 8,955 cy. Thus, the total excavation required to meet the SCLs at both areas is approximately 30,175 cy, all of which is subject to off-site disposal. In addition, approximately 2,790 cy of soil removal has been added to the total estimated volume of soil removal for the Site (approximately 1,840 cy at the Elm Street Area and approximately 950 cy at the Mill Street Area). This volume of additional soil removal is based on the sloping of excavations, illustrated on Technical Drawings S-2 (Elm Street Area) and S-9 (Mill Street Area), which is required to safely implement the Remedial Action. However, as further described below, the soils from areas requiring at least two feet of additional excavation beyond that to achieve the SCLs as part of these excavation sloping will not be subject to off-site disposal.

As indicated in GE's December 22, 2006, January 26, 2007, February 28, 2007, May 2, 2007 and May 18, 2007 submittals, the Remedial Design currently includes a proposal to perform additional excavation at the Elm Street Area, beyond that required to achieve the applicable subsurface SCL (i.e., 100 mg/kg), to address Town comments related to future

use of the Elm Street Area. Specifically, additional excavation was previously proposed for the purpose of: (1) installing a 40-inch thick engineered cover system in lieu of the asphalt cap specified in the ROD and proposed in the Preliminary Design Report; and (2) establishing utility and tree planting corridors for future use by the Town. That proposal was based on certain conditions, as further described in GE's May 2, 2007 submittal, including: (1) the location and depth (and, for the utility corridors, width) of the utility and tree planting corridors would be as shown in figures included within that submittal; (2) the over-excavated material would be used as backfill in deeper excavations that are located within the horizontal extent of the engineered cover system; and (3) confirmation soil sampling would not be required in any areas within which the depth of over-excavation is one foot or more. Based on comments on the Intermediate LTTD and OSD Design Reports, this latter condition has been modified such that confirmation soil sampling is not required in areas within which the depth of over-excavation is two feet or greater. As noted in Section 2.4, the Town of Milford subsequently notified EPA and GE that the Town had elected to eliminate the proposed memorial park restoration design for the Elm Street Area in lieu of a design that proposed additional parking. This modification resulted in the elimination of all of the utility corridors proposed in the December 2007 Final Design Report, except for the corridors associated with the replacement storm sewer line and the existing water line along Keyes Drive. As indicated in the response to comments submitted with the December 2007 Final Design Report, if EPA requires confirmation sampling even in areas where the over-excavation equals or exceeds 2 feet, then an alternate approach will be considered that is more consistent with that envisioned by the ROD. For the alternate approach, the replacement storm sewer utility corridor would be sampled below the excavation required to meet the 100 mg/kg subsurface SCL to determine if the 25 mg/kg SCL set for the utility and tree planting corridors is achieved, and only those soils that do not meet the 25 mg/kg SCL would be sent off-site for disposal. Such sampling could be performed before initiation of the soil remedy, or incrementally after completing the required excavation in the applicable areas.

GE has estimated that the over-excavation necessary to install the engineered cover system, replacement storm sewer, storm water retention area, and gabion wall restoration components at the Elm Street Area would involve the excavation of an additional 1,310 cy of soil at the Elm Street Area (as indicated in Table 11), which would be used as backfill for the deeper excavations under the cover system. Similar to the soil removal limits necessary to achieve the SCLs at the Elm and Mill Street Area, certain of the excavations associated with the installation of the engineered soil cover and/or storm water retention may require excavation sloping or the installation of excavation supports to perform the work in a safe manner. The soil removal limits for the excavation cells subject to such additional excavation are identified on Figure 10 and Technical Drawing G-11.

As previously indicated, to help support the excavations, the limits of excavation in this revised Final Design Report include sloping some of the excavation sidewalls. Such excavation sidewall sloping is illustrated on of Technical Drawings S-2 and S-9, and involves additional over-excavation. Specifically, this sloping of the excavation sidewalls increases the volume of excavation at the Elm Street Area by approximately 1,840 cy, and increases the volume of excavation by approximately 950 cy at the Mill Street Area.

In summary, the combined limits of excavation associated with achievement of the SCLs and over-excavation for the installation of the cover system, establishing the replacement storm sewer utility, storm water retention area, and gabion wall restoration components at the Elm Street Area are presented on Figure 11 and Technical Drawings G-12 and S-2 for the Elm Street Area and Figure 12 and Technical Drawings G-15 and S-9 for the Mill Street Area. As indicated in Table 12, the revised total volume of material subject to excavation at the Elm and Mill Street Areas is approximately 36,305 cy, which includes approximately 2,000 cy of slurry material associated with the installation of the SPTC walls at the Mill Street Area that will also require off-site disposal.

As indicated earlier in this section, the limits of soil removal were developed using a next cleanest point methodology. This approach to determining the limits of excavation is, in conjunction with the extensive pre-design and supplemental design investigations that were performed (which involved collection of over 1,800 surface and subsurface soil samples), sufficiently conservative to eliminate the need for a site-wide confirmatory soil sampling program (and the negative impacts on constructability of such a program). However, as requested by EPA in its February 13, 2007 letter, a VSP was developed and included in the Intermediate Design Reports. Based on comments provided by EPA in their November 1, 2007 comment letter for those submittals, a revised VSP was provided in Appendix A of the December 2007 Final Design Report. That VSP was revised again to incorporate the results of the pre-construction verification soil sampling activities performed under the SDDC Work Plan between May and October 2012. The revised VSP provided in Appendix A involves of the collection of approximately 200 confirmation samples for excavation bottoms and sidewalls at both the Elm and Mill Street Areas. As indicated therein, the results of those confirmation samples could warrant still further revisions to the limits of soil removal described in this herein. Additional details regarding the confirmation sampling activities that will be performed at the Site are provided in VSP in Appendix A to this revised Final Design Report.

3. Site Preparation Activities

3.1 Overview

Several site preparation activities will be conducted prior to initiating construction of the OU-1 soil remedy. These activities will include, but will not be limited to:

- Performance of certain accelerated Remedial Action items (ARAIs) described in the July 2012 TSOW;
- Contractor procurement;
- Providing for site controls and access;
- Obtaining appropriate approvals;
- Identifying substantive requirements and achieving same;
- Identifying and establishing the exclusion zones (EZs), contaminant reduction zones (CRZs), and support zones (SZs);
- Identifying and protecting utilities;
- Establishing erosion and sedimentation controls;
- Site clearing;
- Protecting/decommissioning groundwater monitoring wells;
- Constructing temporary staging areas and decontamination areas; and
- Implementing the traffic control measures specified in the TR/TA Report (see Appendix E).

This section provides a general overview of various tasks and procedures associated with these activities. Specific details regarding the ARAIs are provided in Section 3.2. Specific details regarding the remainder of the site preparation activities will be included in project control documents specified in Section 1.6 (i.e., the RAWP) and/or project-related submittals provided by the selected remedial contractor (the Remedial Action Contractor). The Remedial Action Contractor will be ultimately responsible for determining the means

and methods for implementing the site preparation activities (excluding the ARAIs); however, the Remedial Action Contractor's approach (as detailed in one or more technical submittals to be prepared by the Remedial Action Contractor prior to performing the applicable activity) will be subject to review by the Design Engineer (on behalf of GE).

3.2 Performance of Accelerated Remedial Action Items

During the November 8, 2011 meeting to discuss EPA's September 30, 2011 letter providing comments on the December 2007 Final Design Report, it was agreed that GE would provide a listing of certain elements of the Remedial Design that could be completed in 2012 prior to the initiation of the Remedial Action pursuant to Section IX of the UAO (as modified). GE provided a listing of six potential ARAIs to EPA for consideration on December 22, 2011. Those potential ARAIs included the following activities:

- Construction of the alternate access/parking area for Keyes Park;
- Construction of parking area improvements for Tax Parcel 25-11;
- Relocation of the southern rail siding adjacent to the Mill Street Area;
- Decommissioning of certain existing monitoring wells;
- Relocation of overhead utilities along Mill Street; and
- Relocation of overhead utilities along Keyes Drive.

EPA subsequently approved five of the six ARAIs (excluding the monitoring well decommissioning) in a letter to GE dated March 28, 2012. In accordance with that letter, GE submitted the draft TSOW for the ARAIs on July 12, 2012. That document provided sufficient details about the ARAIs for prospective contractors to prepared proposals to perform the work associated with those ARAIs. That submittal also included responses to certain comments provided in EPA's September 30, 2011 letter responding to the December 2007 Final Design Report that applied to the ARAIs. EPA provided approval of the TSOW in a letter to GE dated August 17, 2012. That approval also included certain comments on the ARAIs, to which GE provided responses in a letter to EPA dated August 27, 2012.

GE conducted a pre-bid meeting with prospective contractors for the Keyes Park alternate access/parking area improvements and Tax Parcel 25-11 parking area improvements on September 12, 2012. The remaining ARAIs were not a part of the contract associated with

the September 12, 2012 pre-bid meeting, as those activities require work by third parties (i.e., Guilford for relocation of the southern rail siding and Public Service of New Hampshire [PSNH]/FairPoint Communications [FairPoint] for the relocation of the overhead utilities along Mill Street and Keyes Drive), as further described below. Addendum #1 to the TSOW for the ARAIs was issued on September 19, 2012 and included responses to questions from the prospective contractors as well as a revision to the layout of the alternate access/parking area for Keyes Park, based on comments provided by the Town of Milford. Concurrently with GE's receipt and review of the prospective contractor's proposals, EPA negotiated access to Tax Parcel 25-11 for the construction and post-construction phases of the Remedial Action. That access agreement was executed on October 19, 2012. Following receipt and review of the various contractor proposals, the contract for the Keyes Park alternate access/parking area improvements and the Tax Parcel 25-11 parking area improvements was awarded to Steve Trombley Excavating, LLC on October 22, 2012. On or about October 11, 2012, the Town of Milford notified EPA that it preferred to postpone the Keyes Park alternate access/parking area improvements until just prior to implementation of the OU-1 soil remedy. As of this submittal, the Tax Parcel 25-11 parking area improvements have been initiated and will be completed in 2012.

With regard to the other ARAIs (i.e., relocation of the overhead utilities along Mill Street and Keyes Drive and relocation of the southern rail line), GE has had extensive discussions over the last several months with the three organizations (i.e., PSNH, FairPoint, and Guilford) that will be responsible for performing the work associated with these ARAIs. As part of those discussions, GE has provided the technical drawings associated with the relocation of the overhead utilities and the relocation of the southern rail siding to the appropriate technical staff within each organization. Additional details are provided below.

GE representatives have twice met representatives of PSNH and FairPoint at the Site to review the proposed overhead utility relocation plans, including most recently on October 17, 2012. Subsequent to that meeting, GE provided the proposed survey coordinates to FairPoint (who will perform the installation of the replacement/temporary utility poles) along with summaries of the soil sample data in the vicinity of the proposed pole locations via electronic mail data November 7, 2012. It should be noted that one of the proposed replacement utility poles will be located on railroad property at the Mill Street Area. Accordingly, Guilford has been provided copies of the overhead utility relocation plan for the Mill Street Area and GE has requested permission to install a new pole on railroad property and relocate the overhead utilities from the existing pole located on railroad property to this new pole.

With regard to the relocation of the southern rail line, GE's May 10, 2007 letter to EPA and the Intermediate LTTD and OSD Design Reports indicated that GE was informed in a

March 28, 2007 meeting with representatives of Guilford that Guilford would, based on current demand, likely approve removal of the southern rail line on a short-term bases (i.e., two to four weeks), but indicated that removal of the southern rail line on a more protracted basis would not be acceptable without changes to its current infrastructure. Guilford also stressed that demand can change on short notice, and that the demand in the future could not be predicted. Since submittal of the Intermediate Design Reports on June 4 and 12, 2007, respectively, Guilford informed GE that it would not allow short-term removal of the southern rail line. Regarding removal of the southern rail line on a long-term basis (i.e., several months), as assumed in the Intermediate LTTD and OSD Design Reports, Guilford indicated that 1,000 feet of alternate siding would need to be constructed to the immediate west of the current location (i.e., between the Mill Street Area and West Street), that such a siding would need to be installed by Guilford, but that Guilford was not willing to incur the cost to construct the alternate siding. No agreement had been reached with Guilford for the long-term removal of the southern rail line prior to submittal of the December 2007 Final Design Report. Since submittal of that report, GE has continued negotiations with Guilford regarding: an access agreement for the construction and post-construction phases of the OU-1 soil remedy; an agreement to relocate the southern rail siding; and an Environmental Protection Easement and Declaration of Restrictive Covenants. While those negotiations have not yet resulted in the execution of the above-listed documents, this revised Final Design Report is based on the assumption that those documents will be successfully executed and the southern rail line will be relocated.

As none of the ARAIs have been completed at the time of this submittal, the applicable Technical Drawings are included herein. Specifically, the following technical drawings are related to the performance of the ARAIs:

- Technical Drawing G-4B – Utility Pole Relocation Plan – Elm Street Area
- Technical Drawing G-4D – Parking Area Plan – Parcel 25-11
- Technical Drawing G-5B – Alternate Access/Parking Area Plan – Keyes Park
- Technical Drawing G-6B – Utility Pole Relocation Plan – Mill Street Area

A specific technical drawing showing the relocation of the southern rail siding is not included in this revised Final Design Report as the design details associated with that work will be developed by Guilford. However, Technical Drawing G-24 has been revised to indicated that the southern rail siding will not be restored adjacent to the Mill Street Area following the completion of the Remedial Action.

3.3 Remedial Action Contractor Procurement

Several activities related to the identification and selection of a qualified remedial contractor to implement the OU-1 soil remedy will be performed prior to the start of construction activities. These activities are anticipated to include, but not be limited to, the following:

- Identification of prospective remedial contractors and submittal of a list of such contractors to the EPA, as required by the UAO (as modified);
- EPA review and comment on the proposed list of remedial contractors;
- Attendance at a pre-bid meeting and site visit;
- Preparation of bid proposals by prospective contractors;
- Review of prospective remedial contractors' bid proposals;
- Selection of the Remedial Action Contractor and execution of the Remedial Action Contract;
- Submittal of the Remedial Action Contractor's letter of acceptance to the EPA, as required by the UAO (as modified); and
- Preparation of contractor submittals for review.

Following EPA approval of the revised Final Design Report, Contract Documents in the form of a bid package will be distributed to EPA-approved, qualified prospective remedial contractors to solicit bids for the performance of the OU-1 soil remedy. Prospective contractors wishing to perform the work will be required to submit a bid proposal in accordance with the requirements contained in the Contract Documents. Following distribution of the bid packages, a pre-bid meeting and site visit will be conducted with all prospective remedial contractors. The pre-bid meeting and site visit will allow the prospective contractors to visually examine existing site conditions and thoroughly acquaint themselves with the work required and potential challenges associated with implementing the remedial action. During the pre-bid meeting and site visit, prospective remedial contractors will have the opportunity to verify all existing site conditions (including, but not limited to, materials of construction, structural conditions, and environmental conditions) to facilitate the preparation of an accurate bid proposal and work schedule.

Following the pre-bid meeting, site visit, and issuance of any addenda, prospective remedial contractors will submit their bid proposals for review. The review of the bid proposals will include, but not be limited to:

- Conformance with the Contract Documents;
- Proposed approach and methods for performing the remediation activities;
- Comparison of bid prices;
- Proposed work schedule;
- Experience and qualifications; and
- Acceptance of or comments on the proposed Remedial Action Contract.

Following review of the bid proposals, the Remedial Action Contractor will be selected and the contracting process will be initiated.

Following award of the contract, the Remedial Action Contractor will be required to provide several pre-mobilization submittals, in accordance with the Contract Documents including the Technical Specifications. The Remedial Action Contractor will not be allowed to mobilize to the Site prior to an acceptable review by GE and ARCADIS of all required pre-mobilization submittals.

3.4 Site Controls, Site Access, and Alternate Residential Access

Throughout the remedial action, the Remedial Action Contractor will be required to institute site controls as a measure for protecting the public health, safety, welfare, and the environment, and to maintain the effectiveness and integrity of the selected remedy. In general, these site controls will consist of fencing and other means to restrict access to the Site. The approximate working limits at and near the Elm and Mill Street Areas (around which such site controls would be placed), are depicted on Technical Drawings G-4A (Elm Street Area), G-5A (Keyes Park), and G-6A (Mill Street Area). The Remedial Action Contractor will be required to restrict all activities associated with the excavation and the off-site disposal of excavated material to the working limits designated on these Technical Drawings. However, off-site staging/storage of clean construction materials or equipment (e.g., parking of personal vehicles, clean backfill/equipment, project trailers, etc.) may be necessary given existing site constraints.

The Remedial Action Contractor will be responsible for providing all elements of work area security necessary to prevent the unauthorized entry of persons onto the Site. Chain-link fencing and jersey barriers will be installed and maintained along the perimeter of the Site, including along the banks of the Souhegan River located adjacent to the Elm Street Area. Warning signs will be posted along the perimeter fencing and in the vicinity of the entrance gates notifying the public that unauthorized entrance to the work area is prohibited. A sign-in/sign-out sheet will be maintained at the Site office trailer(s) for the duration of the remediation activities. Streets adjacent to the Site may be closed, or partially closed, except for emergency vehicle use, as necessary, during certain periods of the construction activities (i.e., excavation and backfilling of materials located within Elm and Mill Streets).

Implementation of safe work practices will also be required to provide for additional security during performance of the remediation activities. Safe work practices that will contribute to overall site security include, at a minimum, the following:

- Installing and maintaining temporary construction barriers (e.g., fencing, warning tape) around all open excavations, cleaning/decontamination areas, stockpile areas, and other potentially dangerous areas;

- Parking heavy equipment within designated, secured areas and removing keys at the end of each work day or during periods of work shutdown;

- Maintaining an organized work area, including proper storage of all tools, materials, and equipment;

- Employing or designating health and safety personnel at the Site while remediation activities are being conducted; and

- Employing or designating security personnel to prevent the entry of unauthorized personnel to the Site and to conduct periodic security checks during non-working hours.

In general, access roads within and outside of the working limits at the Site will be maintained to allow for uninterrupted equipment/personnel access. To provide equipment access to the work areas, temporary access roads and gravel equipment pads may be constructed for the staging of clean equipment and/or materials. Access roads will be constructed by first performing limited grading (if necessary), then placing a geotextile and gravel on the graded surface. The actual locations of the temporary access roads will be determined by the Remedial Action Contractor based upon equipment limitations and access requirements.

A discussion regarding certain specific site controls to be implemented by the Remedial Action Contractor at both the Elm and Mill Street Areas is provided below, as well as on the Technical Drawings (which are further discussed in Section 8.1 and included in Appendix B) and the appropriate Technical Specifications (which are further discussed in Section 8.2 and included in Appendix C). Additional details regarding site access as it pertains to the establishment of support zones, contaminant reduction zones, and exclusion zones are provided in Section 3.6.

3.4.1 Elm Street Area

The main portion of the Elm Street Area (Tax Parcel 25-12) is currently owned by the Town, the majority of which is enclosed by fencing (Technical Drawing G-4A). The Elm Street Area is bounded east by Tax Parcel 25-13 (a Revolutionary-War era cemetery, also owned by the Town), to the north by the Souhegan River, to the west by Keyes Drive (a paved access road to Keyes Field, located northwest of the Site, and also owned by the Town), and to the south by Elm Street. Access to Tax Parcel 25-12 will be gained via Elm Street and Keyes Drive.

Prior to commencement of the OU-1 soil remedy, the Remedial Action Contractor will be responsible for making any necessary improvements/relocation and/or construction of new temporary fencing to secure the Site from unauthorized access. Excavation activities are required within Elm Street, as shown on Technical Drawing G-12. As illustrated on that drawing, the excavation activities extend through the northern (west-bound) lane of Elm Street; the southern (east-bound) lane of Elm Street will remain open maintaining two-way, one lane traffic and will not be excavated, except for one necessary excavation to install a portion of a replacement storm sewer utility, as further discussed in Section 3.7. Prior to performance of the excavation activities within Elm Street, the northern (west-bound) lane of Elm Street will be temporarily closed (as further discussed in Section 4.7.3). The existing chain-link fencing located along the southern side of the Elm Street Area (i.e., northern side of Elm Street) will be realigned to include the northern lane of Elm Street, thereby facilitating access to the areas requiring excavation from the Elm Street Area, and to secure the area from unauthorized access. GE, ARCADIS, and the Remedial Action Contractor will review the T-series technical drawings provided in Appendix B and the results of the traffic analysis provided in Appendix E to determine the methodology and schedule for the excavation activities. Periods of non-peak traffic will be considered for the performance of this work. Once the excavation and backfilling activities within Elm Street are complete, the Remedial Action Contractor will restore the Elm Street right-of-way and Elm Street will be reopened for vehicular use. Pedestrian traffic along the northern side of Elm Street (adjacent to the Elm Street Area) will not be restored until the end of the Remedial Action. The traffic control activities during this work are discussed in Section 3.14.

Based on the scope of the Remedial Action described in Section 4, it is currently anticipated that Keyes Drive will be closed to the public for the duration of the Remedial Action. During site preparation activities or periods when limited remedial actions are ongoing, the southernmost portion of Keyes Drive (adjacent to Elm Street) will remain open (if possible) to provide access to the residence on Tax Parcel 25-11 (located on the corner of Keyes Drive and Elm Street), as indicated on Technical Drawing G-4A. As indicated in Section 1.2, GE provided details regarding parking area improvements for this property in a letter to EPA dated November 2, 2009. Based on subsequent discussions with the property owner, revisions to that plan were incorporated into Technical Drawing 3 of the July 2012 TSOW, as described in Section 3.2. Technical Drawing G-4D (Appendix B) provides the latest version of the design for the parking area improvements that will be implemented at this property as an ARAI prior to the initiation of the Remedial Action for the OU-1 soil remedy. During full-scale excavation or treatment activities, approximately one-half the width of the southernmost section of Keyes Drive will remain open to provide access to the residents of Tax Parcel 25-11, as indicated on Technical Drawing G-4C. No special provisions for access to the property are necessary for the chiropractor's business at this property because the parking for the business is located along Elm Street.

3.4.2 Keyes Park

As discussed in the previous section, the implementation of the Remedial Action will require the closure of Keyes Drive for the duration of the OU-1 soil remedy. Based on comments provided by the Town of Milford and EPA regarding the closure of Keyes Drive during the Remedial Design, GE has had numerous discussions with the Town regarding the provision of alternate vehicular access to Keyes Park during the implementation of the OU-1 soil remedy. The Town has indicated that alternate access to Keyes Park is possible via a gate located on the western property boundary of Keyes Field and the former Permattach property. As described in Section 3.2, alternate access/parking area improvements have been designed for this area, with input provided by the Town of Milford. GE provided initial details regarding the alternate access/parking area for Keyes Park in a letter to EPA dated October 14, 2008. Based on subsequent discussions with the Town of Milford, revisions to that plan were incorporated into Technical Drawing 2 of the July 2012 TSOW. Technical Drawing G-5B (Appendix B) provides the latest version of the design for the alternate access/parking area improvements that will be implemented as an ARAI prior to the initiation of the Remedial Action in order to facilitate public access to Keyes Park during the OU-1 soil remedy. The alternate access to Keyes Park will not be used to implement the OU-1 soil remedy. However, the alternate access would allow the Town to continue using those portions of Keyes Field that are not needed to implement the OU-1 soil remedy, and could also be used on a long-term basis for emergency purposes. Upon completion of the remediation activities and restoration of Keyes Drive, the Remedial Action Contractor will

remove the alternate access/parking area and restored the affected area, unless the Town elects to maintain the alternate access/parking area.

3.4.3 Mill Street Area

The Mill Street Area (Tax Parcel 25-111) is currently owned by the Town. Temporary fencing was installed around the perimeter of this parcel during the PDI. This property is bounded to the west by Tax Parcel 25-110 owned by Draper, to the north by an active railroad owned and operated by Guilford, to the east by Cottage Street, and to the south by Mill Street. Excavation of material subject to off-site disposal will be performed in all of these areas, including a small portion of Cottage Street. Access to this area will be gained via Mill Street.

As shown on Technical Drawing G-15, excavation activities will be conducted within Mill Street. Based on space limitations at and near the Mill Street Area, it is currently anticipated that portions of Mill Street adjacent to Tax Parcels 25-110 and 25-111 will be closed at various times during the performance of the remedial action. In addition, it is anticipated that the remediation activities at the Mill Street Area will be performed in two phases such that partial access to the driveway on Tax Parcel 25-94 will be maintained throughout the performance of the OU-1 soil remedy, if possible, as indicated on Technical Drawing G-6C. Upon completion of the Remedial Action (including the realignment and restoration of Mill Street), Mill Street will be reopened for pedestrian and vehicular use. Traffic control activities to be performed during excavation activities within and near Mill Street and Cottage Street are discussed in Section 3.14 below.

Because closure of the street will impact access to certain residential properties located on the south side of Mill Street, GE has further evaluated providing temporary alternate access to the affected property owners. With respect to Tax Parcels 25-93, 25-93A, and 25-94, GE has evaluated providing alternate access at the locations illustrated on Technical Drawing G-6C. As indicated in Section 1.2, revisions to portions of the alternate access plan for these properties were provided in GE's April 21 and December 2, 2010 letters to the EPA. Technical Drawing G-6C provides additional details regarding alternate access to these residential properties. Under this scenario, the Remedial Action Contractor would install privacy fencing along the southern boundary of the work area to serve as a visual, dust, and noise barrier, at the locations indicated on Technical Drawing G-6C. Upon realignment and restoration of Mill Street, the temporary access to the properties on the south side of Mill Street will be removed and the portions of those properties where the temporary access was provided will be restored to their preconstruction conditions. As discussed in the Intermediate Design Report, GE initiated discussions regarding this project, its potential impacts, and the provision of alternate access during the project with the owners of Tax

Parcels 25-93, 25-93A and 25-94. Based on the discussions to date, GE has determined that relocation of certain impacted residents will not be necessary during the remedial action.

Regarding access for the residence (Tax Parcel 25-109) abutting the west side of the Draper property (Tax Parcel 25-110), GE anticipates implementation of the Remedial Action such that access to Tax Parcel 25-109 will be maintained, as indicated on Technical Drawing G-7. Specifically, with the exception of some limited coordination with construction equipment coming to and from the Site, it is expected that the residents of Tax Parcel 25-109 will have full access to their property.

3.5 Substantive Requirements of Regulations Imposing Permitting Requirements

As provided under the Comprehensive Environmental Response, Compensation, and Liability Act (CERCLA), ARARs must be identified and achieved. The identification and achievement of ARARs is discussed in Section 7.

3.6 Identification and Establishment of Exclusion Zones, Contaminant Reduction Zones, and Support Zones

As part of the Remedial Action Contractor's site preparation activities, an EZ, CRZ, and SZ will be established at both the Elm and Mill Street Areas. Additional information regarding the purpose of the EZs, CRZs, and SZ and the anticipated management of access to the work areas is presented in the following sections.

3.6.1 Exclusion Zones

An EZ is typically established to isolate portions of a site where remediation activities are ongoing; thereby preventing personnel not associated with the remediation activities from coming in direct contact with COCs at the Site. Therefore, only personnel with the proper health and safety training, medical clearance (as needed) and equipment, as identified in the Remedial Action Contractor's site-specific HASP, are allowed into an EZ.

The EZ(s) will be delineated by any one or a combination of the following methods:

- Use of the perimeter fence around the area as the boundary of the EZ;
- Placement of orange high-density polyethylene (HDPE) fencing around the perimeter of the EZ; and/or

- Placement of yellow caution tape and cones around the perimeter of the EZ.

Access to and egress from the EZs must be through CRZs (further described below), which is where the only break in the fencing delineating the EZs will be permitted. As previously indicated, the final locations of the EZ(s) for each area will be determined by the Remedial Action Contractor based on site-specific conditions, logistics/sequencing of the Remedial Action, and health and safety considerations.

3.6.2 Contaminant Reduction Zones

A CRZ or transition zone is established immediately adjacent to the entrance(s) of an EZ. The purpose of the CRZ is to provide a transition area between the EZ and SZ. One primary function of the CRZ is to establish an area where site personnel preparing to enter the EZ can perform final equipment preparation and donning of appropriate personal protective equipment (PPE). The second function of the CRZ is to serve as the location where decontamination procedures for personnel/equipment previously performing remedial activities can be performed prior to leaving the work area. Specifically, the CRZ is the location where personnel typically perform the following activities:

<u>Personnel Entering the EZ</u>

- Final operational equipment check;
- Donning of any necessary protective over-boots, gloves, and/or respiratory equipment; and
- Taping of all interfaces between Tyvek over-suit and gloves/boots.

<u>Personnel Exiting the EZ</u>

- Performance of equipment decontamination procedures;
- Performance of personal decontamination procedures as identified in the Remedial Action Contractor's HASP; and
- Containerization of all disposable equipment and PPE for subsequent off-site disposal.

A CRZ will be established at both the Elm and Mill Street Areas. Consistent with the approach for the EZs discussed above, the location of the CRZs will be established by the Remedial Action Contractor based on site-specific conditions, the final logistics/sequencing

of the OU-1 soil remedy, as well as health and safety considerations. Similar to the EZs, the CRZs will likely be positioned at different locations throughout the performance of the remediation activities. As a result, the CRZs are not illustrated on the enclosed Technical Drawings. Nevertheless, the CRZ will be immediately adjacent to the entrance(s)/exit(s) to the EZ. Similar to the EZs, the boundary of the CRZs must be delineated by any combination of fencing, warning tape and/or cones.

3.6.3 Support Zone

The SZ is the location where all field offices, project trailers, and/or clean construction equipment/materials are located. The SZ serves as the location where most non-intrusive remedial activities take place, such as project-related meetings and safety meetings. The SZ also serves as the clean equipment and materials storage area, break/eating and drinking area, location of sanitary facilities, preliminary equipment maintenance area (clean equipment only), preliminary PPE donning area, etc. With the possible exception of portable sanitary restroom facilities and/or limited staging areas for clean construction equipment/materials (both of which may also be located at the Mill Street Area), the main SZ for the Site will be established in the portion of Keyes Park adjacent to the Elm Street Area, as shown on Technical Drawing G-5A. However, the final location/configuration of the SZ(s) will be determined by the Remedial Action Contractor and will be based on discussions with the Town and the location/availability of the necessary utilities (e.g., electric, telephone, etc.).

3.6.4 Establishment of Zones and Management of Access

For the purposes of this revised Final Design Report, the perimeter of the Elm and Mill Street Areas are considered the primary EZs due to the fact that the majority of each area contains impacted materials that are subject to excavation. In this manner, the Remedial Action Contractor will be required to limit access to the Elm and Mill Street Areas in their entirety. Such access will be primarily maintained by the existing perimeter fencing, augmented as necessary with additional jersey barriers and/or chain-link fencing equipped with privacy slats. Access to these areas will be managed through project trailers located in the support zone at Keyes Park and restricted to only those personnel possessing the proper health and safety training and wearing the appropriate personal protective equipment.

With the primary EZs, it is anticipated that access to the work areas will be managed in the following manner. The Remedial Action Contractor will establish smaller, secondary EZs around the areas of active excavation, material handling/loading, and restoration activities. These secondary EZs will be delineated with high visibility construction fencing with

designated personnel and equipment access points. Separate personnel and vehicular CRZs will be constructed adjacent to each secondary EZ and within the perimeter fencing. If, necessary, clean access paths/walkways or roads (constructed of geotextile, woodchips, and/or gravel, etc.) will be constructed over portions of the Elm and Mill Street Areas that have not yet been subject to remediation so that personnel and vehicles exiting the CRZs can access the gates in the perimeter fencing. In this manner, contractor personnel and vehicles can travel from the active work zones (i.e., secondary EZs) without coming into contact with impacted site soils. This conceptual approach will also enable the Remedial Action Contractor to relocate active work zones (secondary EZs) and CRZs as the remediation activities progress across the Elm and Mill Street Areas.

3.7 Utility Services

The Remedial Action Contractor will be responsible for coordinating with local utility companies to procure service for several of the temporary on-site facilities that will be utilized during implementation of the Remedial Action (e.g., temporary water treatment system, field office trailers, etc.). In addition, the Remedial Action Contractor will be responsible for identifying, protecting, relocating, or abandoning both aboveground and underground utilities, as required to facilitate performance of the Remedial Action. As such, the Remedial Action Contractor will be required to contact the appropriate utility-locating agencies (e.g., Dig-Safe, Underground Facilities Protective Organization [UFPO], etc.) prior to the start of excavation activities. Certain active utilities, if located within/adjacent to the excavation areas, will require demarcation and implementation of precautionary measures or temporary relocation to safeguard the utilities during intrusive activities. These activities shall be coordinated by the Remedial Action Contractor with the appropriate utility companies. The Remedial Action Contractor will also be required to perform monitoring during intrusive activities to verify that a minimum safe distance is maintained during any site work performed in proximity to above-ground or underground utilities.

Figures 2 and 3 and Technical Drawings G-2 and G-3 illustrate the utilities present at the Elm and Mill Street Areas. Based on the scope of the Remedial Action and the location of the utilities presented on these figures, GE has identified certain utilities at the Elm and Mill Street Areas that will either require protection or removal and replacement to facilitate performance of the OU-1 soil remedy. Specifically, GE has identified the following utilities that may be impacted by the performance of the Remedial Action:

<u>Elm Street Area</u>

- Utility poles located on along Elm Street and adjacent to Keyes Drive;

- Water line adjacent to Keyes Drive; and
- Storm sewer located along the east portion of the Elm Street Area.

Mill Street Area

- Utility poles located on along Mill Street; and
- Water and sewer lines within Mill Street.

With respect to all Site utilities, the Remedial Action Contractor will be responsible for determining the need to protect or relocate these utilities based on a number of factors, such as: the location of the utilities; the scope of the remediation activities or other components of the OU-1 remedy proposed in the vicinity of the utilities; the duration for which the utilities would need to be protected; the feasibility of protection versus interruption, relocation, and/or replacement of the utility; the overhead clearance for above grade utilities or amount of cover over underground utilities, etc. Regardless, it is anticipated that some or all of the utilities may need to be relocated to facilitate performance of the Remedial Action. In such an instance, the Remedial Action Contractor will be responsible for ensuring that minimal, if any, interruption of service is observed by adjacent property owners and residents. Additional specific details regarding the relocation of overhead utilities at the Elm and Mill Street Areas and the construction of the replacement storm sewer utility at the Elm Street Area are provided in the following sections.

3.7.1 Relocation of Overhead Utilities

As indicated in Section 3.2, the relocation of overhead utilities located along Mill Street and Keyes Drive was identified by GE as a potential ARAI. Technical Drawings G-4B and G-6B of the TSOW provided details regarding the proposed relocation of these overhead utilities. As also noted therein, GE has participated in ongoing discussions with representatives of PSNH and FairPoint regarding the relocation of the existing overhead utilities along Mill Street and Keyes Drive. GE has also provided information to Guilford regarding the replacement of one utility pole located on railroad property adjacent to the Mill Street Area with another pole on railroad property in support of the proposed relocation of the overhead utilities. To facilitate these ongoing discussions and the planning for the relocation of these overhead utilities, GE has provided the above referenced technical drawings to PSNH and FairPoint along with survey coordinates and summaries of the soil sample data in the vicinity of the proposed new utility pole locations. GE has also provided a copy of the technical drawing for the relocation of the overhead utilities at the Mill Street Area to Guilford to facilitate the review of the location for the proposed new utility pole on railroad

property. As indicated in Section 3.2, it is anticipated that the relocation of the overhead utilities along Mill Street and Keyes Drive will be implemented prior to the initiation of the OU-1 soil remedy.

3.7.2 Replacement Storm Sewer Utility

Regarding the storm sewer utility located along the east side of the Elm Street Area, the ROD (as amended) requires the closure in place of the existing utility and the installation of a replacement storm sewer in a utility corridor that is accessible to future Town of Milford utility workers. As shown on Figure 2, the existing storm sewer line conveys storm water from the drainage ditch originating at the Mill Street Pond, into a culvert running under the Elm Street Area, to the Souhegan River via Outfall 05. In support of the sewer replacement at the Elm Street Area, GE performed a comprehensive utility survey of the storm sewers and outfall pipes in the vicinity of the Elm Street Area. That utility survey (which included a video survey) was included as Attachment E of Addendum No.1 to the Preliminary Design Report.

The results of the video inspection indicated that the storm sewer contains obstructions in at least two locations, including one location under Elm Street (where the pipe appears to have collapsed) and a second location on the Elm Street Area at monitoring well MW-02A, which was installed through the storm sewer during the RI. Because flow through this pipe was significantly restricted, causing storm water to back up, the Town installed an 8-inch diameter overflow pipe connecting catch basin CB-1 (located on Cottage Street) to adjacent manhole DMH-1 (also located on Cottage Street). Manhole DMH-1 is connected to the 12-inch storm sewer line that runs east down Elm Street. Thus, during surcharge conditions, storm water in catch basin CB-1 is diverted away from the storm sewer line that runs to Outfall 05. Storm water will continue to flow through this bypass pipe until the replacement storm sewer is installed. Further, the overflow pipe between catch basin CB-1 and manhole DMH-1 will remain in service following construction of the replacement storm sewer for the purpose of providing overflow capacity.

Based on a review of the information presented in the aforementioned utility survey, GE proposes to replace the section of the existing 18-inch-diameter storm sewer line from catch basin CB-1 located on Cottage Street, adjacent to the Snack Corner Mobil station, to Outfall 05 at the Souhegan River. GE anticipates performing a portion of this work during the site preparation phase of the OU-1 soil remedy. Specifically, GE proposes to replace the portion of the storm sewer between catch basin CB-1 and new manhole MH-1, which GE proposes to install on the Elm Street Area (see Technical Drawing G-20), during the site preparation phase, prior to initiating the soil excavation work, for the following reasons:

- Installation of the portion of the sewer pipe located between catch basin CB-1 and proposed new manhole MH-1 could possibly be performed as a non-remedial activity because such excavation activities would require minimal, if any, excavation of soils subject to removal to achieve the SCLs applicable to the Elm Street Area.

- Installation of new manhole MH-1 on the Elm Street Area and the replacement storm sewer piping to catch basin CB-1 from new manhole MH-1 would enable GE to pump miscellaneous remediation-related waters (e.g. excavation water, collected precipitation, decontamination waters, etc.) from MH-1 to the temporary water treatment facility staged at the Mill Street Area via hoses that run through the restored sewer pipe and along the drainage ditch to the Mill Street Area, obviating the need to transport these waters via tanker truck.

- Replacement of this portion of the utility will require trenching across Elm Street. It is anticipated that installation of the replacement sewer pipe would be performed using a trench box. In an attempt to minimize the impact to local traffic, GE proposes to install the pipe across Elm Street followed by backfilling and temporary restoration of the excavated trench (i.e., backfilling the excavation to surface grade with gravel materials), prior to the remedial excavations thereby minimizing the length of interruption associated with the remedial excavations. However, final restoration of the pavement for the excavated trench may be performed at the same time as the restoration for the remedial excavations within Elm Street.

The route and depth of the replacement storm sewer are shown on Technical Drawing G-20. The ROD (as amended) specifies that the Town will provide the replacement storm sewer piping; this is also a requirement of the Town's Consent Decree with the EPA, dated February 8, 1999, as stated in Section VI.9.B therein. GE obtained the Town's relevant standard specification packages, including *Infrastructure Design, Construction, & Administration Standards* (October 1, 2007) and *Standard Regulations and Specifications for Design and Construction of Water and Sewer Infrastructure* (April 2007), relevant portions of which have been incorporated into the Technical Specifications included in Attachment C. Technical Drawing G-20 has been revised to include a reference to this specification for the miscellaneous components of the replacement storm sewer utility.

The initial section of the replacement storm sewer (from existing catch basin CB-1 on Cottage Street to new manhole MH-1 on the north side of Elm Street), which is about 115 linear feet, will be installed at a depth of approximately 10 to 12 feet below grade, which is approximately 4 feet below the 8-inch diameter line that is currently receiving the overflow discharge from catch basin CB-1. Installation of the replacement storm sewer at this depth should result in the replacement storm sewer pipe being installed below the existing utilities

on Cottage and Elm Streets. The Remedial Action Contractor will be required to protect/support the existing utilities during installation of the replacement storm sewer. Further, the Remedial Action Contractor will be required to install a temporary manhole between new manholes MH-1 and MH-2, at the location shown on Technical Drawing G-20, to connect the initial section of the replacement storm sewer from MH-1 to the existing storm sewer. This temporary connection will allow storm sewer flow to continue until the remaining section of the replacement storm sewer is installed. During installation of this section of the replacement storm sewer, GE anticipates that there will be impacts to the normal traffic flow, but closure of the Cottage Street and Elm Street roadways and detours should not be necessary. The traffic control measures associated with installation of this section of the new storm sewer piping are described below and included in the T-series of Technical Drawings presented in Appendix B and the TR/TA Report presented in Appendix E of this revised Final Design Report.

As noted therein and in Section 3.4.1, it is the current intent that the replacement storm sewer trenching activities across Elm Street will be performed in such a manner as to maintain one lane, two-way traffic during the installation of this portion of the replacement storm sewer across Elm Street. As such, the Remedial Action Contractor will be responsible for using necessary means and methods to maintain safe and orderly vehicular and pedestrian travel around the work area. The Remedial Action Contractor will provide flagman, lights, signs, barricades, detours, or temporary roadways, as necessary to complete the storm sewer replacement activities. At a minimum, traffic warning and control methods and devices will be designed, constructed, placed, and installed in accordance with the United States Department of Transportation Federal Highway Administration Manual on Uniform Traffic Control Devices (most current edition). Local police and emergency services, the Town Department of Public Works and school dispatchers will be notified by the Remedial Action Contractor prior to these and all utility replacement activities (as appropriate). In addition, GE, ARCADIS, and the Remedial Action Contractor will review the T-series technical drawings and the results of the traffic analysis provided in Appendix E to determine the methodology and schedule for the replacement storm sewer activities in an attempt to minimize (to the extent possible) impacts to vehicular traffic and the community. To the extent possible, these storm sewer replacement activities will be performed during non-peak traffic hours. Any temporary interruptions of access to public or private property will be coordinated with public officials and/or property owners, as appropriate.

Once this portion of the replacement storm sewer is installed and connected to the existing storm sewer and the temporary water treatment system (described in Section 4.6) has been constructed, the Remedial Action Contractor will be responsible for flushing the existing storm sewer system from the temporary water treatment system discharge location at the

Mill Street Area to Outfall 05. As part of these activities, the Remedial Action Contractor will be responsible for removing blockages present within the drainage system that can be reasonably be removed. The Remedial Action Contractor will be responsible for placing controls to prevent the flushed materials from entering the Souhegan River and will further be responsible for consolidating those materials for subsequent off-site disposal. Once the storm sewer system has been flushed, the temporary water treatment system will become operational and begin discharging to the drainage ditch adjacent to the Mill Street Area (following the necessary system startup testing described in Section 4.6.

The remaining section of the replacement storm sewer (i.e., the portion from the temporary manhole MH-1 to the new riverbank outfall) will subsequently be installed by the Remedial Action Contractor as part of the backfilling and site restoration activities at the Elm Street Area and following the completion of the remedial excavation activities. As shown on Figure 8, the new pipeline will be located in a utility corridor running along the east side of the Elm Street Area and outside the cover system until manhole MH-3 to facilitate future access by Town utility workers. A total of three new manholes and will be installed to provide access for future Town utility workers and facilitate future maintenance activities. The Remedial Action Contractor will coordinate the in-place closure of the existing stone culvert/storm sewer, either following completion of the remedial excavation activities or as part of the site restoration activities. Although the existing storm sewer system is damaged and provides limited drainage, this system will not be taken out of service/closed in place until after installation of the replacement storm sewer. The temporary manhole may be utilized to perform the in-place closure of the existing storm sewer. Finally, the Remedial Action Contractor will remove the temporary manhole between new manholes MH-1 and MH-2 and the associated service connection to the existing storm sewer pipeline will be removed at this time.

3.8 Erosion and Sedimentation Controls

Erosion and sedimentation controls will be installed at the Site before initiating the soil excavation work. The specific locations of these controls will be determined and/or modified in the field based on site-specific considerations related to drainage, topography, work activities, etc. The selection of specific erosion and sedimentation control measures for use during the Remedial Action will be based on, but not limited to, the scope of activities (e.g., proposed alteration of the area, sequencing of earth-moving activities, etc.), Site topography, type of ground cover, amount of anticipated run-off from the project area, and operational/maintenance considerations. In addition to the various physical controls that will be installed, certain operational and management practices (to be defined in the Remedial Action Contractor's site-specific plans) will be implemented throughout the project to provide an additional measure of erosion and sedimentation control.

Before initiating excavation activities, appropriate erosion control measures will be installed to minimize the potential for rainfall- or flood-induced migration of soils into or out of the areas subject to disturbance. These measures will likely include, at a minimum, the placement of silt fencing and/or staked hay bales along the edge of the Souhegan River, around active excavation areas, and/or upgradient and downgradient portions of the project area perimeter. Technical Drawings G-4A and G-6A show the approximate locations at which the Remedial Action Contractor will install the erosion and sedimentation controls at the Site. It should be noted that the locations of these controls may shift during the performance of the Remedial Action. For example, the Remedial Action Contractor will install erosion and sedimentation controls along the riverbank at the Elm Street Area during the site preparation phase of the project. However, the Remedial Action Contractor will not be required to maintain these controls once the steel sheeting is installed along the riverbank at the Elm Street Area (as further described in Section 4.2). Following restoration of the riverbank, erosion and sedimentation controls will be reinstalled at the top of the riverbank (since the riverbank will be restored with rip-rap) until such time that the vegetative cover is established. Typical construction details for silt fencing and staked hay bales are presented on Technical Drawing G-25.

Erosion and sedimentation control devices will be monitored and maintained and/or modified throughout the duration of the OU-1 soil remedy, as necessary, based on Site conditions and activities. The erosion and sedimentation control devices will be maintained for the duration of the project until such time that the final surface cover installed during site restoration activities is established (as appropriate).

3.9 Site Clearing Activities

After the erosion controls are in place, and before construction activities begin, brush, trees, and other debris will be removed, as required, to provide access to the work areas. Above-grade vegetative materials that are cleared from the excavation areas will be chipped, shredded, and/or cut for potential subsequent use as landscaping or soil bulking materials. Below-grade vegetative materials (i.e., tree stumps and roots) and debris that were previously in contact with impacted materials will be transported off-site to an approved disposal facility.

As requested by the Town, the report figures and Technical Drawings that depict the Elm Street Area include the surveyed location of the oak tree located in the cemetery adjacent to the Elm Street Area. The Town has requested that GE attempt to protect this tree during the performance of the OU-1 soil remedy. As shown on Figure 2, the oak tree is located in the cemetery adjacent to the Elm Street Area, at a higher elevation than the Elm Street Area. Further, the excavation activities associated with the Elm Street Area do not currently

extend to the location of the oak tree, as indicated in Figure 11. While every attempt will be made to implement the Remedial Action such that the root structure for the oak tree is not impacted, GE cannot guarantee the survival of this tree following implementation of the Remedial Action.

3.10 Protection/Decommissioning of Groundwater Monitoring Wells, Pumping Wells, and Temporary Piezometers

Certain existing monitoring wells, pumping wells, and temporary piezometers located within the proposed limits of excavation will be decommissioned as part of the Remedial Action. All well decommissioning activities will be performed in accordance with the procedures specified in Appendix V of the FSP and applicable NHDES regulations, if any. Additional details regarding the decommissioning of existing monitoring wells, pumping wells, and temporary piezometers will be provided in future Remedial Action submittals. At this time, it is anticipated that the following monitoring wells, pumping wells, and temporary piezometers will be decommissioned prior to initiation of active excavation activities:

<u>Elm Street Area</u>

- MW-01A;
- MW-01B;
- MW-02A;
- MW-02AR;
- MW-02B;
- MW-03A;
- MW-03B;
- MW-26A;
- MW-26B; and
- MW-29B.

<u>Mill Street Area:</u>

- MW-07A;
- MW-09A;

- MW-09B;
- MW-21C;
- MW-22A;
- MW-22B;
- MW-22C;
- PW-1;
- PW-2
- PZ-07B;
- PZ-07C;
- PZ-21A; and
- PZ-21B.

In addition to the above-listed wells, monitoring wells MW-04A, MW-04B, MW-04C, MW-18B, MW-28A, and MW-28B are also currently located within the proposed excavation limits at the Elm Street Area. However, these monitoring wells are located within remedial excavations measuring 2 feet in depth or less. As such, it is anticipated that these monitoring wells can be protected during the excavation activities and ultimately maintained for use during post-construction groundwater monitoring.

The locations of the monitoring wells, pumping wells, and temporary piezometers subject to decommissioning prior to the Remedial Action, protection during the Remedial Action, or installation (new wells) and replacement (decommissioned wells) following completion of the Remedial Action are presented on Figure 14 for the Elm Street Area and Figure 15 for the Mill Street Area. In addition, the locations of the monitoring wells, pumping wells, and temporary piezometers subject to decommissioning, protection, or installation/replacement have been added to Technical Drawings G-2 and G-3.

Section 5.5 provides additional details regarding the need to replace the above-listed monitoring wells for future long-term monitoring of the effectiveness of the OU-1 groundwater remedy, as required by the ROD (as amended) and the UAO (as modified). That section also provides information regarding two new wells that GE is proposing to install at the Site following performance of the Remedial Action. Additional details regarding the decommissioning and subsequent replacement of the groundwater monitoring wells

impacted by the Remedial Action (as well as the installation of the new wells) are provided in the revised WMP and EMP, which were submitted to EPA on July 30, 2007, revised through GE's response on December 31, 2007 to EPA's groundwater-related comments dated November 1, 2007, and revised a second time on April 14, 2008.

3.11 Clean Materials/Equipment Staging Area

As part of the site preparation activities, access roads and clean equipment/material staging pads will be constructed by first performing limited grading (if necessary), then placing a geotextile and gravel on the graded surface. The actual locations of the temporary access roads and gravel equipment pads will be identified by the Remedial Action Contractor based on equipment limitations and access requirements. Additional information regarding such clean material/equipment staging areas is presented on Technical Drawing G-25. Upon completion of the remediation activities, the clean materials/equipment staging areas (including liner materials) will be removed and transported off-site to an appropriate disposal facility and the areas will be restored to pre-construction conditions. Since these areas will only be used for the staging of clean equipment and materials and will not contact impacted materials or equipment, it is not currently anticipated that testing of these materials will be necessary or off-site disposal. However, the source area for the materials used to construct the clean equipment/material areas will be subject to verification sampling prior to the materials arriving on-site, as indicated in the VSP included in Appendix A. Although it is currently anticipated that the clean materials/equipment staging areas will be among the last areas restored to pre-existing conditions, in the event that such areas are no longer needed prior to the completion of Site restoration activities, the materials used to construct such staging areas may be utilized as a source of clean backfill materials for site restoration activities. Otherwise, these materials will be consolidated and sent off-site for disposal at an appropriate off-site disposal facility permitted to receive materials that are neither hazardous waste under RCRA nor subject to disposal restrictions under the Toxic Substances Control Act (TSCA, 40 CFR 761.61).

3.12 Temporary Staging/Vehicle Loading Areas for Excavated Soils

As further discussed in Section 4.7 and Appendix D, it is currently anticipated that all temporary staging and vehicle loading areas for excavated soils will be located on impacted materials during the implementation of the OSD soil remedy. To the extent feasible and practicable, temporary staging and vehicle loading areas will not be established in locations that may interfere with construction operations or necessary traffic flow. In addition, temporary staging areas will be located so as to account for site topography and avoid (to the extent possible) low-lying drainage areas where surface runoff is likely to accumulate. However, the entire Elm and Mill Street Areas are subject to excavation as part of the OU-1

soil remedy, as indicated on Figures 11 and 12. Therefore, similar to the secondary EZs and CRZs (described in Sections 3.6.1 and 3.6.2), the temporary staging and vehicle loading areas will necessarily be relocated within the Elm and Mill Street Areas during the performance of the OU-1 soil remedy. The Remedial Action Contractor will ultimately determine the final site layout, sequencing of the excavation activities at the Elm and Mill Street Areas, and location(s) of equipment, material staging and vehicle loading areas.

In the event that it is necessary to locate temporary staging and vehicle loading areas in non-impacted or backfilled areas based on physical site constraints, these areas may be constructed using the following methods and materials:

- The area will be graded and sloped to a collection sump;
- The re-graded area will be compacted to form a smooth surface with no protruding objects;
- A minimum 4-inch thick layer of granular material will be placed over the re-graded and compacted area;
- Soil berms or Jersey barriers will be installed along the perimeter of the re-graded and compacted area;
- A layer of geotextile fabric, followed by a 40-mil thick HDPE liner and an additional layer of geotextile fabric will be installed over the compacted surface and berms/Jersey barriers;
- An HDPE liner will be placed over the temporary soil stockpiles when active material handling activities are not ongoing; and,
- A 12-inch-thick granular fill layer and access ramps will be installed over the geotextile.

Additional details regarding the construction of the temporary staging/vehicle loading areas are presented on Technical Drawing G-25. Throughout performance of the Remedial Action, excavated soil stockpiles and vehicle loading areas will be managed in a manner that limits dust generation and precipitation infiltration/contact. In general, excavated soil stockpiles will be covered at the end of each work day and during periods of work shutdown. As indicated in Section 4.7.6, additional operational procedures will be implemented to minimize the potential for the spread of excavated materials during vehicle loading operations. Upon completion of remediation activities, the temporary

staging/vehicle loading areas (including liner materials) will be removed, sampled/characterized, and transported off-site to an appropriate disposal facility.

3.13 Decontamination Area(s)

As part of the site preparation activities, the Remedial Action Contractor will construct decontamination areas for transportation vehicles, equipment, and personnel that come into contact with impacted materials during performance of the OU-1 soil remedy. In general, personnel and small equipment decontamination areas will be located within the CRZs (Section 3.6.2) at the Elm and Mill Street Areas. Heavy equipment and vehicle decontamination areas will be constructed by the Remedial Action Contractor in appropriate areas adjacent to the vehicle loading areas (which will likely be located along the boundary of the secondary EZs and CRZs). As indicated in the previous section, the locations of these vehicle loading areas will be selected based on the logistics and sequencing of the Remedial Action. Further, it is anticipated that construction equipment/vehicles associated with excavation activities at either the Elm or Mill Street Areas will be dedicated to that area, with decontamination activities performed following the completion of the handling of impacted materials, prior to handling of clean/treated materials, and/or prior to departure from the Site. The decontamination areas will be constructed using the following methods and materials:

- The area will be graded and sloped to a collection sump;
- The re-graded area will be compacted to form a smooth surface with no protruding objects;
- A soil berm will be constructed along the perimeter of the re-graded and compacted area;
- A layer of geotextile fabric, followed by a 40-mil thick HDPE liner and an additional layer of geotextile fabric will be placed over the compacted surface and berms;
- A 12-inch thick granular fill layer will be placed over the geotextile fabric; and
- An access ramp will be constructed on two ends of the decontamination area for equipment/personnel ingress/egress.

Upon completion of remediation activities, the decontamination area (including liner materials) will be removed, sampled/characterized, and transported off-site to an approved disposal facility.

3.14 Traffic Control

Several submittals related to the identification of preliminary truck routes and traffic counts have been made during the remedial design phase of the project, including:

- *Truck Route and Traffic Analysis Preliminary Report* (Preliminary Traffic Report) prepared by Vannasse, Hangen, Brustlin, Inc. (VHB), presented as Appendix A to Addendum No.1 (May 11, 2006);

- TR/TA Report presented as Appendix E of the *Intermediate (60%) Design Report for the LTTD Remedy* (Intermediate LTTD Design Report) (June 4, 2007); and

- TR/RA Report presented as Appendix E of the *Intermediate (60%) Design Report for the OSD Remedy* (Intermediate OSD Design Report) (June 12, 2007).

Concurrently with the Intermediate OSD Design Report, GE also submitted a Remedy Comparison Document on June 12, 2007, which provided a comparison of the traffic information associated with the implementation of the OSD soil remedy (as presented in the Intermediate OSD Design Report) and similar information associated with the implementation of the LTTD remedy (as presented in the Intermediate LTTD Design Report).

In support of the December 2007 Final Design Report, a revised TR/TA Report, providing information regarding the impacts to the vehicular and pedestrian traffic patterns in the vicinity of the Site, was prepared and included therein as Appendix E. That report provided the following information: an analysis of the traffic data collected during the remedial design phase of the project; recommended truck routes for transportation of clean materials to and impacted materials from the Site; a traffic capacity analysis for the recommended truck routes; an evaluation of the impacts associated with the implementation of the OSD soil remedy in light of the traffic capacity analysis; and an evaluation of the need for measures to mitigate such impacts. As indicated in Section 1.2, revisions to the TR/TA Report (including the identification of new primary and alternate truck staging areas) were provided in submittals to the EPA dated October 30, 2008 and June 22 and August 13, 2009. Technical Drawings G-8 and G-9 provide information regarding the modifications that the Remedial Action Contractor will make to the primary and overflow truck staging areas in preparation for the implementation of the OU-1 soil remedy.

In addition, Appendix B of this revised Final Design Report includes traffic–related technical drawings, which provide the following information:

- Reconstruction Detour Plan - Mill Street Area (Technical Drawing T-1);
- Reconstruction Phasing and Drive Access Plan - Mill Street Area (Technical Drawing T-2);
- Vehicular Maintenance of Traffic Plan - Elm Street Area (Technical Drawing T-3);
- Pedestrian Maintenance of Traffic Plan - Elm Street Area (Technical Drawing T-4);
- Pavement Repair Details and Notes - Elm Street Area (Technical Drawing T-5);
- Typical Sections - Mill Street Area (Technical Drawing T-6);
- Plan and Profile STA 5+59.09 to STA 9+50.00 - Mill Street Area (Technical Drawing T-7);
- Grading Plan - Mill Street Area (Technical Drawing T-8);
- Cross Section STA 5+25 to STA 5+75 - Mill Street Area (Technical Drawing T-9);
- Cross Section STA 6+00 to STA 6+50 - Mill Street Area (Technical Drawing T-10);
- Cross Section STA 6+75 to STA 7+25 - Mill Street Area (Technical Drawing T-11);
- Cross Section STA 7+50 to STA 7+75 - Mill Street Area (Technical Drawing T-12);
- Cross Section STA 8+00 to STA 8+25 - Mill Street Area (Technical Drawing T-13);
- Cross Section STA 8+50 to STA 8+81 - Mill Street Area (Technical Drawing T-14); and
- Cross Section STA 9+00 to STA 10+00 - Mill Street Area (Technical Drawing T-15).

As indicated in this revised Final Design Report, it is anticipated that portions of both Elm and Mill Streets will be closed or partially closed periodically during the performance of the Remedial Action (i.e., during excavation activities within and directly adjacent to Mill and Elm Streets). However, to minimize impacts to pedestrian and vehicular traffic in the vicinity of the Site, it is currently anticipated that the remedy will be sequenced in such a manner that both streets (or portions thereof) will not be closed or partially closed at the same time. To that end, it is further anticipated that the excavations within Elm Street will be performed

prior to the Phase 1 excavations at the Elm and Mill Street Areas, as further described in Section 4.7.3.

4. Implementation of Remedial Action

4.1 Overview

This section of the revised Final Design Report provides additional details regarding the implementation of the OU-1 soil remedy, and includes the following information:

- Installation of engineering controls, including fixed excavation structural support systems at the Elm and Mill Street Areas;
- Relocation of the sand cap at the Elm Street Area;
- Design overview of the Mill Street Area excavation dewatering system;
- Design overview and staging/construction of temporary water treatment system and ancillary equipment at the Mill Street Area;
- Performance testing of the temporary water treatment system;
- Performance/sequencing of the Remedial Action; and
- Off-site transportation and disposal of excavated materials.

Additional details regarding the activities associated with each of these tasks are provided in the remainder of this section. Site preparation activities were previously discussed in Section 3, while site restoration and demobilization activities are discussed in Section 5.

4.2 Installation of Engineering Controls

Section 2.6 of this document discussed the CSM, including updated excavation limits and removal volumes. As indicated in Table 10, approximately 30,175 cy of material will be excavated from the Elm Street Area (21,220 cy) and the Mill Street Area (8,955 cy) to achieve the SCLs specified in the ROD (as amended). Consistent with the Intermediate Design Reports and the development of the limits of excavation as discussed in Section 2.6 of this revised Final Design Report, the limits of excavation (and the corresponding estimated volume of soil removal) for the Elm and Mill Street Areas were developed in such a manner that certain samples identified during the PDI as containing PCBs in excess of the SCLs are not entirely within the limits of excavation. However, as previously indicated in Section 2.6, GE has previously proposed (and EPA has explicitly approved) not including certain of these samples in the limits of excavation. It is also noted that EPA's November 1,

2007 letter on the Intermediate Design Reports did not provide comments on the other samples which contained PCBs in excess of the SCLs but that are not included within the limits of excavation. Section 2.6 provides additional information regarding such samples as they pertain to the requirement in the UAO/SOW (as modified) that GE provide certification following remedy implementation of the achievement of the Performance Standards and SCLs specified in the ROD (as amended). Finally, an extensive confirmation sampling program is proposed in Appendix A of this revised Final Design Report to confirm the appropriateness of the limits of excavation.

Regarding the excavations at the Elm Street Area, approximately 1,310 cy of additional excavation (i.e., over-excavation) is proposed at the Elm Street Area to facilitate installation of the proposed cover system, replacement storm sewer, storm water retention area and gabion wall (Table 11). Performance of the excavation activities to the limits and depths indicated on Figures 11 (Elm Street Area) and 12 (Mill Street Area) will result in the need for engineering controls (i.e., fixed structural supports and/or excavation sloping) for the following reasons: (1) constructability and dewatering activities associated with excavations below the water table at the Mill Street Area; (2) flood protection for certain excavations which will be performed in close proximity to the level of the Souhegan River at the Elm Street Area; and (3) performance of the Remedial Action in accordance with applicable Occupational Safety and Health Administration (OSHA) regulations. Additional details regarding the design, location, and installation of fixed structural supports are provided below.

As discussed in the Preliminary Design Report for the LTTD soil remedy, several different types of fixed structural supports were evaluated for their ability to: (1) conform with applicable OSHA regulations; (2) protect against potential floods at the Elm Street Area; and, (3) serve as a cut-off barrier to restrict groundwater infiltration into excavations below the water table at the Mill Street Area. The types of structural supports/flow barriers evaluated during the preliminary design phase included soldier piles and lagging, steel sheeting, cement/bentonite slurry walls, secant pile walls, and SPTC walls. Based on that evaluation, the structural supports selected for certain excavation cells at the Elm Street Area consist of steel sheeting and soldier piles and lagging, while excavation sloping will be employed for certain cells in lieu of the installation of excavation supports. For the Mill Street Area, Appendix B of the Preliminary Design Report presented an evaluation of the various potential structural support/flow barriers that were considered for use. Based on the information provide therein, the structural supports selected for certain excavation cells at the Mill Street Area consist of SPTC walls, supplemented with wood lagging at elevations above the water table, while excavation sloping will be employed for certain cells in lieu of the installation of excavation supports. The design calculations for the excavation support systems (excluding sloping) are included in Appendix F.

Based on physical constraints and space limitations, it is anticipated that the Remedial Action Contractor will mobilize to the Site prior to initiation of soil removal activities associated with the OU-1 remedy and install the fixed excavation supports or, for areas where installation of soldier pile and lagging walls are proposed, the soldier piles. All spoils generated during the installation of the fixed excavation supports will either be transported off-site for disposal during these activities, or will be consolidated at the Elm Street Area for subsequent off-site disposal during the full-scale implementation of the OU-1 soil remedy. Should the latter option be selected, these materials will be placed in a temporary staging area for excavated materials (as described in Section 3.12). Following installation of all fixed structural supports, if the Remedial Action Contractor demobilizes from the Site, it will perform equipment decontamination activities in accordance with the procedures specified in Section 5.6. Additional details regarding the specific engineering controls proposed for use at the Elm and Mill Street Areas are provided in the following sections.

4.2.1 Elm Street Area Excavations

Excavation of material subject to off-site disposal at the Elm Street Area will require fixed structural supports in certain areas. Structural support is generally required for excavations that will extend deeper than 4 feet below existing grade or the base elevation of adjacent excavations and/or where site constraints and/or cost considerations prohibit the use of sloped excavations. Where installation of fixed structural supports is not required, construction slopes and/or benched excavations will be used to achieve stable excavation configurations. Finally, if the depth of excavation at the Elm Street Area coincides with the seasonal low water table, dewatering will be performed utilizing sumps and pumps, as required. However, it should be noted that the Remedial Action Contractor may elect to excavate such areas "in the wet" (i.e., excavation dewatering will not be performed), as further described in Section 4.7.3 below.

Structural excavation support at the Elm Street Area will consist of a combination of soldier piles and lagging and steel sheeting. Use of soldier piles and lagging has advantages over steel sheeting where control of lateral groundwater infiltration is not required, including: cost; easier installation through potential obstructions (e.g., debris, cobbles, and boulders); and, better control of wall alignment. Therefore, because the majority of excavations at the Elm Street Area are located well above the water table, the majority of the structural excavation supports at the Elm Street Area will consist of soldier piles and lagging.

As described in Section 2.4, GE made several submittals to EPA between May and September 2009 proposing to perform supplemental geotechnical investigation activities along the riverbank and adjacent to the cemetery at the Elm Street Area in 2009. Those investigations were proposed to provide additional geotechnical data to assist with the

design of the proposed excavation supports adjacent to the cemetery and along the riverbank at the Elm Street Area. The results of the supplemental geotechnical investigations were provided in a December 28, 2009 letter to the EPA and have been incorporated into the support of excavation designs included in this revised Final Design Report.

Steel sheeting will be installed along the riverbank of the Souhegan River to protect certain excavation cells that will be excavated to depths in close proximity to the elevation of the groundwater table and/or Souhegan River. As a conservative measure, subsurface excavations (i.e., those excavations greater than one foot in depth) extending to elevations below the estimated 25-year floodplain were protected from potential flooding associated with Souhegan River surface water infiltration. The elevation of the 25-year floodplain was determined to be located at approximately 243 feet AMSL. Therefore, the Preliminary Design Report for the LTTD soil remedy indicated that two excavation cells at the Elm Street Area would require installation of steel sheeting to protect against a 25-year flood event. However, based on comments on that submittal, the location of the steel sheeting was revised in the Intermediate Design Reports to be installed continuously from Excavation Cell G to Excavation Cell V, as indicated on Technical Drawing S-1 of that submittal. Steel sheeting is currently proposed along the length of the riverbank adjacent to areas subject to excavation at the location/elevation identified as the low-water mark on the Technical Drawings. As indicated on Technical Drawing S-2, the steel sheeting around Excavation Cells F, J, and W was designed to provide protection from infiltration of river water during flood events. For the remaining shallow excavation areas (e.g., 1-foot excavation areas located within the 25-year floodplain, along the riverbank northwest of Excavation Cell F between Excavation Cells J and W and northeast of Excavation Cell W, the steel sheeting proposed for installation along the riverbank is designed to act as a demarcation of the extent of removal for OU-1 soils and, as such, will offer minimal protection from surface water infiltration. Such protection is unnecessary since other engineering controls will be employed for such areas. For example, it is anticipated that such shallow excavations can be cleared, excavated, and backfilled over a period of one day so that these areas would not remain exposed to flood waters. As previously indicated, GE is proposing to leave the steel sheeting in place along the bottom of the riverbank following performance of the Remedial Action to serve as a line of demarcation during future potential OU-2 remedial actions, if necessary. Therefore, it is anticipated that the steel sheeting will be cut down and to a height adjacent to the gabion wall, as shown on Technical Drawing 27) following completion of the OU-1 soil removal and backfilling activities.

Technical Drawings S-1 and S-2 show the proposed locations and types of engineering controls (e.g., soldier piles and lagging, sloping/benching, etc.) that will be implemented for

the various excavation cells at the Elm Street Area. Depending on the depth of excavation, the soldier piles and lagging or sheetpile walls will be supported laterally using internal steel bracing and/or ground anchor tie-backs. Additional design details regarding the excavation supports at the Elm Street Area and the internal bracing for those supports are provided in Technical Drawings S-3 through S-7.

4.2.2 Mill Street Area Excavations

Similar to the Elm Street Area, excavation of material subject to off-site disposal at the Mill Street Area will require structural supports for certain excavation cells. Again, structural support is generally required for excavations that will extend deeper than 4 feet below existing grade, or the base elevation of adjacent excavations, and/or where site constraints and/or cost considerations prohibit the use of sloped excavations. Where installation of fixed structural supports is not required, construction slopes and/or benched excavations will be used to achieve stable excavation configurations.

A review of the regional and site-specific geologic and hydrogeologic properties, combined with the results of specific capacity testing performed during the PDI, indicates that a groundwater cut-off wall is necessary around certain excavations at the Mill Street Area that will extend below the elevation of the groundwater table. Based on elevation monitoring performed during the PDI and during quarterly monitoring events under the WMP, the water table is typically located between 252 and 254 feet AMSL, as indicated in Table 13. Excavation dewatering at the Mill Street Area is necessary for several reasons, including to:

- Limit groundwater infiltration into open excavations.
- Facilitate handling of material subject to excavation and treatment as part of the Remedial Action.
- Allow access to the base of each excavation for verification that the required depth of excavation was achieved (through the performance of survey activities).
- Allow access to the excavation bottoms for confirmation sampling (for those cells not extending to bedrock).
- Facilitate compaction of treated and/or clean backfill materials under dry conditions.

As previously indicated, several types of fixed excavation structural support/groundwater cut-off wall designs were evaluated during the preliminary design phase. To assist with the selection of the appropriate design for the excavation supports/groundwater cutoff walls to

be installed at the Mill Street Area, a groundwater model was developed to estimate anticipated flow rates into various excavation cells. A report describing the model design and assumptions, predictive simulations, sensitivity analysis, and selection of the appropriate excavation support/groundwater cut-off wall design was presented in Appendix B of the Preliminary Design Report. As indicated in Section 2.4, supplemental hydraulic testing activities were performed at the Mill Street Area under the SDDC Work Plan. The purpose of those supplemental investigations was to verify the estimated dewatering rates that were anticipated to be necessary during the implementation of the OU-1 soil remedy. The results of the supplemental hydraulic testing activities were used to update and recalibrate the groundwater flow model. As described in Section 2.4, the updated, recalibrated groundwater flow model generally confirmed the estimated dewatering rates; therefore, no modifications to the support of excavation or dewatering designs were necessary for this revised Final Design Report.

As documented in Appendix B of the Preliminary Design Report, it was determined that an SPTC wall design provides the best combination of structural support/barrier to groundwater infiltration. SPTC walls will be installed to provide structural support around the two deep excavation areas (referred to herein as the East and West Bedrock Cells) and to act as a lateral groundwater flow cut-off in these areas. As shown on Technical Drawing S-9, each of these bedrock cells will be further divided in two to facilitate groundwater management during the performance of the excavation activities.

An SPTC wall is generally constructed using the following steps:

- Excavation and installation of concrete guide walls for the subsequent installation of the SPTC wall (see Detail 3, Technical Drawing S-16).

- Once the guide walls are installed, the soils and the top few inches of bedrock located between within an approximately 30-inch wide trench located between the guide walls are excavated with a clamshell bucket. Slurry is utilized to keep the excavated trench open.

- Upon excavation of the soils, steel H-piles are driven/drilled and grouted into bedrock approximately every 5 to 6 feet on center (see Technical Drawings S-9, S-10, and S-16).

- The portions of the H-piles located below the water table are then embedded in a concrete wall approximately 30 inches in width (see Detail 3, Technical Drawing S-16). The concrete portion of the SPTC walls will be installed from the top of bedrock to an

approximate elevation of 254 feet AMSL, which generally corresponds to the seasonal high groundwater table at the Mill Street Area (see Technical Drawing S-14).

- Excavation support above the water table will be achieved through the use of timber lagging between the sheet piles (see Technical Drawings S-13 through S-15). During backfilling and/or site restoration, the timber lagging will be removed and the steel H-piles will be cut at least 5 feet from surface grade, to facilitate potential future installation of utilities/development of the Mill Street Area, as requested by the Town.

- Depending on the depth of excavation, the SPTC walls will be supported laterally using internal steel bracing and/or using ground anchor tie-backs. Additional design details regarding the excavation supports and the internal bracing for those supports are provided in Technical Drawings S-10 through S-17.

- Approximately 1,700 cy of excavated soils associated with installation of the SPTC wall will be loaded into trucks for off-site disposal or stockpiled for subsequent off-site disposal with the remaining materials subject to excavation and off-site disposal at the Mill Street Area. If the excavated materials are stockpiled, they will be placed in a temporary staging area (as described in Section 3.12).

- In addition, as the concrete material is placed to make the SPTC walls it will displace the slurry. It is estimated that up to 2,000 cy of slurry material will be generated as part of the SPTC wall construction process. That material will similarly be stockpiled in a temporary staging area for subsequent characterization and off-site disposal.

Technical Drawing S-9 shows the preliminary locations and type of engineering controls (e.g., SPTC walls, sloping/benching) that will be implemented for the various excavation cells at the Mill Street Area. Prior to installation of the fixed excavation supports at the Mill Street Area, the Remedial Action Contractor will implement the vehicular and pedestrian traffic control plan for the Mill Street Area. This will likely involve closing Mill Street to local through traffic for significant periods during the performance of the Remedial Action. Additional details regarding the temporary closure of Mill Street are provided in Section 3.14, the T-series of Technical Drawings (Appendix B) and the TR/TA Report (Appendix E). As further discussed in Section 4.4, two to four groundwater extraction wells will be installed in each of the four excavation cells located within the SPTC walls to assist with dewatering activities. The dewatering design also specifies the installation of an observation well within each of these excavation cells. Such wells will be installed following construction of the SPTC walls at the Mill Street Area. For excavation cells located outside the SPTC walls (that also require excavation below the water table, but not down to bedrock), a well point system will be utilized as further described in Section 4.4. Additional wells and/or sumps

may be utilized to assist with dewatering activities in certain excavations in the vicinity of the water table. Additional details regarding the dewatering system to be used at the Mill Street Area are provided in Section 4.4.

4.3 Relocation of Sand Cap at the Elm Street Area

As indicated in Section 1.4.1, the EPA demolished and removed the one-story building located at the Elm Street Area between December 2000 and January 2001. Following completion of this work, a temporary geotextile liner and a sand cap were placed over the footprint of the former building. These activities were described in a document titled *Asbestos Removal and Building Demolition Source Control Remedial Action – Final Completion Report* (Final Completion Report) (USACE, May 2002). Because these clean cap materials are isolated from the underlying impacted soils, these materials may be reused as supplemental backfill during site restoration activities.

To avoid mixing of the clean cap materials with impacted soils, a few inches of the clean cap materials will be left over the temporary liner as a conservative measure. Based on information provided in the Final Completion Report, an estimated 1,000 cy of sand are available for reuse as clean backfill materials. Prior to performance of excavation activities for impacted materials, the portion of the sand cap available for reuse will be removed and stockpiled in a clean materials staging area, similar to that described in Section 3.11. Finally, as indicated in a response to an EPA comment on the Preliminary Design Report for the LTTD soil remedy (included in the May 2006 Addendum No.1 to the Preliminary Design Report), the stockpiled sand cap materials will be subject to confirmation sampling to verify that such soils contain PCBs at concentrations less than the applicable SCLs for the Elm Street Area prior to the use of such materials as backfill in excavations at the Elm Street Area. Such confirmation sampling is further described in the VSP provided in Appendix A. If these materials contain PCBs less at concentrations equal to or less than 1 mg/kg, they are eligible for use as backfill materials in any excavation at the Elm Street Area. However, if these materials contain PCBs at concentrations greater than 1 mg/kg but less than or equal to the subsurface SCL of 100 mg/kg, they will be used as backfill under the soil cover.

4.4 Design of Mill Street Area Excavation Dewatering Systems

As indicated on Technical Drawing DW-1, excavation of soils located beneath the water table is required for certain excavation cells at the Mill Street Area. Certain of these excavation cells extend only slightly into the water table (typically located between elevation 252 feet AMSL and elevation 254 feet AMSL, as shown in Table 13), while other excavations cells extend up to 16 feet below the water table, to the top of bedrock (which is

also illustrated on Technical Drawing DW-1). Since the scope of dewatering activities within these two types of excavations will differ, two types of dewatering systems have been designed, including: (1) dewatering within SPTC walls installed to provide structural support of deep excavations and serve as a groundwater flow barrier for deep excavations extending to bedrock; and (2) a well point system for excavations extending only slightly into the water table. Additional design details regarding these two dewatering systems are provided below.

4.4.1 Dewatering of SPTC Cells

Section 4.2.2 of this revised Final Design Report, and Appendix B of the Preliminary Design Report for the LTTD soil remedy, provide details regarding the design and installation of fixed structural supports and groundwater flow cut-off barriers for certain excavations at the Mill Street Area. To support the final dewatering design for the SPTC cells, groundwater modeling simulations were performed using Visual MODFLOW to evaluate the proposed deep well locations. Specifically, pumping wells were modeled with extraction rates sufficient to manage the seepage rates (up to 150 gpm) predicted by modeling performed during the preliminary design phase. As indicated in Section 2.4, supplemental hydraulic testing activities were performed at the Mill Street Area under the SDDC Work Plan. The purpose of those supplemental investigations was to verify the estimated dewatering rates that were anticipated to be necessary during the implementation of the OU-1 soil remedy. The results of the supplemental hydraulic testing activities were used to update and recalibrate the groundwater flow model. As described in Section 2.4, the updated, recalibrated groundwater flow model generally confirmed the estimated dewatering rates; therefore, no modifications to the support of excavation or dewatering designs were necessary for this revised Final Design Report. The results of the previous modeling indicated that the deep well network proposed herein can generate sufficient drawdown across the excavation areas, without exceeding available drawdown at the individual deep wells. A calculation set describing the model input parameters and output is provided in Appendix F.

The potential for developing critical hydraulic gradients at the base of the excavation(s) was addressed in the dewatering and excavation support system designs. First, critical gradients are problematic with respect to soils, but not through crystalline bedrock (i.e., the rock type underlying the Site), and the Remedial Design requires the installation of the SPTC walls to bedrock. The SPTC cutoff walls will force seepage flowpaths through the fractured bedrock, which will have the effect of eliminating critical gradients in soils at the base of the excavation. The design includes grouted toe-pin boreholes to further limit seepage beneath the SPTC wall. Therefore, if the SPTC wall fails to reach bedrock due to boulders or other obstructions, the toe-pin grouting program will limit seepage and

associated exit gradients through these soil "windows" below the SPTC wall. Lastly, the drill holes for deep wells will be advanced either to bedrock or approximately 6 feet into bedrock to maximize available drawdown at the deep wells. Deep well sumps will be grouted into bedrock and screen bottoms will be located only about 1 ft below the bedrock surface. Based on these design measures, the extraction wells should be capable of controlling groundwater levels and gradients throughout the soil column to and below the proposed depths of excavation.

It is anticipated that the four excavation cells within the SPTC walls will be dewatered, excavated, and backfilled sequentially. As described in Section 4.4.2, two to four 8-inch (minimum) steel extraction wells will be installed into bedrock within each of the four SPTC cells. In addition, one observation well with also be installed within each cell to assist with monitoring of the dewatering activities. Both the dewatering and observation wells will be installed following the installation of the SPTC walls at the Mill Street Area. Technical Drawings DW-2 through DW-5 illustrate the proposed locations of the dewatering wells and observation wells within each SPTC cell and the discharge piping, which routes the extracted groundwater to the temporary water treatment system. Technical Drawing DW-7 provides typical construction details for the extraction and observation wells.

Dewatering activities will be initiated prior to the excavation reaching the initial water table elevation. As the water level is reduced within each dewatering cell, the available saturated thickness within the excavation cell will also decline, which will result in a corresponding decrease in the available pumping rate for the extraction wells. As a result, sumps and/or horizontal wells may be installed within the base of the excavation cell(s) to continue removing groundwater as the excavation approaches the specified vertical depth/bedrock, if necessary. Technical Drawing DW-7 provides typical construction details for dewatering sumps.

4.4.2 Dewatering of Shallow Water Table Excavations

As indicated on Technical Drawing DW-1, soil removal for Excavation Cells E and N (which border certain SPTC cells) will likely proceed slightly into the water table at the Mill Street Area, which is generally located between elevation 252 feet AMSL and 254 feet AMSL, as indicated on Table 13. Since these excavations will not require excavation to bedrock, installation of an SPTC wall serving as a hydraulic barrier is not required. Rather, it is anticipated that dewatering/depression of the water table in the vicinity of these cells using a well point system will be sufficient to allow the required excavation and subsequent confirmation sampling activities. The well point system will generally consist of a series of well points installed approximately 5 feet on center around the perimeter of the excavation cell (with the exception of where SPTC wall(s) are located), as illustrated on Technical

Drawing DW-6. That drawing also presents the proposed locations of the well point pumps and discharge piping, which routes the extracted groundwater to the temporary water treatment facility. Finally, Technical Drawing DW-7 provides typical construction details for the well point system.

Similar to the dewatering activities for the SPTC cells, the dewatering activities for the shallow water table excavations will be initiated prior to the excavation reaching the initial water table elevation. Also, sumps and/or horizontal wells may be installed within the base of the excavation cell(s) to continue removing groundwater as the excavation approaches the specified vertical depth, if necessary. Technical Drawing DW-7 provides typical construction details for dewatering sumps.

4.5 Design Overview and Staging/Construction of Temporary Water Treatment System and Ancillary Equipment

Concurrent with the activities described in Sections 4.2 and 4.3 above, staging/construction and performance testing of the temporary water treatment system and ancillary equipment will be performed. GE proposes to construct the temporary water treatment system on the Tax Parcel 25-110 for several reasons. First, the majority of the water generated will be associated with dewatering activities for the excavations extending below the water table at or near the Mill Street Area. Second, it is anticipated that minimal dewatering activities, if any, will be required at the Elm Street Area since the ROD (as amended) requires excavation of impacted soils at the Elm Street Area to a maximum depth of the seasonal low water table. Nevertheless, certain excavations in the vicinity of the seasonal low water table may encounter saturated soils (depending upon the time of year in which such excavations are performed). In such an instance, the Remedial Action Contractor may elect to excavate soils from the bottom of excavations in the vicinity of the seasonal low water table "in the wet", rather than performing active dewatering activities. Dewatering of such soils would be achieved either through the mixing of those soils with dry soils from the overlying excavation or through gravity dewatering. Liquids generated during gravity dewatering of excavated soils will be temporarily stored in water storage tanks staged at the Elm Street Area for consolidation, along with precipitation from stockpiles or other staging areas for impacted materials and liquids generated during personnel/equipment decontamination. Consolidated liquids will be transported via tanker truck or pumped via a temporary pipeline running from the temporary manhole or new manhole MH-1 through the restored portion of the storm sewer utility (see Section 3.7.2) and along the drainage ditch/culvert system to the Mill Street Area where the pipeline would be run to the temporary water treatment system for ultimate treatment and discharge. Finally, Mill Street is a convenient location for the temporary water treatment system based on the proximity to the

proposed discharge location, which is the drainage ditch on the Draper parcel (which ultimately leads to the Souhegan River via the on-site drainage ditch/culvert system).

The remainder of this section summarizes the design, staging, and construction of the temporary water treatment system. The information presented in this section describes the temporary water treatment system that was designed based on both site-specific and industry-accepted design principles, utilizing proven treatment technologies and configurations. The design described in this revised Final Design Report incorporates certain design modifications resulting from the hydraulic testing activities performed under the SDDC Work Plan between May and October 2012, as described in Section 2.4. This includes the treatment and discharge of accumulated waters that were generated as part of those hydraulic testing activities in a temporary on-site treatment system. Although the design presented herein is comprehensive, it is not necessarily meant to represent the final design that will be implemented by the Remedial Action Contractor. Instead, the Remedial Action Contractor will be given the opportunity to propose an alternate water treatment system design that, at a minimum, meets the performance standards and design, construction, and operational intent established herein. The remainder of this section provides an overview of the design objective, influent characteristics, treated effluent discharge requirements, and an overview/description of the temporary water treatment system.

4.5.1 Objective of Temporary Water Treatment System

The objective of the on-site temporary water treatment system is to reduce the concentration of certain parameters in the liquid waste streams generated during performance of the OU-1 soil remedy to levels allowing the discharge of the treated water to the Souhegan River.

4.5.2 Influent Characteristics

The temporary water treatment system design is based on anticipated influent characteristics as determined by a review of groundwater samples collected during the PDI, quarterly monitoring events performed under the WMP since July 2007, as well as baseline and post-hydraulic testing under the SDDC Work Plan. Based on the analytical results of the groundwater samples, the following maximum influent design parameters for the temporary water treatment system have been identified:

Design Parameters	Maximum Value	Average Value
Total PCBs	1,300 µg/L	43 µg/L
1,2-Dichloroethane	44 µg/L	10 µg/L
cis-1,2-Dichloroethene	91 µg/L	7 µg/L
Trichloroethene	760 µg/L	43 µg/L
1,3-Dichlorobenzene	6 µg/L	2 µg/L
1,4-Dichlorobenzene	12 µg/L	3 µg/L
Acetone	1,400 µg/L	37 µg/L
Methyl-Tert-Butyl Ether	2,500 µg/L	55 µg/L
Benzene	2,700 µg/L	63 µg/L
Ethylbenzene	6,700 µg/L	607 µg/L
Toluene	11,000 µg/L	662 µg/L
Total Xylenes	49,000 µg/L	5,010 µg/L
Dimethyl Phthalate	1 µg/L	1 µg/L
Di-n-Butylphthalate	4 µg/L	1 µg/L
Di-n-Octylphthalate	3 µg/L	1 µg/L
Butyl Benzyl Phthalate	30 µg/L	11 µg/L
Fluorene	2 µg/L	1 µg/L
Naphthalene	120 µg/L	18 µg/L
Phenanthrene	3 µg/L	2 µg/L
Total Phenol	790 µg/L	129 µg/L

It should be noted that the elevated concentrations of certain constituents (e.g., benzene, toluene, ethylbenzene, and xylene) are associated with UST releases on the gas station and former gas station properties located south of Elm Street. As confirmed by quarterly sampling performed since July 2007 as well as the baseline and post-hydraulic water quality testing under the SDDC Work Plan, these constituents are typically observed in monitoring wells MW-03B, MW-27A, MW-27B, and MW-28B at the Elm Street Area (as well as the monitoring wells located across Elm Street at the current/former gas station properties). At this time, Excavation Cell W is the only cell proposed to be excavated to the seasonal low water table at the Elm Street Area. As previously indicated in this revised Final Design Report, the maximum depth of excavation at the Elm Street Area corresponds to the seasonal low groundwater table. Also, the Remedial Action Contractor may elect to excavate soils in the vicinity of the seasonal low water table at the Elm Street Area "in the wet". As a result, the need for excavation dewatering activities, and therefore, the volume of water generated by such activities at the Elm Street Area is expected to be minimal.

Finally, liquid waste generated at the Elm Street Area may be transported for off-site disposal if it is determined to be more economical than pumping/transporting such liquids to the temporary water treatment system located at the Mill Street Area.

For the reasons cited above, the constituent concentrations for benzene, ethylbenzene, toluene and xylene are not believed to be representative of the influent groundwater concentrations that will be observed at the temporary water treatment system during implementation of the OU-1 soil remedy. Moreover, these constituents are rarely observed at the Mill Street Area, where the majority of the water subject to treatment will be generated. Therefore, as demonstrated during the treatment of waters generated during the hydraulic testing activities under the SDDC Work Plan, a liquid-phase granular activated carbon system will be sufficient for the removal of any volatile organic compounds present in the dewatered groundwater. Additionally, based on a review of the available analytical data and the temporary water treatment system process, additional equipment for the removal of metals is not necessary. Metals were also predominantly observed in the groundwater samples collected from monitoring wells located within or adjacent to the Elm Street Area and the treatment of waters generated during the hydraulic testing activities under the SDDC Work Plan demonstrated achievement of the discharge criteria for metals using only organo-clay filtration, granular activated carbon filtration, and bag filters.

4.5.3 Design Overview of Temporary Water Treatment System

The temporary water treatment system is designed to treat a maximum instantaneous flow rate of 150 gpm. As indicated in Section 2.4, normal influent flow rates are anticipated to be less than the design maximum flow conditions and highly variable (i.e., dependent on site conditions such as precipitation events, the area where excavation activities are being conducted, the rate of surface water and groundwater infiltration, duration of dewatering activities, etc.). The temporary water treatment system will be constructed and operated by the Remedial Action Contractor in accordance with the information provided in this section and the Technical Specifications provided in Appendix C. Specifically, the substantive requirements for the water discharges are included in Technical Specification 13602 (Temporary Water Treatment System). The Remedial Action Contractor will be given the opportunity to propose an alternate temporary water treatment system design that, at a minimum, will meet the performance standards and design, construction, and operational intent in the Technical Drawings (Appendix B) and Technical Specifications (Appendix C). The temporary water treatment system will likely consist of the following components:

- Influent settling tanks;
- Influent storage tanks;

- Oil/water separator (OWS);
- Oil storage drum;
- Centrifugal transfer pumps;
- Double diaphragm pumps;
- Transfer pump station(s);
- Chemical injection system;
- Multi-media filter (MMF) system;
- Organo-clay filtration;
- Liquid-phase granular activated carbon (GAC) systems;
- Bag filter system;
- Solids holding tank;
- Effluent storage tanks;
- Sump pump system;
- Piping and appurtenances;
- Flow meters;
- Level transmitters;
- Level switches;
- Pressure gauges; and
- Air compressor.

A process flow diagram of the temporary water treatment system is shown on Technical Drawing M-1. Brief descriptions of each of the key components of the temporary water treatment system are presented below.

Influent Settling Tanks - Water generated during the Remedial Action will be pumped into the influent settling tanks. The influent settling tanks will consist of two 20,000 gallon (nominal) weir tanks equipped with over and under weirs to induce settling of solids and to capture floatables. These two tanks, operating in parallel operation, will provide up to

approximately 4 hours retention time at a maximum influent flow rate of 150 gpm. Following influent settling, the water will flow via gravity to four influent storage tanks for additional equalization. The influent settling tanks will be equipped with a solids/sludge settling chamber. The sludge will be pumped from the tank chambers to a solids holding tank and/or tanker truck via a pneumatic, double-diaphragm pump.

Influent Storage Tanks - The treatment system will have a minimum influent storage capacity of 84,000 gallons, consisting of four 21,000 gallon (nominal) tanks (i.e., approximately 2 hours of combined storage at the maximum influent flow rate of 150 gpm). Following storage, the water will be pumped to an OWS via centrifugal pump(s).

Oil/Water Separator – The OWS will be rated for a maximum flow rate of 200 gpm. This unit is oversized by approximately 33% for the purpose of providing additional retention time for any light-phase (i.e., floating) oil removal and residual solids settling. The OWS will be a gravity-type rectangular channel coalescing OWS capable of removing gross free oil and similar floatable products and will include integral collection chambers for settable sludge/solids recovery. The OWS will also have an adjustable oil skimming assembly that will skim floating oil to an oil collection chamber, where it will gravity discharge to a 55-gallon oil storage drum. The OWS will have a sludge removal system that will collect settled sludge in a hopper. The sludge will be pumped from the hopper to a solids holding tank via a pneumatic, double-diaphragm pump.

Transfer Pump Station – Process water leaving the OWS will gravity-flow into a pump station, consisting of a small holding tank with integrated centrifugal pump(s). The pumps (including an installed spare) will be capable of a pumping rate of 150 gpm at the required head necessary to pump through the downstream filtration, including the organo-clay and liquid phase granular activated carbon systems described below. From the pump station, process water will be pumped through an MMF system, as described below.

Chemical Injection System – Process water leaving the OWS transfer pump station will be amended with polymer/coagulant via a metering pump and static mixer designed to increase both particulate size and the effectiveness of solids removal through the downstream filtration systems. Particulate size distribution analysis was performed on the influent and treated groundwater during water treatment activities associated with the hydraulic testing activities under the SDDC Work Plan. Results from those analyses indicated that a large percentage of suspended solids present in the groundwater were smaller than 0.5 micron in size. Therefore, a chemical injection system has been added to the design to promote coagulation of these sub-micron particles into larger suspended particles which can be more easily removed via downstream filtration.

MMF System – Amended process water pumped from the OWS transfer pump station will be directed through an MMF system via centrifugal pumps (including an installed spare) to remove suspended solids. From the MMF, process water will be directed through an organo-clay filtration system, as described below.

Organo-clay Filtration System – Process water leaving the MMF system will be directed through two organo-clay vessels arranged in parallel for the removal of any remaining emulsified oils/light phase product.

Liquid-Phase GAC System – Process water leaving the air stripper will be directed through two liquid-phase GAC systems in parallel for the removal of VOCs, SVOCs, and PCBs. Each liquid-phase GAC system will consist of two 5,000 pound liquid-phase GAC vessels configured for series operation.

Bag Filter System – Water from the liquid-phase GAC vessels will be directed through two bag filter systems installed in parallel (two housings per bag filter system), for final polishing of the treated water.

Solids Holding Tank – Sludge that collects in the OWS or the bottom of the influent storage tanks will be directed to a 4,200 gallon solids holding tank with a 30-degree conical bottom. Accumulated solids can be removed from the bottom of the solids holding tank using a solids pump and sent off-site for proper disposal. Decant water from the solids holding tank can be pumped back to the influent storage tanks.

Effluent Holding Tanks – Following treatment, process water will flow to one of two 21,000-gallon (nominal) effluent storage tanks for final equalization prior to discharge to the outfall.

Sump Pump System – Rain water collected in the treatment system area will be directed to a sump system. In addition, water decanted from the solids settling tank will be directed to this sump. The sump will be equipped with a submersible pump. From the sump, collected water will be pumped to the influent settling tanks for treatment.

System Controls – The temporary water treatment system will be manually operated by the Remedial Action Contractor. The influent storage tanks, oil/water separator, pump station tank, solids settling tank, sump, and effluent storage tanks will be equipped with level switches necessary to identify high level conditions and control pump operation. The treatment system will also be equipped with in-line flow meters necessary to manually control pump operation and overall system flow rate.

Additional details regarding each of the major system components are provided in the Technical Specifications provided in Appendix C.

4.5.4 Staging/Construction of Temporary Water Treatment System and Ancillary Equipment

Technical Drawings M-2 and M-3 present the process and instrumentation flow diagrams for the temporary water treatment system based on the design components specified above. As previously indicated, although the design presented herein is comprehensive, it may not necessarily represent the final design that will be implemented by the Remedial Action Contractor. Nevertheless, the intent of this design is that the staging and construction of the temporary water treatment system and ancillary equipment will be performed next to the Mill Street Area (i.e., on Tax Parcel 25-110) during site preparation activities, installation of the fixed structural supports, and/or relocation of the sand cap at the Elm Street Area.

The temporary water treatment system will be constructed on a minimum 8-inch bermed containment area by the Remedial Action Contractor as described in the Technical Specifications (Appendix C) to provide secondary containment equal to a minimum of 110% of one storage tank for the temporary water treatment system (approximately 23,100 gallons), and a one-year, 24-hour storm event of approximately 2.5 inches. Following construction of the temporary water treatment system, it is anticipated that the performance testing activities for the system will also be performed during site preparation activities, installation of the fixed structural supports, and/or relocation of the sand cap at the Elm Street Area, so that full-scale dewatering and water treatment activities are possible upon initiation of the full-scale excavation activities.

Finally, as illustrated in the Project Construction Schedule for implementation of the OU-1 soil remedy presented in Appendix G, the duration for the active excavation, dewatering, and backfilling activities is sufficiently short to allow the performance of these activities during a typical construction season. Accordingly, the temporary water treatment system was designed to operate during a non-winter period only. As a result, it is not anticipated that the system will need to be enclosed in a structure to protect the system from freezing. Finally, enclosing the system is not practicable given the severe space constraints at the Mill Street Area.

4.6 Temporary Water Treatment System Performance Testing

During treatment system start-up testing, the treated water will be held and sampled in the effluent storage tanks until it is determined that the water is suitable to be discharged to the

on-site drainage ditch. If the water is not suitable for discharge, the water will be recycled to the influent tank and retreated. During start-up, up to 40,000 gallons of water will be treated in batch mode and tested appropriately to demonstrate treatment system performance and compliance with effluent discharge criteria.

Water sampling during start-up of the temporary water treatment system will consist of one round of sampling following treatment of approximately 10,000, 25,000, and 40,000 gallons. Start-up water samples will be collected in accordance with the following table:

Constituent and USEPA Method Number	Sample Location		
	Influent	Effluent	Mid-Process
PCBs (608)	X	X	X
VOCs (624)	X	X	X
SVOCs (625)	X	X	
Metals (200.7)	X	X	
Total Suspended Solids (TSS) and Metals (160.2)	X	X	

Note:

Mid-process samples will be collected downstream of the oil/water separator, MMF system, organio-clay filtration system, liquid-phase GAC vessels, and bag filters. Where the treatment train is divided into parallel streams, samples from each parallel stream will be collected. Samples will be collected during startup testing of the system and during normal operations. Some or all of these mid-process locations may be eliminated as operating experience is gained. Metals analyses (all total) include Arsenic, Cadmium, Chromium, Copper, Nickel, Zinc and Iron.

Effluent requirements, including allowable concentrations and sampling frequencies, are provided in the Technical Specifications (Appendix C). The temporary water treatment system is designed to meet the substantive requirements summarized in Table 1 included in Technical Specification 13602 (Temporary Water Treatment System).

4.7 Performance/Sequencing of the Remedial Action

This section provides a description of the proposed sequencing of the OU-1 soil remedy. Similar to the Preliminary Design Report for the LTTD soil remedy, more than one scenario for the performance and sequencing of the OSD soil remedy was evaluated. Specifically, as described in the Intermediate OSD Design Report, the implementation of the OSD soil remedy was evaluated under two different scenarios, including:

- Scenario 1 – In this scenario, all operations and materials of construction will be located within the limits of the Elm and/or Mill Street Areas, with the exception of the following items, which will be located in Keyes Park:

  - Site office/support trailers;
  - Portable sanitary services; and
  - Personal vehicles for contractors and authorized visitors.

  This scenario involved the performance of excavation, dewatering and water treatment (as necessary), vehicle loading, off-site transportation and disposal, and backfilling/restoration activities for the Elm Street Area followed by the performance of similar activities for the Mill Street Area (i.e., the sequential approach to the Remedial Action).

- Scenario 2 – This scenario is consistent with Scenario 1, except the excavation, dewatering and water treatment (as necessary), vehicle loading, off-site transportation and disposal, and backfilling/restoration activities for the Elm and Mill Street Areas would be performed concurrently (but sequenced such that Mill Street would not be closed at the same time the westbound lane of Elm Street is closed). This scenario involves the same limited use of Keyes Park contemplated for Scenario 1.

As a common element to both scenarios, it was assumed that the temporary water treatment system will be staged Tax Parcel 25-110 next to the Mill Street Area. It was also assumed that any liquids generated at the Elm Street Area will be stored in temporary tanks located at the Elm Street Area and transported and/or pumped to the Mill Street Area for treatment and discharge, as necessary. In addition, since: (1) the remedy requires the excavation of the entire Mill Street Area and portions of adjacent properties (i.e., the railroad property, Tax Parcel 25-110); and (2) the Mill Street Area measures only approximately 10,000 square feet, it was assumed that little or no space will be available at the Mill Street Area for staging of equipment, materials, or facilities, beyond the areas designated for staging of the temporary water treatment system and excavation equipment.

Additional details regarding the sequential scenario for implementation of the OU-1 soil remedy are provided in Appendix D of the Intermediate OSD Design Report. However, since the concurrent excavation scenario has been selected for implementation of the OU-1 soil remedy, that scenario is presented in Appendix D of this revised Final Design Report. As previously indicated, the Remedial Action Contractor will be ultimately responsible for the performance and sequencing of the OSD soil remedy. Therefore, the sequencing

information provided in this revised Final Design Report represents one possible approach to the implementation of the OU-1 soil remedy. Details regarding the Remedial Action Contractor's proposed approach for implementation and sequencing of the Remedial Action will be incorporated into the RAWP for submittal to the EPA. Nevertheless, the remainder of this section discusses the performance and sequencing of the OSD soil remedy under Scenario 2. Under that scenario, it is anticipated that the performance of the material excavation portion of the OU-1 soil remedy would involve the following major activities:

- Full-scale operation of temporary water treatment system;
- Full-scale dewatering operations at the Mill Street Area;
- Excavation of Phase 1 impacted materials at the Elm and Mill Street Areas;
- Excavation of Phase 2 impacted materials from the Elm and Mill Street Areas;
- Temporary staging/material handling areas;
- Vehicle loading for transportation of excavated materials to off-site disposal facilities; and
- Verification of limits of excavation.

Additional details regarding each of the above-listed activities are provided in the following sections. Details regarding backfilling and site restoration activities are provided in Section 5.

4.7.1 Full-Scale Operation of Temporary Water Treatment System

Upon successful completion of the performance testing for the temporary water treatment system, full-scale dewatering activities will be initiated prior to performance of excavation activities at the Elm and Mill Street Areas. As indicated on Technical Drawings S-9 and S-10, there are four SPTC cells requiring active dewatering that extend below the water table at the Mill Street Area and two other excavation cells which are anticipated to extend slightly into the water table. Full-scale operation of the temporary water treatment system will be phased to coincide with the dewatering and excavation activities for these cells. Once all cells requiring dewatering activities are backfilled to the level of the water table, operation of the temporary water treatment system will be scaled back to accommodate treatment of miscellaneous waters generated during other phases of the project (e.g., precipitation collected from stockpiles/staging areas for impacted soils/equipment, equipment and

personnel decontamination fluids, dewatering liquids generated during excavation of the Elm Street Area soils [if any], etc.). Throughout the operating period, treated water may be used as backwash for the liquid-phase GAC vessels or for equipment and personnel cleaning activities.

During the first month of operation, sampling of the temporary water treatment system will be conducted once per week. During and after the second month of operation, extending until system shutdown, testing will be conducted once a month. Operational water samples will be collected in accordance with the table presented in Section 4.6.

The temporary water treatment system will be manually operated and controlled by the Remedial Action Contractor. As such, the Remedial Action Contractor will have a water treatment system operator on-site during operation of the system. The system will be manually controlled by the operator through a series of valves, visual readings, and local pump controls as required to accommodate the various modes of operation. As operating experience is gained, the Remedial Action Contractor may be able to reduce the need for an on-site operator based on the operational results and/or by adding additional controls/alarms.

The Remedial Action Contractor will prepare an O&M Manual prior to treatment system start-up. At a minimum, the O&M Manual will include the following information:

- Start-up testing, normal (daily) operations, trouble shooting, and shut-down procedures;
- Preventative and/or routine maintenance requirements;
- Sampling plan, including schedule;
- Recommended spare parts list;
- Calibration and alignment information; and
- Manufacturer's O&M manuals.

4.7.2 Full-Scale Dewatering Activities at the Mill Street Area

Prior to initiation of the Phase 1 excavations at the Elm and Mill Street Areas, full-scale dewatering activities will commence at the Mill Street Area in preparation for the excavation of materials below the water table. As illustrated on Technical Drawings S-9 and S-10, there are six excavation cells that extend below the water table at the Mill Street Area and

will require active dewatering activities (including four SPTC cells and two shallow water table cells). Operation of the temporary water treatment system will be phased to coincide with the dewatering and excavation activities for these six cells. Once all cells requiring active dewatering at the Mill Street Area are backfilled to the level of the water table, operation of the temporary water treatment system will be scaled back as necessary to accommodate treatment of miscellaneous waters generated during the remainder of the project (e.g., collected precipitation, equipment and personnel decontamination fluids, etc.).

4.7.3 Excavation of Phase 1 Impacted Materials at the Elm and Mill Street Areas

As indicated in Appendix D, it is anticipated that the Remedial Action Contractor will generally implement the Remedial Action at the Elm and Mill Street Areas in two phases. The excavations at the Elm and Mill Street Areas will be performed using standard excavation equipment (e.g., tracked excavators, rubber-tire backhoes, etc.). It is anticipated that the construction equipment utilized to excavate and handle impacted materials at these areas will be dedicated to those operations. Therefore, cleaning of such equipment will only be required prior to handling and placement of clean backfill (as described in Section 5.2) or prior to demobilization from the Site (as described in Section 5.6). Additional information regarding the Phase 1 excavations at the Elm and Mill Street Areas is provided below.

4.7.3.1 Phase 1 Excavation - Elm Street Area

The Phase 1 excavation activities at the Elm Street Area will involve two distinct activities, including: (1) the performance of the excavations located within Elm Street; and (2) the performance of the deep excavations (defined herein as excavations greater than 3 feet in depth), which are generally located in the central and northern portions of the Elm Street Area and include several excavations along the banks of the Souhegan River (Figure D-2 in Appendix D). Each of these activities is further described below.

In response to EPA and Town comments on the Intermediate Design Reports, the Elm Street excavations will be initiated prior to initiation of excavation activities at the Mill Street Area for the purpose of ensuring that the northern (i.e., west-bound) lane of Elm Street is not closed concurrently with the closure of the eastern end of Mill Street. Performance of the Elm Street excavations will require the temporary closure of the northern (i.e., west-bound) lane of Elm Street while excavation and backfilling activities are ongoing in that area. In an attempt to minimize disruption to the local community, the excavation activities for the impacted materials beneath Elm Street may be performed during non-peak hours. In such a situation, the Remedial Action Contractor would have clean imported fill available for immediate backfilling and restoration of the affected portions of Elm Street following verification, through survey, of achievement of the limits of excavation.

During performance of the Elm Street excavations, traffic control activities will be implemented in accordance with Section 3.14, the T-series of Technical Drawings provided in Appendix B, and the TR/TA Report provided in Appendix E. Performance of the Elm Street excavations will involve the removal of approximately 135 cy of material. The Remedial Action Contractor may either elect to place the excavated materials directly into vehicles for transportation to the applicable off-site disposal facility, or may stockpile the excavated soils in a temporary staging area (described in Section 3.12) for subsequent loading and off-site disposal concurrently with the other Phase 1 excavation activities, as further described below. Upon verification that the limits of excavation have been achieved in these cells (i.e., through survey and confirmation sampling, as further described in Section 4.7.7), the cells will be backfilled with gravel to surface grade, followed by restoration of the normal vehicular traffic patterns for Elm Street (pedestrian traffic will still be rerouted to the opposite side of the street until completion of the Remedial Action). Final surface restoration (i.e., paving of the street) will occur during site restoration activities and in accordance with the Town's standard specifications (see Appendix C). It should be noted that the Remedial Action Contractor may elect to perform these excavation activities within Elm Street concurrently with the replacement storm sewer installation activities beneath Cottage and Elm Street (described in Section 3.7).

Following completion of the Elm Street excavations described above, the Remedial Action Contractor will commence with performance of the remaining Phase 1 excavations at the Elm Street Area, which will involve the removal of approximately 16,150 cy of material. This volume includes approximately 825 cy of material associated with excavation sloping and to facilitate construction of the engineered cover system, replacement storm sewer and gabion wall. As indicated in Section 4.2.1, fixed excavation supports including steel sheeting and soldier piles will be installed at the Elm Street Area following the site preparation activities described in Section 3. Wood lagging will be added to the soldier piles as the Phase 1 excavation activities proceed to the specified depths, as required to provide the necessary support for the excavation sidewalls. As previously indicated, limited dewatering activities may be required during the performance of the excavation activities at the Elm Street Area. As the vertical limit of excavation for the Elm Street Area is the seasonal low water table, the Remedial Action Contractor may elect to excavate saturated soils in the vicinity of the seasonal low water table (as encountered, depending on the time of year during which the excavations are performed) "in the wet", in which case active dewatering activities for the subject excavations would not be required.

The Phase 1 excavation activities at the Elm Street Area will also include the removal of three existing USTs at the Site. As documented in Section 4.5.3 of the PD Report, the location, orientation, and contents of the USTs were determined during the pre-design investigation. As discussed therein, a geophysical survey was performed to confirm the

location and alignment of the USTs. Once the USTs were located, they were uncovered and inspected to determine their physical conditions (e.g., obvious structural integrity issues) and to collect samples of their contents.

The results of UST characterization activities were presented in the August and September 2003 Monthly Progress Reports and summarized in Table 3 of the PD Report and are included in Tables 14 and 15 herein for ease of reference. The locations of the three USTs were surveyed and the USTs were identified as M-12, M14-N, and M14-S based on their relative location to the sample grid implemented at the Elm Street Area. These USTs are shown on Figure 2 and Technical Drawings G-2. Based upon the UST characterization activities specified above, the following observations were made regarding each UST:

- UST M12: This UST was used for storm water control/retention. The UST has a grate inlet in the center of the tank and measured approximately 3 to 3.5 feet in diameter. The UST was full of water with soft sediment layer on bottom.

- UST M14-N: This UST has dimensions measuring approximately 15 feet long by 5 feet wide. Approximately two inches of liquid with a strong odor were present in the UST and included a very thin water layer under product.

- UST M14-S: This UST has similar dimensions to M14-N and also had a film/sheen on bottom of UST, exhibiting a similar odor as the contents of M14-N.

Figure D-2 in Appendix D shows potential locations for: personnel and equipment decontamination areas; temporary water storage tanks; an excavated material staging/transportation vehicle loading area; and a clean backfill staging area. The Remedial Action Contractor will relocate these various areas as necessary throughout the performance of excavation activities to accommodate performance of the Remedial Action. Whenever possible, excavated materials will be staged directly on soils subject to future excavation and immediately adjacent to active excavation areas such that precipitation run-off from the stockpile can be directed back to the active excavation. However, if excavated soils will be staged on areas not subject to future excavation and/or over restored excavation areas, such stockpiles will be constructed as described in Section 3.12.

As indicated on the Project Construction Schedule (see Appendix G), backfilling activities will generally be performed concurrently with excavation activities at the Elm Street Area. Specifically, upon verification of achievement of the limits of removal for an excavation cell or group of cells (i.e., through survey and confirmation sampling, as further described in Section 4.7.7), placement and compaction of clean backfill material in the excavation cell(s) will commence in accordance with the procedures described in Section 5.2. As indicated

on the Project Construction Schedule, it is estimated that the Phase 1 excavation activities at the Elm Street Area will have a duration of approximately 64 days.

4.7.3.2 Phase 1 Excavation - Mill Street Area

The Phase 1 excavation activities at the Mill Street Area will involve the performance of the deep excavations (again, defined herein as excavations greater than 3 feet in depth), which are generally located in the central portion of the Mill Street Area (Figure D-3 in Appendix D). Performance of these excavations will involve the removal of approximately 8,600 cy of material. This volume includes approximately 700 cy of material associated with excavation sloping. As indicated in Section 4.4, active dewatering activities are required for certain excavation cells extending below the water table at the Mill Street Area. To facilitate dewatering and soil removal activities for those excavations extending far below the water table, fixed excavation supports (i.e., an SPTC wall) will be installed at the Mill Street Area following site preparation activities to provide excavation sidewall support and serve as a groundwater cutoff wall barrier, as described in Section 4.2.2. For the excavation cells extending only slightly into the water table, a well point system will be installed to facilitate the dewatering and soil removal activities in these areas, as described in Section 4.4.2. In summary, the Phase 1 excavations would generally entail the excavation of the excavation cells requiring active dewatering activities located in the interior of the Mill Street Area, followed by the performance of the shallower excavation activities adjacent to these cells.

Figure D-3 in Appendix D also shows potential locations for: the temporary water treatment system; a personnel and equipment decontamination area; potential excavated material staging/transportation vehicle loading area and a clean backfill staging area. With the exception of the temporary water treatment system (which will remain at the proposed location for the duration of the Remedial Action), the Remedial Action Contractor will relocate these various areas as necessary throughout the performance of excavation activities to accommodate performance of the Remedial Action. Similar to the Elm Street Area, wherever possible, excavated materials will be staged directly on soils subject to future excavation and immediately adjacent to active excavation areas such that precipitation run-off from the stockpile can be directed back to the active excavation. However, if excavated materials will be staged over soils not subject to future excavation and/or restored excavation areas, such stockpiles will be constructed as described in Sections 3.12.

As previously indicated, space limitations at the Mill Street Area will require the temporary closure of the western end of Mill Street during the Phase 1 excavation activities at the Mill Street Area. Additional details regarding the temporary closure of Mill Street are provided in

Section 3.14, the T-series of Technical Drawings provided in Appendix B, and the TR/TA Report provided in Appendix E.

Consistent with the performance of similar activities at the Elm Street Area, it is assumed that backfilling activities will generally be performed concurrently with excavation activities at the Mill Street Area, as indicated on the Project Construction Schedule (see Appendix G). Specifically, upon verification of achievement of the limits of removal for an excavation cell or group of cells (i.e., through survey and confirmation sampling, as further described in Section 4.7.7), placement and compaction of clean backfill material in the excavation cell will commence in accordance with the procedures described in Section 5.2. Further, it is anticipated that the Remedial Action Contractor will commence backfilling activities within the bedrock excavation cells immediately upon verification of the removal of all impacted materials to minimize the amount of water generated during dewatering activities, as further discussed in Section 5.2. As indicated on the Project Construction Schedule, it is estimated that the Phase 1 excavation activities at the Elm Street Area will have a duration of approximately 34 days.

4.7.4 Excavation of Phase 2 Impacted Materials at the Elm and Mill Street Areas

Upon completion of the Phase 1 excavation activities described above, it is anticipated that the Remedial Action Contractor will proceed with performance of the Phase 2 excavations activities at both the Elm and Mill Street Areas. Similar to Phase 1, the Phase 2 excavations at the Elm and Mill Street Areas will be performed using standard excavation equipment (e.g., tracked excavators, rubber-tire backhoes, etc.). It is anticipated that the construction equipment utilized to excavate and handle impacted materials at these areas will be dedicated to those operations. Therefore, cleaning of such equipment will only be required prior to handling and placement of clean backfill (as described in Section 5.2) or prior to demobilization from the Site (as described in Section 5.6). Additional information regarding the Phase 2 excavations at the Elm and Mill Street Areas is provided below.

4.7.4.1 Phase 2 Excavation - Elm Street Area

The Phase 2 excavations generally consist of excavation activities for the shallow excavation cells (i.e., excavations to 3 feet or less in depth) located on the periphery of the Elm Street Area (e.g., along Keyes Drive), as illustrated on Figure D-4 in Appendix D. Performance of these excavations will involve the removal of approximately 8,115 cy of material. This volume includes approximately 2,325 cy of material associated with excavation sloping and to facilitate construction of the engineered cover system, replacement storm sewer, storm water retention area, and gabion wall.

Figure D-4 in Appendix D also shows potential locations for: personnel and equipment decontamination areas; excavated material and transportation vehicle loading areas; and a clean backfill staging area. The Remedial Action Contractor will relocate these various areas as necessary throughout the performance of excavation activities to accommodate performance of the Remedial Action. Similar to the Phase 1 excavation activities, wherever possible, excavated materials will be staged directly on soils subject to future excavation and immediately adjacent to active excavation areas such that precipitation run-off from the stockpile can be directed back to the active excavation. However, if excavated materials will be staged over soils not subject to future excavation and/or restored excavation areas, such stockpiles will be constructed as described in Section 3.12.

As indicated on the Project Construction Schedule (see Appendix G), backfilling activities will generally be performed concurrently with excavation activities at the Elm Street Area. Specifically, upon verification of achievement of the limits of removal for an excavation cell or group of cells (i.e., through survey and confirmation sampling, as further described in Section 4.7.7), placement and compaction of clean backfill material in the excavation cell will commence in accordance with the procedures described in Section 5.2. As indicated therein, it is estimated that the duration of the Phase 2 excavation activities at the Elm Street Area will be approximately 32 days.

4.7.4.2 Phase 2 Excavation - Mill Street Area

Similar to the Elm Street Area, the Phase 2 excavations at the Mill Street Area generally consist of excavation activities for the shallow excavation cells (i.e., excavations to 3 feet or less in depth) located on the periphery of the Mill Street Area (e.g., along Mill Street, and the easternmost and westernmost excavations), as illustrated on Figure D-5 in Appendix D. Performance of these excavations will involve the removal of approximately 1,305 cy of material. This volume includes approximately 250 cy of material associated with excavation sloping.

Figure D-5 in Appendix D also shows potential locations for: personnel and equipment decontamination areas; excavated material and transportation vehicle loading areas; and the temporary water treatment system staging area. The Remedial Action Contractor will relocate these various areas as necessary throughout the performance of excavation activities to accommodate performance of the remedial action. Similar to the Phase 1 excavation activities, wherever possible, excavated materials will be staged directly on soils subject to future excavation and immediately adjacent to active excavation areas such that precipitation run-off from the stockpile can be directed back to the active excavation. However, if excavated materials will be staged over soils not subject to future excavation

and/or restored excavation areas, such stockpiles will be constructed as described in Sections 3.12.

As previously indicated, space limitations at the Mill Street Area will require the temporary closure of the eastern end of Mill Street during the Phase 2 excavation activities at the Mill Street Area. Additional details regarding the temporary closure of Mill Street are provided in Section 3.14, the T-series of Technical Drawings provided in Appendix B, and the TR/TA Report provided in Appendix E.

As indicated on the Project Construction Schedule (see Appendix G), backfilling activities will generally be performed concurrently with excavation activities at the Mill Street Area. Specifically, upon verification of achievement of the limits of removal for an excavation cell or group of cells (i.e., through survey and confirmation sampling, as further described in Section 4.7.7), placement and compaction of clean backfill material in the excavation cell will commence in accordance with the procedures described in Section 5.2. As indicated therein, it is estimated that the duration of the Phase 2 excavation activities at the Mill Street Area will be approximately six days.

4.7.5 Management of Temporary Staging/Material Handling Areas

As previously indicated, whenever possible, excavated materials will be staged directly on soils subject to future excavation and immediately adjacent to active excavation areas. In this manner precipitation run-off from the stockpile(s) can be directed back to the active excavation areas. In instances where staging of impacted materials on areas subject to future excavation is not possible and it is not possible to directly load excavated materials into transportation vehicles (e.g., the vehicle loading area cannot be positioned next to the excavation area(s), excavated materials are saturated and require conditioning/gravity dewatering prior to off-site transportation, etc.), the use of lined temporary staging/material handling areas will be required. In such instances, lined temporary staging/material handling areas will be constructed as defined in Section 3.12.

Regardless of whether lined or unlined temporary staging or material handling areas are used, such areas will be subject to the following operational management requirements:

- The staging/material handling areas will be managed such that precipitation falling on impacted materials is directed back into the active excavation areas.

- Impacted soils containing excess moisture will be stabilized using drying and dewatering methods including blending with drier, previously-excavated material, gravity dewatering, air-drying, or the addition of drying agents.

- Materials placed within the temporary staging/material handling areas will be removed as expeditiously as possible.

- At the end of a work day or during a period of prolonged inactivity, materials within the temporary staging/material handling area will be covered with properly anchored tarps until it can be loaded onto transportation vehicles for off-site disposal.

4.7.6 Loading of Vehicles for Transportation of Excavated Materials to Off-Site Disposal Facilities

As previously indicated, excavated materials will be direct-loaded into vehicles for transportation to the appropriate off-site disposal facilities, to the extent practicable. Therefore, transportation vehicles will be staged for loading in close proximity to the areas of excavation. To the extent possible, vehicle loading operations during performance of the Phase 1 excavations will occur over impacted materials subject to future excavation. As a result, construction of a vehicle loading area using all of the materials described in Section 3.12 may not be required. In such an instance, it would likely be sufficient to isolate the wheels of the transportation vehicles from the underlying impacted materials through the use of clean soil/granular fill materials and/or geosynthetic materials. To the extent possible, vehicle loading operations during performance of the Phase 2 excavations will also occur over impacted materials. However, as the Remedial Action is nearing completion in each area, it may be necessary to perform vehicle loading activities on backfilled or previously non-impacted areas. Under this scenario, vehicle loading areas will be constructed as described in Section 3.12.

The following operational practices will be implemented to mitigate the potential spread of materials during vehicle loading operations and subsequent off-site transportation:

- The vehicle loading area will be constructed in accordance with the requirements of Section 3.12 (unless modified as described above).

- After a general safety check of the transportation vehicle, the bed of each receiving vehicle may be lined with polyethylene sheeting (or equivalent) prior to loading of excavated materials. Once the vehicle is loaded, the bed of the vehicle will be covered with a tarp prior to off-site transport. Containers holding excavated materials must also be covered with tarps when they are staged at the Site and are not being actively loaded.

- Polyethylene sheeting may be draped over the side of the receiving vehicle to protect the exterior of the vehicle from coming into contact with excavated material during vehicle loading operations.

- Prior to leaving the site, the transportation vehicles will be routed through an equipment decontamination area for performance of the appropriate cleaning activities described in Section 5.6 (i.e., gross removal of any excavated materials located on the exterior of the vehicle and pressure/wheel washing, if necessary).

- After another safety check of the vehicle and placarding prior to leaving the Site, the drivers of the transportation vehicles will receive the appropriate shipping paperwork (e.g., bills of lading or hazardous waste manifests) with estimated quantities of materials. The final, actual tonnage of material shipped to the off-site disposal facilities will be based on weight measurements at the applicable receiving facility.

- The transportation vehicles will exit the Site and proceed to the appropriate off-site disposal facility.

- Additional details regarding the transportation of excavated materials to the appropriate off-site disposal facilities are provided in Section 4.8.2.

4.7.7 Verification of Limits of Excavation

The Remedial Action Contractor will be responsible for performing detailed horizontal and vertical control surveys during various stages of the Remedial Action. For example, detailed survey activities will be required for verification of the achievement of the limits of excavation (as well as following backfilling and site restoration activities). As previously indicated in Section 2.6, confirmatory soil sampling activities are required in certain excavation cells at the Elm and Mill Street Areas. GE performed certain pre-construction verification soil sampling activities for the Elm Street Area under the SDDC Work Plan, as described in Section 2.4. The results of that sampling have been incorporated into the VSP provided in Appendix A. The remainder of the confirmatory sampling activities and the evaluation of the data from those sampling activities will be performed in accordance with the procedures specified in the VSP presented in Appendix A of this revised Final Design Report.

4.8 Waste Management and Off-Site Disposal of Excavated Materials, Process Residuals and Other Miscellaneous Materials

Implementation of the OSD soil remedy will require the off-site disposal of excavated materials, residuals from the temporary water treatment system and miscellaneous waste materials generated during the performance of general site operational activities. In support of future waste management activities associated with the implementation of the OU-1 soil remedy and as described in Section 2.4, GE performed extensive soil characterization sampling activities under the SDDC Work Plan. Specifically, GE collected 89 soil characterization samples (including 39 samples at the Elm Street Area and 50 samples at the Mill Street Area) for various TCLP and PCB analyses. As also described in Section 2.4, four of the 89 samples (three samples containing lead at the Elm Street Area and one sample containing heptachlor at the Mill Street Area) contained constituent concentrations greater than the applicable TCLP regulatory limits, which would require management as RCRA hazardous waste. Those soil characterization data and the results of any waste characterization performed during the PDI will be provided to the Remedial Action Contractor to assist with the development of a Waste Management Plan that will be included as part of the forthcoming RAWP. That plan will provide details regarding the handling, characterization, manifesting, and off-site treatment/disposal of such materials and provide a summary of the anticipated waste streams that may be encountered during performance of the Remedial Action. Additional details regarding the management and disposition of such materials are provided in the following sections.

4.8.1 Management of Excavated Materials and Other Project-Related Waste

This section describes the management and disposition of excavated materials, other miscellaneous wastes (e.g. PPE, absorbent booms, disposable equipment, miscellaneous construction debris, etc.), and residuals from the temporary water treatment facility that will be generated during performance of the OU-1 soil remedy. To the extent possible, materials from similar waste streams and/or exhibiting similar constituent concentrations will be consolidated for off-site transportation and disposal. Additional management requirements for each of these residual streams are defined below.

Excavated Materials – Excavated material and debris will require management and transportation to an appropriate off-site disposal facility, in accordance with applicable regulations. Additional waste characterization sampling may be performed by GE or the Remedial Action Contractor prior to or during implementation of the OU-1 soil remedy, to further delineate the volume of soils subject to RCRA disposal regulations.

Treated Liquids – As previously indicated, the design of the temporary water treatment system is based on the groundwater data collected during the PDI, quarterly monitoring events performed under the WMP since July 2007, and the baseline and post-hydraulic testing water quality sampling under the SDDC Work Plan. As a result, it is fully anticipated that all treated water will meet the substantive requirements for water discharge to the drainage ditch at the Mill Street Area (that ultimately leads to the Souhegan River via the on-site drainage ditch/culvert system). However, should treated liquids be generated that exceed the discharge criteria (even after multiple rounds of treatment), arrangements will be made to transport such material to an appropriate off-site treatment or disposal facility, in accordance with applicable regulations.

Organo-Clay and Spent Granular Activated Carbon – Organo-clay and spent liquid-phase GAC generated by the temporary water treatment system will require characterization and transportation to an appropriate off-site disposal, treatment, or regeneration facility, in accordance with applicable regulations.

Solids from Holding Tank – Solids produced during backwash of the liquid-phase GAC vessels will be directed to the solids holding tank. In addition, solids settled in the bottom of the settling tanks, influent storage tanks or the OWS will be directed to the solids holding tank. Decant water from the solids holding tank can be pumped back to the influent storage tanks. Accumulated solids can be removed from the bottom of the solids holding tank into appropriate shipping containers using a solids pump. These materials will require characterization and transportation to an appropriate off-site disposal facility, in accordance with applicable regulations.

Spent Filters from Bag Filter Units – The filters in the bag filter units will be periodically changed out. Although this unit is designed as the final polishing step for the treated water prior to discharge (and will likely be exposed to very low-levels of constituents, if any), these materials will be subject to characterization and transportation to an appropriate off-site disposal facility, in accordance with all applicable regulations.

Oil – Although significant quantities of oil are not anticipated, an OWS was included in the design of the temporary water treatment system to handle oils separated from the water stream. Separated oil will require characterization and transportation to an appropriate off-site treatment or disposal facility, in accordance with applicable regulations.

Other Miscellaneous Wastes - Other miscellaneous wastes generated during operation of the temporary water treatment system or performance of the OU-1 soil remedy will include PPE and other construction-related materials. These materials will require characterization

and transportation to an appropriate off-site disposal facility, in accordance with applicable regulations.

4.8.2 Waste Characterization, Transportation, and Disposition of Residuals

As previously indicated, the data collected during the pre-design and supplemental design phases of the project will be provided to the applicable off-site treatment or disposal facilities to assist with characterization of the various waste streams. As indicated on Figures 9 and 12, sampling and analysis conducted during the PDI indicate that certain Site soils contain PCBs at concentrations greater than 50 mg/kg and thus are regulated for disposal under TSCA. Specifically, it is estimated that the volume of excavated material subject to TSCA disposal regulations includes approximately 20,070 cy of excavated material from the Elm Street Area and 6,915 cy of excavated material from the Mill Street Area, as indicated on Table 10. As previously indicated, some of the excavated materials also contain other constituents (i.e., lead and heptachlor) at concentrations sufficient to cause those excavated materials to be considered characteristic hazardous waste under RCRA regulations. If additional waste characterization activities are necessary beyond the activities performed to date, those activities will be performed in accordance with the requirements of the appropriate off-site treatment or disposal facilities and the Waste Management Plan that will be part of the RAWP.

At this time, it is anticipated that residuals from four distinct waste streams may be generated during the performance of the Remedial Action: hazardous liquids, non-hazardous liquids, hazardous solids, non-hazardous solids. It is further anticipated that these waste streams may be routed to the following facilities:

- Hazardous liquids - Waste Management, Inc. (WMI) facility in Port Arthur, Texas.
- Non-hazardous liquids - Numerous facilities are available for the treatment/disposal of such liquids.
- Hazardous solids - WMI facility in Model City, New York.
- Non-hazardous solids - WMI facility in Rochester, New Hampshire.

Additional details regarding the specific waste disposal facilities that will be used during the implementation of the OU-1 soil remedy, the means of transportation to those facilities, and the management, disposition, and waste characterization requirements associated with each facility will be provided in the Waste Management Plan, which will be included in the forthcoming RAWP.

Segregated materials requiring transportation to one of the above-listed off-site disposal facilities will be managed and loaded into transportation vehicles in accordance with the procedures specified in Section 4.7.6. As indicated in the Project Construction Schedule provided in Appendix G, it is currently anticipated that approximately 450 tons of excavated material (or 15 trucks loaded with approximately 20 cy [i.e., about 30 tons] of excavated material per truck) will be sent off-site for disposal on a typical day during implementation of the OU-1 soil remedy. The Remedial Action Contractor will be responsible for providing coordination for the off-site transportation and disposal of these excavated materials. As part of these activities, the Remedial Action Contractor will be responsible for complying with all federal, state, and/or local transportation requirements, including applicable U.S. Department of Transportation (DOT) regulations. Additional details regarding such requirements (e.g, placarding, weights, etc.) will be provided in future design documents and/or contractor submittals.

In addition to the activities relating to the loading of excavated materials for off-site transportation (as specified in Section 4.7.6), the Remedial Action Contractor will be required to implement the following operational procedures for the off-site transportation of excavated materials from the Site:

- Employ qualified personnel trained per DOT requirements for handling and shipping hazardous materials, with such training to include general safety, emergency response, exposure protection, accident prevention, preparation of shipping papers, and securing loads;

- Employ drivers that have a Commercial Driver's License (CDL) with a Hazardous Materials Endorsement;

- Utilize trucks that are DOT-approved;

- Include in its Health and Safety Plan, Operations Plan, and Contingency Plan detailed provisions for responding to transportation emergencies such as spills, releases, or other incidents;

- Prepare and submit to GE a daily summary sheet that indicates the work site, date, and, at a minimum, the following information regarding each truck load:

  - Load number (sequential);

  - Truck identification (ID) number (license plate number of the truck and/or trailer used);

- Time of departure from the work site;
- Estimated net load weight;
- A copy of the signed Uniform Hazardous Waste Manifest or Bill of Lading and any other required shipping papers (e.g., completed Land Disposal Regulation forms); and
- Designation of transported material (e.g., TSCA, non-TSCA, RCRA, etc.).

- Use of the Paint Filter Test (EPA Method 9095A), as necessary to confirm that the materials are suitable for transport (i.e., no free liquids).

Regarding transportation of excavated materials and the miscellaneous project-related waste streams to the appropriate off-site disposal facilities, the TR/TA Report provided in Appendix E of this revised Final Design Report identifies trucking routes from the Elm and Mill Street Areas to NH Route 101, after which the transportation vehicles would travel on state and federal highways to the appropriate off-site disposal facilities.

5. Site Restoration

5.1 Overview

Following completion of excavation and off-site disposal activities for the impacted soils, several site restoration activities will be conducted. These will include, but may not be limited to, the following:

- Backfilling of excavations with imported clean backfill, sand from the cap placed by EPA over the former Elm Street building slab (assuming verification sampling confirms that this material does not contain PCBs at concentrations greater than the SCLs), and/or over-excavated soils (i.e., soils excavated beyond the limits required to meet the applicable SCLs, including for installation of the cover system, and establishment of the utility corridors and tree planting corridors);
- Restoration of final surfaces;
- Groundwater monitoring well replacement, and installation of additional monitoring wells;
- Subsurface utility installation (e.g., replacement storm sewer at the Elm Street Area);
- Contractor demobilization; and
- Post-removal site control activities.

This section generally describes the minimum requirements of the site restoration activities. While the Remedial Action Contractor will be ultimately responsible for determining the means and methods for implementing the site restoration activities, the Remedial Action Contractor's approach (as detailed in one or more technical submittals to be prepared by the Remedial Action Contractor prior to implementing the OU-1 soil remedy) will be subject to review and approval by the Engineer (on behalf of GE).

5.2 Backfilling of Excavations

Backfilling operations will be initiated as soon as practicable following completion and proper documentation of excavation activities (e.g., survey control, confirmatory sampling, etc.). It is anticipated that the excavations will be backfilled and compacted using conventional construction equipment (e.g., tracked excavators or rubber-tire backhoes equipped with compaction attachments). If such construction equipment was utilized for the

excavation and handling of impacted materials, that equipment will be cleaned at the appropriate equipment cleaning/decontamination areas before it is used for backfilling and compaction activities. Such equipment cleaning activities will generally consist of gross solids removal, followed by pressure cleaning, and wipe sampling to confirm that the equipment is clean prior to handling of clean backfill materials. Additional information regarding equipment cleaning and wipe sampling procedures to be implemented by the Remedial Action Contractor are provided in Section 5.6 below.

In areas where confirmatory excavation sampling is not required (e.g., excavations to bedrock at the Mill Street Area, excavations to the seasonal low water level at the Elm Street Area, excavations where soils have been over-excavated to 2 feet or deeper than that needed to meet the applicable SCLs, etc.), gravel and/or flowable fill material may be used to partially backfill excavations that could contain accumulated groundwater (i.e., excavations to bedrock at the Mill Street Area or in the vicinity of the seasonal low water table at the Elm Street Area). Backfill material (former sand cap materials that have been tested to verify that PCBs are not present at concentrations greater than the SCLs, imported backfill that has been tested to verify that it is clean, and/or over-excavated soils [i.e., soils excavated beyond the limits required to meet the applicable SCLs, including for installation of the cover system and establishment of the utility corridors and tree planting corridors]) will be placed in maximum 12-inch-thick lifts in a loose state. Any stones present in the backfill material shall not exceed 2 inches in greatest dimension and shall be distributed throughout the mass. Each layer of backfill material will be thoroughly tamped or rolled consistent with the requirements specified in the applicable Technical Specifications (see Section 8) prior to placing an additional layer of backfill in the excavation. Backfill placed within load-bearing excavation areas (e.g., areas over which structures, driveways, sidewalks, etc. are to be constructed), will be compacted to a minimum 95% of maximum dry density consistent with the testing requirements specified in the applicable Technical Specifications. Other areas will be compacted to obtain a minimum 90% maximum dry density. Consecutive layers of backfill will be placed and compacted until the excavation is brought up to the designed subgrade elevation prior to installing the final surface materials (e.g., engineered cover system, simple vegetated soil cover, pavement/roadway, rip-rap, etc.).

As mentioned above, several different types of material may be utilized to backfill the excavations, including:

- Excavated, stockpiled, and sampled materials from the sand cap installed by the EPA over the former building footprint at the Elm Street Area. As indicated in Section 4, these materials will be removed and stockpiled prior to performance of excavation activities for the existing soils at the Elm Street Area. As required by EPA's April 5,

2007 approval with modifications letter on the Preliminary Design Report for the LTTD soil remedy, these materials will be sampled to verify that such material contains total PCBs below the applicable SCLs and, therefore, is suitable for use as backfill material at the Elm Street Area.

- Soils removed as part of the over-excavation activities required to install the engineered cover system at the Elm Street Area and/or the Town's utility and tree planting corridors for the Elm Street Area. As indicated in GE's May 2, 2007 submittal to the EPA, such materials would be used to backfill the deeper excavations within the limits of the cover system at the Elm Street Area. As also indicated therein, GE proposed to over-excavate the soils in the utility and tree planting corridors on the condition that the over-excavated areas would not be subject to confirmation sampling if the depth of over-excavation is 2 feet or greater.

- Additional backfill will be imported from an off-site source(s) (as necessary) that is certified clean through performance of the confirmation sampling activities specified in the VSP included in Appendix A. This certification, at a minimum, is anticipated to include laboratory analytical data for one or more discrete soil samples representing a specific type and source of backfill material.

As previously indicated, the Remedial Action Contractor will be responsible for verifying that, regardless of the source, the proposed backfill materials are suitable for use as backfill. Specifically, the Remedial Action Contractor will be responsible for ensuring that the over-excavated soils or imported backfill material will be free from excessive moisture, frost, stumps, trees, roots, sod, muck, marl, vegetative matter, or other unsuitable materials so as to facilitate proper settlement, permeability, and compaction.

5.3 Protection and Restoration of Utilities

As indicated in Section 3.7, the Remedial Action Contractor will be responsible for identifying, protecting, relocating, or abandoning both aboveground and underground utilities, as required to facilitate performance of the OU-1 soil remedy. In general, any utilities that are temporarily relocated as part of the site preparation activities will be restored in accordance with the agreements entered into between the Remedial Action Contractor and the organizations that own the utilities and/or the land on which such utilities are located. Aside from these general utility replacement activities, the Remedial Action Contractor will be responsible for the following specific activities related to certain utilities at the Elm and Mill Street Areas.

As previously indicated in Section 3.7, the ROD (as amended) requires the closure in place of the existing storm sewer utility which runs under the east portion of the Elm Street Area (at depths up to 17 feet bgs) and the installation of a replacement storm sewer in a utility corridor that is accessible to future Town utility workers. GE modified the alignment of the replacement storm sewer utility illustrated on Technical Drawing G-20 based upon the results of the pre-construction verification soil sampling performed under the SDDC Work Plan. As also indicated in Section 3.7, GE proposes to install the non-remedial portion of this work (i.e., installation of the portion of the storm sewer from catch basin CB-1 to a proposed new manhole MH-1) during the site preparation phase of the OU-1 remedy. As indicated in the ROD (as amended) and specified in Section VI.9.B of the Town's February 8, 1999 Consent Decree with EPA, the Town is responsible for providing the materials of construction for this replacement storm sewer. The Town's standard specifications were purchased from the Town, and relevant portions have been added to the Technical Specifications included in Attachment C. Technical Drawing G-20 has also been revised to reference the Town's specifications for the materials and construction of the miscellaneous components of the replacement storm sewer utility. The Design Engineer and/or the Remedial Action Contractor will continue to coordinate with the Town (on behalf of GE) regarding the restoration of this utility, as necessary.

The remainder of the replacement storm sewer utility (i.e., the portion of the replacement storm sewer from new manhole MH-1 to Outfall 05 at the Souhegan River) will be installed upon verification that the soil excavations were performed to the limits specified by the Remedial Design (through the performance of survey and confirmation sampling, where appropriate) and concurrently with the appropriate backfilling activities. The route and depth of the replacement storm sewer are shown on Technical Drawing G-20. Following replacement of the storm sewer utility, the Remedial Action Contractor will coordinate the in-place closure of the existing culvert/storm sewer, either following completion of the remedial excavation activities or as part of the site restoration activities. Although the existing storm sewer system is damaged and provides limited drainage, this system will not be taken out of service/closed in place prior to installation of the replacement storm sewer in its entirety.

As indicated in Section 2.4, the Town provided comments on the Preliminary Design Report for the LTTD soil remedy indicating its desire that the site restoration for the Elm Street Area be modified from the asphalt cover contemplated in the Preliminary Design Report to a cover that would be consistent with the Town's conceptual development plan for the Elm Street Area (which contemplates a park with a new war monument, a plaza, a gazebo, etc.). The Town's conceptual development plan also proposed the locations of several utility corridors associated with the miscellaneous structures at the future park. Consistent with those comments and subsequent discussions with the Town and EPA, GE has made several submittals to EPA regarding the cover system and utility corridors at the Elm Street

Area (other than the replacement storm sewer utility described above), as documented in Section 1.2. (Certain of those submittals also included information regarding the identification of tree planting corridors at the Elm Street Area, based on comments provided by the Town.) The Town of Milford subsequently notified EPA and GE via an electronic mail dated December 7, 2010 that the Town had elected to eliminate the proposed memorial park restoration design for the Elm Street Area in lieu of a design that proposed additional parking. This modification also resulted in the elimination of all of the utility corridors proposed in the December 2007 Final Design Report, except for the corridors associated with the replacement storm sewer line and the existing water line along Keyes Drive. GE, EPA, and the Town of Milford subsequently participated in several discussions and exchanged conceptual drawings associated with the design of a hybrid soil cover and parking area restoration design for the Elm Street Area and the associated utility corridors. As indicated in Section 1.2, GE provided revised drawings for design of the utility corridors and the restoration of the Elm Street Area to EPA via electronic mail dated May 2, 2012.

Consistent with GE's May 2, 2007 submittal to EPA on the Elm Street Area cover system, utility corridors, and tree planting corridors, GE is proposing to excavate the soils within the replacement storm sewer utility corridor and also most of the tree planting corridors as part of the OU-1 soil remedy, subject to certain conditions that were discussed in Section 2.6. Upon excavation of the applicable utility corridor, the Remedial Action Contractor will install the components of the replacement storm sewer utility in accordance with the Town's specifications, as discussed in Section 3.7.2.

Finally, following completion of the OU-1 soil remedy, a new utility pole will be installed on the Mill Street Area and the overhead utilities will be relocated from the temporary pole installed on the south side of Mill Street during the site preparation activities to a permanent location on the north side of Mill Street, as illustrated on Technical Drawing G-6B. As noted in Section 3.7.1, GE has provided the proposed overhead utility relocation plan to representatives of PSNH and FairPoint and has participated in on-site meetings to discuss the scope of the overhead utility relocation activities shown on Technical Drawings G-4B and G-6B. As these are ongoing discussions, this plan is not final and is subject to modification/approval by PSNH and FairPoint.

5.4 Restoration of Final Surfaces

Restoration of final surfaces will be performed upon completion of backfilling activities. As indicated throughout this revised Final Design Report, the EPA, Town, and GE have had extensive discussions regarding the restoration of the Elm Street Area subsequent to submittal of the Preliminary Design Report for the LTTD soil remedy. In accordance with those discussions, GE has made several submittals to EPA regarding the proposed cover

system for the Elm Street Area, all of which were documented in Section 1.2. Those submittals indicated that the asphalt cap proposed in the Preliminary Design Report for the Elm Street Area was replaced with an engineered cover system, which is consistent with the Town's conceptual development plan for the Elm Street Area. Most recently, the Town of Milford notified EPA and GE via an electronic mail dated December 7, 2010 that the Town had elected to eliminate the proposed memorial park restoration design for the Elm Street Area in lieu of a design that proposed additional parking.

In general, the site restoration activities will entail the following activities, which will be performed in a manner consistent with the anticipated future uses of the Site:

Elm Street Area

- Final surface restoration consisting of the grading and placement of a 40-inch engineered, low permeability soil cover over consolidated soils (from over-excavation to install the soil cover and/or the utility and tree planting corridors) and clean imported backfill materials.

- Placement of asphalt pavement in areas designated for parking, consistent with the final grading plans and future anticipated use of the Elm Street Area.

- Installation of rip-rap along the riverbank of the Souhegan River and cemetery embankment, and gabion retaining walls along the toe of slope along the riverbank of the Souhegan River.

- Vegetative restoration of remaining areas with topsoil and grass seed or sod.

Mill Street Area and Storm Drainage Ditch System

- Restoration of the area consistent with the anticipated future use of the Mill Street Area, including realignment of Mill Street, resulting in the placement of pavement over a portion of the Mill Street Area.

- Restoration of the railroad property in accordance with Guilford requirements.

- Vegetative restoration of remaining areas with topsoil and grass seed or sod.

- Re-grading and repair of the storm drainage ditch system, as necessary, to promote/convey surface water flow away from the Mill Street Area.

- Installation of erosion controls, if necessary, to prevent erosion or debris from restricting the conveyance of storm water away from the Mill Street Area or future storm water flow in the ditch.

Other types of restoration may include the repair/replacement of surfaces, sidewalks, streets, curbs, culverts, and other appurtenant features disturbed, damaged, or destroyed during the performance of the OU-1 soil remedy. This includes areas utilized for the staging of clean equipment and materials, as well as other support areas used during the performance of the Remedial Action. Additional specific details regarding certain elements of the restoration design are provided below.

The engineered, low permeability cover system for the Elm Street Area will be 40 inches in thickness and consist of an 18-inch layer of low permeability soils, overlain by an 18-inch layer of sand and a 4-inch layer of vegetated topsoil. Additional details regarding the limits and construction of this cover system are provided on Technical Drawings G-21, G-23, G-28, G-30, and G-31. As illustrated therein, the engineered cover system will be installed over the central portion of the Elm Street Area, with the areas outside the cover system consisting of utility and tree planting corridors, riprap-protected slopes, an asphalt parking area, sidewalks and roadways. Engineering calculations related to the design and stability of the cover system including certain storm water features (e.g., anticipated drainage, swales, collection pipes, etc.) are provided in Appendix F.

As indicated in Section 5.3, GE has proposed to excavate and backfill the utility and tree planting corridors subject to certain conditions documented in GE's May 2, 2007 submittal to EPA, as subsequently revised herein and described in Section 2.6. As such, it is currently anticipated that these utility and tree planting corridors will be restored with imported clean backfill, overlain by a 4-inch layer of vegetated topsoil (also imported and verified to be clean).

With respect to the Mill Street Area, GE and the Town have participated in discussions regarding the realignment of Mill Street. In a March 25, 2007 meeting, GE presented the Town with two potential options (i.e., Options #1 and #2) for the realignment of Mill Street. Both options left the intersection of Mill and Cottage Streets unchanged, but differed in the orientation of Mill Street traveling west from the intersection, and thus also differed in the northward shift of the street. Based on comments received from the Town, Option #1 (which did not involve as much northward shift in Mill Street versus Option #2) was selected for the realignment of Mill Street. Technical Drawings T-7 through T-15 present details regarding the proposed realignment of Mill Street. The remainder of the Mill Street Area will be restored in accordance with the requirements of Technical Drawings G-22 and G-24.

Although the ROD and the SOW provide guidance regarding restoration activities for certain areas of the Site, additional areas that will be subject to specific restoration requirements provided by third parties were identified during preparation of the Preliminary Design Report for the LTTD soil remedy. For example, this revised Final Design Report includes additional details for certain portions of Town-owned property (e.g., Mill Street, Keyes Drive, and Keyes Park) and the railroad, based on feedback provided by the Town and Guilford in discussions subsequent to submittal of the Preliminary Design Report. Those details were developed based upon the Town's standard specifications that were purchased from the Town, and specifications that were provided by Guilford for such restoration activities.

In addition to the specific restoration activities described above, the temporary access roads, equipment pads, and materials used to protect existing surface(s) during performance of the OU-1 soil remedy will be removed upon completion of the soil remediation and backfilling activities. For clean equipment and material staging pads, the removed materials will be used as backfill (if backfilling/restoration activities have not been completed) or consolidated and sent off-site for disposal as non-regulated materials, as described in Section 3.11. For other areas the removed materials will be stockpiled and sampled to determine if the material can be reused or must be disposed off-site, as described in Sections 3.12 and 3.13. Each area disturbed during the performance of the Remedial Action will then be restored to pre-construction conditions, as appropriately modified to reflect future uses of the properties.

In summary, Technical Drawings G-21 and G-22 provide final grading details for the Elm and Mill Street Areas, respectively. Technical Drawings G-23 and G-24 provide site restoration details for the Elm and Mill Street Areas, respectively. Finally, Technical Drawings G-27 through G-31 provide standard details regarding types of surface covers. Following the performance of the site restoration activities, a walkover of the entire Site will be conducted to observe and document restored conditions for all areas impacted by the performance of the Remedial Action as a baseline for the post-remedial action monitoring activities further described in Section 5.7.

5.5 Groundwater Monitoring Well Replacement/New Well Installation

As discussed in Section 3.10, several existing monitoring wells, pumping wells, and temporary piezometers are located within the limits of excavation at or near the Elm and Mill Street Areas. As indicated therein, the following monitoring wells will be decommissioned during performance of the OU-1 soil remedy, in accordance with the procedures specified in Appendix V of the FSP:

- Elm Street Area - MW-01A, MW-01B, MW-02A, MW-02AR, MW-02B, MW-03A, MW-03B, MW-26A, MW-26B, and MW-29B; and

- Mill Street Area - MW-07A, MW-09A, MW-09B, MW-21C, MW-22A, MW-22B, MW-22C, PW-1, PW-2, PZ-07B, PZ-07C, PZ-21A, and PZ-21B.

It is anticipated that the majority of these monitoring wells will be replaced to support the post-construction monitoring activities proposed in the EMP, which was submitted to EPA on July 30, 2007, as revised on December 31, 2007 and April 14, 2008. As indicated therein, with the exception of MW-02A (which was replaced by MW-02AR), PW-1, PW-2, PZ-07B, PZ-07C, PZ-21A, and PZ-21B, each of the above-listed wells are included in the list of wells subject to post-construction sampling under the EMP. As a result, replacement wells will be installed and developed for each of the above-listed wells, except for MW-02A (which was installed during the RI through the existing storm sewer utility at the Elm Street Area and subsequently replaced as part of GE's PDI) and PW-1, PW-2, PZ-07B, PZ-07C, PZ-21A, and PZ-21B (which were installed in support of the hydraulic testing activities under the SDDC Work Plan). The replacement wells will be installed following the performance of the OU-1 soil remedy using the procedures specified in Appendix E of the FSP. At the time of this submittal, it has not been determined whether the wells will be replaced by the Remedial Action Contractor as part of the OU-1 soil remedy or as a separate activity performed shortly after completion of the OU-1 soil remedy. Nevertheless, additional details regarding the replacement of these wells are included herein. It is currently proposed that the replacement monitoring wells will be installed at the same approximate locations of the wells prior to remedy implementation, as shown on Figures 14 (Elm Street Area) and 15 (Mill Street Area). It is currently anticipated that the replacement wells will be constructed in a manner similar to the existing monitoring wells. To that end, Table 16 presents well construction details for the existing monitoring wells.

Finally, GE previously proposed in various submittals related to the Remedial Design and WMP to install seven new groundwater monitoring wells (including five bedrock monitoring wells and two overburden monitoring wells) to assist with delineation of the GMZ boundary presented in the IC/AR Plan. EPA approved the installation of all seven monitoring wells, including: MW-09C, MW-11C, MW-26C, MW-30A, MW-30B, MW-30C, and MW-31C. GE subsequently installed monitoring wells MW-11C, MW-30B, MW-30C, and MW-31C prior to implementation of the OU-1 soil remedy and has included each of those wells in the quarterly monitoring events under the WMP performed subsequent to their installation. As agreed to with EPA, MW-30A was eliminated due to the relatively limited overburden thickness observed in the vicinity of the MW-30 monitoring well cluster. EPA also agreed with GE's proposal to install monitoring wells MW-09C and MW-26C following implementation of the OU-1 soil remedy (since the locations of those monitoring wells are

within areas of significant soil excavation during the Remedial Action). The locations of the monitoring wells MW-09C, MW-26C, and MW-31C are shown on Figures 14 (Elm Street Area) and 15 (Mill Street Area). The locations of monitoring well MW-11C and the MW-30 cluster were provided in revised versions of Figures 6 and 7 of the WMP, EMP, and IC/AR Plan, and are included in the quarterly WMRs.

5.6 Equipment/Materials Cleaning and Demobilization

Contractor equipment and materials will be demobilized from the Site as the OU-1 soil remedy is completed. Equipment and materials that did not contact impacted materials will be demobilized from the Site once such materials are no longer required for performance of the Remedial Action. Non-disposable contractor equipment that comes into contact with impacted materials during performance of the remedy will be cleaned prior to demobilizing from the Site.

In general, the equipment cleaning activities will consist of gross solids removal, followed by pressure cleaning, and wipe sampling to confirm that the equipment is clean prior to leaving the Site. These procedures will be generally consistent with the Technical Specifications provided in Appendix C. In accordance with Section VI.B of the SOW (as modified), GE will submit a RAWP and revised POP (which includes the FSP) prior to the initiating the OU-1 soil remedy (i.e., following completion of the Remedial Design and selection of the Remedial Action Contractor). The RAWP will include additional details regarding the required equipment cleaning and wipe sampling activities for the Remedial Action Contractor's equipment and materials.

However, it is known at this time that certain equipment (i.e., applicable portions of the water treatment facilities) will be cleaned in place prior to demobilization since such equipment will be staged in lined/bermed areas equipped with sumps. Cleaning activities for other pieces of contractor equipment will be performed at the appropriate equipment cleaning/decontamination areas. Upon completion of the equipment cleaning activities, the equipment decontamination pads and residual liquids will be consolidated, sampled/characterized, and sent to appropriate off-site disposal facilities in accordance with the requirements of the Waste Management Plan, to be included in the RAWP, followed by demobilization of all remaining contractor equipment and materials.

5.7 Post-Construction Monitoring Activities and Site Control

Section VI.G of the SOW (as modified) requires the preparation of certain documents which describe the post-construction activities to be performed at the OU-1 portion of the Site, for submittal at the 75% construction completion stage. One such document is an EMP.

Specifically, the SOW requires that the EMP define the monitoring activities proposed to demonstrate progress toward and, ultimately, achievement of the groundwater ICLs. At a minimum, this plan is required to provide details regarding how the ICLs have been or will be attained. As required in the SOW (as modified), the EMP will be developed in accordance with the requirements of 40 CFR 264.97 and shall include at a minimum, the following information:

- Sampling locations;
- Sampling frequency;
- Appropriate statistical modeling or other data interpretation techniques; and
- A proposal to demonstrate that the ICLs have been sustained for three consecutive years.

As previously indicated herein, GE has prepared an EMP for post-construction groundwater monitoring of the OU-1 soil remedy. Although not required to submit this document until the 75% construction completion stage, GE submitted the EMP on July 30, 2007. That document was revised through GE's response on December 31, 2007 to EPA's groundwater-related comments dated November 1, 2007 and revised a second time on April 14, 2008. In addition to the items listed above, the EMP also included details regarding groundwater elevation monitoring, laboratory analyses, reporting, monitoring well network inspections, and, as necessary, monitoring well repair or abandonment and replacement procedures.

In addition to the EMP, Section VI.G of the SOW (as modified) requires the preparation of a Long-term Maintenance Plan (LMP) to promote the long-term, continued effectiveness of each component of the OU-1 soil remedy. As specified therein, the LMP will include the following information:

- A description of required long-term maintenance;
- A description of potential maintenance problems;
- A description of routine monitoring and analysis, and methods for evaluating the monitoring data for compliance with ARARs;
- A description of contingency and monitoring;
- An annual maintenance budget;

- Record-keeping and reporting requirements;
- A well maintenance program including, at a minimum, the following:
  - A provision for prompt and proper abandonment, as appropriate, of wells used during the RI and/or PDI, which are currently unusable or which become unusable during the construction phase;
  - A provision for inspection, continued maintenance and repair, if necessary, of all wells used during the RI and PDI, and not abandoned; and
  - A provision for continued maintenance or abandonment of wells used during RI and PDI, and any additional wells to be used during the post-construction phase.
- Site closure and post-closure monitoring;
- A cost estimate for post-closure care consistent with 40 CFR Part 264;
- Establishment of a financial assurance mechanism for post-closure care consistent with 40 CFR Part 264 or paragraph 137 of the Order; and
- A post-closure inspection schedule and provisions for implementing such activities consistent with 40 CFR Part 264.

Concurrent with the July 2007 and April 2008 EMPs, GE prepared and submitted an IC/AR Plan focused on the access requirements, access restrictions and institutional controls associated with the construction and post-construction phases of the OU-1 soil remedy. The institutional controls include restrictions to prevent unauthorized access to subsurface soils and limit the future use of the Elm and Mill Street Areas (both currently owned by the Town) and two other parcels adjacent to the Mill Street Area. In addition, institutional controls are required to restrict the use of groundwater at properties within the GMZ until the interim and/or final groundwater cleanup levels have been achieved.

Finally, in addition to the above-listed documents, the SOW requires the preparation of a revised POP, which will include necessary and appropriate updates required to perform the activities proposed in the EMP and LMP. As stated previously, the POP includes a SMP, a SAP (which consists of an FSP and QAPP), and a CRSP. Updates to the HASP may also be warranted for the post-construction phase of the OU-1 soil remedy.

6. Groundwater Monitoring Zone

As stated in Section 1.5, the OU-1 soil remedy includes establishing a GMZ within which groundwater use would be restricted. Concurrently with the Intermediate OSD Design Report, GE prepared an EMP and IC/AR Plan, which were submitted on July 30, 2007. The EMP provides specific details regarding the scope of the post-construction groundwater monitoring activities, including groundwater elevation monitoring, groundwater quality sampling, laboratory analyses, reporting, monitoring well network inspections and, as necessary, monitoring well repair or abandonment and replacement. The IC/AR Plan focuses on the construction and post-construction phases of the project, and provides specific details regarding access requirements, institutional controls and access restrictions. That document also includes specific details regarding the GMZ for the OU-1 soil remedy, including the properties within the GMZ and the method(s) proposed to establish the GMZ. Since those two documents were submitted at approximately the same time as the Intermediate OSD Design Report, additional details regarding the GMZ and related post-construction groundwater monitoring were provided in the EMP and IC/AR Plan.

EPA provided comments on certain elements of the IC/AR Plan and EMP in a letter to GE dated November 1, 2007. As requested, GE has provided responses to those comments in a separate document submitted to EPA with the December 2007 Final Design Report. EPA's November 1, 2007 letter indicated that EPA had not completed its review of the IC/AR Plan and EMP. As previously indicated, GE performed additional revisions to the IC/AR Plan and EMP and submitted those revised documents to EPA on April 14, 2008.

7. Evaluation of Applicable or Relevant and Appropriate Requirements (ARARs)

The Remedial Action to be conducted at the Site will be subject to several ARARs. Many of these ARARs were identified in Tables 27 through 32 of the ROD. Tables 17 through 19 summarize the chemical-specific, action-specific, and location-specific ARARs for the selected remedy and provide detailed statements of how the ARARs are met, and statements of the assumptions and the plans, drawings, and specifications necessary to support the analysis of compliance with the ARARs.

Although not identified as ARARs on Tables 17 through 19, the Remedial Action will also comply with applicable OSHA regulations for worker safety and with applicable RCRA, TSCA, and Department of Transportation (DOT) regulations for the off-site transportation and disposal of remediation wastes.

8. Technical Drawings and Specifications

8.1 Technical Drawings

Six categories of Technical Drawings were prepared in support of this Remedial Design for the OU-1 soil remedy, including:

- General Drawings (G series), which provide details regarding most aspects of the OU-1 soil remedy, including site preparation, soil removal, backfilling, and site restoration;
- Mechanical Drawings (M series), which provide process flow diagrams and instrumentation for certain components of the temporary water treatment facility;
- Structural Drawings (S series), which present specific details regarding the location, orientation, and construction of the excavation supports that will be utilized at the Site to facilitate performance of the OU-1 soil remedy;
- Traffic Drawings (T series), which present details regarding the restoration of impacted streets in the vicinity of the Elm and Mill Street Areas, including realignment of Mill Street, as well as details regarding the vehicular and pedestrian detours/traffic control measures to be implemented during the performance of the Remedial Action.
- Electrical Drawing (E series), which presents specific details regarding the electrical requirements for the temporary water treatment system, as currently configured.
- Dewatering Drawings (DW series), which present specific details regarding the location and components of the dewatering system that will be utilized to dewater the excavation cells at the Mill Street Area that require excavation to depths below the water table.

The following Technical Drawings are provided in Appendix B of this revised Final Design Report for the OU-1 soil remedy:

General

G-1 General Site Plan

G-2 Existing Conditions - Elm Street Area

G-3 Existing Conditions - Mill Street Area

G-4A	Site Preparation Plan - Elm Street Area
G-4B	Utility Pole Relocation Plan – Elm Street Area
G-4C	Temporary Residential Access Roadway Plan - Elm Street Area
G-4D	Parking Area Plan – Parcel 25-11
G-5A	Site Preparation Plan - Keyes Park
G-5B	Alternate Access/Parking Area Plan – Keyes Park
G-6A	Site Preparation Plan - Mill Street Area
G-6B	Utility Pole Relocation Plan – Mill Street Area
G-6C	Temporary Residential Access Roadway Plan - Mill Street Area
G-7	Staging Plan – Mill Street Area
G-8	Primary Truck Staging Area Site Modifications
G-9	Overflow Truck Staging Area Site Modifications
G-10	Soil Removal Limits (To Achieve Non-Corridor SCLs) - Elm Street Area
G-11	Additional Soil Removal Beyond That Required To Achieve SCLs - Elm Street Area
G-12	Final Soil Removal Limits - Elm Street Area
G-13	Phase 1 Soil Removal Areas - Elm Street Area
G-14	Phase 2 Soil Removal Areas - Elm Street Area
G-15	Soil Removal Limits - Mill Street Area
G-16	Phase 1 Soil Removal Areas - Mill Street Area
G-17	Phase 2 Soil Removal Areas - Mill Street Area
G-18	Utility Corridor Plan - Elm Street Area
G-19	Tree Planting Corridors - Elm Street Area
G-20	Replacement Storm Sewer Utility - Elm Street Area

G-21	Final Grading Plan - Elm Street Area
G-22	Final Grading Plan - Mill Street Area
G-23	Site Restoration Plan - Elm Street Area
G-24	Site Restoration Plan - Mill Street Area
G-25	Site Preparation Details
G-26	Excavation Details – Mill Street Area
G-27	Site Restoration Details – Elm Street Area
G-28	Site Restoration Details – Elm Street Area
G-29	Site Restoration Details – Elm Street Area
G-30	Site Restoration Details – Elm Street Area
G-31	Restoration Details – Keyes Drive and Elm Street Area
G-320	General Notes

Mechanical

M-1	Temporary Water Treatment System - Process Flow Diagram - Mill Street Area
M-2	Temporary Water Treatment System - Process and Instrumentation Diagram - Mill Street Area
M-3	Temporary Water Treatment System - Process and Instrumentation Diagram - Mill Street Area

Structural

S-1	Soil Removal Limits and Support of System Layout - Elm Street Area
S-2	Soil Removal Slopes and Support of System Layout - Elm Street Area
S-3	Bracing Layout of Soil Removal Cells W, S/T, and D - Elm Street Area
S-4	Elevation Sections - Sheet 1 of 3 - Elm Street Area
S-5	Elevation Sections - Sheet 2 of 3 - Elm Street Area

S-6 Elevation Sections - Sheet 3 of 3 - Elm Street Area

S-7 Details - Elm Street Area

S-8 Soil Removal Limits and Support of Excavation System Layout - Mill Street Area

S-9 Soil Removal Slopes and Support of Excavation System Layout - Mill Street Area

S-10 Construction Surcharge and Excavation Limitations - Mill Street Area

S-11 Upper Level Bracing Layout - Mill Street Area

S-12 Lower Level Bracing Layout - Mill Street Area

S-13 Elevation Sections - 1 of 3 - Mill Street Area

S-14 Elevation Sections - 2 of 3 - Mill Street Area

S-15 Elevation Section - 3 of 3 - Mill Street Area

S-16 Details - Sheet 1 of 2 - Mill Street Area

S-17 Details - Sheet 2 of 2 - Mill Street Area

Traffic

T-1 Reconstruction Detour Plan - Mill Street Area

T-2 Reconstruction Phasing and Drive Access Plan - Mill Street Area

T-3 Vehicular Maintenance of Traffic Plan - Elm Street Area

T-4 Pedestrian Maintenance of Traffic Plan - Elm Street Area

T-5 Pavement Repair Detail and Notes - Elm Street Area

T-6 Typical Sections - Mill Street Area

T-7 Plan & Profile STA 5+59.09 to STA 9+50.00 - Mill Street Area

T-8 Grading Plan - Mill Street Area

T-9 Cross Section STA 5+25 to STA 5+75 - Mill Street Area

T-10 Cross Section STA 6+00 to STA 6+50 - Mill Street Area

T-11 Cross Section STA 6+75 to STA 7+25 - Mill Street Area

T-12 Cross Section STA 7+50 to STA 7+75 - Mill Street Area

T-13 Cross Section STA 8+00 to STA 8+25 - Mill Street Area

T-14 Cross Section STA 8+50 to STA 8+81 - Mill Street Area

T-15 Cross Section STA 9+00 to STA 10+00 - Mill Street Area

Electrical

E-1 Temporary Water Treatment System - One-line Diagram - Mill Street Area

Dewatering

DW-1 Excavation Dewatering Master Plan - Mill Street Area

DW-2 SPTC Excavation Area 1 Dewatering System Requirements - Mill Street Area

DW-3 SPTC Excavation Area 2 Dewatering System Requirements - Mill Street Area

DW-4 SPTC Excavation Area 3 Dewatering System Requirements - Mill Street Area

DW-5 SPTC Excavation Area 4 Dewatering System Requirements - Mill Street Area

DW-6 SPTC Phase 2 Dewatering System Requirements - Mill Street Area

DW-7 SPTC Details Dewatering System Requirements - Mill Street Area

Please note that these Technical Drawings will form the basis for the Contract Drawings to be provided to prospective remedial contractors as part of the Contract Documents. Also, although this document represents the revised Final Design Report for the OU-1 soil remedy, the Technical Drawings provided herein will not be signed and stamped until after EPA approval of this revised Final Design Report has been received. At that time, the entire revised Final Design Report, including the individual Technical Drawings, will be signed and stamped for inclusion in the Contract Documents to be provided to prospective remedial contractors.

8.2 Technical Specifications

Several Technical Specifications describing the materials to be used by the Remedial Action Contractor and performance requirements associated with the implementation of the OU-1 soil remedy have been developed in support of this Remedial Design. The following list identifies the Technical Specifications that have been included in Appendix C of this revised Final Design Report. Additional Technical Specifications may be identified based on comments to the Remedial Design provided by the EPA and NHDES, as well as ongoing discussions with the Town and Guilford regarding the scope and performance of the OU-1 soil remedy:

Division 1 – General Requirement Specifications

Section 00580 - Submittals

Section 01140 - Work Restrictions

Section 01160 - Survey Control

Section 01180 - Project Utility Sources

Section 01350 - Health and Safety Plan

Section 01355 - Hazardous Materials Control

Section 01410 - Town and Railroad Requirements

Section 01450 - Quality Control

Section 01460 - Remedial Action Work Plan Submittals

Section 01500 - Temporary Facilities and Controls

Section 01540 - Site Security

Section 01710 - Examination

Section 01715 - Preconstruction Condition Survey

Section 01720 - Preparation

Section 01733 - Construction Waste Management

Section 01740 - Cleaning

Section 01750 - Decontamination and Wipe Sampling of Equipment

Section 01760 - Protecting of Existing and Installed Construction

Section 01770 - Contract Closeout Procedures

Section 01906 - Work Schedule

Division 2 – Site Construction

Section 02015 - Geotechnical Instrumentation and Monitoring

Section 02120 - Removal and Disposal of Underground Storage Tanks

Section 02160 - Lateral Support of Excavation

Section 02201 - Earthwork

Section 02203 - Structural Excavation, Backfill, and Compaction

Section 02204 - Utility Corridor Trenching

Section 02208 - Restoration of Surfaces

Section 02209 - Site Clearing

Section 02210 - Topsoil and Seeding

Section 02240 - Construction Dewatering

Section 02260 - Dust, Soil Erosion, and Sedimentation Control

Section 02270 - Geotextile Fabric

Section 02280 - Rock Filled Gabion Retaining Wall

Section 02300 - Monitoring Well Protection and Abandonment

Section 02370 - Riprap

Section 02400 - Soldier Pile and Tremie Concrete Wall Construction

Section 02500 - Storm Drains

Section 02645 - Bituminous Concrete Pavements

Section 02711 - Galvanized Chain Link Fence

Section 02722 - Granite Curb

Section 02811 - Guiderail

Section 03001 - Concrete

Division 13 - Special Construction

Section 13602 - Temporary Water Treatment System

Section 13810 - Material Transport and Off-Site Disposal

It should be noted that the list of Technical Specifications provided herein differs slightly from the list provided in Section 8.2 of the Intermediate OSD Design Report and Section 8.2 of the December 2007 Final Design Report, due to the fact that certain specifications were combined, while others were eliminated (due either to duplicate information or a determination that the specification was no longer needed). Please note that these Technical Specifications will form the basis for the Materials and Performance Specifications to be provided to prospective remedial contractors as part of the Contract Documents.

9. Remedy Implementation Construction Cost Estimate and Schedule

9.1 Remedy Implementation Construction Cost

An estimated cost for implementation of the OU-1 soil remedy was prepared based on the understanding of the scope of the OU-1 soil remedy at this 100% design stage. That estimated cost is approximately $21,500,000.

9.2 Remedy Implementation Construction Schedule

Based on the understanding of the scope of the OU-1 soil remedy at this 100% design stage, the baseline estimated duration for implementation of the OSD soil remedy is approximately 32.5 months, assuming there are no unusually long delays (e.g., due to inclement weather, access, etc.). This time frame will allow the requisite activities – such as procurement of the Remedial Action Contractor, community participation activities, and preparation/approval of the RAWP – to occur following the submittal of this revised Final Design Report and prior to mobilization. Based on the scope of work to be performed, the on-site portion of the schedule for remedy implementation is approximately 16 months, including mobilization, site preparation, and site restoration activities. The Project Construction Schedule is provided in Appendix G.

10. Future Activities and Schedule

This section provides a description and schedule for activities associated with completing the Remedial Design phase of the project and initiating the Remedial Action phase of the project. Additional details regarding the specific activities and schedule associated with each of these items are presented in the following subsections.

10.1 Future Remedial Design Activities and Schedule

Modifications to certain aspects of the Remedial Design may be appropriate following submittal of this revised Final Design Report based on comments received by EPA on this revised Final Design Report and ongoing discussions with other parties impacted by implementation of the OU-1 soil remedy. Such changes might relate, but not be limited, to the following:

- Ongoing discussions with PSNH, FairPoint, and Guilford regarding the relocation of overhead utilities; and

- Additional discussions with Guilford regarding the scope and implementation of Remedial Action on the railroad property.

10.2 Future Remedial Action Activities and Schedule

Upon receipt of EPA approval or approval with modifications of the revised Final Design Report, the project will proceed to the Remedial Action phase. As specified in the UAO (as modified), certain activities would be required prior to initiation of field activities associated with the OU-1 soil remedy including, but not necessarily limited to, the following:

- Notification of the Supervising Contractor for the Remedial Action in accordance with the requirements of Paragraph 86 of the UAO (as modified);

- EPA approval or disapproval and resubmittal of a list of potential Supervising Contractors in accordance with the requirements of Paragraph 87 of the UAO (as modified);

- Submittal of a letter of acceptance from the Supervising Contractor in accordance with the requirements of Paragraph 88 of the UAO (as modified);

- Preparation of a RAWP in accordance with the requirements of Paragraph 89 of the UAO (as modified);

- Participation in a Pre-Construction Conference with EPA, NHDES, and any other party involved in the remedial action in accordance with the requirements of Paragraph 91 of the UAO (as modified);

- Submittal of construction contractor solicitation documents in accordance with the requirements of Paragraph 92 of the UAO (as modified); and

- Notification of the construction contractor (i.e., the Remedial Action Contractor) for the OU-1 soil remedy in accordance with the requirements of Paragraph 93 of the UAO (as modified).

Tables

TABLE 1
HISTORIC PCB SOIL SAMPLE DATA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in parts per million, ppm)

SAMPLE ID	DEPTH	DATE	TOTAL PCBs (ppm)
ELM STREET - GE BUILDING DEMOLITION DATA			
1-CG-S07-A	0-2	1/15/2001	0.023 J
1-CG-S08-A	2-4	1/15/2001	ND(0.042)
1-CG-S09-A	4-6	1/15/2001	ND(0.042)
1-CS-S01-A	0-1	1/10/2001	1.20
1-CS-S02-A	0-1	1/10/2001	0.20
1-CS-S03-A	0-1	1/10/2001	2.20 [1.90]
2-CG-S01-A	0-2	1/15/2001	3.40
2-CG-S02-A	2-4	1/15/2001	ND(0.040)
2-CG-S03-A	4-6	1/15/2001	ND(0.044)
2-CG-S04-A	0-2	1/15/2001	4.90
2-CG-S05-A	2-4	1/15/2001	27.90
2-CG-S06-A	4-6	1/15/2001	218
2-CS-S04-A	0-1	1/15/2001	111
2-CS-S05-A	0-1	1/17/2001	1,560
3-CS-S06-A	0-1	1/17/2001	9.60
3-CS-S07-A	0-1	1/17/2001	3.90
3-CS-S08-A	0-1	1/17/2001	7.90
3-CS-S09-A	0-1	1/17/2001	1.40
ELM STREET - EPA BUILDING DEMOLITION DATA			
1-CG-S07-A	0-2	1/15/2001	ND
1-CG-S08-A	2-4	1/15/2001	ND
1-CG-S09-A	4-6	1/15/2001	ND
1-CS-S01-A	0-1	1/10/2001	0.66
1-CS-S02-A	0-1	1/10/2001	ND
1-CS-S03-A	0-1	1/10/2001	2.9 [2.5]
2-CG-S01-A	0-2	1/15/2001	2.8
2-CG-S02-A	2-4	1/15/2001	ND
2-CG-S03-A	4-6	1/15/2001	ND
2-CG-S04-A	0-2	1/15/2001	2
2-CG-S05-A	2-4	1/15/2001	28
2-CG-S06-A	4-6	1/15/2001	110
2-CS-S04-A	0-1	1/15/2001	130
2-CS-S05-A	0-1	1/17/2001	1,000
3-CS-S06-A	0-1	1/17/2001	13
3-CS-S07-A	0-1	1/17/2001	3.20
3-CS-S08-A	0-1	1/17/2001	13
3-CS-S09-A	0-1	1/17/2001	2.2 [3.4]

TABLE 1
HISTORIC PCB SOIL SAMPLE DATA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in parts per million, ppm)

SAMPLE ID	DEPTH	DATE	TOTAL PCBs (ppm)
ELM STREET - RI DATA			
EB-01A	40-41.5	10/30/91	ND*
EB-01B	20-21.5	11/04/91	ND*
EB-02A	1-3	10/30/92	12.0
EB-02A	24-28	10/30/92	1.2 J
EB-02B	25-28	11/21/93	0.46
EB-03A	45-46.5	11/08/91	0.041
EB-03B	7-9	11/13/91	20.0 J
EB-03B	11-13	11/13/91	150 J
EB-03B	15-21	11/13/91	3.70 J
EB-03B	15-21	11/13/91	5.70 J
EB-04A	17-19	11/19/91	0.29
EB-05A	12-14	11/21/91	0.027 J
EB-05A	42-44	11/21/91	ND(0.086)
EB-06C	20-22	11/26/91	ND(0.084)
EB-06C	53-55	12/02/91	ND(0.073)
EB-11A	30-31.5	12/04/91	0.023 J
EB-11A	73-77	12/04/91	ND(0.074)
EB-15	1-2.5	11/06/91	5,000 J
EB-15	24-26	11/06/91	8.8 J
EB-16	20-21.5	11/14/91	0.069 J
EB-16	38-39.5	11/14/91	0.019 J
EB-17	10-12	11/04/91	11.0 J
EB-17	27-29	11/05/91	90.0 J
EB-18B	17-18	12/12/91	ND(0.077)
EB-18B	22-25	12/12/91	ND(0.080)
EB-18B	55-56.5	12/12/91	ND(0.077)
EB-20A	0-4	11/30/93	6.20 J
EB-20A	0-4	11/30/93	0.130
EB-20A	12-14	11/30/93	2.60 J
EB-20A	26-30	12/01/93	13.0 J
SS-04	0-0.5	12/03/91	ND(0.3)
SS-04	7-9	12/03/91	0.052
SS-15	0-1	11/09/93	1,100 J
SS-16	0-1	11/04/93	1.97 J
SS-17	0-1	11/09/93	550 J
SS-18	0-1	11/04/93	7.8 J
SS-19	0-1	11/09/93	227
SS-20	0-1	11/09/93	311
SS-21	0-1	11/08/93	280 J
SS-22	0-1	11/09/93	2.8 J
SS-23	0-1	11/09/93	93.0 J
SS-24	0-1	11/09/93	ND*
SS-25	0-1	11/04/93	1.09 J
SS-26	0-1	11/10/93	1,300 J
SS-27	0-1	11/08/93	1.54 J
SS-28	0-1	11/09/93	14.6 J
SS-29	0-1	11/08/93	0.196 J
SS-32	0-1	11/05/93	ND*

TABLE 1
HISTORIC PCB SOIL SAMPLE DATA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in parts per million, ppm)

SAMPLE ID	DEPTH	DATE	TOTAL PCBs (ppm)
ELM STREET - RI DATA (continued)			
SS-33	0-1	11/05/93	0.088 J
SS-34	0-1	11/05/93	0.019 J
SS-35	0-1	11/08/93	ND*
SS-36	0-1	11/08/93	0.107
SS-37	0-1	11/08/93	ND*
SS-37 DUP	0-1	11/08/93	ND*
SS-38	0-1	11/09/93	100.0 J
SS-39	0-1	11/08/93	19.8 J
SS-39 DUP	0-1	11/08/93	21.1 J
SS-40	0-1	11/10/93	2.07 J
SS-40	0-1	11/10/93	8.20 J
MILL STREET - RI DATA			
EB-07A	4-5.5	11/15/91	0.89
EB-08A	4-6	12/11/91	ND(0.076)
EB-09A DUP	4-8	12/02/91	0.220
EB-09A DUP	4-8	12/02/91	0.210
EB-10A	8-9.5	11/20/91	ND(0.080)
EB-10A	17.5-20	11/20/91	ND(0.075)
EB-11A	30-31.5	12/04/91	0.023 J
EB-11A	73-77	12/09/91	ND(0.074)
EB-12	1-3	11/06/91	26,700 J
EB-13	5-8.5	11/13/91	13.0 J
EB-13	15-16.5	11/13/91	1.40 J
EB-14	4-6	11/07/91	20.0
EB-14	12-16	11/07/91	0.99
EB-19	18-21.5	12/10/91	ND(0.16)
EB-21C	0-4	11/22/93	9,400 J
EB-21C DUP	0-4	11/22/93	9,600 J
EB-21C	0-4	11/22/93	100.0
EB-21C	0-4	11/22/93	89.0
EB-21C	8-10	11/22/93	780 J
EB-21C	12-14	11/22/93	190 J
SS-01	0-0.5	11/19/91	3.0
SS-01	6-7	11/19/91	0.072
SS-02	0-0.5	11/20/91	6.9
SS-02	6.5-8	11/20/91	0.079
SS-03	0-0.5	12/02/91	42.0
SS-03	5.5-7.5	12/02/91	0.32
SS-05	0-1	11/04/93	19.0 J
SS-06	0-1	11/04/93	0.32 J
SS-07	0-1	11/04/93	36.0 J
SS-08	0-1	11/04/93	13.0 J
SS-09	0-1	11/04/93	2.90 J
SS-10	0-1	11/04/93	1.60 J
SS-11	0-1	11/04/93	5.40 J
SS-11	0-1	11/04/93	3.00 J
SS-12	0-1	11/04/93	6.29 J
SS-13	0-1	12/02/93	7.60 J
SS-14	0-1	11/04/93	20.80 J

TABLE 1
HISTORIC PCB SOIL SAMPLE DATA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

Notes:

1. J = Estimated.
2. ND = Not detected. Detection limits are presented in parentheses.
3. ND* = Not detected. Information concerning detection limits is not available.
4. Duplicate results are presented in brackets.
5. Data from samples beginning with SS (surface sample) or EB (exploratory boring) were obtained from the following sources:
   Elm and Mill Street Surface Soil Chemical Data Summary Tables (Tables 4-13 and 4-22, respectively); and Elm and Mill Street Exploratory Boring Sampling Chemical Data Summary Tables (Tables 4-14 and 4-23, respectively) from the *Final Remedial Investigation for Fletcher's Paint Site* , *Milford, NH,* July 1, 1994. Detection limits and sample dates for certain samples were obtained from other tables or boring logs contained in that document.
6. Data from samples with CG (confirmatory geoprobe) or CS (confirmatory surface) prefixes are samples collected during building demolition activities performed by EPA at the Elm Street Area between December 2000 and January 2001. Split samples were collected by Blasland, Bouck & Lee, Inc. and submitted to CT&E Environmental Services, Inc. for PCB analyses.

TABLE 2
SUMMARY OF PDI PCB SAMPLE DATA - ELM STREET AREA SURFACE SOILS

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
ESSB-A02	0 - 1	2/3/2004	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	0.029 J	ND(0.041)	0.029 J
ESSB-C02	0 - 1	2/3/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.11 JN	0.097	ND(0.038)	0.20 JN
ESSB-C04	0 - 1	2/4/2004	ND(0.46)	ND(0.46)	ND(0.46)	ND(0.46)	2.3	ND(0.46)	ND(0.46)	2.3
ESSB-E02	0 - 1	2/3/2004	ND(0.19)	ND(0.19)	ND(0.19)	ND(0.19)	1.1 EB	ND(0.19)	ND(0.19)	1.1 EB
ESSB-E04	0 - 1	2/5/2004	ND(0.21)	ND(0.21)	ND(0.21)	ND(0.21)	3.3	ND(0.21)	ND(0.21)	3.3
ESSB-E06	0 - 1	2/6/2004	ND(1.2)	ND(1.2)	ND(1.2)	ND(1.2)	8.3	ND(1.2)	ND(1.2)	8.3
ESSB-G04	0 - 1	2/3/2004	ND(1.0)	ND(1.0)	ND(1.0)	ND(1.0)	21	ND(1.0)	ND(1.0)	21
ESSB-G06	0 - 1	2/9/2004	ND(4.4)	ND(4.4)	ND(4.4)	ND(4.4)	54	ND(4.4)	ND(4.4)	54
ESSB-H03	0 - 1	12/2/2003	ND(4.0)	ND(4.0)	ND(4.0)	ND(4.0)	51	ND(4.0)	ND(4.0)	51
ESSB-H06	0 - 1	12/5/2003	ND(0.14)	ND(0.14)	ND(0.14)	ND(0.14)	0.19	ND(0.14)	ND(0.14)	0.19
ESSB-I04	0 - 1	2/2/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.30 J	ND(0.038)	ND(0.038)	0.30 J
ESSB-I05	0 - 1	1/30/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.10	0.039	ND(0.035)	0.14
ESSB-I06	0 - 1	2/10/2004	ND(4.3) [ND(0.014)]	ND(4.3) [ND(0.014)]	ND(4.3) [ND(0.014)]	ND(4.3) [ND(0.014)]	64 J [0.17 J]	ND(4.3) [ND(0.014)]	ND(4.3) [ND(0.014)]	64 J [0.17 J]
ESSB-I07	0 - 1	12/5/2003	ND(0.068)	ND(0.068)	ND(0.068)	ND(0.068)	0.17	ND(0.068)	ND(0.068)	0.17
ESSB-I08	0 - 1	2/11/2004	ND(59)	ND(59)	ND(59)	ND(59)	560	ND(59)	ND(59)	560
ESSB-J06	0 - 1	7/29/2004	ND(0.28)	ND(0.28)	ND(0.28)	ND(0.28)	1.8 JN	ND(0.28)	ND(0.28)	1.8 JN
ESSB-J07	0 - 1	12/5/2003	ND(3.5)	ND(3.5)	ND(3.5)	ND(3.5)	27	ND(3.5)	ND(3.5)	27
ESSB-J18	0 - 1	12/18/2003	ND(0.70)	ND(0.70)	ND(0.70)	ND(0.70)	7.7	ND(0.70)	ND(0.70)	7.7
ESSB-K06	0 - 1	2/2/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)
ESSB-K08	0 - 1	2/11/2004	ND(270)	ND(270)	ND(270)	ND(270)	4500	ND(270)	ND(270)	4500
ESSB-K10	0 - 1	2/11/2004	ND(250)	ND(250)	ND(250)	ND(250)	2900	ND(250)	ND(250)	2900
ESSB-K16	0 - 1	2/9/2004	ND(13)	ND(13)	ND(13)	ND(13)	130	ND(13)	ND(13)	130
ESSB-K18	0 - 1	12/18/2003	ND(3.6)	ND(3.6)	ND(3.6)	ND(3.6)	19	ND(3.6)	ND(3.6)	19
ESSB-L12	0 - 1	2/10/2004	ND(95)	ND(95)	ND(95)	ND(95)	240	110	ND(95)	360
ESSB-L13	0 - 1	4/16/2004	ND(1.0)	ND(1.0)	ND(1.0)	ND(1.0)	12	ND(1.0)	ND(1.0)	12
ESSB-L14	0 - 1	2/10/2004	ND(36)	ND(36)	ND(36)	ND(36)	350	ND(36)	ND(36)	350
ESSB-L15	0 - 1	1/28/2004	ND(11)	ND(11)	ND(11)	ND(11)	290	ND(11)	ND(11)	290
ESSB-L16	0 - 1	1/28/2004	ND(2.5)	ND(2.5)	ND(2.5)	ND(2.5)	58	34	ND(2.5)	93
ESSB-L17	0 - 1	1/28/2004	ND(2.8)	ND(2.8)	ND(2.8)	ND(2.8)	24	14	ND(2.8)	39
ESSB-L18	0 - 1	1/28/2004	ND(0.98)	ND(0.98)	ND(0.98)	ND(0.98)	16	ND(0.98)	ND(0.98)	16
ESSB-M08	0 - 1	2/3/2004	ND(3.1)	ND(3.1)	ND(3.1)	ND(3.1)	57 JEB	ND(3.1)	ND(3.1)	57 JEB
ESSB-M10	0 - 1	2/5/2004	ND(5.2)	ND(5.2)	ND(5.2)	ND(5.2)	140	ND(5.2)	ND(5.2)	140
ESSB-M12	0 - 1	2/5/2004	ND(110)	ND(110)	ND(110)	ND(110)	1200	ND(110)	ND(110)	1200
ESSB-M14	0 - 1	12/22/2003	ND(380)	ND(380)	ND(380)	ND(380)	890	ND(380)	ND(380)	890
ESSB-M16	0 - 1	2/4/2004	ND(280)	ND(280)	ND(280)	ND(280)	5300	ND(280)	ND(280)	5300
ESSB-M17	0 - 1	1/28/2004	ND(0.40)	ND(0.40)	ND(0.40)	ND(0.40)	12	ND(0.40)	ND(0.40)	12
ESSB-M18	0 - 1	2/4/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.40	ND(0.035)	ND(0.035)	0.40
ESSB-M19	0 - 1	4/15/2004	ND(0.28)	ND(0.28)	ND(0.28)	ND(0.28)	0.86	ND(0.28)	ND(0.28)	0.86
ESSB-N18	0 - 1	1/28/2004	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	1.1	0.75	ND(0.24)	1.9
ESSB-O10	0 - 1	1/29/2004	ND(4.0)	ND(4.0)	ND(4.0)	ND(4.0)	83	51	ND(4.0)	130
ESSB-O12	0 - 1	1/29/2004	ND(100)	ND(100)	ND(100)	ND(100)	1800	ND(100)	ND(100)	1800
ESSB-O14	0 - 1	2/2/2004	ND(180)	ND(180)	ND(180)	1900	ND(180)	ND(180)	ND(180)	1900
ESSB-O16	0 - 1	2/4/2004	ND(1.0) [ND(2.5)]	ND(1.0) [ND(2.5)]	ND(1.0) [ND(2.5)]	ND(1.0) [33 J]	15 J [ND(2.5)]	ND(1.0) [ND(2.5)]	ND(1.0) [ND(2.5)]	15 J [33 J]
ESSB-O18	0 - 1	1/28/2004	ND(3.7)	ND(3.7)	ND(3.7)	ND(3.7)	21	34	ND(3.7)	55
ESSB-P17	0 - 1	1/20/2004	ND(38)	ND(38)	ND(38)	ND(38)	120	ND(38)	ND(38)	120
ESSB-Q10	0 - 1	1/27/2004	ND(5.1)	ND(5.1)	ND(5.1)	ND(5.1)	74	ND(5.1)	ND(5.1)	74
ESSB-Q12	0 - 1	1/29/2004	ND(160)	ND(160)	ND(160)	ND(160)	3000	ND(160)	ND(160)	3000
ESSB-Q14	0 - 1	1/22/2004	ND(260)	ND(260)	ND(260)	ND(260)	1800	1300	ND(260)	3100
ESSB-Q16	0 - 1	1/22/2004	ND(0.41)	ND(0.41)	ND(0.41)	ND(0.41)	3.4	5.2	ND(0.41)	8.6
ESSB-Q18	0 - 1	1/28/2004	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	0.56	1.1	ND(0.24)	1.7
ESSB-R18	0 - 1	1/27/2004	ND(0.22)	ND(0.22)	ND(0.22)	ND(0.22)	0.55	0.50	ND(0.22)	1.0
ESSB-R22	0 - 1	1/27/2004	ND(2.5)	ND(2.5)	ND(2.5)	ND(2.5)	44	20	ND(2.5)	64

TABLE 2
SUMMARY OF PDI PCB SAMPLE DATA - ELM STREET AREA SURFACE SOILS

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
ESSB-A02	0 - 1	2/3/2004	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	0.029 J	ND(0.041)	0.029 J
ESSB-S11	0 - 1	1/19/2004	ND(38)	ND(38)	ND(38)	ND(38)	140	ND(38)	ND(38)	140
ESSB-S11S	0 - 1	4/21/2004	ND(10)	ND(10)	ND(10)	ND(10)	94	ND(10)	ND(10)	94
ESSB-S11SS	0 - 1	4/21/2004	ND(0.17)	ND(0.17)	ND(0.17)	ND(0.17)	0.98	ND(0.17)	ND(0.17)	0.98
ESSB-S11W	0 - 1	4/21/2004	ND(0.20)	ND(0.20)	ND(0.20)	ND(0.20)	3.4	ND(0.20)	ND(0.20)	3.4
ESSB-S12	0 - 1	1/26/2004	ND(3.9) [ND(5.2)]	ND(3.9) [ND(5.2)]	ND(3.9) [ND(5.2)]	ND(3.9) [ND(5.2)]	110 [92]	ND(3.9) [ND(5.2)]	ND(3.9) [ND(5.2)]	110 [92]
ESSB-S14	0 - 1	1/21/2004	ND(3.8)	ND(3.8)	ND(3.8)	ND(3.8)	37	36	ND(3.8)	73
ESSB-S16	0 - 1	1/21/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.14	0.21	ND(0.037)	0.36
ESSB-S18	0 - 1	1/21/2004	ND(0.036) [ND(0.036)]	ND(0.036) [ND(0.036)]	ND(0.036) [ND(0.036)]	ND(0.036) [ND(0.036)]	0.035 J [0.028 J]	0.033 J [0.027 J]	ND(0.036) [ND(0.036)]	0.068 [0.054]
ESSB-S20	0 - 1	12/30/2003	ND(7.4)	ND(7.4)	ND(7.4)	ND(7.4)	50	ND(7.4)	ND(7.4)	50
ESSB-S22	0 - 1	1/21/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.44	0.31	ND(0.035)	0.75
ESSB-T16	0 - 1	12/23/2003	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.20	0.14	ND(0.036)	0.35
ESSS-A01	0 - 1	12/22/2003	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	0.045	ND(0.040)	0.045	0.090
ESSS-A03	0 - 1	12/22/2003	ND(0.049)	ND(0.049)	ND(0.049)	ND(0.049)	ND(0.049)	0.066	ND(0.049)	0.066
ESSS-A04	0 - 1	4/26/2004	ND(0.047)	ND(0.047)	ND(0.047)	ND(0.047)	0.10	0.032 J	ND(0.047)	0.13
ESSS-B02	0 - 1	12/22/2003	ND(0.043)	ND(0.043)	ND(0.043)	ND(0.043)	ND(0.043)	0.050	ND(0.043)	0.050
ESSS-B03	0 - 1	12/22/2003	ND(0.043)	ND(0.043)	ND(0.043)	ND(0.043)	ND(0.043)	0.074	ND(0.043)	0.074
ESSS-B04	0 - 1	12/22/2003	ND(0.048)	ND(0.048)	ND(0.048)	ND(0.048)	ND(0.048)	0.26	ND(0.048)	0.26
ESSS-B05	0 - 1	4/26/2004	ND(0.050)	ND(0.050)	ND(0.050)	ND(0.050)	0.093	0.11	ND(0.050)	0.20
ESSS-C01	0 - 1	1/30/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.13	0.15	ND(0.034)	0.28
ESSS-C03	0 - 1	12/22/2003	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.078	ND(0.037)	0.078
ESSS-C05	0 - 1	4/28/2004	ND(0.049)	ND(0.049)	ND(0.049)	ND(0.049)	0.081	0.068	ND(0.049)	0.15
ESSS-D00	0 - 1	2/11/2004	ND(0.045)	ND(0.045)	ND(0.045)	ND(0.045)	0.26 JN	0.36	0.088	0.71 JN
ESSS-D01	0 - 1	1/30/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.033 J	0.032 J	ND(0.036)	0.065
ESSS-D02	0 - 1	12/22/2003	ND(0.085)	ND(0.085)	ND(0.085)	ND(0.085)	ND(0.085)	0.22	ND(0.085)	0.22
ESSS-D03	0 - 1	12/22/2003	ND(0.078)	ND(0.078)	ND(0.078)	ND(0.078)	ND(0.078)	0.85	ND(0.078)	0.85
ESSS-D05	0 - 1	4/14/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.092 JN	0.047	ND(0.034)	0.14 JN
ESSS-D06	0 - 1	4/14/2004	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	1.2	ND(0.24)	ND(0.24)	1.2
ESSS-D07	0 - 1	4/26/2004	ND(0.044)	ND(0.044)	ND(0.044)	ND(0.044)	0.21	0.16	ND(0.044)	0.37
ESSS-E00	0 - 1	4/15/2004	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	0.10	ND(0.042)	ND(0.042)	0.10
ESSS-E01	0 - 1	1/30/2004	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	0.013 J	0.043	ND(0.042)	0.056
ESSS-E02NE	0 - 1	4/27/2004	ND(0.93)	ND(0.93)	ND(0.93)	ND(0.93)	9.3	ND(0.93)	ND(0.93)	9.3
ESSS-E02W	0 - 1	4/27/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)
ESSS-E03	0 - 1	12/22/2003	ND(0.37)	ND(0.37)	ND(0.37)	ND(0.37)	1.9	ND(0.37)	ND(0.37)	1.9
ESSS-E07	0 - 1	4/14/2004	ND(28)	ND(28)	ND(28)	ND(28)	110	ND(28)	ND(28)	110
ESSS-F00	0 - 1	4/27/2004	ND(0.043)	ND(0.043)	ND(0.043)	ND(0.043)	0.027 J	0.075 JN	ND(0.043)	0.10 JN
ESSS-F01	0 - 1	4/27/2004	ND(0.054)	ND(0.054)	ND(0.054)	ND(0.054)	0.23 JN	0.24	ND(0.054)	0.48 JN
ESSS-F02	0 - 1	1/30/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.010 J	ND(0.034)	ND(0.034)	0.010 J
ESSS-F04	0 - 1	12/22/2003	ND(3.6) [ND(3.8)]	ND(3.6) [ND(3.8)]	ND(3.6) [ND(3.8)]	ND(3.6) [ND(3.8)]	38 [48]	ND(3.6) [ND(3.8)]	ND(3.6) [ND(3.8)]	38 [48]
ESSS-F05	0 - 1	4/14/2004	ND(0.25)	ND(0.25)	ND(0.25)	ND(0.25)	1.5	ND(0.25)	ND(0.25)	1.5
ESSS-F06	0 - 1	4/14/2004	ND(0.22)	ND(0.22)	ND(0.22)	ND(0.22)	1.6	ND(0.22)	ND(0.22)	1.6
ESSS-F07	0 - 1	4/26/2004	ND(0.62)	ND(0.62)	ND(0.62)	ND(0.62)	5.2	ND(0.62)	ND(0.62)	5.2
ESSS-G03	0 - 1	1/30/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.025 J	0.010 J	ND(0.035)	0.035
ESSS-G04NW	0 - 1	4/27/2004	ND(230)	ND(230)	ND(230)	ND(230)	480	ND(230)	ND(230)	480
ESSS-G05	0 - 1	12/5/2003	ND(0.18)	ND(0.18)	ND(0.18)	ND(0.18)	0.59	ND(0.18)	ND(0.18)	0.59
ESSS-G07	0 - 1	4/14/2004	ND(0.54)	ND(0.54)	ND(0.54)	ND(0.54)	6.1	ND(0.54)	ND(0.54)	6.1
ESSS-G08	0 - 1	4/14/2004	ND(1.0)	ND(1.0)	ND(1.0)	ND(1.0)	12	ND(1.0)	ND(1.0)	12
ESSS-G09	0 - 1	4/26/2004	ND(6.5)	ND(6.5)	ND(6.5)	ND(6.5)	64	ND(6.5)	ND(6.5)	64
ESSS-H02	0 - 1	12/2/2003	ND(0.82)	ND(0.82)	ND(0.82)	ND(0.82)	2.0	ND(0.82)	ND(0.82)	2.0
ESSS-H02W	0 - 1	4/27/2004	ND(0.048)	ND(0.048)	ND(0.048)	ND(0.048)	0.12 J	ND(0.048)	ND(0.048)	0.12 J
ESSS-H03NW	0 - 1	4/27/2004	ND(5.4)	ND(5.4)	ND(5.4)	ND(5.4)	26	ND(5.4)	ND(5.4)	26
ESSS-H03SE	0 - 1	4/27/2004	ND(1.1)	ND(1.1)	ND(1.1)	ND(1.1)	14 J	ND(1.1)	ND(1.1)	14 J
ESSS-H03SW	0 - 1	4/27/2004	ND(0.048)	ND(0.048)	ND(0.048)	ND(0.048)	0.23	ND(0.048)	ND(0.048)	0.23

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GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
ESSB-A02	0 - 1	2/3/2004	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	0.029 J	ND(0.041)	0.029 J
ESSS-H05	0 - 1	12/22/2003	ND(4.2)	ND(4.2)	ND(4.2)	ND(4.2)	43	ND(4.2)	ND(4.2)	43
ESSS-H05S	0 - 1	4/27/2004	ND(0.21)	ND(0.21)	ND(0.21)	ND(0.21)	1.7	ND(0.21)	ND(0.21)	1.7
ESSS-H07	0 - 1	4/15/2004	ND(2.0)	ND(2.0)	ND(2.0)	ND(2.0)	31	ND(2.0)	ND(2.0)	31
ESSS-H08	0 - 1	4/15/2004	ND(5.6) [ND(25)]	ND(5.6) [ND(25)]	ND(5.6) [ND(25)]	ND(5.6) [ND(25)]	60 [86]	ND(5.6) [ND(25)]	ND(5.6) [ND(25)]	60 [86]
ESSS-H09	0 - 1	4/26/2004	ND(5.8)	ND(5.8)	ND(5.8)	ND(5.8)	70	ND(5.8)	ND(5.8)	70
ESSS-H10	0 - 1	4/26/2004	ND(28)	ND(28)	ND(28)	ND(28)	280	ND(28)	ND(28)	280
ESSS-H17	0 - 1	4/26/2004	ND(0.36)	ND(0.36)	ND(0.36)	ND(0.36)	0.67	ND(0.36)	ND(0.36)	0.67
ESSS-H18	0 - 1	4/15/2004	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	0.17	0.16	ND(0.041)	0.33
ESSS-H19	0 - 1	4/15/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.038	ND(0.035)	ND(0.035)	0.038
ESSS-I03	0 - 1	12/2/2003	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.073 J	ND(0.038)	ND(0.038)	0.073 J
ESSS-I09	0 - 1	4/15/2004	ND(12)	ND(12)	ND(12)	ND(12)	350	ND(12)	ND(12)	350
ESSS-I10	0 - 1	4/26/2004	ND(1.0)	ND(1.0)	ND(1.0)	ND(1.0)	16	ND(1.0)	ND(1.0)	16
ESSS-I11	0 - 1	4/15/2004	ND(1.7)	ND(1.7)	ND(1.7)	ND(1.7)	17	ND(1.7)	ND(1.7)	17
ESSS-I15	0 - 1	4/26/2004	ND(120)	ND(120)	ND(120)	ND(120)	750	ND(120)	ND(120)	750
ESSS-I16	0 - 1	4/26/2004	ND(0.60)	ND(0.60)	ND(0.60)	ND(0.60)	6.2	ND(0.60)	ND(0.60)	6.2
ESSS-I17	0 - 1	4/26/2004	ND(0.36)	ND(0.36)	ND(0.36)	ND(0.36)	1.4	ND(0.36)	ND(0.36)	1.4
ESSS-I18	0 - 1	4/26/2004	ND(0.27)	ND(0.27)	ND(0.27)	ND(0.27)	0.56	ND(0.27)	ND(0.27)	0.56
ESSS-I19	0 - 1	4/15/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.14	ND(0.036)	ND(0.036)	0.14
ESSS-J03	0 - 1	12/2/2003	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	0.032 J	ND(0.039)	ND(0.039)	0.032 J
ESSS-J04	0 - 1	12/2/2003	ND(0.081)	ND(0.081)	ND(0.081)	ND(0.081)	0.10	ND(0.081)	ND(0.081)	0.10
ESSS-J10	0 - 1	4/15/2004	ND(460)	ND(460)	ND(460)	ND(460)	5800	ND(460)	ND(460)	5800
ESSS-J11	0 - 1	4/15/2004	ND(5.0)	ND(5.0)	ND(5.0)	ND(5.0)	26	ND(5.0)	ND(5.0)	26
ESSS-J12	0 - 1	4/26/2004	ND(71)	ND(71)	ND(71)	ND(71)	710	ND(71)	ND(71)	710
ESSS-J13	0 - 1	4/16/2004	ND(260)	ND(260)	ND(260)	ND(260)	3600	ND(260)	ND(260)	3600
ESSS-J14	0 - 1	4/16/2004	ND(52)	ND(52)	ND(52)	ND(52)	940	ND(52)	ND(52)	940
ESSS-J15	0 - 1	4/15/2004	ND(47)	ND(47)	ND(47)	ND(47)	1500	ND(47)	ND(47)	1500
ESSS-J16	0 - 1	4/15/2004	ND(13)	ND(13)	ND(13)	ND(13)	76	ND(13)	ND(13)	76
ESSS-J17	0 - 1	4/26/2004	ND(1.3)	ND(1.3)	ND(1.3)	ND(1.3)	11 J	ND(1.3)	ND(1.3)	11 J
ESSS-J19	0 - 1	4/15/2004	ND(0.21) [ND(0.21)]	ND(0.21) [ND(0.21)]	ND(0.21) [ND(0.21)]	ND(0.21) [ND(0.21)]	0.93 [1.0]	ND(0.21) [ND(0.21)]	ND(0.21) [ND(0.21)]	0.93 [1.0]
ESSS-K05	0 - 1	12/2/2003	ND(0.41) [ND(0.40)]	ND(0.41) [ND(0.40)]	ND(0.41) [ND(0.40)]	ND(0.41) [ND(0.40)]	0.72 [0.58]	ND(0.41) [ND(0.40)]	ND(0.41) [ND(0.40)]	0.72 [0.58]
ESSS-K07W	0 - 1	4/27/2004	ND(1.0)	ND(1.0)	ND(1.0)	ND(1.0)	10	ND(1.0)	ND(1.0)	10
ESSS-K08SW	0 - 1	4/27/2004	ND(5.7)	ND(5.7)	ND(5.7)	ND(5.7)	34 J	ND(5.7)	ND(5.7)	34 J
ESSS-K11	0 - 1	4/15/2004	ND(140)	ND(140)	ND(140)	ND(140)	2300	ND(140)	ND(140)	2300
ESSS-K12	0 - 1	4/15/2004	ND(24)	ND(24)	ND(24)	ND(24)	140	ND(24)	ND(24)	140
ESSS-K13	0 - 1	4/16/2004	ND(110)	ND(110)	ND(110)	ND(110)	670	ND(110)	ND(110)	670
ESSS-K14	0 - 1	4/16/2004	ND(120)	ND(120)	ND(120)	ND(120)	1200	ND(120)	ND(120)	1200
ESSS-K17	0 - 1	4/15/2004	ND(0.25)	ND(0.25)	ND(0.25)	ND(0.25)	2.3	ND(0.25)	ND(0.25)	2.3
ESSS-K19	0 - 1	4/15/2004	ND(0.22)	ND(0.22)	ND(0.22)	ND(0.22)	2.9 J	ND(0.22)	ND(0.22)	2.9 J
ESSS-L04	0 - 1	12/2/2003	ND(0.080)	ND(0.080)	ND(0.080)	ND(0.080)	0.14 J	ND(0.080)	ND(0.080)	0.14 J
ESSS-L06	0 - 1	12/10/2003	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.048	0.044	ND(0.035)	0.091
ESSS-L19	0 - 1	4/15/2004	ND(0.20)	ND(0.20)	ND(0.20)	ND(0.20)	3.2 J	ND(0.20)	ND(0.20)	3.2 J
ESSS-M05	0 - 1	12/2/2003	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)
ESSS-M07	0 - 1	12/10/2003	ND(0.18)	ND(0.18)	ND(0.18)	ND(0.18)	0.27	ND(0.18)	ND(0.18)	0.27
ESSS-M08W	0 - 1	4/27/2004	ND(1.2)	ND(1.2)	ND(1.2)	ND(1.2)	19 J	ND(1.2)	ND(1.2)	19 J
ESSS-N06	0 - 1	12/2/2003	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	0.021 J	ND(0.041)	0.021 J
ESSS-N08	0 - 1	4/27/2004	ND(10)	ND(10)	ND(10)	ND(10)	61	ND(10)	ND(10)	61
ESSS-N09	0 - 1	4/27/2004	ND(2.0)	ND(2.0)	ND(2.0)	ND(2.0)	15	ND(2.0)	ND(2.0)	15
ESSS-N19	0 - 1	4/27/2004	ND(1.9)	ND(1.9)	ND(1.9)	11	ND(1.9)	ND(1.9)	ND(1.9)	11
ESSS-O07	0 - 1	12/10/2003	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.082	ND(0.036)	0.082
ESSS-O09	0 - 1	4/27/2004	ND(5.2)	ND(5.2)	ND(5.2)	ND(5.2)	79	ND(5.2)	ND(5.2)	79
ESSS-P07	0 - 1	12/10/2003	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.023 J	ND(0.035)	ND(0.035)	0.023 J
ESSS-P08	0 - 1	12/10/2003	ND(0.045)	ND(0.045)	ND(0.045)	ND(0.045)	ND(0.045)	0.32	ND(0.045)	0.32

TABLE 2
SUMMARY OF PDI PCB SAMPLE DATA - ELM STREET AREA SURFACE SOILS

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
ESSB-A02	0 - 1	2/3/2004	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	0.029 J	ND(0.041)	0.029 J
ESSS-P09	0 - 1	4/27/2004	ND(1.2) [ND(1.1)]	ND(1.2) [ND(1.1)]	ND(1.2) [ND(1.1)]	ND(1.2) [ND(1.1)]	8.5 [7.6]	ND(1.2) [ND(1.1)]	ND(1.2) [ND(1.1)]	8.5 [7.6]
ESSS-P18	0 - 1	1/28/2004	ND(0.18)	ND(0.18)	ND(0.18)	ND(0.18)	0.96	0.67	ND(0.18)	1.6
ESSS-Q09	0 - 1	12/10/2003	ND(1.4)	ND(1.4)	ND(1.4)	ND(1.4)	7.6	ND(1.4)	ND(1.4)	7.6
ESSS-Q09W	0 - 1	4/27/2004	ND(0.25)	ND(0.25)	ND(0.25)	ND(0.25)	1.2	ND(0.25)	ND(0.25)	1.2
ESSS-Q17	0 - 1	1/20/2004	ND(0.91)	ND(0.91)	ND(0.91)	ND(0.91)	2.1	3.4	ND(0.91)	5.5
ESSS-R08	0 - 1	12/10/2003	ND(0.069)	ND(0.069)	ND(0.069)	0.48 J	ND(0.069)	ND(0.069)	ND(0.069)	0.48 J
ESSS-R09	0 - 1	12/10/2003	ND(3.4)	ND(3.4)	ND(3.4)	ND(3.4)	34	ND(3.4)	ND(3.4)	34
ESSS-R09S	0 - 1	4/21/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.019 J	ND(0.034)	ND(0.034)	0.019 J
ESSS-R09W	0 - 1	4/21/2004	ND(0.26)	ND(0.26)	ND(0.26)	ND(0.26)	3.1	ND(0.26)	ND(0.26)	3.1
ESSS-R10	0 - 1	1/20/2004	ND(2.3)	ND(2.3)	ND(2.3)	ND(2.3)	9.8	ND(2.3)	ND(2.3)	9.8
ESSS-R10S	0 - 1	4/21/2004	ND(0.24) [ND(0.39)]	ND(0.24) [ND(0.39)]	ND(0.24) [ND(0.39)]	3.5 [3.1]	ND(0.24) [ND(0.39)]	ND(0.24) [ND(0.39)]	ND(0.24) [ND(0.39)]	3.5 [3.1]
ESSS-R11	0 - 1	1/20/2004	ND(21)	ND(21)	ND(21)	ND(21)	71	ND(21)	ND(21)	71
ESSS-R17	0 - 1	1/20/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.12	0.11	ND(0.034)	0.23
ESSS-R18E	0 - 1	4/23/2004	ND(0.18) [ND(0.21)]	ND(0.18) [ND(0.21)]	ND(0.18) [ND(0.21)]	ND(0.18) [ND(0.21)]	0.45 J [0.85 J]	0.54 [0.82]	ND(0.18) [ND(0.21)]	0.98 J [1.7 J]
ESSS-R19	0 - 1	1/27/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)
ESSS-R19N	0 - 1	4/23/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.27	0.32 J	ND(0.037)	0.59 J
ESSS-R20	0 - 1	1/27/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
ESSS-R20N	0 - 1	4/23/2004	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	0.86	1.5	ND(0.24)	2.4
ESSS-R21	0 - 1	1/27/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.035)	ND(0.034)	ND(0.034)	ND(0.035)
ESSS-R21N	0 - 1	4/23/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.17	0.23	ND(0.038)	0.40
ESSS-R22N	0 - 1	4/23/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.10	0.16	ND(0.038)	0.26
ESSS-S11WW	0 - 1	4/21/2004	ND(0.20)	ND(0.20)	ND(0.20)	ND(0.20)	0.54	ND(0.20)	ND(0.20)	0.54
ESSS-S12S	0 - 1	4/21/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.044	0.015 J	ND(0.034)	0.058
ESSS-S13	0 - 1	1/19/2004	ND(1.2)	ND(1.2)	ND(1.2)	ND(1.2)	21	17	ND(1.2)	39
ESSS-S13S	0 - 1	4/21/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.093	0.047 J	ND(0.034)	0.14 J
ESSS-S14S	0 - 1	4/21/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.036 J	0.015 J	ND(0.035)	0.051 J
ESSS-S17	0 - 1	1/19/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.051	0.030 J	ND(0.034)	0.081
ESSS-T15	0 - 1	1/23/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.17	0.17	ND(0.036)	0.34
ESSS-T17	0 - 1	1/23/2004	ND(0.034)	ND(0.034)	ND(0.034)	0.13	ND(0.034)	0.061	ND(0.034)	0.19
ESSS-T18	0 - 1	1/23/2004	ND(0.038)	ND(0.038)	ND(0.038)	0.19	ND(0.038)	0.12	ND(0.038)	0.31
ESSS-T19	0 - 1	1/23/2004	ND(0.036)	ND(0.036)	ND(0.036)	0.14	ND(0.036)	0.10	ND(0.036)	0.25
ESSS-T20	0 - 1	1/23/2004	ND(0.19)	ND(0.19)	ND(0.19)	ND(0.19)	1.3	0.88	ND(0.19)	2.2
ESSS-T20S	0 - 1	4/21/2004	ND(0.22)	ND(0.22)	ND(0.22)	ND(0.22)	1.0	0.67	ND(0.22)	1.7
ESSS-T20SS	0 - 1	4/21/2004	ND(0.18)	ND(0.18)	ND(0.18)	ND(0.18)	1.6	0.72	ND(0.18)	2.3
ESSS-T21	0 - 1	4/21/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.012 J	ND(0.036)	ND(0.036)	0.012 J
SS-16NE	0 - 1	4/27/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.0098 J	ND(0.034)	ND(0.034)	0.0098 J
SS-16NW	0 - 1	4/27/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.012 J	ND(0.034)	ND(0.034)	0.012 J
SS-16SE	0 - 1	4/27/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
SS-16SW	0 - 1	4/27/2004	ND(0.043)	ND(0.043)	ND(0.043)	ND(0.043)	0.14	0.18	ND(0.043)	0.32
SS-18E	0 - 1	4/27/2004	ND(4.9)	ND(4.9)	ND(4.9)	ND(4.9)	26	ND(4.9)	ND(4.9)	26
SS-25NE	0 - 1	4/27/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)
SS-25NW	0 - 1	4/27/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
SS-25SE	0 - 1	4/27/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.025 J	ND(0.035)	ND(0.035)	0.025 J
SS-25SW	0 - 1	4/27/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.012 J	ND(0.034)	ND(0.034)	0.012 J

TABLE 2
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GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Notes:
1. Samples were collected by Blasland, Bouck & Lee, Inc., and submitted to Severn Trent Laboratories, Inc. for analysis of PCBs.
2. ND - Analyte was not detected. The number in parentheses is the associated detection limit.
3. Field duplicate sample results are presented in brackets.
4. In the areas where temporary cover materials have been placed (e.g., geotextile and soil cover), the 0- to 1-foot surface soil sampling interval began at the depth of the geotextile installed by EPA, which is considered to represent the boundary between clean barrier soils and native Site soils.

Data Qualifiers:
EB - The compound was identified in an aqueous equipment blank that was used to assess field contamination associated with soil/sediment samples, its presence in the sample may be suspect.

J - The compound was positively identified; however, the associated numerical value is an estimated concentration only.
JN - The analysis indicates the presence of a compound for which there is presumptive evidence to make a tentative identification. The associated numerical value is an estimated concentration only.

TABLE 3
SUMMARY OF PDI PCB SAMPLE DATA - ELM STREET AREA SUBSURFACE SOILS

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GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
3-CS-S08-A	1 - 3	8/17/2004	ND(18) [ND(11)]	ND(18) [ND(11)]	ND(18) [ND(11)]	ND(18) [ND(11)]	460 [320]	ND(18) [92]	ND(18) [ND(11)]	460 [410]
	3 - 5	8/17/2004	ND(0.22)	ND(0.22)	ND(0.22)	ND(0.22)	1.6	ND(0.22)	ND(0.22)	1.6
	5 - 7	8/17/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.060 J	ND(0.034)	ND(0.034)	0.060 J
	7 - 9	8/17/2004	ND(0.20)	ND(0.20)	ND(0.20)	ND(0.20)	ND(0.20)	ND(0.20)	0.57	0.57
	9 - 11	8/17/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
EB-03B	1 - 3	8/17/2004	ND(37) [ND(21)]	ND(37) [ND(21)]	ND(37) [ND(21)]	ND(37) [ND(21)]	390 [410]	ND(37) [ND(21)]	ND(37) [ND(21)]	390 [410]
	3 - 5	8/17/2004	ND(21)	ND(21)	ND(21)	ND(21)	370	ND(21)	ND(21)	370
	5 - 7	8/17/2004	ND(280)	ND(280)	ND(280)	2000	ND(280)	ND(280)	ND(280)	2000
	9 - 11	8/17/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	0.055	ND(0.033)	ND(0.033)	0.055
	13 - 15	8/17/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.096	ND(0.034)	ND(0.034)	0.096
EB-03BE	1 - 3	8/19/2004	ND(24)	ND(24)	ND(24)	ND(24)	670	ND(24)	ND(24)	670
	3 - 5	8/19/2004	ND(12)	ND(12)	ND(12)	ND(12)	180	ND(12)	ND(12)	180
	5 - 7	8/19/2004	ND(9.7)	ND(9.7)	ND(9.7)	ND(9.7)	140	ND(9.7)	ND(9.7)	140
EB-03BN	1 - 3	8/23/2004	ND(4.5)	ND(4.5)	ND(4.5)	ND(4.5)	34	ND(4.5)	ND(4.5)	34
	3 - 5	8/23/2004	ND(4.1)	ND(4.1)	ND(4.1)	ND(4.1)	6.8	ND(4.1)	ND(4.1)	6.8
	5 - 7	8/23/2004	ND(0.38)	ND(0.38)	ND(0.38)	ND(0.38)	1.9	ND(0.38)	ND(0.38)	1.9
	9 - 11	8/23/2004	ND(0.032)	ND(0.032)	ND(0.032)	ND(0.032)	0.094	ND(0.032)	ND(0.032)	0.094
	11 - 13	8/23/2004	ND(14)	ND(14)	ND(14)	ND(14)	300	ND(14)	ND(14)	300
	13 - 15	8/23/2004	ND(0.22)	ND(0.22)	ND(0.22)	ND(0.22)	1.0 JN	ND(0.22)	ND(0.22)	1.0 JN
	15 - 17	8/23/2004	ND(0.18)	ND(0.18)	ND(0.18)	ND(0.18)	0.54 J	ND(0.18)	ND(0.18)	0.54 J
EB-03BS	1 - 3	8/19/2004	ND(0.74) J	ND(0.74) J	ND(0.74) J	ND(0.74) J	9.0 J	ND(0.74) J	ND(0.74) J	9.0 J
	3 - 5	8/19/2004	ND(1.3)	ND(1.3)	ND(1.3)	ND(1.3)	21	ND(1.3)	ND(1.3)	21
	5 - 7	8/19/2004	ND(20)	ND(20)	ND(20)	ND(20)	890	ND(20)	ND(20)	890
EB-15	2.5 - 4.5	8/11/2004	ND(0.035) [ND(0.035)]	ND(0.035) [ND(0.035)]	ND(0.035) [ND(0.035)]	ND(0.035) [ND(0.035)]	0.15 [0.16]	0.033 J [0.034 J]	ND(0.035) [ND(0.035)]	0.19 [0.20]
	4.5 - 6.5	8/11/2004	ND(0.035)	ND(0.035)	ND(0.035)	0.24	ND(0.035)	0.047	ND(0.035)	0.29
	6.5 - 8.5	8/11/2004	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	0.15 JN	ND(0.039)	ND(0.039)	0.15 JN
	8.5 - 10.5	8/11/2004	ND(0.25)	ND(0.25)	ND(0.25)	0.72	ND(0.25)	ND(0.25)	ND(0.25)	0.72
	10.5 - 12	8/11/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.067 JN	ND(0.038)	ND(0.038)	0.067 JN
	14 - 14.5	8/11/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.22	0.059	ND(0.034)	0.28
	14.5 - 16.5	8/11/2004	ND(0.040)	ND(0.040)	ND(0.040)	0.037 J	ND(0.040)	ND(0.040)	ND(0.040)	0.037 J
	16.5 - 18.5	8/11/2004	ND(0.044)	ND(0.044)	ND(0.044)	0.056 J	ND(0.044)	ND(0.044)	ND(0.044)	0.056 J
	18.5 - 20.5	8/11/2004	ND(0.057)	ND(0.057)	ND(0.057)	0.027 J	ND(0.057)	ND(0.057)	ND(0.057)	0.027 J
	20.5 - 22.5	8/11/2004	ND(0.044)	ND(0.044)	ND(0.044)	0.036 J	ND(0.044)	ND(0.044)	ND(0.044)	0.036 J
EB-15SE	1 - 2.5	8/10/2004	ND(48)	ND(48)	ND(48)	ND(48)	390	150	ND(48)	540
	2.5 - 4.5	8/10/2004	ND(54)	ND(54)	ND(54)	ND(54)	500	380	ND(54)	880
EB-15SW	1 - 3	8/10/2004	ND(200)	ND(200)	ND(200)	ND(200)	1100	320	ND(200)	1500
	3 - 5	8/10/2004	ND(210)	ND(210)	ND(210)	ND(210)	710	270	ND(210)	980
	5 - 7	8/10/2004	ND(130)	ND(130)	ND(130)	ND(130)	660	560	ND(130)	1200
	7 - 9	8/10/2004	ND(10)	ND(10)	ND(10)	ND(10)	42	27	ND(10)	69
	9 - 11	8/10/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.36	0.33	ND(0.037)	0.69
	11 - 13	8/10/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.065	0.047	ND(0.037)	0.11
	13 - 15	8/10/2004	ND(0.044)	ND(0.044)	ND(0.044)	ND(0.044)	0.12	0.065	ND(0.044)	0.19
	15 - 17	8/10/2004	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	0.011 J	ND(0.041)	ND(0.041)	0.011 J
	17 - 19	8/10/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.034 J	0.019 J	ND(0.038)	0.053
	19 - 21	8/10/2004	ND(0.045)	ND(0.045)	ND(0.045)	ND(0.045)	0.036 J	ND(0.045)	ND(0.045)	0.036 J
	21 - 23	8/10/2004	ND(0.049)	ND(0.049)	ND(0.049)	ND(0.049)	0.057	0.035 J	ND(0.049)	0.091
EB-20A	1 - 3	8/17/2004	ND(21)	ND(21)	ND(21)	ND(21)	250	ND(21)	ND(21)	250
	3 - 5	8/17/2004	ND(1.2)	ND(1.2)	ND(1.2)	ND(1.2)	12	5.4 EB	ND(1.2)	17 EB
	5 - 7	8/17/2004	ND(12)	ND(12)	ND(12)	ND(12)	120	84 EB	ND(12)	210 EB
	7 - 9	8/17/2004	ND(12)	ND(12)	ND(12)	ND(12)	69	34 EB	ND(12)	100 EB
	9 - 11	8/17/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.053	ND(0.037)	ND(0.037)	0.053

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Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
ESSB-A02	1 - 3	2/3/2004	ND(0.046)	ND(0.046)	ND(0.046)	ND(0.046)	0.18	ND(0.046)	ND(0.046)	0.18
	3 - 5	2/3/2004	ND(0.045) [ND(0.044)]	ND(0.045) [ND(0.044)]	ND(0.045) [ND(0.044)]	0.022 J [ND(0.044)]	ND(0.045) [0.018 JEB]	ND(0.045) [ND(0.044)]	ND(0.045) [ND(0.044)]	0.022 J [0.018 JEB]
	5 - 7	2/3/2004	ND(0.046)	ND(0.046)	ND(0.046)	ND(0.046)	ND(0.046)	ND(0.046)	ND(0.046)	ND(0.046)
ESSB-C02	1 - 3	2/3/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)
	3 - 5	2/3/2004	ND(0.044)	ND(0.044)	ND(0.044)	ND(0.044)	ND(0.044)	ND(0.044)	ND(0.044)	ND(0.044)
ESSB-C04	1 - 3	2/4/2004	ND(0.42) [ND(0.33)]	ND(0.42) [ND(0.33)]	ND(0.42) [ND(0.33)]	ND(0.42) [ND(0.33)]	4.4 [3.2]	ND(0.42) [ND(0.33)]	ND(0.42) [ND(0.33)]	4.4 [3.2]
	3 - 5	2/4/2004	ND(0.31)	ND(0.31)	ND(0.31)	2.8	ND(0.31)	ND(0.31)	ND(0.31)	2.8
	5 - 7	2/4/2004	ND(0.30)	ND(0.30)	ND(0.30)	3.1	ND(0.30)	ND(0.30)	ND(0.30)	3.1
ESSB-E02	1 - 3	2/3/2004	ND(0.032)	ND(0.032)	ND(0.032)	ND(0.032)	0.011 JEB	ND(0.032)	ND(0.032)	0.011 JEB
	3 - 5	2/3/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	0.084 EB	ND(0.033)	ND(0.033)	0.084 EB
	5 - 7	2/3/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.10 EB	ND(0.035)	ND(0.035)	0.10 EB
	7 - 9	2/3/2004	ND(0.044)	ND(0.044)	ND(0.044)	ND(0.044)	0.021 JEB	ND(0.044)	ND(0.044)	0.021 JEB
	9 - 11	2/3/2004	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)
	11 - 13	2/3/2004	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)
ESSB-E04	1 - 3	2/5/2004	ND(0.035) [ND(0.035)]	ND(0.035) [ND(0.035)]	ND(0.035) [ND(0.035)]	ND(0.035) [ND(0.035)]	0.36 [0.44]	ND(0.035) [ND(0.035)]	ND(0.035) [ND(0.035)]	0.36 [0.44]
	3 - 5	2/5/2004	ND(2.3)	ND(2.3)	ND(2.3)	ND(2.3)	6.0	ND(2.3)	ND(2.3)	6.0
	5 - 7	2/5/2004	ND(0.20)	ND(0.20)	ND(0.20)	ND(0.20)	2.1	ND(0.20)	ND(0.20)	2.1
	7 - 9	2/5/2004	ND(11)	ND(11)	ND(11)	ND(11)	26	ND(11)	ND(11)	26
	9 - 11	2/5/2004	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	0.29	ND(0.042)	ND(0.042)	0.29
ESSB-E06	1 - 3	2/6/2004	ND(1.2)	ND(1.2)	ND(1.2)	ND(1.2)	12	ND(1.2)	ND(1.2)	12
	3 - 5	2/6/2004	ND(1.9)	ND(1.9)	ND(1.9)	ND(1.9)	36	ND(1.9)	ND(1.9)	36
	5 - 7	2/6/2004	ND(0.44)	ND(0.44)	ND(0.44)	ND(0.44)	6.1	ND(0.44)	ND(0.44)	6.1
	7 - 9	2/6/2004	ND(1.4)	ND(1.4)	ND(1.4)	ND(1.4)	11	ND(1.4)	ND(1.4)	11
	9 - 11	2/6/2004	ND(3.9)	ND(3.9)	ND(3.9)	ND(3.9)	47	ND(3.9)	ND(3.9)	47
	11 - 13	2/6/2004	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	0.046	ND(0.039)	ND(0.039)	0.046
ESSB-G04	1 - 3	2/3/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.22	ND(0.034)	ND(0.034)	ND(0.034)
	3 - 5	2/3/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.030 J	0.025 J	ND(0.034)	0.055
	5 - 7	2/3/2004	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]
	7 - 9	2/3/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.024 J	ND(0.035)	ND(0.035)	0.024 J
	9 - 11	2/3/2004	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)
	11 - 13	2/3/2004	ND(0.043)	ND(0.043)	ND(0.043)	ND(0.043)	ND(0.043)	ND(0.043)	ND(0.043)	ND(0.043)
	13 - 15	2/3/2004	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)
ESSB-G06	1 - 3	2/9/2004	ND(4.0)	ND(4.0)	ND(4.0)	ND(4.0)	58	ND(4.0)	ND(4.0)	58
	3 - 5	2/9/2004	ND(4.8)	ND(4.8)	ND(4.8)	52	ND(4.8)	ND(4.8)	ND(4.8)	52
	5 - 7	2/9/2004	ND(4.3)	ND(4.3)	ND(4.3)	34	ND(4.3)	ND(4.3)	ND(4.3)	34
	7 - 9	2/9/2004	ND(1.0)	ND(1.0)	ND(1.0)	ND(1.0)	17	ND(1.0)	ND(1.0)	17
	9 - 11	2/9/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.58	ND(0.036)	ND(0.036)	0.58
	11 - 13	2/9/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.054	ND(0.037)	ND(0.037)	0.054
ESSB-H03	1 - 2	4/27/2004	ND(4.9)	ND(4.9)	ND(4.9)	ND(4.9)	46 J	ND(4.9)	ND(4.9)	46 J
	2 - 3	4/27/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.30 J	ND(0.035)	ND(0.035)	0.30 J
ESSB-H06	1 - 3	7/29/2004	ND(43)	ND(43)	ND(43)	220	ND(43)	ND(43)	ND(43)	220
	3 - 5	7/29/2004	ND(0.42) [ND(0.26)]	ND(0.42) [ND(0.26)]	ND(0.42) [ND(0.26)]	6.8 [5.4]	ND(0.42) [ND(0.26)]	ND(0.42) [ND(0.26)]	ND(0.42) [ND(0.26)]	6.8 [5.4]
	5 - 7	7/29/2004	ND(14)	ND(14)	ND(14)	85	ND(14)	ND(14)	ND(14)	85
	7 - 9	7/29/2004	ND(0.61)	ND(0.61)	ND(0.61)	8.8	ND(0.61)	ND(0.61)	ND(0.61)	8.8
	9 - 11	7/29/2004	ND(0.24)	ND(0.24)	ND(0.24)	2.7	ND(0.24)	ND(0.24)	ND(0.24)	2.7
ESSB-I04	1 - 3	2/2/2004	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	0.98	0.64	ND(0.24)	1.6
	3 - 5	2/2/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.068	ND(0.035)	ND(0.035)	0.068
	5 - 7	2/2/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
	7 - 9	2/2/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.38	ND(0.034)	ND(0.034)	0.38
	9 - 11	2/2/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.044)	ND(0.034)	ND(0.034)	ND(0.044)
	11 - 13	2/2/2004	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)
	13 - 15	2/2/2004	ND(0.044)	ND(0.044)	ND(0.044)	ND(0.044)	ND(0.044)	ND(0.044)	ND(0.044)	ND(0.044)

TABLE 3
SUMMARY OF PDI PCB SAMPLE DATA - ELM STREET AREA SUBSURFACE SOILS

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
ESSB-I05	1 - 3	8/13/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
	3 - 5	8/13/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
	5 - 7	8/13/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
	7 - 9	8/13/2004	ND(0.038) [ND(0.036)]	ND(0.038) [ND(0.036)]	ND(0.038) [ND(0.036)]	ND(0.038) [ND(0.036)]	0.016 J [0.013 J]	ND(0.038) [0.012 J]	ND(0.038) [ND(0.036)]	0.016 J [0.025 J]
	9 - 11	8/13/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)
ESSB-I06	1 - 3	2/10/2004	ND(130)	ND(130)	ND(130)	ND(130)	1300	ND(130)	ND(130)	1300
	3 - 5	2/10/2004	ND(0.93)	ND(0.93)	ND(0.93)	ND(0.93)	17	ND(0.93)	ND(0.93)	17
	5 - 7	2/10/2004	ND(1.1)	ND(1.1)	ND(1.1)	ND(1.1)	21	ND(1.1)	ND(1.1)	21
	7 - 9	2/10/2004	ND(24)	ND(24)	ND(24)	ND(24)	310	ND(24)	ND(24)	310
	9 - 11	2/10/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.18 J	ND(0.036)	ND(0.036)	0.18 J
	11 - 13	2/10/2004	ND(0.17)	ND(0.17)	ND(0.17)	ND(0.17)	1.4	ND(0.17)	ND(0.17)	1.4
	13 - 15	2/10/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.15 J	ND(0.038)	ND(0.038)	0.15 J
ESSB-I07	1 - 3	8/13/2004	ND(27)	ND(27)	ND(27)	ND(27)	91	ND(27)	ND(27)	91
	3 - 5	8/13/2004	ND(1.1)	ND(1.1)	ND(1.1)	ND(1.1)	16	ND(1.1)	ND(1.1)	16
	5 - 7	8/13/2004	ND(0.38)	ND(0.38)	ND(0.38)	ND(0.38)	6.6	ND(0.38)	ND(0.38)	6.6
	7 - 9	8/13/2004	ND(12)	ND(12)	ND(12)	ND(12)	88	ND(12)	ND(12)	88
	9 - 11	8/13/2004	ND(0.25)	ND(0.25)	ND(0.25)	ND(0.25)	5.9	ND(0.25)	ND(0.25)	5.9
	11 - 13	8/13/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.063	ND(0.034)	ND(0.034)	0.063
ESSB-I08	1 - 3	2/11/2004	ND(2.5)	ND(2.5)	ND(2.5)	ND(2.5)	58	ND(2.5)	ND(2.5)	58
	3 - 5	2/11/2004	ND(0.19)	ND(0.19)	ND(0.19)	ND(0.19)	0.89	ND(0.19)	ND(0.19)	0.89
	5 - 7	2/11/2004	ND(0.25) [ND(0.22)]	ND(0.25) [ND(0.22)]	ND(0.25) [ND(0.22)]	ND(0.25) [ND(0.22)]	3.4 [3.1]	ND(0.25) [ND(0.22)]	ND(0.25) [ND(0.22)]	3.4 [3.1]
	7 - 9	2/11/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.12	ND(0.035)	ND(0.035)	0.12
	9 - 11	2/11/2004	ND(5.4)	ND(5.4)	ND(5.4)	ND(5.4)	120	ND(5.4)	ND(5.4)	120
	11 - 13	2/11/2004	ND(1.2)	ND(1.2)	ND(1.2)	ND(1.2)	15	ND(1.2)	ND(1.2)	15
	13 - 15	2/11/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.071	ND(0.038)	ND(0.038)	0.071
ESSB-I08NW	7 - 9	8/19/2004	ND(1.2)	ND(1.2)	ND(1.2)	ND(1.2)	11	ND(1.2)	ND(1.2)	11
	9 - 11	8/19/2004	ND(1.9)	ND(1.9)	ND(1.9)	ND(1.9)	17	ND(1.9)	ND(1.9)	17
	11 - 13	8/19/2004	ND(0.92)	ND(0.92)	ND(0.92)	ND(0.92)	9.9	ND(0.92)	ND(0.92)	9.9
ESSB-J06	1 - 3	7/29/2004	ND(0.23)	ND(0.23)	ND(0.23)	ND(0.23)	1.2 JN	ND(0.23)	ND(0.23)	1.2 JN
	3 - 5	7/29/2004	ND(0.23)	ND(0.23)	ND(0.23)	ND(0.23)	2.0 JN	ND(0.23)	ND(0.23)	2.0 JN
	5 - 7	7/29/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.033 J	ND(0.038)	ND(0.038)	0.033 J
	7 - 9	7/29/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.014 J	ND(0.036)	ND(0.036)	0.014 J
	9 - 11	7/29/2004	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)
ESSB-J07	1 - 3	8/13/2004	ND(4.3)	ND(4.3)	ND(4.3)	ND(4.3)	46	ND(4.3)	ND(4.3)	46
	3 - 5	8/13/2004	ND(0.22)	ND(0.22)	ND(0.22)	ND(0.22)	0.36 J	ND(0.22)	ND(0.22)	0.36 J
	5 - 7	8/13/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.13	ND(0.034)	ND(0.034)	0.13
	9 - 11	8/13/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.29	0.14	ND(0.038)	0.43
	11 - 13	8/13/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.019 J	0.0092 J	ND(0.034)	0.028 J
	13 - 15	8/13/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.045	ND(0.034)	ND(0.034)	0.045
ESSB-J18	1 - 3	12/18/2003	ND(1.9)	ND(1.9)	ND(1.9)	ND(1.9)	8.6	ND(1.9)	ND(1.9)	8.6
	3 - 5	12/18/2003	ND(0.23)	ND(0.23)	ND(0.23)	ND(0.23)	1.6	ND(0.23)	ND(0.23)	1.6
	5 - 7	12/18/2003	ND(0.18)	ND(0.18)	ND(0.18)	ND(0.18)	0.67	ND(0.18)	ND(0.18)	0.67
	7 - 9	12/18/2003	ND(0.18)	ND(0.18)	ND(0.18)	ND(0.18)	1.1	ND(0.18)	ND(0.18)	1.1
	11 - 13	12/18/2003	ND(6.8)	ND(6.8)	ND(6.8)	ND(6.8)	73	ND(6.8)	ND(6.8)	73
	13 - 15	12/18/2003	ND(0.068)	ND(0.068)	ND(0.068)	ND(0.068)	0.24	ND(0.068)	ND(0.068)	0.24
	15 - 17	12/18/2003	ND(6.9) [ND(3.4)]	ND(6.9) [ND(3.4)]	ND(6.9) [ND(3.4)]	ND(6.9) [ND(3.4)]	46 [30]	ND(6.9) [ND(3.4)]	ND(6.9) [ND(3.4)]	46 [30]
	17 - 19	12/18/2003	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	0.33	ND(0.039)	ND(0.039)	0.33
	19 - 21	12/18/2003	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.074	ND(0.037)	ND(0.037)	0.074
	21 - 23	12/18/2003	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.069	ND(0.037)	ND(0.037)	0.069

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GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
ESSB-K06	1 - 3	2/2/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.042)	ND(0.034)	ND(0.034)	ND(0.042)
	3 - 5	2/2/2004	ND(0.035) [ND(0.034)]	ND(0.035) [ND(0.034)]	ND(0.035) [ND(0.034)]	ND(0.035) [ND(0.034)]	ND(0.035) [ND(0.034)]	ND(0.035) [ND(0.034)]	ND(0.035) [ND(0.034)]	ND(0.035) [ND(0.034)]
	5 - 7	2/2/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
	7 - 9	2/2/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
	9 - 11	2/2/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
	11 - 13	2/2/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.056	0.044 J	ND(0.035)	0.10 J
	13 - 15	2/2/2004	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)
	15 - 17	2/2/2004	ND(0.043)	ND(0.043)	ND(0.043)	ND(0.043)	ND(0.043)	ND(0.043)	ND(0.043)	ND(0.043)
ESSB-K07	1 - 3	8/13/2004	ND(450)	ND(450)	ND(450)	ND(450)	2100	ND(450)	ND(450)	2100
	3 - 5	8/13/2004	ND(0.23)	ND(0.23)	ND(0.23)	ND(0.23)	2.8	ND(0.23)	ND(0.23)	2.8
ESSB-K08	1 - 3	2/11/2004	ND(130)	ND(130)	ND(130)	ND(130)	1000	ND(130)	ND(130)	1000
	3 - 5	2/11/2004	ND(4.9) [ND(2.0)]	ND(4.9) [ND(2.0)]	ND(4.9) [ND(2.0)]	ND(4.9) [ND(2.0)]	47 [30]	20 [18]	ND(4.9) [ND(2.0)]	68 [48]
	5 - 7	2/11/2004	ND(0.21)	ND(0.21)	ND(0.21)	ND(0.21)	1.8	0.58	ND(0.21)	2.3
	7 - 9	2/11/2004	ND(0.25)	ND(0.25)	ND(0.25)	ND(0.25)	0.99	0.42	ND(0.25)	1.4
	9 - 11	2/11/2004	ND(0.27)	ND(0.27)	ND(0.27)	ND(0.27)	0.76	ND(0.27)	ND(0.27)	0.76
	11 - 13	2/11/2004	ND(0.044)	ND(0.044)	ND(0.044)	ND(0.044)	0.15	0.091 J	ND(0.044)	0.24 J
	13 - 15	2/11/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.034 J	0.0099 J	ND(0.036)	0.044
	15 - 17	2/11/2004	ND(0.19)	ND(0.19)	ND(0.19)	ND(0.19)	ND(0.19)	ND(0.19)	ND(0.19)	ND(0.19)
	17 - 19	2/11/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.14	ND(0.038)	ND(0.038)	0.14
ESSB-K09	1 - 3	8/4/2004	ND(540)	ND(540)	ND(540)	4300	ND(540)	ND(540)	ND(540)	4300
	3 - 5	8/4/2004	ND(10)	ND(10)	ND(10)	ND(10)	41	27	ND(10)	68
ESSB-K10	1 - 3	2/11/2004	ND(4.4)	ND(4.4)	ND(4.4)	ND(4.4)	50	ND(4.4)	ND(4.4)	50
	3 - 5	2/11/2004	ND(1.0)	ND(1.0)	ND(1.0)	ND(1.0)	7.4	ND(1.0)	ND(1.0)	7.4
	5 - 7	2/11/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.064	ND(0.037)	ND(0.037)	0.064
	7 - 9	2/11/2004	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	4.0 J	0.62	ND(0.24)	4.6 J
	9 - 11	2/11/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.037 JN	ND(0.036)	ND(0.036)	0.037 JN
	11 - 13	2/11/2004	ND(0.26)	ND(0.26)	ND(0.26)	ND(0.26)	2.1	ND(0.26)	ND(0.26)	2.1
	13 - 15	2/11/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.051	ND(0.038)	ND(0.038)	0.051
	15 - 17	2/11/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.16	0.094 J	ND(0.036)	0.25 J
	17 - 19	2/11/2004	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	0.036 J	ND(0.041)	ND(0.041)	0.036 J
ESSB-K16	1 - 3	2/9/2004	ND(5.0)	ND(5.0)	ND(5.0)	ND(5.0)	62	ND(5.0)	ND(5.0)	62
	3 - 5	2/9/2004	ND(0.20)	ND(0.20)	ND(0.20)	ND(0.20)	2.4	ND(0.20)	ND(0.20)	2.4
	5 - 7	2/9/2004	ND(0.20)	ND(0.20)	ND(0.20)	ND(0.20)	4.3	ND(0.20)	ND(0.20)	4.3
	7 - 9	2/9/2004	ND(0.22)	ND(0.22)	ND(0.22)	ND(0.22)	1.7	ND(0.22)	ND(0.22)	1.7
	9 - 11	2/9/2004	ND(22)	ND(22)	ND(22)	ND(22)	190	ND(22)	ND(22)	190
	11 - 13	2/9/2004	ND(0.22)	ND(0.22)	ND(0.22)	ND(0.22)	1.7	0.98	ND(0.22)	2.7
	13 - 15	2/9/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.14 J	ND(0.036)	ND(0.036)	0.14 J
	15 - 17	2/9/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.64	ND(0.037)	ND(0.037)	0.64
	17 - 19	2/9/2004	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	0.048 J	ND(0.039)	ND(0.039)	0.048 J
	19 - 21	2/9/2004	ND(1.4)	ND(1.4)	ND(1.4)	22	ND(1.4)	ND(1.4)	1.7	24
	21 - 23	2/9/2004	ND(14)	ND(14)	ND(14)	140	ND(14)	ND(14)	6.8 J	140
ESSB-K18	1 - 2	12/18/2003	ND(0.78)	ND(0.78)	ND(0.78)	ND(0.78)	6.0	ND(0.78)	ND(0.78)	6.0
	2 - 4	12/18/2003	ND(1.9)	ND(1.9)	ND(1.9)	ND(1.9)	6.1	ND(1.9)	ND(1.9)	6.1
	4 - 6	12/18/2003	ND(40)	ND(40)	ND(40)	ND(40)	490	ND(40)	ND(40)	490
	6 - 8	12/18/2003	ND(8.1)	ND(8.1)	ND(8.1)	ND(8.1)	110	ND(8.1)	ND(8.1)	110
	8 - 10	12/18/2003	ND(3.4)	ND(3.4)	ND(3.4)	ND(3.4)	28	ND(3.4)	ND(3.4)	28
	10 - 12	12/18/2003	ND(6.8)	ND(6.8)	ND(6.8)	ND(6.8)	150	ND(6.8)	ND(6.8)	150
	12 - 14	12/18/2003	ND(7.0)	ND(7.0)	ND(7.0)	ND(7.0)	38	31	ND(7.0)	70
	14 - 16	12/18/2003	ND(7.4)	ND(7.4)	ND(7.4)	ND(7.4)	65	29	ND(7.4)	94

TABLE 3
SUMMARY OF PDI PCB SAMPLE DATA - ELM STREET AREA SUBSURFACE SOILS

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
ESSB-K18E	1 - 3	8/24/2004	ND(5.0) [ND(9.5)]	ND(5.0) [ND(9.5)]	ND(5.0) [ND(9.5)]	ND(5.0) [ND(9.5)]	75 [120]	ND(5.0) [ND(9.5)]	ND(5.0) [ND(9.5)]	75 [120]
	3 - 5	8/24/2004	ND(2.1)	ND(2.1)	ND(2.1)	ND(2.1)	22	6.8	ND(2.1)	29
	5 - 7	8/24/2004	ND(0.20)	ND(0.20)	ND(0.20)	ND(0.20)	1.6	ND(0.20)	ND(0.20)	1.6
	7 - 9	8/24/2004	ND(0.18)	ND(0.18)	ND(0.18)	ND(0.18)	1.5	ND(0.18)	ND(0.18)	1.5
	9 - 11	8/24/2004	ND(0.033)	ND(0.033)	ND(0.033)	0.23	ND(0.033)	ND(0.033)	ND(0.033)	0.23
	11 - 13	8/24/2004	ND(0.033)	ND(0.033)	ND(0.033)	0.10	ND(0.033)	ND(0.033)	ND(0.033)	0.10
	13 - 15	8/24/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)
	15 - 17	8/24/2004	ND(0.21)	ND(0.21)	ND(0.21)	ND(0.21)	2.7	ND(0.21)	ND(0.21)	2.7
	17 - 19	8/24/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)
	19 - 21	8/24/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
	21 - 23	8/24/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.018 J	ND(0.034)	ND(0.034)	0.018 J
	23 - 24	8/24/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.030 J	ND(0.038)	ND(0.038)	0.030 J
ESSB-K18N	1 - 3	8/20/2004	ND(4.2) [ND(12)]	ND(4.2) [ND(12)]	ND(4.2) [ND(12)]	ND(4.2) [ND(12)]	45 [73]	ND(4.2) [ND(12)]	ND(4.2) [ND(12)]	45 [73]
	3 - 5	8/20/2004	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	0.11 J	ND(0.040)	ND(0.040)	0.11 J
	5 - 7	8/20/2004	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	0.070 J	ND(0.042)	0.028 J	0.098
	7 - 9	8/20/2004	ND(0.30)	ND(0.30)	ND(0.30)	ND(0.30)	0.14 J	ND(0.30)	ND(0.30)	0.14 J
	9 - 11	8/20/2004	ND(0.25)	ND(0.25)	ND(0.25)	ND(0.25)	2.6	ND(0.25)	ND(0.25)	2.6
	11 - 13	8/20/2004	ND(0.21)	ND(0.21)	ND(0.21)	ND(0.21)	1.3	ND(0.21)	ND(0.21)	1.3
	13 - 15	8/20/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.087	ND(0.036)	0.097	0.18
	15 - 17	8/20/2004	ND(0.93)	ND(0.93)	ND(0.93)	ND(0.93)	7.7	ND(0.93)	ND(0.93)	7.7
	17 - 19	8/20/2004	ND(2.0)	ND(2.0)	ND(2.0)	ND(2.0)	17	ND(2.0)	ND(2.0)	17
	19 - 21	8/20/2004	ND(5.0)	ND(5.0)	ND(5.0)	56	ND(5.0)	ND(5.0)	ND(5.0)	56
	21 - 23	8/20/2004	ND(0.21)	ND(0.21)	ND(0.21)	2.2	ND(0.21)	ND(0.21)	ND(0.21)	2.2
ESSB-K18W	1 - 3	8/19/2004	ND(2.5) [ND(3.6)]	ND(2.5) [ND(3.6)]	ND(2.5) [ND(3.6)]	ND(2.5) [ND(3.6)]	22 J [38 J]	ND(2.5) [ND(3.6)]	ND(2.5) [ND(3.6)]	22 J [38 J]
	3 - 5	8/19/2004	ND(13)	ND(13)	ND(13)	ND(13)	280	ND(13)	ND(13)	280
	5 - 7	8/19/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.22	ND(0.034)	ND(0.034)	0.22
	7 - 9	8/19/2004	ND(10)	ND(10)	ND(10)	ND(10)	50	ND(10)	ND(10)	50
	9 - 11	8/19/2004	ND(11)	ND(11)	ND(11)	ND(11)	300	ND(11)	ND(11)	300
	11 - 13	8/19/2004	ND(20)	ND(20)	ND(20)	ND(20)	720	ND(20)	ND(20)	720
	13 - 15	8/19/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.098	ND(0.036)	ND(0.036)	0.098
	15 - 17	8/19/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.020 J	ND(0.036)	ND(0.036)	0.020 J
	17 - 19	8/19/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)
	19 - 21	8/19/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.21 JN	ND(0.037)	ND(0.037)	0.21 JN
ESSB-L08	1 - 3	8/13/2004	ND(19)	ND(19)	ND(19)	ND(19)	62 J	49	ND(19)	110
	3 - 5	8/13/2004	ND(0.19)	ND(0.19)	ND(0.19)	ND(0.19)	0.41	0.53	ND(0.19)	0.94
ESSB-L12	1 - 3	2/10/2004	ND(10)	ND(10)	ND(10)	ND(10)	140	ND(10)	ND(10)	140
	3 - 5	2/10/2004	ND(1.1)	ND(1.1)	ND(1.1)	ND(1.1)	40	ND(1.1)	ND(1.1)	40
	5 - 7	2/10/2004	ND(2.4)	ND(2.4)	ND(2.4)	ND(2.4)	44	ND(2.4)	ND(2.4)	44
	7 - 9	2/10/2004	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	0.26	0.15	ND(0.042)	0.42
	9 - 11	2/10/2004	ND(5.9)	ND(5.9)	ND(5.9)	ND(5.9)	52	ND(5.9)	ND(5.9)	52
	11 - 13	2/10/2004	ND(3.9)	ND(3.9)	ND(3.9)	ND(3.9)	58	ND(3.9)	ND(3.9)	58
	13 - 15	2/10/2004	ND(2.8)	ND(2.8)	ND(2.8)	ND(2.8)	22	18	ND(2.8)	40
	15 - 17	2/10/2004	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	0.14	0.094	ND(0.040)	0.23
	17 - 19	2/10/2004	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	0.17	0.062	ND(0.040)	0.23
ESSB-L12N	1 - 3	8/26/2004	ND(18)	ND(18)	ND(18)	ND(18)	240	ND(18)	ND(18)	240
	3 - 5	8/26/2004	ND(10)	ND(10)	ND(10)	ND(10)	140	ND(10)	ND(10)	140
ESSB-L12SE	1 - 3	8/9/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.18	0.075	ND(0.038)	0.26
	3 - 5	8/9/2004	ND(0.23)	ND(0.23)	ND(0.23)	ND(0.23)	0.63	0.18 J	ND(0.23)	0.81

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GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
ESSB-L12SW	1 - 3	8/4/2004	ND(400)	ND(400)	ND(400)	ND(400)	10000	ND(400)	ND(400)	10000
	3 - 5	8/4/2004	ND(1300)	ND(1300)	ND(1300)	ND(1300)	19000	ND(1300)	ND(1300)	19000
	5 - 7	8/25/2004	ND(530)	ND(530)	ND(530)	ND(530)	4100	ND(530)	ND(530)	4100
	7 - 9	8/25/2004	ND(1000)	ND(1000)	ND(1000)	ND(1000)	8800	ND(1000)	ND(1000)	8800
	9 - 11	8/25/2004	ND(430)	ND(430)	ND(430)	ND(430)	2800	ND(430)	ND(430)	2800
	11 - 13	8/25/2004	ND(21)	ND(21)	ND(21)	ND(21)	240	ND(21)	ND(21)	240
	13 - 15	8/25/2004	ND(4.0)	ND(4.0)	ND(4.0)	ND(4.0)	43	ND(4.0)	ND(4.0)	43
	15 - 17	8/25/2004	ND(1.2)	ND(1.2)	ND(1.2)	ND(1.2)	15	ND(1.2)	ND(1.2)	15
ESSB-L13	4 - 5	8/26/2004	ND(13) [ND(10)]	ND(13) [ND(10)]	ND(13) [ND(10)]	ND(13) [ND(10)]	150 [120]	ND(13) [ND(10)]	ND(13) [ND(10)]	150 [120]
	5 - 6	8/26/2004	ND(20)	ND(20)	ND(20)	ND(20)	230	ND(20)	ND(20)	230
	6 - 7	8/26/2004	ND(10)	ND(10)	ND(10)	ND(10)	220	ND(10)	ND(10)	220
ESSB-L14	1 - 3	2/10/2004	ND(230)	ND(230)	ND(230)	ND(230)	7200	ND(230)	ND(230)	7200
	3 - 5	2/10/2004	ND(0.96)	ND(0.96)	ND(0.96)	ND(0.96)	23	ND(0.96)	ND(0.96)	23
	5 - 7	2/10/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.44 J	ND(0.034)	ND(0.034)	0.44 J
	7 - 9	2/10/2004	ND(0.44)	ND(0.44)	ND(0.44)	ND(0.44)	6.7	3.4	ND(0.44)	10
	9 - 11	2/10/2004	ND(0.47)	ND(0.47)	ND(0.47)	ND(0.47)	4.5	2.2	ND(0.47)	6.7
ESSB-L14E	1 - 3	8/4/2004	ND(21)	ND(21)	ND(21)	ND(21)	420	ND(21)	ND(21)	420
	3 - 5	8/4/2004	ND(11)	ND(11)	ND(11)	ND(11)	200	ND(11)	ND(11)	200
	5 - 7	8/25/2004	ND(11)	ND(11)	ND(11)	ND(11)	ND(51)	ND(11)	ND(11)	ND(51)
	7 - 9	8/25/2004	ND(8.9)	ND(8.9)	ND(8.9)	ND(8.9)	200	ND(8.9)	ND(8.9)	200
	9 - 11	8/25/2004	ND(240)	ND(240)	ND(240)	ND(240)	3900	ND(240)	ND(240)	3900
ESSB-L14W	1 - 3	8/4/2004	ND(94) [ND(240)]	ND(94) [ND(240)]	ND(94) [ND(240)]	3200 [3300]	ND(94) [ND(240)]	ND(94) [ND(240)]	ND(94) [ND(240)]	3200 [3300]
	3 - 5	8/4/2004	ND(0.20)	ND(0.20)	ND(0.20)	2.3	ND(0.20)	ND(0.20)	ND(0.20)	2.3
ESSB-L15	1 - 2	4/28/2004	ND(130)	ND(130)	ND(130)	ND(130)	1100	ND(130)	ND(130)	1100
	2 - 3	4/28/2004	ND(1.1)	ND(1.1)	ND(1.1)	ND(1.1)	10 J	ND(1.1)	ND(1.1)	10 J
ESSB-L15E	1 - 2	8/4/2004	ND(26)	ND(26)	ND(26)	ND(26)	520	ND(26)	ND(26)	520
	3 - 5	8/25/2004	ND(25) [ND(22)]	ND(25) [ND(22)]	ND(25) [ND(22)]	ND(25) [ND(22)]	470 [610]	ND(25) [ND(22)]	ND(25) [ND(22)]	470 [610]
	5 - 7	8/25/2004	ND(3.9)	ND(3.9)	ND(3.9)	ND(3.9)	32	ND(3.9)	ND(3.9)	32
	19 - 21	10/20/05	ND(1,100)	ND(1,100)	6,400	ND(1,100)	ND(1,100)	640 J	ND(1,100)	7,100
	21 - 23	10/20/05	ND(2,200)	ND(2,200)	9,500	ND(2,200)	ND(2,200)	1,700 J	ND(2,200)	11,000
ESSB-L15S	1 - 2	8/4/2004	ND(4.2)	ND(4.2)	ND(4.2)	ND(4.2)	40	ND(4.2)	ND(4.2)	40
ESSB-L16	7 - 9	8/24/2004	ND(0.26) [ND(0.24)]	ND(0.26) [ND(0.24)]	ND(0.26) [ND(0.24)]	ND(0.26) [ND(0.24)]	3.7 [2.4]	1.9 [1.6]	ND(0.26) [ND(0.24)]	5.6 [4.0]
	9 - 11	8/24/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.17	0.15 J	ND(0.036)	0.32 J
	11 - 13	8/24/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.16	ND(0.036)	ND(0.036)	0.16
	19 - 21	8/24/2004	ND(0.20)	ND(0.20)	ND(0.20)	ND(0.20)	3.6	ND(0.20)	ND(0.20)	3.6
	21 - 23	8/24/2004	ND(47)	ND(47)	ND(47)	1200	ND(47)	ND(47)	ND(47)	1200
ESSB-L17	7 - 9	8/24/2004	ND(38)	ND(38)	ND(38)	ND(38)	890	ND(38)	ND(38)	890
	9 - 11	8/24/2004	ND(1.3)	ND(1.3)	ND(1.3)	ND(1.3)	19	ND(1.3)	ND(1.3)	19
	11 - 13	8/24/2004	ND(0.88)	ND(0.88)	ND(0.88)	8.1	ND(0.88)	ND(0.88)	ND(0.88)	8.1
	19 - 21	8/24/2004	ND(0.23)	ND(0.23)	ND(0.23)	ND(0.23)	1.1	ND(0.23)	ND(0.23)	1.1
	21 - 23	8/24/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.31	ND(0.036)	ND(0.036)	0.31
ESSB-L18	1 - 3	8/19/2004	ND(0.70)	ND(0.70)	ND(0.70)	ND(0.70)	3.5	ND(0.70)	ND(0.70)	3.5
	3 - 5	8/19/2004	ND(0.19)	ND(0.19)	ND(0.19)	ND(0.19)	1.8	ND(0.19)	ND(0.19)	1.8
	5 - 7	8/19/2004	ND(0.19)	ND(0.19)	ND(0.19)	ND(0.19)	4.8	ND(0.19)	ND(0.19)	4.8
	7 - 9	8/19/2004	ND(0.21)	ND(0.21)	ND(0.21)	ND(0.21)	0.52	ND(0.21)	ND(0.21)	0.52
	9 - 11	8/19/2004	ND(1.7)	ND(1.7)	ND(1.7)	ND(1.7)	6.8	3.6	ND(1.7)	10
	11 - 13	8/19/2004	ND(0.20)	ND(0.20)	ND(0.20)	ND(0.20)	3.6	ND(0.20)	ND(0.20)	3.6
	13 - 15	8/19/2004	ND(0.70)	ND(0.70)	ND(0.70)	ND(0.70)	2.1	ND(0.70)	ND(0.70)	2.1
	15 - 17	8/19/2004	ND(0.17)	ND(0.17)	ND(0.17)	ND(0.17)	1.2 J	ND(0.17)	ND(0.17)	1.2 J
	17 - 19	8/19/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.16	0.10 J	ND(0.035)	0.26 J
	19 - 21	8/19/2004	ND(0.074)	ND(0.074)	ND(0.074)	ND(0.074)	0.45	ND(0.074)	0.31	0.76

TABLE 3
SUMMARY OF PDI PCB SAMPLE DATA - ELM STREET AREA SUBSURFACE SOILS

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
ESSB-M08	1 - 3	2/3/2004	ND(0.46)	ND(0.46)	ND(0.46)	ND(0.46)	7.2 EB	ND(0.46)	ND(0.46)	7.2 EB
	3 - 5	2/3/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.079 EB	ND(0.037)	ND(0.037)	0.079 EB
	5 - 7	2/3/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.080 EB	ND(0.036)	ND(0.036)	0.080 EB
	7 - 9	2/3/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.035 JEB	ND(0.036)	ND(0.036)	0.035 JEB
	9 - 11	2/3/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
	11 - 13	2/3/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
	13 - 15	2/3/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)
	15 - 16	2/3/2004	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)
	20 - 22	2/3/2004	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	0.024 J	ND(0.039)	ND(0.039)	0.024 J
ESSB-M10	1 - 3	2/5/2004	ND(0.23)	ND(0.23)	ND(0.23)	ND(0.23)	2.2	0.73	ND(0.23)	2.9
	3 - 5	2/5/2004	ND(0.22)	ND(0.22)	ND(0.22)	ND(0.22)	1.5	0.99	ND(0.22)	2.5
ESSB-M10E	1 - 3	8/25/2004	ND(37) [ND(21)]	ND(37) [ND(21)]	ND(37) [ND(21)]	ND(37) [ND(21)]	740 [450]	ND(37) [ND(21)]	ND(37) [ND(21)]	740 [450]
	3 - 5	8/25/2004	ND(11)	ND(11)	ND(11)	ND(11)	ND(46)	ND(11)	ND(11)	ND(46)
	5 - 7	8/25/2004	ND(0.22)	ND(0.22)	ND(0.22)	ND(0.22)	5.1	1.6	ND(0.22)	6.6
	7 - 9	8/25/2004	ND(0.97)	ND(0.97)	ND(0.97)	ND(0.97)	11	5.4	ND(0.97)	16
	9 - 11	8/25/2004	ND(4.9)	ND(4.9)	ND(4.9)	ND(4.9)	23	13	ND(4.9)	36
	11 - 13	8/25/2004	ND(0.28)	ND(0.28)	ND(0.28)	ND(0.28)	0.83	0.51	ND(0.28)	1.3
ESSB-M12	1 - 3	2/5/2004	ND(7.4) [ND(9.5)]	ND(7.4) [ND(9.5)]	ND(7.4) [ND(9.5)]	ND(7.4) [ND(9.5)]	52 [77]	26 [35]	ND(7.4) [ND(9.5)]	78 [110]
	3 - 5	2/5/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.36	0.14	ND(0.038)	0.50
	5 - 7	2/5/2004	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	0.23	0.077 J	ND(0.042)	0.31 J
	7 - 9	2/5/2004	ND(0.044)	ND(0.044)	ND(0.044)	ND(0.044)	0.29	0.16	ND(0.044)	0.45
	9 - 11	2/5/2004	ND(0.045)	ND(0.045)	ND(0.045)	ND(0.045)	0.27	0.18	ND(0.045)	0.45
	11 - 13	2/5/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.034 J	ND(0.036)	ND(0.036)	0.034 J
	13 - 15	2/5/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)
	15 - 17	2/5/2004	ND(0.19)	ND(0.19)	ND(0.19)	ND(0.19)	1.8	ND(0.19)	ND(0.19)	1.8
	17 - 19	2/5/2004	ND(0.28)	ND(0.28)	ND(0.28)	ND(0.28)	ND(0.28)	ND(0.28)	ND(0.28)	ND(0.28)
	19 - 21	2/5/2004	ND(0.038)	ND(0.038)	ND(0.038)	0.38	ND(0.038)	ND(0.038)	ND(0.038)	0.38
	21 - 23	2/5/2004	ND(0.24)	ND(0.24)	ND(0.24)	2.7	ND(0.24)	ND(0.24)	ND(0.24)	2.7
ESSB-M14	1 - 3	12/22/2003	ND(200)	ND(200)	ND(200)	ND(200)	84 J	ND(200)	ND(200)	84 J
	3 - 5	12/22/2003	ND(0.73)	ND(0.73)	ND(0.73)	ND(0.73)	5.7	3.7	ND(0.73)	9.4
	5 - 7	12/22/2003	ND(39)	ND(39)	ND(39)	ND(39)	80	ND(39)	ND(39)	80
	7 - 9	12/22/2003	ND(3.8)	ND(3.8)	ND(3.8)	ND(3.8)	21	ND(3.8)	ND(3.8)	21
	9 - 11	12/22/2003	ND(0.074) [ND(3.8)]	ND(0.074) [ND(3.8)]	ND(0.074) [ND(3.8)]	ND(0.074) [ND(3.8)]	0.74 J [19 J]	ND(0.074) [ND(3.8)]	ND(0.074) [ND(3.8)]	0.74 J [19 J]
	11 - 13	12/22/2003	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.39	ND(0.038)	ND(0.038)	0.39
	13 - 15	12/22/2003	ND(0.73)	ND(0.73)	ND(0.73)	ND(0.73)	2.8	ND(0.73)	ND(0.73)	2.8
	16 - 18	12/22/2003	ND(0.046)	ND(0.046)	ND(0.046)	ND(0.046)	0.14	0.094	ND(0.046)	0.24
	18 - 20	12/22/2003	ND(0.043)	ND(0.043)	ND(0.043)	ND(0.043)	0.14	0.12	ND(0.043)	0.25
	20 - 22	12/22/2003	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	0.025 J	0.027 J	ND(0.041)	0.051
ESSB-M16	1 - 3	2/4/2004	ND(2.6)	ND(2.6)	ND(2.6)	ND(2.6)	31	ND(2.6)	ND(2.6)	31
	3 - 5	2/4/2004	ND(1.7)	ND(1.7)	ND(1.7)	ND(1.7)	11	ND(1.7)	ND(1.7)	11
	5 - 7	2/4/2004	ND(5.5)	ND(5.5)	ND(5.5)	ND(5.5)	67	19	ND(5.5)	86
	7 - 9	2/4/2004	ND(4.3)	ND(4.3)	ND(4.3)	ND(4.3)	42	ND(4.3)	ND(4.3)	42
	9 - 11	2/4/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.20	0.049	ND(0.035)	0.25
	11 - 13	2/4/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.32	0.15	ND(0.036)	0.47
	13 - 15	2/4/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.087	0.028 J	ND(0.036)	0.12
	15 - 17	2/4/2004	ND(0.044)	ND(0.044)	ND(0.044)	ND(0.044)	0.67	0.70 J	ND(0.044)	1.4 J
	17 - 19	2/4/2004	ND(0.043)	ND(0.043)	ND(0.043)	ND(0.043)	0.23	0.53 JN	ND(0.043)	0.75 JN
ESSB-M17	1 - 3	8/12/2004	ND(0.20)	ND(0.20)	ND(0.20)	ND(0.20)	3.2 J	2.3	ND(0.20)	5.5 J
	3 - 5	8/12/2004	ND(1100)	ND(1100)	ND(1100)	11000	ND(1100)	ND(1100)	ND(1100)	11000
	5 - 7	8/12/2004	ND(19)	ND(19)	ND(19)	180	ND(19)	ND(19)	ND(19)	180

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GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
ESSB-M18	1 - 3	2/4/2004	ND(2.3)	ND(2.3)	ND(2.3)	ND(2.3)	60 JN	36	ND(2.3)	96 JN
	3 - 5	2/4/2004	ND(92)	ND(92)	ND(92)	ND(92)	580	ND(92)	ND(92)	580
	5 - 7	2/4/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.29	0.11	ND(0.037)	0.40
	7 - 9	2/4/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.12	ND(0.037)	ND(0.037)	0.12
	9 - 11	2/4/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.024 J	ND(0.036)	ND(0.036)	0.024 J
	11 - 13	2/4/2004	ND(0.22)	ND(0.22)	ND(0.22)	ND(0.22)	1.8	1.0	ND(0.22)	2.8
	13 - 15	2/4/2004	ND(0.19)	ND(0.19)	ND(0.19)	ND(0.19)	1.1 JN	0.57	ND(0.19)	1.7 JN
	15 - 17	2/4/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.014 J	ND(0.034)	ND(0.034)	0.014 J
	17 - 19	2/4/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.0096 J	ND(0.036)	ND(0.036)	0.0096 J
	19 - 21	2/4/2004	ND(0.047)	ND(0.047)	ND(0.047)	ND(0.047)	ND(0.047)	ND(0.047)	ND(0.047)	ND(0.047)
	21 - 23	2/4/2004	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)
ESSB-M18N	1 - 3	8/12/2004	ND(0.23) [ND(0.18)]	ND(0.23) [ND(0.18)]	ND(0.23) [ND(0.18)]	ND(0.23) [ND(0.18)]	2.1 [1.9]	ND(0.23) [0.60]	ND(0.23) [ND(0.18)]	2.1 [2.5]
	3 - 5	8/12/2004	ND(21)	ND(21)	ND(21)	ND(21)	170	73	ND(21)	240
	5 - 7	8/12/2004	ND(12)	ND(12)	ND(12)	ND(12)	110	30	ND(12)	140
ESSB-M18S	1 - 3	8/12/2004	ND(0.20)	ND(0.20)	ND(0.20)	ND(0.20)	1.8	1.0	ND(0.20)	2.8
	3 - 5	8/12/2004	ND(1.3)	ND(1.3)	ND(1.3)	ND(1.3)	11	4.7	ND(1.3)	16
	5 - 7	8/12/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	0.14	0.10	ND(0.033)	0.24
ESSB-M19	1 - 3	8/17/2004	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	1.0	0.96	ND(0.24)	2.0
	3 - 5	8/17/2004	ND(0.20)	ND(0.20)	ND(0.20)	ND(0.20)	1.9 JN	3.2	ND(0.20)	5.2 JN
	5 - 7	8/17/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	0.050	0.034	ND(0.033)	0.084
ESSB-N14	1 - 3	8/24/2004	ND(200)	ND(200)	ND(200)	6900	ND(200)	ND(200)	ND(200)	6900
	3 - 5	8/24/2004	ND(1000)	ND(1000)	ND(1000)	7800	ND(1000)	ND(1000)	ND(1000)	7800
	5 - 7	8/24/2004	ND(48)	ND(48)	ND(48)	810	ND(48)	ND(48)	ND(48)	810
	7 - 9	8/24/2004	ND(21)	ND(21)	ND(21)	360	ND(21)	ND(21)	ND(21)	360
	9 - 11	8/24/2004	ND(0.25)	ND(0.25)	ND(0.25)	1.5	ND(0.25)	ND(0.25)	ND(0.25)	1.5
	11 - 13	8/24/2004	ND(0.20)	ND(0.20)	ND(0.20)	4.0	ND(0.20)	ND(0.20)	ND(0.20)	4.0
	13 - 15	8/24/2004	ND(0.22)	ND(0.22)	ND(0.22)	0.91	ND(0.22)	ND(0.22)	ND(0.22)	0.91
	15 - 17	8/24/2004	ND(0.23)	ND(0.23)	ND(0.23)	1.4	ND(0.23)	ND(0.23)	ND(0.23)	1.4
	17 - 19	8/24/2004	ND(0.55)	ND(0.55)	ND(0.55)	ND(0.55)	6.0	ND(0.55)	ND(0.55)	6.0
	19 - 21	8/24/2004	ND(0.048)	ND(0.048)	ND(0.048)	ND(0.048)	ND(0.13)	ND(0.048)	ND(0.048)	ND(0.13)
	21 - 23	8/24/2004	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.061)	ND(0.039)	ND(0.039)	ND(0.061)
ESSB-N16	1 - 3	8/17/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.076	ND(0.034)	ND(0.034)	0.076
	3 - 5	8/17/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.18	ND(0.034)	ND(0.034)	0.18
	5 - 7	8/17/2004	ND(21)	ND(21)	ND(21)	ND(21)	900	ND(21)	ND(21)	900
	7 - 9	8/17/2004	ND(120)	ND(120)	ND(120)	ND(120)	1700	ND(120)	ND(120)	1700
	9 - 11	8/17/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.15	ND(0.035)	ND(0.035)	0.15
ESSB-N18	1 - 3	8/17/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.16	ND(0.034)	ND(0.034)	0.16
	3 - 5	8/17/2004	ND(10)	ND(10)	ND(10)	ND(10)	55	67	ND(10)	120
	5 - 7	8/17/2004	ND(1.0) J	ND(1.0) J	ND(1.0) J	ND(1.0) J	8.0 J	9.6 J	ND(1.0) J	18 J
	7 - 8	8/17/2004	ND(0.38)	ND(0.38)	ND(0.38)	ND(0.38)	4.9	3.4	ND(0.38)	8.3
	8 - 10	8/17/2004	ND(0.23)	ND(0.23)	ND(0.23)	ND(0.23)	1.7	1.0	ND(0.23)	2.7
ESSB-O10	1 - 3	1/29/2004	ND(0.58)	ND(0.58)	ND(0.58)	ND(0.58)	14	9.9	ND(0.58)	23
	3 - 5	1/29/2004	ND(0.20)	ND(0.20)	ND(0.20)	ND(0.20)	4.2 J	3.6 J	ND(0.20)	7.8 J
	5 - 7	1/29/2004	ND(0.20) [ND(2.0)]	ND(0.20) [ND(2.0)]	ND(0.20) [ND(2.0)]	ND(0.20) [ND(2.0)]	8.6 J [20 J]	5.8 J [14 J]	ND(0.20) [ND(2.0)]	14 J [34 J]
	7 - 9	1/29/2004	ND(2.0)	ND(2.0)	ND(2.0)	ND(2.0)	30	16	ND(2.0)	46
	9 - 11	1/29/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.022 J	ND(0.036)	ND(0.036)	0.022 J
	11 - 13	1/29/2004	ND(0.046)	ND(0.046)	ND(0.046)	ND(0.046)	0.13	ND(0.046)	ND(0.046)	0.13
	13 - 15	1/29/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.044	ND(0.037)	ND(0.037)	0.044
	15 - 17	1/29/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.030 J	ND(0.037)	ND(0.037)	0.030 J
	17 - 19	1/29/2004	ND(0.058)	ND(0.058)	ND(0.058)	ND(0.058)	ND(0.058)	ND(0.058)	ND(0.058)	ND(0.058)
	19 - 21	1/29/2004	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	0.021 J	0.030 J	ND(0.042)	0.051
	21 - 23	1/29/2004	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)
ESSB-O12	1 - 3	1/29/2004	ND(4.6)	ND(4.6)	ND(4.6)	ND(4.6)	92	ND(4.6)	ND(4.6)	92
	3 - 5	1/29/2004	ND(1.2)	ND(1.2)	ND(1.2)	ND(1.2)	8.7	5.7	ND(1.2)	14
	5 - 7	1/29/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.032 J	0.020 J	ND(0.034)	0.052
	7 - 9	1/29/2004	ND(0.40)	ND(0.40)	ND(0.40)	ND(0.40)	6.6	4.2	ND(0.40)	11
	9 - 11	1/29/2004	ND(0.22) [ND(0.036)]	ND(0.22) [ND(0.036)]	ND(0.22) [ND(0.036)]	ND(0.22) [ND(0.036)]	1.3 J [0.14 J]	0.90 J [0.098 J]	ND(0.22) [ND(0.036)]	2.2 J [0.23 J]
	11 - 13	1/29/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.11)	0.090	ND(0.035)	0.090
	13 - 15	1/29/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)
	15 - 17	1/29/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.21	0.12	ND(0.038)	0.33
	17 - 19	1/29/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.080)	ND(0.038)	0.0092 J	0.0092 J

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Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
	19 - 21	1/29/2004	ND(0.049)	ND(0.049)	ND(0.049)	ND(0.049)	0.81	0.38	ND(0.049)	1.2
ESSB-O14	1 - 3	2/2/2004	ND(2100) [ND(880)]	ND(2100) [ND(880)]	ND(2100) [ND(880)]	17000 [12000]	ND(2100) [ND(880)]	ND(2100) [ND(880)]	ND(2100) [ND(880)]	17000 [12000]
	3 - 5	2/2/2004	ND(980)	ND(980)	ND(980)	16000	ND(980)	ND(980)	ND(980)	16000
	5 - 7	2/2/2004	ND(5600)	ND(5600)	ND(5600)	40000	ND(5600)	ND(5600)	ND(5600)	40000
	7 - 9	2/2/2004	ND(56)	ND(56)	ND(56)	240	ND(56)	ND(56)	ND(56)	240
	9 - 11	2/2/2004	ND(46)	ND(46)	ND(46)	490	ND(46)	ND(46)	ND(46)	490
	11 - 13	2/2/2004	ND(2.1)	ND(2.1)	ND(2.1)	19	ND(2.1)	ND(2.1)	ND(2.1)	19
	15 - 17	2/2/2004	ND(13)	ND(13)	ND(13)	150	ND(13)	ND(13)	ND(13)	150
	17 - 19	2/2/2004	ND(2.2)	ND(2.2)	ND(2.2)	19	ND(2.2)	ND(2.2)	ND(2.2)	19
	19 - 21	2/2/2004	ND(0.27)	ND(0.27)	ND(0.27)	1.2	ND(0.27)	ND(0.27)	ND(0.27)	1.2
	21 - 23	2/2/2004	ND(0.24)	ND(0.24)	ND(0.24)	1.2	ND(0.24)	ND(0.24)	ND(0.24)	1.2
ESSB-O14E	1 - 3	8/11/2004	ND(2400)	ND(2400)	ND(2400)	21000	ND(2400)	ND(2400)	ND(2400)	21000
	3 - 5	8/11/2004	ND(2200)	ND(2200)	ND(2200)	8500	ND(2200)	ND(2200)	ND(2200)	8500
	5 - 7	8/11/2004	ND(2200) [ND(2200)]	ND(2200) [ND(2200)]	ND(2200) [ND(2200)]	15000 [17000]	ND(2200) [ND(2200)]	ND(2200) [ND(2200)]	ND(2200) [ND(2200)]	15000 [17000]
	7 - 9	8/11/2004	ND(12)	ND(12)	ND(12)	34	ND(12)	ND(12)	ND(12)	34
	9 - 11	8/11/2004	ND(0.46)	ND(0.46)	ND(0.46)	4.4	ND(0.46)	ND(0.46)	ND(0.46)	4.4
	11 - 13	8/11/2004	ND(0.26)	ND(0.26)	ND(0.26)	2.4	ND(0.26)	ND(0.26)	ND(0.26)	2.4
	13 - 15	8/11/2004	ND(0.27)	ND(0.27)	ND(0.27)	2.3	ND(0.27)	ND(0.27)	ND(0.27)	2.3
	15 - 17	8/11/2004	ND(0.20)	ND(0.20)	ND(0.20)	ND(0.20)	0.51	ND(0.20)	ND(0.20)	0.51
	17 - 19	8/11/2004	ND(0.042)	ND(0.042)	ND(0.042)	0.23	ND(0.042)	ND(0.042)	ND(0.042)	0.23
	19 - 21	8/11/2004	ND(0.051)	ND(0.051)	ND(0.051)	0.10	ND(0.051)	ND(0.051)	ND(0.051)	0.10
	21 - 23	8/11/2004	ND(0.040)	ND(0.040)	ND(0.040)	0.28	ND(0.040)	ND(0.040)	ND(0.040)	0.28
ESSB-O14N	1 - 3	8/12/2004	ND(1900)	ND(1900)	ND(1900)	24000	ND(1900)	ND(1900)	ND(1900)	24000
	3 - 5	8/12/2004	ND(420)	ND(420)	ND(420)	14000	ND(420)	ND(420)	ND(420)	14000
	5 - 7	8/12/2004	ND(3.7)	ND(3.7)	ND(3.7)	25	ND(3.7)	ND(3.7)	ND(3.7)	25
	7 - 9	8/12/2004	ND(24)	ND(24)	ND(24)	220	ND(24)	ND(24)	ND(24)	220
	9 - 11	8/12/2004	ND(0.22)	ND(0.22)	ND(0.22)	2.7	ND(0.22)	ND(0.22)	ND(0.22)	2.7
	11 - 11.4	8/12/2004	ND(0.27)	ND(0.27)	ND(0.27)	1.1	ND(0.27)	ND(0.27)	ND(0.27)	1.1
	15 - 15.5	8/12/2004	ND(0.44)	ND(0.44)	ND(0.44)	5.3	ND(0.44)	ND(0.44)	ND(0.44)	5.3
ESSB-O14W	1 - 3	8/11/2004	ND(48)	ND(48)	ND(48)	ND(48)	640	ND(48)	ND(48)	640
	3 - 5	8/11/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.14	0.064	ND(0.035)	0.20
	5 - 7	8/11/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.037	0.015 J	ND(0.035)	0.052
	7 - 9	8/11/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.024 J	ND(0.034)	ND(0.034)	0.032 J
	9 - 11	8/11/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.0096 J	0.012 J	ND(0.034)	0.022 J
	11 - 13	8/11/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.11	0.067	ND(0.036)	0.17
	13 - 15	8/11/2004	ND(1.4)	ND(1.4)	ND(1.4)	ND(1.4)	0.65 J	ND(1.4)	ND(1.4)	0.65 J
	15 - 17	8/11/2004	ND(0.43)	ND(0.43)	ND(0.43)	ND(0.43)	ND(0.43)	ND(0.43)	ND(0.43)	ND(0.43)
	17 - 19	8/11/2004	ND(0.046)	ND(0.046)	ND(0.046)	ND(0.046)	0.25	ND(0.046)	ND(0.046)	0.25
	19 - 21	8/11/2004	ND(0.051)	ND(0.051)	ND(0.051)	ND(0.051)	0.040 J	ND(0.051)	ND(0.051)	0.040 J
	21 - 23	8/11/2004	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	0.017 J	ND(0.039)	ND(0.039)	0.020 J

TABLE 3
SUMMARY OF PDI PCB SAMPLE DATA - ELM STREET AREA SUBSURFACE SOILS

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
ESSB-O16	1 - 3	2/4/2004	ND(200)	ND(200)	ND(200)	4600	ND(200)	ND(200)	ND(200)	4600
	3 - 5	2/4/2004	ND(100)	ND(100)	ND(100)	540	ND(100)	ND(100)	ND(100)	540
	5 - 7	2/4/2004	ND(0.23)	ND(0.23)	ND(0.23)	1.3	ND(0.23)	ND(0.23)	ND(0.23)	1.3
	7 - 9	2/4/2004	ND(23)	ND(23)	ND(23)	190	ND(23)	ND(23)	ND(23)	190
	9 - 11	2/4/2004	ND(0.21)	ND(0.21)	ND(0.21)	0.87	ND(0.21)	ND(0.21)	ND(0.21)	0.87
	11 - 13	2/4/2004	ND(0.036)	ND(0.036)	ND(0.036)	0.045	ND(0.036)	ND(0.036)	ND(0.036)	0.045
	13 - 15	2/4/2004	ND(0.034)	ND(0.034)	ND(0.034)	0.020 J	ND(0.034)	ND(0.034)	ND(0.034)	0.020 J
	15 - 17	2/4/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.036 J	ND(0.037)	ND(0.037)	0.036 J
	17 - 19	2/4/2004	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	0.049	ND(0.040)	ND(0.040)	0.049
	19 - 21	2/4/2004	ND(0.044)	ND(0.044)	ND(0.044)	ND(0.044)	0.21	0.19 JN	ND(0.044)	0.40 JN
	21 - 23	2/4/2004	ND(0.046)	ND(0.046)	ND(0.046)	ND(0.046)	ND(0.046)	ND(0.046)	ND(0.046)	ND(0.046)
ESSB-O17	1 - 3	8/17/2004	ND(1.1)	ND(1.1)	ND(1.1)	ND(1.1)	8.6	9.9 EB	ND(1.1)	18 EB
	3 - 5	8/17/2004	ND(2.4)	ND(2.4)	ND(2.4)	ND(2.4)	16	21 EB	ND(2.4)	37 EB
	5 - 7	8/17/2004	ND(10)	ND(10)	ND(10)	ND(10)	150	ND(10)	ND(10)	150
	7 - 9	8/17/2004	ND(0.20)	ND(0.20)	ND(0.20)	ND(0.20)	1.6	0.79 JEB	ND(0.20)	2.4 JEB
	9 - 11	8/17/2004	ND(0.19)	ND(0.19)	ND(0.19)	ND(0.19)	1.9	0.75 EB	ND(0.19)	2.7 EB
ESSB-O18	1 - 2	1/28/2004	ND(53)	ND(53)	ND(53)	ND(53)	810	1000	ND(53)	1800
	2 - 4	1/28/2004	ND(54)	ND(54)	ND(54)	ND(54)	1300	1300	ND(54)	2700
	4 - 6	1/28/2004	ND(40)	ND(40)	ND(40)	ND(40)	1000	1100	ND(40)	2100
	6 - 8	1/28/2004	ND(40)	ND(40)	ND(40)	ND(40)	220	230	ND(40)	450
	8 - 10	1/28/2004	ND(0.23)	ND(0.23)	ND(0.23)	ND(0.23)	1.3	1.2	ND(0.23)	2.5
	10 - 12	1/28/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.54	0.40	ND(0.035)	0.93
	12 - 14	1/28/2004	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	0.018 J	ND(0.039)	0.048 J
	14 - 16	1/28/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.043	0.043	ND(0.035)	0.086
	16 - 18	1/28/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)
	18 - 20	1/28/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	0.030 J	ND(0.033)	0.030 J
	20 - 22	1/28/2004	ND(0.039) [ND(0.039)]	ND(0.039) [ND(0.039)]	ND(0.039) [ND(0.039)]	ND(0.039) [ND(0.039)]	ND(0.039) [ND(0.039)]	ND(0.039) [ND(0.039)]	ND(0.039) [ND(0.039)]	ND(0.039) [ND(0.039)]
ESSB-O18E	1 - 3	8/17/2004	ND(0.24) [ND(0.19)]	ND(0.24) [ND(0.19)]	ND(0.24) [ND(0.19)]	ND(0.24) [ND(0.19)]	0.76 JN [0.70 JN]	0.82 [0.76]	ND(0.24) [ND(0.19)]	1.6 JN [1.5 JN]
	3 - 5	8/17/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	0.021 J	ND(0.033)	ND(0.033)	0.021 J
	5 - 7	8/17/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)
	7 - 8	8/17/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.071	0.042 J	ND(0.035)	0.11 J
	8 - 10	8/17/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	0.094	0.030 J	ND(0.033)	0.12
ESSB-P17	1 - 2	4/29/2004	ND(0.99)	ND(0.99)	ND(0.99)	ND(0.99)	9.1	ND(0.99)	ND(0.99)	9.1
ESSB-P18E	1 - 3	8/17/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	0.048 J	0.032 J	ND(0.033)	0.080 J
	3 - 5	8/17/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)
	5 - 7	8/17/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
	7 - 8	8/17/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)
	8 - 10	8/17/2004	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)
ESSB-Q10	1 - 3	1/27/2004	ND(0.25)	ND(0.25)	ND(0.25)	ND(0.25)	1.0	0.52	ND(0.25)	1.5
	3 - 5	1/27/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.16	0.064	ND(0.034)	0.22
	5 - 7	1/27/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	0.14	0.056	ND(0.033)	0.19
	7 - 9	1/27/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)
	9 - 11	1/27/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
	11 - 13	1/27/2004	ND(0.051)	ND(0.051)	ND(0.051)	ND(0.051)	ND(0.051)	ND(0.051)	ND(0.051)	ND(0.051)
	13 - 15	1/27/2004	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)
	15 - 17	1/27/2004	ND(0.046)	ND(0.046)	ND(0.046)	ND(0.046)	0.40	0.33	ND(0.046)	0.72
	17 - 19	1/27/2004	ND(0.34)	ND(0.34)	ND(0.34)	ND(0.34)	1.4 J	1.1	ND(0.34)	2.5 J
	19 - 21	1/27/2004	ND(0.19)	ND(0.19)	ND(0.19)	ND(0.19)	0.56	0.42	ND(0.19)	0.98
ESSB-Q11	1 - 3	8/6/2004	ND(0.18)	ND(0.18)	ND(0.18)	ND(0.18)	0.25 JN	ND(0.18)	ND(0.18)	0.25 JN
	3 - 4	8/6/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.011 J	ND(0.036)	ND(0.036)	0.011 J
	4 - 6	8/6/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	0.025 J	0.022 J	ND(0.033)	0.047

TABLE 3
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FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
ESSB-Q12	1 - 2	1/29/2004	ND(12)	ND(12)	ND(12)	ND(12)	150	92	ND(12)	240
	2 - 4	1/29/2004	ND(11)	ND(11)	ND(11)	ND(11)	130	ND(11)	ND(11)	130
	4 - 6	1/29/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.043	0.033 J	ND(0.037)	0.076
	6 - 8	1/29/2004	ND(0.23)	ND(0.23)	ND(0.23)	ND(0.23)	1.8	0.88	ND(0.23)	2.6
	8 - 10	1/29/2004	ND(0.044)	ND(0.044)	ND(0.044)	ND(0.044)	0.13	0.055	ND(0.044)	0.19
	10 - 12	1/29/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.094	ND(0.034)	ND(0.034)	0.094
	12 - 14	1/29/2004	ND(0.043)	ND(0.043)	ND(0.043)	ND(0.043)	0.012 J	ND(0.043)	ND(0.043)	0.012 J
	14 - 16	1/29/2004	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	0.17	0.18	ND(0.041)	0.34
	16 - 18	1/29/2004	ND(0.043)	ND(0.043)	ND(0.043)	ND(0.043)	0.029 J	0.043	ND(0.043)	0.072
	18 - 20	1/29/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.14	0.065	ND(0.038)	0.20
	20 - 22	1/29/2004	ND(0.044)	ND(0.044)	ND(0.044)	ND(0.044)	0.020 J	ND(0.044)	ND(0.044)	0.020 J
ESSB-Q12E	1 - 3	8/6/2004	ND(25)	ND(25)	ND(25)	ND(25)	120	80	ND(25)	200
	3 - 4	8/6/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.17	0.11	ND(0.035)	0.27
	4 - 6	8/6/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.036	0.022 J	ND(0.036)	0.058
ESSB-Q12N	1 - 3	8/6/2004	ND(17)	ND(17)	ND(17)	ND(17)	200	95	ND(17)	300
	3 - 4	8/6/2004	ND(0.20)	ND(0.20)	ND(0.20)	ND(0.20)	1.5	0.87	ND(0.20)	2.4
	4 - 6	8/6/2004	ND(0.19) [ND(0.19)]	ND(0.19) [ND(0.19)]	ND(0.19) [ND(0.19)]	ND(0.19) [ND(0.19)]	3.3 [3.3]	1.9 [2.0]	ND(0.19) [ND(0.19)]	5.2 [5.3]
ESSB-Q14	1 - 3	1/22/2004	ND(270)	ND(270)	ND(270)	ND(270)	5800	3300	ND(270)	9100
	3 - 5	1/22/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.12	0.042	ND(0.036)	0.16
	5 - 7	1/22/2004	ND(0.036) [ND(0.036)]	ND(0.036) [ND(0.036)]	ND(0.036) [ND(0.036)]	ND(0.036) [ND(0.036)]	0.064 [0.053]	0.037 [0.026 J]	ND(0.036) [ND(0.036)]	0.10 [0.079]
	11 - 13	1/22/2004	ND(2.5)	ND(2.5)	ND(2.5)	ND(2.5)	26	18	ND(2.5)	44
	13 - 15	1/22/2004	ND(0.27)	ND(0.27)	ND(0.27)	ND(0.27)	3.0	2.2	ND(0.27)	5.2
ESSB-Q14E	1 - 3	8/9/2004	ND(490)	ND(490)	ND(490)	15000	ND(490)	ND(490)	ND(490)	15000
	3 - 5	8/9/2004	ND(380)	ND(380)	ND(380)	7700	ND(380)	ND(380)	ND(380)	7700
ESSB-Q14W	1 - 3	8/9/2004	ND(4.3)	ND(4.3)	ND(4.3)	ND(4.3)	22	13	ND(4.3)	35
	3 - 5	8/9/2004	ND(0.19)	ND(0.19)	ND(0.19)	ND(0.19)	ND(0.19)	4.2	ND(0.19)	4.2
ESSB-Q16	1 - 3	1/22/2004	ND(2.2)	ND(2.2)	ND(2.2)	ND(2.2)	ND(2.2)	24	ND(2.2)	24
	3 - 5	1/22/2004	ND(1.2) [ND(1.2)]	ND(1.2) [ND(1.2)]	ND(1.2) [ND(1.2)]	ND(1.2) [ND(1.2)]	9.3 [12]	13 [19]	ND(1.2) [ND(1.2)]	22 [31]
	5 - 7	1/22/2004	ND(5.0)	ND(5.0)	ND(5.0)	ND(5.0)	18	38	ND(5.0)	56
ESSB-Q16E	2 - 4	8/10/2004	ND(19)	ND(19)	ND(19)	ND(19)	33	42	ND(19)	75
	4 - 6	8/10/2004	ND(0.23)	ND(0.23)	ND(0.23)	ND(0.23)	0.52	0.52	ND(0.23)	1.0
	6 - 8	8/10/2004	ND(0.18)	ND(0.18)	ND(0.18)	ND(0.18)	0.51	0.69	ND(0.18)	1.2
ESSB-Q16N	2 - 4	8/10/2004	ND(49) [ND(13)]	ND(49) [ND(13)]	ND(49) [ND(13)]	ND(49) [ND(13)]	50 [57]	69 [81]	ND(49) [ND(13)]	120 [140]
	4 - 6	8/10/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.22	0.38	ND(0.037)	0.60
	6 - 8	8/10/2004	ND(0.20)	ND(0.20)	ND(0.20)	ND(0.20)	1.5	2.9	ND(0.20)	4.4
ESSB-Q16W	2 - 4	8/10/2004	ND(1.0)	ND(1.0)	ND(1.0)	ND(1.0)	ND(1.0)	15	ND(1.0)	15
	4 - 6	8/10/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.097	ND(0.035)	0.097
	6 - 8	8/10/2004	ND(0.21)	ND(0.21)	ND(0.21)	ND(0.21)	ND(0.21)	0.91	ND(0.21)	0.91
ESSB-Q18	1 - 3	1/28/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.036)	0.038	ND(0.033)	0.038
	3 - 5	1/28/2004	ND(0.034) [ND(0.036)]	ND(0.034) [ND(0.036)]	ND(0.034) [ND(0.036)]	ND(0.034) [ND(0.036)]	ND(0.034) [ND(0.036)]	0.0097 J [ND(0.036)]	ND(0.034) [ND(0.036)]	0.0097 J [ND(0.036)]
	5 - 7	1/28/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
	7 - 9	1/28/2004	ND(0.036)	ND(0.036)	ND(0.036)	0.016 J	ND(0.036)	0.014 J	ND(0.036)	0.030
	9 - 11	1/28/2004	ND(0.035)	ND(0.035)	ND(0.035)	0.014 J	ND(0.035)	ND(0.035)	ND(0.035)	0.014
	11 - 13	1/28/2004	ND(0.036)	ND(0.036)	ND(0.036)	0.024 J	ND(0.036)	0.019 J	ND(0.036)	0.042
	13 - 15	1/28/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)
	15 - 17	1/28/2004	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	0.024 J	ND(0.042)	0.024 J
ESSB-R12	1 - 3	8/6/2004	ND(400)	ND(400)	ND(400)	ND(400)	4200	ND(400)	ND(400)	4200
	3 - 4	8/6/2004	ND(51)	ND(51)	ND(51)	ND(51)	190	150	ND(51)	340
	4 - 6	8/6/2004	ND(0.21)	ND(0.21)	ND(0.21)	ND(0.21)	0.62	0.30	ND(0.21)	0.92
ESSB-R14	1 - 3	8/9/2004	ND(120)	ND(120)	ND(120)	ND(120)	880	520	ND(120)	1400
	3 - 5	8/9/2004	ND(0.23)	ND(0.23)	ND(0.23)	ND(0.23)	1.5	1.0	ND(0.23)	2.6

TABLE 3
SUMMARY OF PDI PCB SAMPLE DATA - ELM STREET AREA SUBSURFACE SOILS

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
ESSB-R16	2 - 4	8/10/2004	ND(0.27)	ND(0.27)	ND(0.27)	ND(0.27)	ND(0.27)	1.2	ND(0.27)	1.2
	4 - 6	8/10/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)
	6 - 8	8/10/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.17	0.041	ND(0.034)	0.21
ESSB-R18	1 - 3	1/27/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.060	0.056	ND(0.034)	0.12
ESSB-R22	1 - 3	1/27/2004	ND(0.47)	ND(0.47)	ND(0.47)	ND(0.47)	4.1	2.8	ND(0.47)	6.9
ESSB-S11	1 - 2	4/27/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.080	ND(0.034)	ND(0.034)	0.080
ESSB-S11E	1 - 2	4/21/2004	ND(43)	ND(43)	ND(43)	ND(43)	1000	ND(43)	ND(43)	1000
	2 - 3	4/21/2004	ND(19)	ND(19)	ND(19)	ND(19)	87	ND(19)	ND(19)	87
ESSB-S11N	1 - 2	4/21/2004	ND(12)	ND(12)	ND(12)	ND(12)	170	ND(12)	ND(12)	170
	2 - 3	4/21/2004	ND(0.19)	ND(0.19)	ND(0.19)	ND(0.19)	0.60 J	ND(0.19)	ND(0.19)	0.60 J
ESSB-S11S	1 - 2	4/21/2004	ND(49)	ND(49)	ND(49)	ND(49)	1000	ND(49)	ND(49)	1000
	2 - 3	4/21/2004	ND(23)	ND(23)	ND(23)	ND(23)	330	ND(23)	ND(23)	330
	3 - 5	10/19/05	ND(0.036) [ND(0.035)]	ND(0.036) [ND(0.035)]	ND(0.036) [0.18]	ND(0.036) [ND(0.035)]	0.030 J [ND(0.035)]	0.061 [0.12]	ND(0.036) [0.0082 J]	0.091 [0.31]
ESSB-S11SS	1 - 2	4/21/2004	ND(0.19)	ND(0.19)	ND(0.19)	ND(0.19)	0.65	ND(0.19)	ND(0.19)	0.65
	2 - 3	4/21/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	0.094	ND(0.033)	0.029 J	0.12
ESSB-S11W	1 - 2	4/21/2004	ND(0.19)	ND(0.19)	ND(0.19)	ND(0.19)	3.3	ND(0.19)	ND(0.19)	3.3
	2 - 3	10/19/05	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)
ESSB-S12	1 - 3	1/26/2004	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	1.3	ND(0.24)	ND(0.24)	1.3
	3 - 5	1/26/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.23	ND(0.036)	ND(0.036)	0.23
	5 - 7	1/26/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.091	ND(0.037)	ND(0.037)	0.091
	7 - 9	1/26/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.051	ND(0.035)	ND(0.035)	0.051
	9 - 11	1/26/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.050	ND(0.035)	ND(0.035)	0.050
	11 - 13	1/26/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.11	ND(0.037)	ND(0.037)	0.11
	13 - 15	1/26/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.089	ND(0.036)	ND(0.036)	0.089
	15 - 17	1/26/2004	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	0.084	ND(0.040)	ND(0.040)	0.084
	17 - 19	1/26/2004	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	0.050	ND(0.040)	ND(0.040)	0.050
ESSB-S14	1 - 3	1/21/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.018 J	0.013 J	ND(0.037)	0.032 J
	3 - 5	1/21/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.0090 J	ND(0.034)	ND(0.034)	0.0090 J
	5 - 7	1/21/2004	ND(4.8)	ND(4.8)	ND(4.8)	ND(4.8)	ND(4.8)	43	ND(4.8)	43
	7 - 9	1/21/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.019 J	0.026 J	ND(0.035)	0.046
	9 - 11	1/21/2004	ND(0.26)	ND(0.26)	ND(0.26)	ND(0.26)	5.0	5.0	ND(0.26)	10
	11 - 13	1/21/2004	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)
	13 - 15	1/21/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.080	0.063	ND(0.035)	0.14
	15 - 17	1/21/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.011 J	0.011 J	ND(0.035)	0.022 J
	17 - 19	1/21/2004	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	0.029 J	0.022 J	ND(0.041)	0.051
	19 - 20	1/21/2004	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	0.031 J	0.024 J	ND(0.041)	0.056
ESSB-S16	1 - 3	1/21/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.030 J	ND(0.038)	ND(0.038)	0.030 J
	3 - 5	1/21/2004	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	0.082	0.066	ND(0.041)	0.15
	5 - 7	1/21/2004	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	0.031 J	0.012 J	ND(0.039)	0.044
	7 - 9	1/21/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.15	0.062	ND(0.037)	0.21
	9 - 11	1/21/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.26	0.12	ND(0.034)	0.37
	11 - 13	1/21/2004	ND(0.20)	ND(0.20)	ND(0.20)	ND(0.20)	2.9	ND(0.20)	ND(0.20)	2.9
	13 - 15	1/21/2004	ND(0.25)	ND(0.25)	ND(0.25)	ND(0.25)	2.7	ND(0.25)	ND(0.25)	2.7
	15 - 17	1/21/2004	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	0.22	0.070	ND(0.041)	0.29
ESSB-S18	1 - 3	1/21/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)
	3 - 5	1/21/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)
	5 - 7	1/21/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
	7 - 9	1/21/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)
	9 - 11	1/21/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.0094 J	ND(0.035)	ND(0.035)	0.0094 J
	11 - 12	1/21/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.072	ND(0.037)	ND(0.037)	0.072

TABLE 3
SUMMARY OF PDI PCB SAMPLE DATA - ELM STREET AREA SUBSURFACE SOILS

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
ESSB-S20	1 - 3	12/30/2003	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.088	ND(0.038)	ND(0.038)	0.088
	3 - 5	12/30/2003	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.076	ND(0.036)	ND(0.036)	0.076
	5 - 7	12/31/2003	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.050)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.050)
	7 - 9	12/30/2003	ND(0.035) [ND(0.035)]	ND(0.035) [ND(0.035)]	ND(0.035) [ND(0.035)]	ND(0.035) [ND(0.035)]	0.042 [0.031 J]	ND(0.035) [ND(0.035)]	ND(0.035) [ND(0.035)]	0.042 [0.031 J]
	9 - 11	12/30/2003	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.068	ND(0.035)	ND(0.035)	0.068
	11 - 13	12/30/2003	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.11	ND(0.038)	ND(0.038)	0.11
	13 - 15	12/30/2003	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	0.057	ND(0.039)	ND(0.039)	0.057
ESSB-S22	1 - 3	1/21/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.0093 J	ND(0.035)	ND(0.035)	0.0093 J
	3 - 5	1/21/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.0095 J	ND(0.034)	ND(0.034)	0.0095 J
	5 - 7	1/21/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
	7 - 9	1/21/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.097	ND(0.035)	ND(0.035)	0.097
	9 - 11	1/21/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
	11 - 13	1/21/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.045	ND(0.035)	ND(0.035)	0.045
	13 - 15	1/21/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.13	ND(0.038)	ND(0.038)	0.13
	15 - 17	1/21/2004	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	0.038 J	ND(0.041)	ND(0.041)	0.038 J
ESSB-T16	1 - 3	12/29/2003	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.028 J	0.026 J	ND(0.036)	0.053
	3 - 5	12/23/2003	ND(0.19)	ND(0.19)	ND(0.19)	ND(0.19)	0.91	0.44	ND(0.19)	1.4
	5 - 7	12/23/2003	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.028 J	ND(0.036)	ND(0.036)	0.028 J
	7 - 9	12/23/2003	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.035 J	0.021 J	ND(0.036)	0.056
	9 - 11	12/23/2003	ND(0.078)	ND(0.078)	ND(0.078)	ND(0.078)	0.68	ND(0.078)	ND(0.078)	0.68
	11 - 13	12/23/2003	ND(3.7)	ND(3.7)	ND(3.7)	ND(3.7)	6.4	ND(3.7)	ND(3.7)	6.4
	13 - 15	12/29/2003	ND(0.073)	ND(0.073)	ND(0.073)	ND(0.073)	0.44	ND(0.073)	ND(0.073)	0.44
	15 - 17	12/29/2003	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.20	ND(0.036)	ND(0.036)	0.20
	17 - 19	12/29/2003	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	0.034 J	ND(0.041)	ND(0.041)	0.034 J
SB-15	1 - 2	4/28/2004	ND(120)	ND(120)	ND(120)	ND(120)	720	570	ND(120)	1300
	1 - 3	8/3/2004	ND(190)	ND(190)	ND(190)	ND(190)	250	150 J	ND(190)	400
	2 - 3	4/28/2004	ND(1100)	ND(1100)	ND(1100)	ND(1100)	1700 JN	1300	ND(1100)	3000 JN
	3 - 5	8/3/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	0.15	0.11	ND(0.033)	0.26
	5 - 7	8/3/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.017 J	ND(0.035)	ND(0.035)	0.017 J
SB-15E	1 - 3	8/3/2004	ND(19)	ND(19)	ND(19)	ND(19)	120	36	ND(19)	160
	3 - 5	8/3/2004	ND(0.22)	ND(0.22)	ND(0.22)	ND(0.22)	4.2	3.4	ND(0.22)	7.7
	5 - 7	8/3/2004	ND(0.23)	ND(0.23)	ND(0.23)	ND(0.23)	2.9	2.6	ND(0.23)	5.5
SB-15S	1 - 3	8/3/2004	ND(96)	ND(96)	ND(96)	ND(96)	290	220	ND(96)	510
	3 - 5	8/3/2004	ND(0.21)	ND(0.21)	ND(0.21)	ND(0.21)	0.40	0.16 J	ND(0.21)	0.56
	5 - 7	8/3/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.032 J	0.017 J	ND(0.034)	0.049
SB-15W	1 - 3	8/3/2004	ND(22)	ND(22)	ND(22)	ND(22)	660	ND(22)	ND(22)	660
	3 - 5	8/3/2004	ND(0.23)	ND(0.23)	ND(0.23)	ND(0.23)	2.1	1.7	ND(0.23)	3.8
	5 - 7	8/3/2004	ND(1.2)	ND(1.2)	ND(1.2)	ND(1.2)	13	6.5	ND(1.2)	20
SB-17	1 - 3	8/4/2004	ND(46)	ND(46)	ND(46)	ND(46)	460	220	ND(46)	680
	3 - 5	8/4/2004	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	1.8	1.0	ND(0.24)	2.9
SB-17W	1 - 3	8/4/2004	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	1.2	1.1	ND(0.24)	2.4
SB-19	1 - 2	4/28/2004	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	2.8 JN	1.6	ND(0.24)	4.4 JN
SB-20	1 - 2	4/28/2004	ND(20)	ND(20)	ND(20)	ND(20)	200	ND(20)	ND(20)	200
	2 - 3	4/28/2004	ND(2.7)	ND(2.7)	ND(2.7)	ND(2.7)	25	ND(2.7)	ND(2.7)	25
SB-20S	3 - 4	8/26/2004	ND(12)	ND(12)	ND(12)	ND(12)	170	ND(12)	ND(12)	170
	4 - 5	8/26/2004	ND(10)	ND(10)	ND(10)	ND(10)	100	ND(10)	ND(10)	100
	5 - 6	8/26/2004	ND(5.5)	ND(5.5)	ND(5.5)	ND(5.5)	71	ND(5.5)	ND(5.5)	71
SB-21	1 - 2	4/28/2004	ND(21)	ND(21)	ND(21)	ND(21)	400	ND(21)	ND(21)	400
	2 - 3	4/28/2004	ND(0.25)	ND(0.25)	ND(0.25)	ND(0.25)	3.3	ND(0.25)	ND(0.25)	3.3
SB-26	1 - 3	8/9/2004	ND(51)	ND(51)	ND(51)	ND(51)	710	240	ND(51)	950
	3 - 5	8/9/2004	ND(49)	ND(49)	ND(49)	ND(49)	260	210	ND(49)	470
SB-38	1 - 2	4/28/2004	ND(1.1) [ND(0.034)]	ND(1.1) [ND(0.034)]	ND(1.1) [ND(0.034)]	ND(1.1) [ND(0.034)]	7.9 J [0.021 J]	ND(1.1) J [0.022 J]	ND(1.1) [ND(0.034)]	7.9 J [0.043 J]

TABLE 3
SUMMARY OF PDI PCB SAMPLE DATA - ELM STREET AREA SUBSURFACE SOILS

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Notes:

1. Samples were collected by Blasland, Bouck & Lee, Inc., and submitted to Severn Trent Laboratories, Inc. for analysis of PCBs.
2. ND - Analyte was not detected. The number in parentheses is the associated detection limit.
3. Field duplicate sample results are presented in brackets.
4. In the areas where temporary cover materials have been placed (e.g., geotextile and soil cover), the 0- to 1-foot surface soil sampling interval began at the depth of the geotextile installed by EPA, which is considered to represent the boundary between clean barrier soils and native Site soils.

Data Qualifiers:

EB - The compound was identified in an aqueous equipment blank that was used to assess field contamination associated with soil/sediment samples, its presence in the sample may be suspect.

J - The compound was positively identified; however, the associated numerical value is an estimated concentration only.

N - The analysis indicates the presence of a compound for which there is presumptive evidence to make a tentative identification. The associated numerical value is an estimated concentration only.

TABLE 4
SUMMARY OF PDI PCB SAMPLE DATA - MILL STREET AREA SURFACE SOILS

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
EB-13S	0 - 1	4/22/2004	ND(12)	ND(12)	ND(12)	ND(12)	82	ND(12)	ND(12)	82
EB-13SS	0 - 1	4/22/2004	ND(0.033)	ND(0.033)	ND(0.033)	0.059	ND(0.033)	ND(0.033)	ND(0.033)	0.059
MSSB-B07	0 - 1	2/18/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.056	0.016 J	ND(0.036)	0.073
MSSB-B09	0 - 1	2/19/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.11	ND(0.037)	0.16	0.26
MSSB-B11	0 - 1	2/18/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.044	0.022 J	ND(0.036)	0.067
MSSB-B13	0 - 1	2/12/2004	ND(0.23)	ND(0.23)	ND(0.23)	ND(0.23)	1.2	0.45	ND(0.23)	1.6
MSSB-B15	0 - 1	2/12/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.31	0.16	ND(0.035)	0.47
MSSB-B17	0 - 1	2/12/2004	ND(0.24)	ND(0.24)	ND(0.24)	2.4	ND(0.24)	ND(0.24)	ND(0.24)	2.4
MSSB-B17N	0 - 1	4/19/2004	ND(0.25)	ND(0.25)	ND(0.25)	ND(0.25)	0.97	ND(0.25)	ND(0.25)	0.97
MSSB-B18	0 - 1	7/7/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.050)	ND(0.033)	ND(0.033)	ND(0.050)
MSSB-B19	0 - 1	7/7/2004	ND(0.034) [ND(0.035)]	ND(0.034) [ND(0.035)]	ND(0.034) [ND(0.035)]	ND(0.034) [ND(0.035)]	ND(0.046) [0.044]	ND(0.034) [ND(0.035)]	ND(0.034) [ND(0.035)]	ND(0.046) [0.044]
MSSB-B20	0 - 1	7/7/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.051)	ND(0.034)	ND(0.034)	ND(0.051)
MSSB-B21	0 - 1	7/7/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)
MSSB-C01	0 - 1	1/13/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.15	ND(0.036)	ND(0.036)	0.15
MSSB-C03	0 - 1	1/20/2004	ND(0.21)	ND(0.21)	ND(0.21)	ND(0.21)	0.73	ND(0.21)	ND(0.21)	0.73
MSSB-C05	0 - 1	1/6/2004	ND(3.7)	ND(3.7)	ND(3.7)	ND(3.7)	7.0	ND(3.7)	ND(3.7)	7.0
MSSB-C06	0 - 1	1/14/2004	ND(0.036) [ND(0.036)]	ND(0.036) [ND(0.036)]	ND(0.036) [ND(0.036)]	ND(0.036) [ND(0.036)]	0.035 J [0.056]	0.014 J [0.032 J]	ND(0.036) [ND(0.036)]	0.049 [0.089]
MSSB-C07	0 - 1	1/6/2004	ND(280)	ND(280)	ND(280)	ND(280)	1500	ND(280)	ND(280)	1500
MSSB-C08	0 - 1	1/12/2004	ND(12)	ND(12)	ND(12)	ND(12)	54	ND(12)	ND(12)	54
MSSB-C09	0 - 1	1/13/2004	ND(0.26)	ND(0.26)	ND(0.26)	ND(0.26)	0.73	ND(0.26)	ND(0.26)	0.73
MSSB-C10	0 - 1	1/12/2004	ND(25)	ND(25)	ND(25)	ND(25)	140	ND(25)	ND(25)	140
MSSB-C11	0 - 1	1/8/2004	ND(1.9)	ND(1.9)	ND(1.9)	ND(1.9)	6.6	ND(1.9)	ND(1.9)	6.6
MSSB-C12	0 - 1	1/12/2004	ND(1100)	ND(1100)	ND(1100)	ND(1100)	3000	ND(1100)	ND(1100)	3000
MSSB-C13	0 - 1	1/8/2004	ND(0.18)	ND(0.18)	ND(0.18)	ND(0.18)	1.4	ND(0.18)	ND(0.18)	1.4
MSSB-C14	0 - 1	1/12/2004	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	0.82	0.46	ND(0.24)	1.3
MSSB-C15	0 - 1	1/6/2004	ND(0.34)	ND(0.34)	ND(0.34)	2.5	ND(0.34)	ND(0.34)	ND(0.34)	2.5
MSSB-C16	0 - 1	1/12/2004	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	0.77	0.63	ND(0.24)	1.4
MSSB-C17	0 - 1	1/7/2004	ND(0.34)	ND(0.34)	ND(0.34)	ND(0.34)	0.73	ND(0.34)	ND(0.34)	0.73
MSSB-C18	0 - 1	1/12/2004	ND(0.30) [ND(0.21)]	ND(0.30) [ND(0.21)]	ND(0.30) [ND(0.21)]	ND(0.30) [ND(0.21)]	0.83 [1.0]	0.60 [0.79]	ND(0.30) [ND(0.21)]	1.4 [1.8]
MSSB-C19	0 - 1	1/7/2004	ND(0.073)	ND(0.073)	ND(0.073)	0.27	ND(0.073)	ND(0.073)	ND(0.073)	0.27
MSSB-C20	0 - 1	1/12/2004	ND(0.23)	ND(0.23)	ND(0.23)	ND(0.23)	0.75	0.46	ND(0.23)	1.2
MSSB-D04	0 - 1	12/18/2003	ND(0.77)	ND(0.77)	ND(0.77)	ND(0.77)	1.9	ND(0.77)	ND(0.77)	1.9
MSSB-D04SW	0 - 1	4/28/2004	ND(0.88)	ND(0.88)	ND(0.88)	ND(0.88)	14	ND(0.88)	ND(0.88)	14
MSSB-D05	0 - 1	12/4/2003	ND(0.72)	ND(0.72)	ND(0.72)	ND(0.72)	3.0	3.6	ND(0.72)	6.5
MSSB-D06	0 - 1	12/4/2003	ND(3.7)	ND(3.7)	ND(3.7)	ND(3.7)	22	15	ND(3.7)	38
MSSB-D07	0 - 1	12/4/2003	ND(3.7)	ND(3.7)	ND(3.7)	ND(3.7)	49	31	ND(3.7)	80
MSSB-D08	0 - 1	12/4/2003	ND(2.0)	ND(2.0)	ND(2.0)	ND(2.0)	3.7	1.7 J	ND(2.0)	5.4
MSSB-D09	0 - 1	12/4/2003	ND(0.36)	ND(0.36)	ND(0.36)	ND(0.36)	1.9	1.2	ND(0.36)	3.1
MSSB-D10	0 - 1	12/4/2003	ND(3.7)	ND(3.7)	ND(3.7)	ND(3.7)	12	8.0	ND(3.7)	20
MSSB-D11	0 - 1	12/4/2003	ND(0.36)	ND(0.36)	ND(0.36)	ND(0.36)	1.2	0.70	ND(0.36)	1.9
MSSB-D13	0 - 1	12/4/2003	ND(0.71) [ND(0.71)]	ND(0.71) [ND(0.71)]	ND(0.71) [ND(0.71)]	ND(0.71) [ND(0.71)]	1.1 [1.2]	0.73 [0.84]	ND(0.71) [ND(0.71)]	1.8 [2.1]
MSSB-D15	0 - 1	12/4/2003	ND(360)	ND(360)	ND(360)	ND(360)	2800	1600	ND(360)	4400
MSSB-D17	0 - 1	12/17/2003	ND(0.69)	ND(0.69)	ND(0.69)	ND(0.69)	3.0	ND(0.69)	ND(0.69)	3.0
MSSB-E01	0 - 1	12/19/2003	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.076)	ND(0.039)	ND(0.039)	ND(0.076)
MSSB-E03	0 - 1	12/23/2003	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.17	ND(0.038)	ND(0.038)	0.17
MSSB-E05	0 - 1	12/4/2003	ND(3.5)	ND(3.5)	ND(3.5)	ND(3.5)	14	9.2	ND(3.5)	23
MSSB-E07	0 - 1	12/9/2003	ND(750)	ND(750)	ND(750)	ND(750)	13000	ND(750)	ND(750)	13000
MSSB-E09	0 - 1	12/9/2003	ND(1.9)	ND(1.9)	ND(1.9)	ND(1.9)	7.7	ND(1.9)	ND(1.9)	7.7
MSSB-E11	0 - 1	12/18/2003	ND(1.8)	ND(1.8)	ND(1.8)	ND(1.8)	28	ND(1.8)	ND(1.8)	28
MSSB-E12	0 - 1	12/18/2003	ND(91)	ND(91)	ND(91)	ND(91)	1400	ND(91)	ND(91)	1400
MSSB-E13	0 - 1	12/17/2003	ND(72)	ND(72)	ND(72)	ND(72)	920	ND(72)	ND(72)	920
MSSB-E13S	0 - 1	4/22/2004	ND(2.1)	ND(2.1)	ND(2.1)	19	ND(2.1)	ND(2.1)	ND(2.1)	19
MSSB-E13SS	0 - 1	4/22/2004	ND(0.75)	ND(0.75)	ND(0.75)	7.8	ND(0.75)	ND(0.75)	ND(0.75)	7.8

TABLE 4
SUMMARY OF PDI PCB SAMPLE DATA - MILL STREET AREA SURFACE SOILS

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
MSSB-E14	0 - 1	12/18/2003	ND(180)	ND(180)	ND(180)	ND(180)	1500	ND(180)	ND(180)	1500
MSSB-E14SE	0 - 1	4/22/2004	ND(0.033)	ND(0.033)	ND(0.033)	0.095	ND(0.033)	ND(0.033)	ND(0.033)	0.095
MSSB-E14SW	0 - 1	4/22/2004	ND(0.033)	ND(0.033)	ND(0.033)	0.021 J	ND(0.033)	ND(0.033)	ND(0.033)	0.021 J
MSSB-E15	0 - 1	12/17/2003	ND(680)	ND(680)	ND(680)	ND(680)	5200	ND(680)	ND(680)	5200
MSSB-E15S	0 - 1	4/22/2004	ND(0.36)	ND(0.36)	ND(0.36)	3.9	ND(0.36)	ND(0.36)	ND(0.36)	3.9
MSSB-F06	0 - 1	12/8/2003	ND(0.72)	ND(0.72)	ND(0.72)	ND(0.72)	7.8	ND(0.72)	ND(0.72)	7.8
MSSB-F07	0 - 1	12/12/2003	ND(0.75)	ND(0.75)	ND(0.75)	ND(0.75)	6.4	ND(0.75)	ND(0.75)	6.4
MSSB-F08	0 - 1	12/18/2003	ND(1.8)	ND(1.8)	ND(1.8)	ND(1.8)	18	ND(1.8)	ND(1.8)	18
MSSB-F09	0 - 1	12/18/2003	ND(1.7)	ND(1.7)	ND(1.7)	ND(1.7)	17	ND(1.7)	ND(1.7)	17
MSSB-F10	0 - 1	12/18/2003	ND(3.5)	ND(3.5)	ND(3.5)	ND(3.5)	61	ND(3.5)	ND(3.5)	61
MSSB-G01	0 - 1	12/11/2003	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.045	ND(0.034)	ND(0.034)	0.045
MSSB-G03	0 - 1	12/16/2003	ND(0.035) [ND(0.034)]	ND(0.035) [ND(0.034)]	ND(0.035) [ND(0.034)]	ND(0.035) [ND(0.034)]	0.046 [ND(0.034)]	ND(0.035) [ND(0.034)]	ND(0.035) [ND(0.034)]	0.046 [ND(0.034)]
MSSB-G05	0 - 1	12/16/2003	ND(0.71)	ND(0.71)	ND(0.71)	ND(0.71)	2.7	ND(0.71)	ND(0.71)	2.7
MSSS-B13E	0 - 1	4/19/2004	ND(0.21)	ND(0.21)	ND(0.21)	ND(0.21)	1.3	ND(0.21)	ND(0.21)	1.3
MSSS-B13N	0 - 1	4/19/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	0.11	ND(0.033)	ND(0.033)	0.11
MSSS-B13W	0 - 1	4/19/2004	ND(0.21)	ND(0.21)	ND(0.21)	ND(0.21)	0.94	ND(0.21)	ND(0.21)	0.94
MSSS-C02	0 - 1	1/12/2004	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	0.58	0.34	ND(0.24)	0.92
MSSS-C04	0 - 1	1/14/2004	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	0.024 J	ND(0.040)	0.024 J
MSSS-C05N	0 - 1	4/28/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.075	ND(0.037)	ND(0.037)	0.075
MSSS-C14N	0 - 1	4/19/2004	ND(0.23)	ND(0.23)	ND(0.23)	ND(0.23)	0.86	ND(0.23)	ND(0.23)	0.86
MSSS-C17NE	0 - 1	4/19/2004	ND(0.20)	ND(0.20)	ND(0.20)	ND(0.20)	1.5	ND(0.20)	ND(0.20)	1.5
MSSS-C18N	0 - 1	4/19/2004	ND(2.1)	ND(2.1)	ND(2.1)	ND(2.1)	8.6	ND(2.1)	ND(2.1)	8.6
MSSS-C20E	0 - 1	4/22/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	0.030 J	0.014 J	ND(0.033)	0.044
MSSS-C20N	0 - 1	4/19/2004	ND(1.0)	ND(1.0)	ND(1.0)	ND(1.0)	13	ND(1.0)	ND(1.0)	13
MSSS-C20S	0 - 1	4/22/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)
MSSS-D03	0 - 1	12/18/2003	ND(0.045)	ND(0.045)	ND(0.045)	ND(0.045)	ND(0.045)	ND(0.045)	ND(0.045)	ND(0.045)
MSSS-D04NE	0 - 1	4/28/2004	ND(0.21)	ND(0.21)	ND(0.21)	ND(0.21)	2.1	ND(0.21)	ND(0.21)	2.1
MSSS-D14	0 - 1	12/4/2003	ND(0.14)	ND(0.14)	ND(0.14)	ND(0.14)	0.48	0.24	ND(0.14)	0.72
MSSS-D17SW	0 - 1	4/22/2004	ND(0.18)	ND(0.18)	ND(0.18)	0.63	ND(0.18)	ND(0.18)	ND(0.18)	0.63
MSSS-E02	0 - 1	12/23/2003	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.061)	ND(0.039)	ND(0.039)	ND(0.061)
MSSS-E16	0 - 1	4/22/2004	ND(0.034)	ND(0.034)	ND(0.034)	0.034	ND(0.034)	ND(0.034)	ND(0.034)	0.034
MSSS-F01	0 - 1	12/8/2003	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.010 J	ND(0.036)	ND(0.036)	0.010 J
MSSS-F02	0 - 1	12/8/2003	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.025 J	ND(0.035)	ND(0.035)	0.025 J
MSSS-F03	0 - 1	12/8/2003	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.014 J	ND(0.037)	ND(0.037)	0.014 J
MSSS-F04	0 - 1	12/8/2003	ND(0.068)	ND(0.068)	ND(0.068)	ND(0.068)	0.38	ND(0.068)	ND(0.068)	0.38
MSSS-F06SW	0 - 1	4/22/2004	ND(0.033)	ND(0.033)	ND(0.033)	0.41	ND(0.033)	ND(0.033)	ND(0.033)	0.41
MSSS-F07SW	0 - 1	4/22/2004	ND(0.18)	ND(0.18)	ND(0.18)	1.7	ND(0.18)	ND(0.18)	ND(0.18)	1.7
MSSS-F08SW	0 - 1	4/22/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)
MSSS-F09SW	0 - 1	4/22/2004	ND(0.033)	ND(0.033)	ND(0.033)	0.016 J	ND(0.033)	ND(0.033)	ND(0.033)	0.016 J
MSSS-F10SW	0 - 1	4/22/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)
MW-23C	0 - 1	1/20/2004	ND(0.054)	ND(0.054)	ND(0.054)	ND(0.054)	0.11	0.072	ND(0.054)	0.19
MW-24C	0 - 1	1/5/2004	ND(0.18)	ND(0.18)	ND(0.18)	ND(0.18)	0.76	ND(0.18)	ND(0.18)	0.76
SF-04g-ISW	0 - 1	4/22/2004	ND(0.032)	ND(0.032)	ND(0.032)	ND(0.032)	ND(0.032)	ND(0.032)	ND(0.032)	ND(0.032)
SS-12E	0 - 1	4/22/2004	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	0.020 J [0.024 J]	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	0.020 J [0.024 J]
SS-12S	0 - 1	4/22/2004	ND(0.033) J	ND(0.033) J	ND(0.033) J	0.046 J	ND(0.033) J	ND(0.033) J	ND(0.033) J	0.046 J
SS-13NE	0 - 1	4/28/2004	ND(0.20)	ND(0.20)	ND(0.20)	ND(0.20)	2.8	ND(0.20)	ND(0.20)	2.8
SS-13SE	0 - 1	4/28/2004	ND(0.21)	ND(0.21)	ND(0.21)	ND(0.21)	1.3	ND(0.21)	ND(0.21)	1.3
SS-13SW	0 - 1	4/28/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.036	ND(0.035)	ND(0.035)	0.036

TABLE 4
SUMMARY OF PDI PCB SAMPLE DATA - MILL STREET AREA SURFACE SOILS

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Notes:

1. Samples were collected by Blasland, Bouck & Lee, Inc., and submitted to Severn Trent Laboratories, Inc. for analysis of PCBs.
2. ND - Analyte was not detected. The number in parentheses is the associated detection limit.
3. Field duplicate sample results are presented in brackets.
4. In the areas where temporary cover materials have been placed (e.g., geotextile and soil cover), the 0- to 1-foot surface soil sampling interval began at the depth of the geotextile installed by EPA, which is considered to represent the boundary between clean barrier soils and native Site soils.

Data Qualifiers:

J - The compound was positively identified; however, the associated numerical value is an estimated concentration only.

TABLE 5
SUMMARY OF PDI PCB SAMPLE DATA - MILL STREET AREA SUBSURFACE SOILS

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
EB-07A	1 - 3	6/30/2004	ND(1300)	ND(1300)	ND(1300)	11000	ND(1300)	ND(1300)	ND(1300)	11000
	3 - 4	6/30/2004	ND(1200)	ND(1200)	ND(1200)	32000	ND(1200)	ND(1200)	ND(1200)	32000
EB-12	3 - 5	6/30/2004	ND(950)	ND(950)	ND(950)	40000	ND(950)	ND(950)	ND(950)	40000
	5 - 7	6/30/2004	ND(980)	ND(980)	ND(980)	10000	ND(980)	ND(980)	ND(980)	10000
	7 - 9	6/30/2004	ND(110)	ND(110)	ND(110)	5500	ND(110)	ND(110)	ND(110)	5500
	9 - 11	6/30/2004	ND(49)	ND(49)	ND(49)	330	ND(49)	ND(49)	ND(49)	330
	11 - 13	6/30/2004	ND(11)	ND(11)	ND(11)	180	ND(11)	ND(11)	ND(11)	180
	13 - 15	6/30/2004	ND(1.1)	ND(1.1)	ND(1.1)	8.7	ND(1.1)	ND(1.1)	ND(1.1)	8.7
	15 - 17	6/30/2004	ND(0.19)	ND(0.19)	ND(0.19)	1.1	ND(0.19)	ND(0.19)	ND(0.19)	1.1
	17 - 19	6/30/2004	ND(200)	ND(200)	ND(200)	2000	ND(200)	ND(200)	ND(200)	2000
	19 - 21	6/30/2004	ND(3.7)	ND(3.7)	ND(3.7)	33	ND(3.7)	ND(3.7)	ND(3.7)	33
	21 - 23	6/30/2004	ND(0.22)	ND(0.22)	ND(0.22)	0.90	ND(0.22)	ND(0.22)	ND(0.22)	0.90
EB-13	1 - 3	6/30/2004	ND(0.89)	ND(0.89)	ND(0.89)	5.2	ND(0.89)	ND(0.89)	ND(0.89)	5.2
	3 - 5	6/30/2004	ND(1.2)	ND(1.2)	ND(1.2)	ND(1.2)	21	ND(1.2)	ND(1.2)	21
	9 - 11	6/30/2004	ND(0.23) [ND(0.27)]	ND(0.23) [ND(0.27)]	ND(0.23) [ND(0.27)]	1.2 [0.93]	ND(0.23) [ND(0.27)]	ND(0.23) [ND(0.27)]	ND(0.23) [ND(0.27)]	1.2 [0.93]
	11 - 13	6/30/2004	ND(0.32)	ND(0.32)	ND(0.32)	0.85	ND(0.32)	ND(0.32)	ND(0.32)	0.85
	13 - 15	6/30/2004	ND(0.28)	ND(0.28)	ND(0.28)	0.85	ND(0.28)	ND(0.28)	ND(0.28)	0.85
	16.5 - 18.5	6/30/2004	ND(0.30)	ND(0.30)	ND(0.30)	0.85	ND(0.30)	ND(0.30)	ND(0.30)	0.85
EB-13S	1 - 3	4/22/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.029 J	ND(0.034)	ND(0.034)	0.029 J
	3 - 5	4/22/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)
	5 - 7	4/22/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
	7 - 9	4/22/2004	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)
	9 - 11	4/22/2004	ND(0.045)	ND(0.045)	ND(0.045)	ND(0.045)	ND(0.045)	ND(0.045)	ND(0.045)	ND(0.045)
	11 - 13	4/22/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.0092 J	ND(0.037)	ND(0.037)	ND(0.037)
	13 - 15	4/22/2004	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)
	15 - 16.5	4/22/2004	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)
	16.5 - 18.5	4/22/2004	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)
EB-13W	1 - 3	7/27/2004	ND(0.46)	ND(0.46)	ND(0.46)	ND(0.46)	11	ND(0.46)	ND(0.46)	11
	3 - 5	7/27/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.16	0.064	ND(0.034)	0.23
	5 - 7	7/27/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	0.030 J	0.015 J	ND(0.033)	0.045
	7 - 9	7/27/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.026 J	0.011 J	ND(0.034)	0.037
	9 - 11	7/27/2004	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	0.040	0.021 J	ND(0.040)	0.061
	11 - 13	7/27/2004	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	0.028 J	0.013 J	ND(0.040)	0.040
	13 - 15	7/27/2004	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	0.071	0.036 J	ND(0.040)	0.11
	15 - 17	7/27/2004	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	0.13	0.075	ND(0.041)	0.21
	17 - 18.5	7/27/2004	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	0.28	0.15	ND(0.041)	0.44
EB-14	6 - 8	6/30/2004	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	0.50	ND(0.24)	ND(0.24)	0.50
EB-14SW	1 - 3	7/21/2004	ND(23)	ND(23)	ND(23)	ND(23)	89	ND(23)	ND(23)	89
	3 - 5	7/21/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.014 J	ND(0.035)	ND(0.035)	0.014 J
	5 - 6	7/21/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.0096 J	ND(0.034)	ND(0.034)	0.0096 J
	6 - 8	7/21/2004	0.13	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.13
EB-21C	4 - 6	7/1/2004	ND(0.50)	ND(0.50)	ND(0.50)	5.3	ND(0.50)	ND(0.50)	ND(0.50)	5.3
	6 - 8	7/1/2004	ND(0.98)	ND(0.98)	ND(0.98)	8.4	ND(0.98)	ND(0.98)	ND(0.98)	8.4
	10 - 12	7/1/2004	ND(0.54)	ND(0.54)	ND(0.54)	2.9	ND(0.54)	ND(0.54)	ND(0.54)	2.9
	14 - 16	7/1/2004	ND(0.19)	ND(0.19)	ND(0.19)	1.0	ND(0.19)	ND(0.19)	ND(0.19)	1.0
	16 - 18	7/1/2004	ND(0.21)	ND(0.21)	ND(0.21)	0.98	ND(0.21)	ND(0.21)	ND(0.21)	0.98
	18 - 20	7/1/2004	ND(0.28)	ND(0.28)	ND(0.28)	2.2	ND(0.28)	ND(0.28)	ND(0.28)	2.2
	20 - 22	7/1/2004	ND(0.24)	ND(0.24)	ND(0.24)	0.61	ND(0.24)	ND(0.24)	ND(0.24)	0.61
MSSB-B01	9 - 11	2/18/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)
	11 - 13	2/18/2004	ND(0.037)	ND(0.037)	ND(0.037)	0.14	ND(0.037)	0.025 J	ND(0.037)	0.16
	13 - 15	2/18/2004	ND(0.036)	ND(0.036)	ND(0.036)	0.046	ND(0.036)	ND(0.036)	ND(0.036)	0.046
	21 - 23	2/18/2004	ND(0.038)	ND(0.038)	ND(0.038)	0.045	ND(0.038)	ND(0.038)	ND(0.038)	0.045
	23 - 25	2/18/2004	ND(0.037)	ND(0.037)	ND(0.037)	0.013 J	ND(0.037)	ND(0.037)	ND(0.037)	0.013 J
	25 - 27	2/18/2004	ND(0.034)	ND(0.034)	ND(0.034)	0.012 J	ND(0.034)	ND(0.034)	ND(0.034)	0.012 J

TABLE 5
SUMMARY OF PDI PCB SAMPLE DATA - MILL STREET AREA SUBSURFACE SOILS

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
MSSB-B06	15 - 17	8/5/2004	ND(0.038) [ND(0.038)]	ND(0.038) [ND(0.038)]	ND(0.038) [ND(0.038)]	ND(0.038) [ND(0.038)]	ND(0.056) [ND(0.038)]	ND(0.038) [ND(0.038)]	ND(0.038) [ND(0.038)]	ND(0.056) [ND(0.038)]
	17 - 19	8/5/2004	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)
	19 - 21	8/5/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.16	ND(0.038)	ND(0.038)	0.16
	21 - 23	8/5/2004	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)
	23 - 23.5	8/5/2004	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)
MSSB-B07	1 - 3	2/18/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.076	0.025 J	ND(0.035)	0.10
	3 - 5	2/18/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.11	0.065	ND(0.034)	0.18
	5 - 7	2/18/2004	ND(0.034)	ND(0.034)	ND(0.034)	0.046 JN	ND(0.034)	ND(0.034)	ND(0.034)	0.046 JN
	7 - 9	2/18/2004	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)
	9 - 11	2/18/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)
	11 - 13	2/18/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
	13 - 15	2/18/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)
	15 - 17	2/18/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)
	17 - 19	2/18/2004	ND(0.037)	ND(0.037)	ND(0.037)	0.041	ND(0.037)	ND(0.037)	ND(0.037)	0.041
	19 - 21	2/18/2004	ND(0.035)	ND(0.035)	ND(0.035)	0.014 J	ND(0.035)	ND(0.035)	ND(0.035)	0.014 J
	21 - 23	2/18/2004	ND(0.036)	ND(0.036)	ND(0.036)	0.031 J	ND(0.036)	ND(0.036)	ND(0.036)	0.031 J
	23 - 25	2/18/2004	ND(0.039)	ND(0.039)	ND(0.039)	0.076	ND(0.039)	ND(0.039)	ND(0.039)	0.076
	25 - 27	2/18/2004	ND(0.043)	ND(0.043)	ND(0.043)	0.016 J	ND(0.043)	ND(0.043)	ND(0.043)	0.016 J
	27 - 28	2/18/2004	ND(0.043)	ND(0.043)	ND(0.043)	0.045	ND(0.043)	ND(0.043)	ND(0.043)	0.045
MSSB-B09	1 - 3	2/19/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)
	3 - 5	2/19/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)
	5 - 7	2/19/2004	ND(0.036)	ND(0.036)	ND(0.036)	0.071 JN	ND(0.036)	0.014 J	ND(0.036)	0.084 JN
	7 - 9	2/19/2004	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)
	9 - 11	2/19/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)
	11 - 13	2/19/2004	ND(0.036) [ND(0.035)]	ND(0.036) [ND(0.035)]	ND(0.036) [ND(0.035)]	ND(0.036) [ND(0.035)]	ND(0.036) [ND(0.035)]	ND(0.036) [ND(0.035)]	ND(0.036) [ND(0.035)]	ND(0.036) [ND(0.035)]
	13 - 14	2/19/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
MSSB-B10	1 - 3	8/5/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.11	0.034	ND(0.034)	0.14
	3 - 5	8/5/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)
	5 - 7	8/5/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.031 J	0.019 J	ND(0.038)	0.050
MSSB-B11	1 - 3	2/18/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.32	0.14	ND(0.035)	0.46
	3 - 5	2/18/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)
	5 - 7	2/18/2004	ND(0.036)	ND(0.036)	ND(0.036)	0.013 J	ND(0.036)	ND(0.036)	ND(0.036)	0.013 J
	7 - 9	2/18/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)
	9 - 11	2/18/2004	ND(0.038)	ND(0.038)	ND(0.038)	0.045 JN	ND(0.038)	ND(0.038)	ND(0.038)	0.045 JN
	11 - 13	2/18/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)
	13 - 15	2/18/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)
	15 - 17	2/18/2004	ND(0.036)	ND(0.036)	ND(0.036)	0.064	ND(0.036)	ND(0.036)	ND(0.036)	0.064
	17 - 19	2/18/2004	ND(0.038) [ND(0.038)]	ND(0.038) [ND(0.038)]	ND(0.038) [ND(0.038)]	0.30 [0.32]	ND(0.038) [ND(0.038)]	ND(0.038) [ND(0.038)]	ND(0.038) [ND(0.038)]	0.30 [0.32]
	19 - 21	2/18/2004	ND(0.040)	ND(0.040)	ND(0.040)	0.40	ND(0.040)	ND(0.040)	ND(0.040)	0.40
	21 - 23	2/18/2004	ND(0.039)	ND(0.039)	ND(0.039)	0.14	ND(0.039)	ND(0.039)	ND(0.039)	0.14
	23 - 25	2/18/2004	ND(0.040)	ND(0.040)	ND(0.040)	0.093	ND(0.040)	ND(0.040)	ND(0.040)	0.093
	25 - 27	2/18/2004	ND(0.038)	ND(0.038)	ND(0.038)	0.14	ND(0.038)	ND(0.038)	ND(0.038)	0.14
	27 - 28	2/18/2004	ND(0.035)	ND(0.035)	ND(0.035)	0.15	ND(0.035)	ND(0.035)	ND(0.035)	0.15
MSSB-B12	7 - 9	8/5/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)
	9 - 11	8/5/2004	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)
	11 - 13	8/5/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)
	13 - 15	8/5/2004	ND(0.25)	ND(0.25)	ND(0.25)	0.97	ND(0.25)	ND(0.25)	ND(0.25)	0.97
	15 - 17	8/5/2004	ND(0.26)	ND(0.26)	ND(0.26)	5.4	ND(0.26)	ND(0.26)	ND(0.26)	5.4
	17 - 19	8/5/2004	ND(0.040)	ND(0.040)	ND(0.040)	0.14	ND(0.040)	ND(0.040)	ND(0.040)	0.14
	19 - 21	8/5/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.14	ND(0.037)	ND(0.037)	0.14
	21 - 23	8/5/2004	ND(0.22)	ND(0.22)	ND(0.22)	0.54	ND(0.22)	ND(0.22)	ND(0.22)	0.54

TABLE 5
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FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
MSSB-B13	1 - 3	2/12/2004	ND(0.036)	ND(0.036)	ND(0.036)	0.034 J	ND(0.036)	ND(0.036)	ND(0.036)	0.034 J
	3 - 5	2/12/2004	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	0.053 [0.055]	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	0.053 [0.055]
	5 - 7	2/12/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)
	7 - 9	2/12/2004	ND(0.039)	ND(0.039)	ND(0.039)	0.13	ND(0.039)	ND(0.039)	ND(0.039)	0.13
	9 - 11	2/12/2004	ND(0.26)	ND(0.26)	ND(0.26)	2.2	ND(0.26)	ND(0.26)	ND(0.26)	2.2
	11 - 13	2/12/2004	ND(0.038)	ND(0.038)	ND(0.038)	0.13	ND(0.038)	ND(0.038)	ND(0.038)	0.13
	13 - 15	2/12/2004	0.90	ND(0.21)	ND(0.21)	ND(0.21)	ND(0.21)	ND(0.21)	ND(0.21)	0.90
	15 - 17	2/12/2004	0.36	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	0.36
	17 - 19	2/12/2004	ND(0.035)	ND(0.035)	ND(0.035)	0.054	ND(0.035)	ND(0.035)	ND(0.035)	0.054
	19 - 21	2/12/2004	ND(0.038)	ND(0.038)	ND(0.038)	0.60	ND(0.038)	ND(0.038)	ND(0.038)	0.60
	21 - 21.6	2/12/2004	ND(0.037)	ND(0.037)	ND(0.037)	0.13	ND(0.037)	ND(0.037)	ND(0.037)	0.13
MSSB-B15	1 - 3	2/12/2004	ND(0.036)	ND(0.036)	ND(0.036)	0.089	ND(0.036)	ND(0.036)	ND(0.036)	0.089
	3 - 5	2/12/2004	ND(0.034)	ND(0.034)	ND(0.034)	0.18	ND(0.034)	ND(0.034)	ND(0.034)	0.18
	5 - 7	2/12/2004	ND(0.035)	ND(0.035)	ND(0.035)	0.056	ND(0.035)	ND(0.035)	ND(0.035)	0.056
	7 - 9	2/12/2004	ND(0.040)	ND(0.040)	ND(0.040)	0.26	ND(0.040)	ND(0.040)	ND(0.040)	0.26
	9 - 11	2/12/2004	ND(0.035)	ND(0.035)	ND(0.035)	0.032 J	ND(0.035)	ND(0.035)	ND(0.035)	0.032 J
	11 - 13	2/12/2004	ND(0.036)	ND(0.036)	ND(0.036)	0.086	ND(0.036)	ND(0.036)	ND(0.036)	0.086
	13 - 15	2/12/2004	ND(0.036)	ND(0.036)	ND(0.036)	0.077	ND(0.036)	ND(0.036)	ND(0.036)	0.077
	15 - 17	2/12/2004	ND(0.037)	ND(0.037)	ND(0.037)	0.058	ND(0.037)	ND(0.037)	ND(0.037)	0.058
	17 - 19	2/12/2004	ND(0.036)	ND(0.036)	ND(0.036)	0.035 J	ND(0.036)	ND(0.036)	ND(0.036)	0.035 J
	19 - 21	2/12/2004	ND(0.042)	ND(0.042)	ND(0.042)	0.11	ND(0.042)	ND(0.042)	ND(0.042)	0.11
	21 - 21.3	2/12/2004	ND(0.036)	ND(0.036)	ND(0.036)	0.32	ND(0.036)	ND(0.036)	ND(0.036)	0.32
MSSB-B17	1 - 3	2/12/2004	ND(0.36)	ND(0.36)	ND(0.36)	2.0	ND(0.36)	ND(0.36)	ND(0.36)	2.0
	3 - 5	2/12/2004	ND(0.24)	ND(0.24)	ND(0.24)	2.7	ND(0.24)	ND(0.24)	ND(0.24)	2.7
	5 - 7	2/12/2004	ND(0.039)	ND(0.039)	ND(0.039)	0.088	ND(0.039)	ND(0.039)	ND(0.039)	0.088
	7 - 9	2/12/2004	ND(0.038)	ND(0.038)	ND(0.038)	0.34	ND(0.038)	ND(0.038)	ND(0.038)	0.34
	9 - 11	2/12/2004	ND(0.049)	ND(0.049)	ND(0.049)	0.098	ND(0.049)	ND(0.049)	ND(0.049)	0.098
	11 - 13	2/12/2004	ND(0.036)	ND(0.036)	ND(0.036)	0.27	ND(0.036)	ND(0.036)	ND(0.036)	0.27
	13 - 15	2/12/2004	ND(0.038)	ND(0.038)	ND(0.038)	0.062	ND(0.038)	ND(0.038)	ND(0.038)	0.062
	15 - 17	2/12/2004	ND(0.052)	ND(0.052)	ND(0.052)	0.078	ND(0.052)	ND(0.052)	ND(0.052)	0.078
	17 - 19	2/12/2004	ND(0.036)	ND(0.036)	ND(0.036)	0.038	ND(0.036)	ND(0.036)	ND(0.036)	0.038
	19 - 19.6	2/12/2004	ND(0.035)	ND(0.035)	ND(0.035)	0.044	ND(0.035)	ND(0.035)	ND(0.035)	0.044
MSSB-B17N	1 - 2	7/9/2004	ND(0.034) [ND(0.033)]	ND(0.034) [ND(0.033)]	ND(0.034) [ND(0.033)]	ND(0.034) [ND(0.033)]	0.026 J [0.022 J]	ND(0.034) [ND(0.033)]	ND(0.034) [ND(0.033)]	0.026 J [0.022 J]
MSSB-B18	1 - 2	7/7/2004	ND(0.034)	ND(0.034)	ND(0.034)	0.042	ND(0.034)	ND(0.034)	ND(0.034)	0.042
MSSB-B19	1 - 2	7/7/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
MSSB-B20	1 - 2	7/7/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)
MSSB-B21	1 - 2	7/7/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.043)	ND(0.033)	ND(0.033)	ND(0.043)
MSSB-C01	1 - 3	1/13/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.089	ND(0.036)	ND(0.036)	0.089
	3 - 5	1/13/2004	ND(0.034)	ND(0.034)	ND(0.034)	0.078	ND(0.034)	ND(0.034)	ND(0.034)	0.078
	5 - 7	1/13/2004	ND(0.034)	ND(0.034)	ND(0.034)	0.031 J	ND(0.034)	ND(0.034)	ND(0.034)	0.031 J
	7 - 9	1/13/2004	ND(0.034)	ND(0.034)	ND(0.034)	0.033 J	ND(0.034)	0.018 J	ND(0.034)	0.050
	9 - 11	1/13/2004	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	0.068	ND(0.040)	ND(0.040)	0.068
	11 - 13	1/13/2004	ND(0.57)	ND(0.57)	ND(0.57)	ND(0.57)	2.5	1.9	ND(0.57)	4.4
	13 - 15	1/13/2004	ND(0.037)	ND(0.037)	ND(0.037)	0.038	ND(0.037)	ND(0.037)	ND(0.037)	0.038
	15 - 17	1/13/2004	ND(0.037)	ND(0.037)	ND(0.037)	0.087	ND(0.037)	0.047	ND(0.037)	0.13
	17 - 19	1/13/2004	ND(0.036)	ND(0.036)	ND(0.036)	0.030 J	ND(0.036)	ND(0.036)	ND(0.036)	0.030 J
	19 - 21	1/13/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.031 J	ND(0.035)	ND(0.035)	0.031 J
	21 - 23	1/13/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.019 J	ND(0.037)	ND(0.037)	0.019 J
	23 - 25	1/13/2004	ND(2.2)	ND(2.2)	ND(2.2)	6.2	ND(2.2)	3.4	ND(2.2)	9.5
	25 - 27	1/13/2004	ND(0.037)	ND(0.037)	ND(0.037)	0.12	ND(0.037)	0.062	ND(0.037)	0.18
	27 - 29	1/13/2004	ND(0.22)	ND(0.22)	ND(0.22)	0.29	ND(0.22)	0.20 J	ND(0.22)	0.49
	29 - 31	1/13/2004	ND(0.039) [ND(0.039)]	ND(0.039) [ND(0.039)]	ND(0.039) [ND(0.039)]	0.018 J [0.045]	ND(0.039) [ND(0.039)]	ND(0.039) [0.022 J]	ND(0.039) [ND(0.039)]	0.018 J [0.067]
	31 - 33	1/13/2004	ND(0.040)	ND(0.040)	ND(0.040)	0.029 J	ND(0.040)	ND(0.040)	ND(0.040)	0.029 J
	33 - 35	1/13/2004	ND(0.039)	ND(0.039)	ND(0.039)	0.042	ND(0.039)	0.024 J	ND(0.039)	0.067
	35 - 36.5	1/13/2004	ND(0.036)	ND(0.036)	ND(0.036)	0.036	ND(0.036)	0.020 J	ND(0.036)	0.056

TABLE 5
SUMMARY OF PDI PCB SAMPLE DATA - MILL STREET AREA SUBSURFACE SOILS

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
MSSB-C03	1 - 3	1/20/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.055	0.044	ND(0.036)	0.099
	3 - 5	1/20/2004	ND(0.034)	ND(0.034)	ND(0.034)	0.021 J	ND(0.034)	ND(0.034)	ND(0.034)	0.021 J
	5 - 7	1/20/2004	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]
	7 - 9	1/20/2004	ND(0.034)	ND(0.034)	ND(0.034)	0.049	ND(0.034)	0.020 J	ND(0.034)	0.068
	9 - 11	1/20/2004	ND(0.041)	ND(0.041)	ND(0.041)	0.012 J	ND(0.041)	ND(0.041)	ND(0.041)	0.012 J
	11 - 13	1/20/2004	ND(0.040)	ND(0.040)	ND(0.040)	0.023 J	ND(0.040)	ND(0.040)	ND(0.040)	0.023 J
	13 - 15	1/20/2004	ND(0.038)	ND(0.038)	ND(0.038)	0.016 J	ND(0.038)	ND(0.038)	ND(0.038)	0.016 J
	15 - 17	1/20/2004	ND(0.041)	ND(0.041)	ND(0.041)	0.016 J	ND(0.041)	ND(0.041)	ND(0.041)	0.016 J
	17 - 19	1/20/2004	ND(0.038)	ND(0.038)	ND(0.038)	0.016 J	ND(0.038)	ND(0.038)	ND(0.038)	0.016 J
	19 - 21	1/20/2004	ND(0.041)	ND(0.041)	ND(0.041)	0.026 J	ND(0.041)	ND(0.041)	ND(0.041)	0.026 J
	21 - 23	1/20/2004	ND(0.042)	ND(0.042)	ND(0.042)	0.018 J	ND(0.042)	ND(0.042)	ND(0.042)	0.018 J
	23 - 25	1/20/2004	ND(0.042)	ND(0.042)	ND(0.042)	0.028 J	ND(0.042)	ND(0.042)	ND(0.042)	0.028 J
	25 - 27	1/20/2004	ND(0.039)	ND(0.039)	ND(0.039)	0.015 J	ND(0.039)	ND(0.039)	ND(0.039)	0.015 J
	27 - 27.4	1/20/2004	ND(0.039)	ND(0.039)	ND(0.039)	0.014 J	ND(0.039)	ND(0.039)	ND(0.039)	0.014 J
MSSB-C05	1 - 3	1/6/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.022 J	ND(0.036)	ND(0.036)	0.022 J
	3 - 5	1/6/2004	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	0.012 J	ND(0.039)	ND(0.039)	0.012 J
	5 - 7	1/6/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.016 J	0.011 J	ND(0.036)	0.027 J
	7 - 9	1/6/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.015 J	ND(0.037)	ND(0.037)	0.015 J
	9 - 11	1/6/2004	ND(0.043)	ND(0.043)	ND(0.043)	ND(0.043)	0.15	0.12	ND(0.043)	0.28
	11 - 13	1/6/2004	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	0.021 J	ND(0.040)	ND(0.040)	0.021 J
	13 - 15	1/6/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.018 J	ND(0.036)	ND(0.036)	0.018 J
	15 - 17	1/6/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.031 J	ND(0.038)	ND(0.038)	0.031 J
	17 - 19	1/6/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.022 J	0.020 J	ND(0.036)	0.042
	19 - 21	1/6/2004	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	0.034 J	0.028 J	ND(0.039)	0.062
	21 - 23	1/6/2004	ND(0.036)	ND(0.036)	ND(0.036)	0.027 J	ND(0.036)	ND(0.036)	ND(0.036)	0.027 J
	23 - 23.4	1/6/2004	ND(0.036)	ND(0.036)	ND(0.036)	0.021 JP	ND(0.036)	ND(0.036)	ND(0.036)	0.021 J
MSSB-C06	1 - 3	2/16/2004	ND(300)	ND(300)	ND(300)	ND(300)	1500	ND(300)	ND(300)	1500
	3 - 5	2/16/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.76	ND(0.035)	ND(0.035)	0.76
	5 - 7	2/16/2004	ND(0.035) [ND(0.036)]	ND(0.035) [ND(0.036)]	ND(0.035) [ND(0.036)]	ND(0.035) [ND(0.036)]	0.10 [0.14]	ND(0.035) [ND(0.036)]	ND(0.035) [ND(0.036)]	0.10 [0.14]
	7 - 9	2/16/2004	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	0.12	ND(0.040)	ND(0.040)	0.12
	9 - 11	2/16/2004	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)
	11 - 13	2/16/2004	ND(0.037)	ND(0.037)	ND(0.037)	0.42	ND(0.037)	ND(0.037)	ND(0.037)	0.42
	13 - 15	2/16/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.024 J	ND(0.037)	ND(0.037)	0.024 J
	15 - 17	2/16/2004	ND(0.035)	ND(0.035)	ND(0.035)	0.095	ND(0.035)	ND(0.035)	ND(0.035)	0.095
	17 - 19	2/16/2004	ND(0.038)	ND(0.038)	ND(0.038)	0.073	ND(0.038)	ND(0.038)	ND(0.038)	0.073
	19 - 21	2/16/2004	ND(0.037)	ND(0.037)	ND(0.037)	0.19	ND(0.037)	ND(0.037)	ND(0.037)	0.19
	21 - 22.5	2/16/2004	ND(0.036)	ND(0.036)	ND(0.036)	0.16	ND(0.036)	ND(0.036)	ND(0.036)	0.16
MSSB-C06N	1 - 3	7/9/2004	ND(0.66)	ND(0.66)	ND(0.66)	ND(0.66)	9.6	ND(0.66)	ND(0.66)	9.6
	3 - 5	7/9/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	0.038	ND(0.033)	ND(0.033)	0.038
MSSB-C07	1 - 3	1/6/2004	ND(1200)	ND(1200)	ND(1200)	ND(1200)	12000	ND(1200)	ND(1200)	12000
	3 - 5	1/6/2004	ND(7.0)	ND(7.0)	ND(7.0)	ND(7.0)	13	ND(7.0)	ND(7.0)	13
	5 - 7	1/6/2004	ND(35)	ND(35)	ND(35)	ND(35)	320	ND(35)	ND(35)	320
	7 - 9	1/6/2004	ND(200)	ND(200)	ND(200)	ND(200)	420	ND(200)	ND(200)	420
	9 - 11	1/6/2004	ND(930)	ND(930)	ND(930)	3600	ND(930)	ND(930)	ND(930)	3600
	11 - 13	1/6/2004	ND(1100)	ND(1100)	ND(1100)	8800	ND(1100)	ND(1100)	ND(1100)	8800
	13 - 15	1/6/2004	ND(5100)	ND(5100)	ND(5100)	25000	ND(5100)	ND(5100)	ND(5100)	25000
	15 - 17	1/6/2004	ND(1000)	ND(1000)	ND(1000)	9400	ND(1000)	ND(1000)	ND(1000)	9400
	17 - 19	1/6/2004	ND(7.5)	ND(7.5)	ND(7.5)	13	ND(7.5)	ND(7.5)	ND(7.5)	13
	19 - 21	1/6/2004	ND(38)	ND(38)	ND(38)	290	ND(38)	ND(38)	ND(38)	290
	21 - 21.4	1/6/2004	ND(6.7)	ND(6.7)	ND(6.7)	13	ND(6.7)	ND(6.7)	ND(6.7)	13

TABLE 5
SUMMARY OF PDI PCB SAMPLE DATA - MILL STREET AREA SUBSURFACE SOILS

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
MSSB-C07E	1 - 3	7/12/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.28 J	ND(0.034)	ND(0.034)	0.28 J
	3 - 5	7/12/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	0.086	ND(0.033)	ND(0.033)	0.086
	5 - 7	7/12/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	0.17 J	ND(0.033)	ND(0.033)	0.17 J
	7 - 9	7/12/2004	ND(0.037) [ND(72)]	ND(0.037) [ND(72)]	ND(0.037) [ND(72)]	ND(0.037) [ND(72)]	0.034 J [230 J]	ND(0.037) [63 J]	ND(0.037) [ND(72)]	0.034 J [290 J]
	7 - 9	7/12/2004	ND(0.037) J [ND(0.035) J]	ND(0.037) J [ND(0.035) J]	ND(0.037) J [ND(0.035) J]	ND(0.037) J [ND(0.035) J]	0.031 J [0.041 J]	0.013 J [0.016 J]	ND(0.037) J [ND(0.035) J]	0.044 J [0.057 J]
	9 - 11	7/12/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.054	ND(0.037)	ND(0.037)	0.054
	11 - 13	7/12/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.019 J	ND(0.037)	ND(0.037)	0.019 J
	13 - 15	7/12/2004	ND(0.046)	ND(0.046)	ND(0.046)	ND(0.046)	ND(0.046)	ND(0.046)	ND(0.046)	ND(0.046)
	15 - 17	7/12/2004	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)
	17 - 19	7/12/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)
	19 - 21	7/12/2004	ND(0.039)	ND(0.039)	ND(0.039)	0.040	ND(0.039)	ND(0.039)	ND(0.039)	0.040
	21 - 22.7	7/12/2004	ND(0.034)	ND(0.034)	ND(0.034)	0.033 J	ND(0.034)	ND(0.034)	ND(0.034)	0.033 J
MSSB-C07NW	3 - 5	7/8/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.020 J	ND(0.035)	ND(0.035)	0.020 J
	5 - 7	7/8/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.30	0.16	ND(0.035)	0.47
	7 - 9	7/8/2004	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)
	9 - 11	7/8/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)
	11 - 13	7/8/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)
	13 - 15	7/8/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.017 J	ND(0.036)	ND(0.036)	0.017 J
	15 - 17	7/8/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
	17 - 19	7/8/2004	ND(4.2)	ND(4.2)	ND(4.2)	ND(4.2)	ND(4.2)	28	ND(4.2)	28
	19 - 21	7/8/2004	ND(5.7)	ND(5.7)	ND(5.7)	ND(5.7)	ND(5.7)	39	ND(5.7)	39
	21 - 23	7/8/2004	ND(4.4)	ND(4.4)	ND(4.4)	ND(4.4)	ND(4.4)	30	ND(4.4)	30
	23 - 25	7/8/2004	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	0.016 J	ND(0.039)	ND(0.039)	0.016 J
	25 - 27	7/8/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.053	ND(0.037)	ND(0.037)	0.053
	27 - 27.5	7/8/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)
MSSB-C07W	1 - 3	7/28/2004	ND(12)	ND(12)	ND(12)	ND(12)	56	ND(12)	ND(12)	56
	3 - 5	7/28/2004	ND(13)	ND(13)	ND(13)	ND(13)	84	ND(13)	ND(13)	84
	5 - 7	7/28/2004	ND(0.21) [ND(0.20)]	ND(0.21) [ND(0.20)]	ND(0.21) [ND(0.20)]	ND(0.21) [ND(0.20)]	0.098 J [0.13 J]	ND(0.21) [ND(0.20)]	ND(0.21) [ND(0.20)]	0.098 J [0.13 J]
	7 - 9	7/28/2004	ND(0.25)	ND(0.25)	ND(0.25)	ND(0.25)	3.0	ND(0.25)	ND(0.25)	3.0
	9 - 11	7/28/2004	1.1	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	1.1
	11 - 13	7/28/2004	0.71	ND(0.26)	ND(0.26)	ND(0.26)	ND(0.26)	ND(0.26)	ND(0.26)	0.71
	13 - 15	7/28/2004	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)
	15 - 17	7/28/2004	0.68	ND(0.26)	ND(0.26)	ND(0.26)	ND(0.26)	ND(0.26)	ND(0.26)	0.68
	17 - 19	7/28/2004	0.56	ND(0.25)	ND(0.25)	ND(0.25)	ND(0.25)	ND(0.25)	ND(0.25)	0.56
	19 - 21	7/28/2004	0.36	ND(0.26)	ND(0.26)	ND(0.26)	ND(0.26)	ND(0.26)	ND(0.26)	0.36
MSSB-C08	1 - 3	2/16/2004	ND(0.28)	ND(0.28)	ND(0.28)	ND(0.28)	2.0	ND(0.28)	ND(0.28)	2.0
	3 - 5	2/16/2004	ND(5.1)	ND(5.1)	ND(5.1)	ND(5.1)	45	ND(5.1)	ND(5.1)	45
	5 - 7	2/16/2004	ND(0.21)	ND(0.21)	ND(0.21)	ND(0.21)	2.4	ND(0.21)	ND(0.21)	2.4
	7 - 9	2/16/2004	ND(0.038)	ND(0.038)	ND(0.038)	0.064	ND(0.038)	ND(0.038)	ND(0.038)	0.064
	9 - 11	2/16/2004	ND(0.038)	ND(0.038)	ND(0.038)	0.12	ND(0.038)	ND(0.038)	ND(0.038)	0.12
	11 - 13	2/16/2004	ND(0.039)	ND(0.039)	ND(0.039)	0.034 J	ND(0.039)	ND(0.039)	ND(0.039)	0.034 J
	13 - 15	2/16/2004	ND(0.039)	ND(0.039)	ND(0.039)	0.12	ND(0.039)	ND(0.039)	ND(0.039)	0.12
	15 - 17	2/16/2004	ND(0.037)	ND(0.037)	ND(0.037)	0.22	ND(0.037)	ND(0.037)	ND(0.037)	0.22
	17 - 19	2/16/2004	ND(0.037)	ND(0.037)	ND(0.037)	0.074	ND(0.037)	ND(0.037)	ND(0.037)	0.074
	19 - 20	2/16/2004	ND(0.038)	ND(0.038)	ND(0.038)	0.086	ND(0.038)	ND(0.038)	ND(0.038)	0.086
MSSB-C08N	3 - 5	7/8/2004	ND(0.034)	ND(0.034)	ND(0.034)	0.011 J	ND(0.034)	ND(0.034)	ND(0.034)	0.011 J
	5 - 7	7/8/2004	ND(0.035)	ND(0.035)	ND(0.035)	0.011 J	ND(0.035)	ND(0.035)	ND(0.035)	0.011 J
	7 - 9	7/8/2004	ND(0.035)	ND(0.035)	ND(0.035)	0.011 J	ND(0.035)	ND(0.035)	ND(0.035)	0.011 J
	9 - 11	7/8/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
	11 - 13	7/8/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.035 J	ND(0.037)	ND(0.037)	0.035 J
	13 - 15	7/8/2004	ND(0.038) [ND(0.037)]	ND(0.038) [ND(0.037)]	ND(0.038) [ND(0.037)]	ND(0.038) [0.011 J]	0.011 J [ND(0.037)]	ND(0.038) [ND(0.037)]	ND(0.038) [ND(0.037)]	0.011 J [0.011 J]
	15 - 17	7/8/2004	ND(0.039)	ND(0.039)	ND(0.039)	0.10	ND(0.039)	ND(0.039)	ND(0.039)	0.10
	17 - 19	7/8/2004	ND(0.036)	ND(0.036)	ND(0.036)	0.20	ND(0.036)	ND(0.036)	ND(0.036)	0.20
	19 - 21	7/8/2004	ND(0.042)	ND(0.042)	ND(0.042)	0.17	ND(0.042)	ND(0.042)	ND(0.042)	0.17
	21 - 23	7/8/2004	ND(0.044)	ND(0.044)	ND(0.044)	0.15	ND(0.044)	ND(0.044)	ND(0.044)	0.15

TABLE 5
SUMMARY OF PDI PCB SAMPLE DATA - MILL STREET AREA SUBSURFACE SOILS

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
MSSB-C09	1 - 3	1/13/2004	ND(5.1) [ND(5.1)]	ND(5.1) [ND(5.1)]	ND(5.1) [ND(5.1)]	ND(5.1) [ND(5.1)]	29 [30]	ND(5.1) [ND(5.1)]	ND(5.1) [ND(5.1)]	29 [30]
	11 - 13	1/13/2004	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	0.087	ND(0.041)	ND(0.041)	0.087
	19 - 21	1/13/2004	ND(0.037)	ND(0.037)	ND(0.037)	0.041	ND(0.037)	ND(0.037)	ND(0.037)	0.041
MSSB-C10	1 - 3	7/21/2004	ND(0.23)	ND(0.23)	ND(0.23)	ND(0.23)	1.2	ND(0.23)	ND(0.23)	1.2
	3 - 5	7/21/2004	ND(0.42)	ND(0.42)	ND(0.42)	ND(0.42)	8.2	ND(0.42)	ND(0.42)	8.2
	5 - 7	7/21/2004	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	5.9	ND(0.24)	ND(0.24)	5.9
	7 - 8	7/21/2004	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	4.9	ND(0.24)	ND(0.24)	4.9
	8 - 10	7/21/2004	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	0.086	ND(0.039)	ND(0.039)	0.086
MSSB-C10NE	1 - 3	7/13/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.38	ND(0.036)	ND(0.036)	0.38
	3 - 5	7/13/2004	ND(170)	ND(170)	ND(170)	ND(170)	430	460	ND(170)	880
	5 - 7	7/13/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.031 J	ND(0.037)	ND(0.037)	0.031 J
	7 - 9	7/13/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.034 J	ND(0.036)	ND(0.036)	0.034 J
	9 - 11	7/13/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)
	11 - 13	7/13/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.011 J	ND(0.034)	ND(0.034)	0.011 J
	13 - 15	7/13/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.15	0.077	ND(0.036)	0.22
MSSB-C11	1 - 3	1/8/2004	ND(37)	ND(37)	ND(37)	ND(37)	110	ND(37)	ND(37)	110
	3 - 5	1/8/2004	ND(200) [ND(170)]	ND(200) [ND(170)]	ND(200) [ND(170)]	ND(200) [ND(170)]	1100 [790]	ND(200) [ND(170)]	ND(200) [ND(170)]	1100 [790]
	5 - 7	1/8/2004	ND(0.37)	ND(0.37)	ND(0.37)	ND(0.37)	2.1	ND(0.37)	ND(0.37)	2.1
	7 - 9	1/8/2004	ND(0.15)	ND(0.15)	ND(0.15)	ND(0.15)	0.42	ND(0.15)	ND(0.15)	0.42
	9 - 11	1/8/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.10	ND(0.038)	ND(0.038)	0.10
	11 - 13	1/8/2004	ND(0.76)	ND(0.76)	ND(0.76)	ND(0.76)	3.7	ND(0.76)	ND(0.76)	3.7
	13 - 15	1/8/2004	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	0.45	ND(0.041)	ND(0.041)	0.45
	15 - 17	1/8/2004	ND(0.081)	ND(0.081)	ND(0.081)	ND(0.081)	0.42	ND(0.081)	ND(0.081)	0.42
	17 - 19	1/8/2004	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	0.31	ND(0.040)	ND(0.040)	0.31
	19 - 21	1/8/2004	ND(0.036)	ND(0.036)	ND(0.036)	0.18	ND(0.036)	0.087	ND(0.036)	0.26
MSSB-C11N	3 - 5	7/7/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)
	5 - 7	7/7/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)
	7 - 9	7/7/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.018 J	ND(0.034)	ND(0.034)	0.018 J
	9 - 11	7/7/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.12	ND(0.035)	ND(0.035)	0.12
	11 - 13	7/7/2004	ND(0.22)	ND(0.22)	ND(0.22)	ND(0.22)	0.38	ND(0.22)	ND(0.22)	0.38
	13 - 15	7/7/2004	ND(0.040)	ND(0.040)	ND(0.040)	0.027 J	ND(0.040)	ND(0.040)	ND(0.040)	0.027 J
	15 - 17	7/7/2004	ND(0.25)	ND(0.25)	ND(0.25)	0.57	ND(0.25)	ND(0.25)	ND(0.25)	0.57
	17 - 19	7/7/2004	ND(0.25) [ND(0.22)]	ND(0.25) [ND(0.22)]	ND(0.25) [ND(0.22)]	ND(0.25) [ND(0.22)]	0.67 J [0.37 J]	ND(0.25) [ND(0.22)]	ND(0.25) [ND(0.22)]	0.67 J [0.37 J]
	19 - 21	7/7/2004	ND(0.26)	ND(0.26)	ND(0.26)	0.48	ND(0.26)	ND(0.26)	ND(0.26)	0.48
	21 - 23	7/7/2004	ND(0.25)	ND(0.25)	ND(0.25)	0.38	ND(0.25)	ND(0.25)	ND(0.25)	0.38
	23 - 23.8	7/7/2004	ND(0.25)	ND(0.25)	ND(0.25)	0.35	ND(0.25)	ND(0.25)	ND(0.25)	0.35
MSSB-C11W	1 - 3	7/22/2004	ND(980)	ND(980)	ND(980)	ND(980)	2100	ND(980)	ND(980)	2100
	3 - 5	7/22/2004	ND(13)	ND(13)	ND(13)	ND(13)	36	ND(13)	ND(13)	36
	5 - 7	7/22/2004	ND(0.21)	ND(0.21)	ND(0.21)	ND(0.21)	1.4	ND(0.21)	ND(0.21)	1.4
	7 - 9	7/22/2004	ND(0.25)	ND(0.25)	ND(0.25)	ND(0.25)	1.5	ND(0.25)	ND(0.25)	1.5
	9 - 11	7/22/2004	ND(0.27)	ND(0.27)	ND(0.27)	ND(0.27)	2.1	ND(0.27)	ND(0.27)	2.1
	11 - 13	7/22/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)
	13 - 15	7/22/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)
MSSB-C12	1 - 3	2/12/2004	ND(290)	ND(290)	ND(290)	ND(290)	6700	ND(290)	ND(290)	6700
	3 - 5	2/12/2004	ND(530)	ND(530)	ND(530)	ND(530)	12000	ND(530)	ND(530)	12000
	5 - 7	2/12/2004	ND(130)	ND(130)	ND(130)	4700	ND(130)	ND(130)	ND(130)	4700
	7 - 9	2/12/2004	ND(210)	ND(210)	ND(210)	2900	ND(210)	ND(210)	ND(210)	2900
	9 - 11	2/12/2004	ND(110) [ND(100)]	ND(110) [ND(100)]	ND(110) [ND(100)]	2600 [1900]	ND(110) [ND(100)]	ND(110) [ND(100)]	ND(110) [ND(100)]	2600 [1900]
	11 - 13	2/12/2004	ND(260)	ND(260)	ND(260)	5700	ND(260)	ND(260)	ND(260)	5700
	13 - 15	2/12/2004	ND(3.2)	ND(3.2)	ND(3.2)	33	ND(3.2)	ND(3.2)	ND(3.2)	33
	15 - 17	2/12/2004	ND(12)	ND(12)	ND(12)	110	ND(12)	ND(12)	ND(12)	110
	17 - 19	2/12/2004	ND(44)	ND(44)	ND(44)	1400	ND(44)	ND(44)	ND(44)	1400
	19 - 19.8	2/12/2004	ND(120)	ND(120)	ND(120)	1300	ND(120)	ND(120)	ND(120)	1300

TABLE 5
SUMMARY OF PDI PCB SAMPLE DATA - MILL STREET AREA SUBSURFACE SOILS

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
MSSB-C12N	3 - 5	7/8/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.022 J	ND(0.034)	ND(0.034)	0.022 J
	5 - 7	7/8/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.020 J	ND(0.034)	ND(0.034)	0.020 J
	7 - 9	7/8/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.13	ND(0.036)	ND(0.036)	0.13
	9 - 11	7/8/2004	ND(330)	ND(330)	ND(330)	690	ND(330)	ND(330)	ND(330)	690
	11 - 13	7/8/2004	ND(1300)	ND(1300)	ND(1300)	3600	ND(1300)	ND(1300)	ND(1300)	3600
	13 - 15	7/8/2004	ND(11)	ND(11)	ND(11)	43	ND(11)	ND(11)	ND(11)	43
	15 - 17	7/8/2004	ND(14)	ND(14)	ND(14)	57	ND(14)	ND(14)	ND(14)	57
	17 - 19	7/8/2004	ND(5.2)	ND(5.2)	ND(5.2)	18	ND(5.2)	ND(5.2)	ND(5.2)	18
	19 - 21	7/8/2004	ND(24)	ND(24)	ND(24)	120	ND(24)	ND(24)	ND(24)	120
	21 - 23	7/8/2004	ND(0.23)	ND(0.23)	ND(0.23)	0.41	ND(0.23)	ND(0.23)	ND(0.23)	0.41
MSSB-C13	1 - 3	1/8/2004	ND(37)	ND(37)	ND(37)	ND(37)	100	ND(37)	ND(37)	100
	3 - 5	1/8/2004	ND(35)	ND(35)	ND(35)	ND(35)	ND(35)	58	ND(35)	58
	5 - 7	1/8/2004	ND(720)	ND(720)	ND(720)	ND(720)	ND(720)	2300	ND(720)	2300
	7 - 9	1/8/2004	ND(39)	ND(39)	ND(39)	ND(39)	ND(39)	47	ND(39)	47
	9 - 11	1/8/2004	ND(0.37) [ND(0.072)]	ND(0.37) [ND(0.072)]	ND(0.37) [ND(0.072)]	ND(0.37) [ND(0.072)]	0.73 [0.51]	0.56 [0.40]	ND(0.37) [ND(0.072)]	1.3 [0.92]
	11 - 13	1/8/2004	ND(1.9)	ND(1.9)	ND(1.9)	ND(1.9)	9.9	7.5	ND(1.9)	17
	13 - 15	1/8/2004	ND(0.39)	ND(0.39)	ND(0.39)	ND(0.39)	1.4	0.88	ND(0.39)	2.3
	15 - 17	1/8/2004	ND(39)	ND(39)	ND(39)	ND(39)	94	63	ND(39)	160
	17 - 18.7	1/8/2004	ND(1.8)	ND(1.8)	ND(1.8)	ND(1.8)	6.9	4.8	ND(1.8)	12
MSSB-C13N	3 - 5	7/13/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.068	0.033 J	ND(0.035)	0.10
	5 - 7	7/13/2004	ND(0.035) [ND(0.038)]	ND(0.035) [ND(0.038)]	ND(0.035) [ND(0.038)]	ND(0.035) [ND(0.038)]	ND(0.035) [ND(0.038)]	ND(0.035) [ND(0.038)]	ND(0.035) [ND(0.038)]	ND(0.035) [ND(0.038)]
	7 - 9	7/13/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)
	9 - 11	7/13/2004	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)
	11 - 13	7/13/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)
	13 - 15	7/13/2004	1.2	ND(0.22)	ND(0.22)	ND(0.22)	ND(0.22)	ND(0.22)	ND(0.22)	1.2
	15 - 17	7/13/2004	1.3	ND(0.28)	ND(0.28)	ND(0.28)	ND(0.28)	ND(0.28)	ND(0.28)	1.3
	17 - 19	7/13/2004	1.2	ND(0.25)	ND(0.25)	ND(0.25)	ND(0.25)	ND(0.25)	ND(0.25)	1.2
	19 - 19.9	7/13/2004	0.058	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.058
MSSB-C13NE	3 - 5	7/26/2004	ND(1800)	ND(1800)	ND(1800)	ND(1800)	7400	4100	ND(1800)	12000
	5 - 7	7/26/2004	ND(19) [ND(9.7)]	ND(19) [ND(9.7)]	ND(19) [ND(9.7)]	ND(19) [ND(9.7)]	82 J [26 J]	33 J [10 J]	ND(19) [ND(9.7)]	120 J [37 J]
	7 - 9	7/26/2004	ND(24)	ND(24)	ND(24)	ND(24)	90	56	ND(24)	140
	9 - 11	7/26/2004	ND(6.1)	ND(6.1)	ND(6.1)	ND(6.1)	18	14	ND(6.1)	32
	11 - 13	7/26/2004	ND(0.41)	ND(0.41)	ND(0.41)	ND(0.41)	5.7	4.8	ND(0.41)	10
	13 - 15	7/26/2004	ND(0.38)	ND(0.38)	ND(0.38)	ND(0.38)	5.5	4.7	ND(0.38)	10
	15 - 16	7/26/2004	ND(0.22)	ND(0.22)	ND(0.22)	ND(0.22)	4.3	3.8	ND(0.22)	8.1
MSSB-C14	1 - 3	2/12/2004	ND(0.21)	ND(0.21)	ND(0.21)	ND(0.21)	0.86	ND(0.21)	ND(0.21)	0.86
	3 - 5	2/12/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.028 J	ND(0.036)	ND(0.036)	0.028 J
	5 - 7	2/12/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)
	7 - 9	2/12/2004	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)
	9 - 11	2/12/2004	ND(0.039)	ND(0.039)	ND(0.039)	0.051 J	ND(0.039)	ND(0.039)	ND(0.039)	0.051 J
	11 - 13	2/12/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)
	13 - 15	2/12/2004	ND(0.20)	ND(0.20)	ND(0.20)	1.6	ND(0.20)	ND(0.20)	ND(0.20)	1.6
	15 - 17	2/12/2004	ND(0.037)	0.39 JN	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.39 JN
	17 - 19	2/12/2004	ND(0.038)	0.29 JN	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.29 JN
	19 - 20	2/12/2004	ND(0.036)	ND(0.036)	ND(0.036)	0.24	ND(0.036)	ND(0.036)	ND(0.036)	0.24
MSSB-C15	1 - 3	1/6/2004	ND(0.17)	ND(0.17)	ND(0.17)	0.86	ND(0.17)	ND(0.17)	ND(0.17)	0.86
	3 - 5	1/6/2004	ND(0.14)	ND(0.14)	ND(0.14)	0.43	ND(0.14)	ND(0.14)	ND(0.14)	0.43
	5 - 7	1/6/2004	ND(0.034)	ND(0.034)	ND(0.034)	0.24	ND(0.034)	ND(0.034)	ND(0.034)	0.24
	7 - 9	1/6/2004	ND(0.36)	ND(0.36)	ND(0.36)	2.6	ND(0.36)	ND(0.36)	ND(0.36)	2.6
	9 - 11	1/6/2004	ND(0.14)	ND(0.14)	ND(0.14)	0.52	ND(0.14)	ND(0.14)	ND(0.14)	0.52
	11 - 13	1/6/2004	ND(0.15)	ND(0.15)	ND(0.15)	1.3	ND(0.15)	ND(0.15)	ND(0.15)	1.3
	13 - 15	1/6/2004	ND(0.19)	ND(0.19)	ND(0.19)	0.57	ND(0.19)	ND(0.19)	ND(0.19)	0.57
	15 - 17	1/6/2004	ND(0.19)	ND(0.19)	ND(0.19)	1.1	ND(0.19)	ND(0.19)	ND(0.19)	1.1
	17 - 19	1/6/2004	ND(0.14)	ND(0.14)	ND(0.14)	0.40	ND(0.14)	ND(0.14)	ND(0.14)	0.40
	19 - 20.4	1/6/2004	ND(0.14)	ND(0.14)	ND(0.14)	0.68	ND(0.14)	ND(0.14)	ND(0.14)	0.68

TABLE 5
SUMMARY OF PDI PCB SAMPLE DATA - MILL STREET AREA SUBSURFACE SOILS

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
MSSB-C16	1 - 2	4/29/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
MSSB-C17	1 - 3	1/7/2004	ND(0.034)	ND(0.034)	ND(0.034)	0.018 J	ND(0.034)	ND(0.034)	ND(0.034)	0.018 J
	3 - 5	1/7/2004	ND(0.70)	ND(0.70)	ND(0.70)	1.7	ND(0.70)	ND(0.70)	ND(0.70)	1.7
	5 - 7	1/7/2004	ND(0.039) [ND(0.039)]	ND(0.039) [ND(0.039)]	ND(0.039) [ND(0.039)]	0.051 [0.11]	ND(0.039) [ND(0.039)]	0.032 J [ND(0.039)]	ND(0.039) [ND(0.039)]	0.084 [0.11]
	7 - 9	1/7/2004	ND(0.71)	ND(0.71)	ND(0.71)	1.6	ND(0.71)	ND(0.71)	ND(0.71)	1.6
	9 - 11	1/7/2004	ND(0.037)	ND(0.037)	ND(0.037)	0.047	ND(0.037)	ND(0.037)	ND(0.037)	0.047
	11 - 13	1/7/2004	ND(0.18)	ND(0.18)	ND(0.18)	0.25	ND(0.18)	ND(0.18)	ND(0.18)	0.25
	13 - 15	1/7/2004	ND(0.039)	ND(0.039)	ND(0.039)	0.044	ND(0.039)	ND(0.039)	ND(0.039)	0.044
	15 - 17	1/7/2004	ND(0.77)	ND(0.77)	ND(0.77)	1.5	ND(0.77)	ND(0.77)	ND(0.77)	1.5
	17 - 19	1/7/2004	ND(0.037)	ND(0.037)	ND(0.037)	0.060	ND(0.037)	ND(0.037)	ND(0.037)	0.060
	19 - 20.2	1/7/2004	ND(0.38)	ND(0.38)	ND(0.38)	0.26 J	ND(0.38)	ND(0.38)	ND(0.38)	0.26 J
MSSB-C17S	1 - 3	7/22/2004	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	0.025 J [ND(0.037)]	0.021 J [0.022 J]	ND(0.034) [ND(0.034)]	0.047 [ND(0.037)]
	3 - 5	7/22/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	0.0099 J	ND(0.033)	0.0099 J
	5 - 7	7/22/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)
	7 - 9	7/22/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
	9 - 11	7/22/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
	11 - 13	7/22/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
	13 - 15	7/22/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)
	15 - 17	7/22/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)
	17 - 18.5	7/22/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.019 J	ND(0.038)	ND(0.038)	0.019 J
MSSB-C18	1 - 2	4/29/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)
MSSB-C19	1 - 3	1/7/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.041)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.041)
	3 - 5	1/7/2004	ND(0.14)	ND(0.14)	ND(0.14)	0.27	ND(0.14)	ND(0.14)	ND(0.14)	0.27
	5 - 7	1/7/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.042)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.042)
	7 - 9	1/7/2004	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	0.25 [0.29]	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	0.25 [0.29]
	9 - 11	1/7/2004	ND(0.034)	ND(0.034)	ND(0.034)	0.093	ND(0.034)	ND(0.034)	ND(0.034)	0.093
	11 - 13	1/7/2004	ND(0.035)	ND(0.035)	ND(0.035)	0.15	ND(0.035)	ND(0.035)	ND(0.035)	0.15
	13 - 15	1/7/2004	ND(0.040)	ND(0.040)	ND(0.040)	0.14	ND(0.040)	ND(0.040)	ND(0.040)	0.14
	15 - 17	1/7/2004	ND(0.038)	ND(0.038)	ND(0.038)	0.10	ND(0.038)	ND(0.038)	ND(0.038)	0.10
	17 - 19	1/7/2004	ND(0.037)	ND(0.037)	ND(0.037)	0.018 J	ND(0.037)	ND(0.037)	ND(0.037)	0.018 J
	19 - 20.2	1/7/2004	ND(0.036)	ND(0.036)	ND(0.036)	0.032 J	ND(0.036)	ND(0.036)	ND(0.036)	0.032 J
MSSB-C20	1 - 2	4/22/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	0.014 J	0.0092 J	ND(0.033)	0.023 J
MSSB-D04	1 - 2	4/28/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)
MSSB-D04SW	1 - 2	7/1/2004	ND(4.2)	ND(4.2)	ND(4.2)	ND(4.2)	37	ND(4.2)	ND(4.2)	37
	2 - 3	7/1/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	0.054	ND(0.033)	ND(0.033)	0.054
	3 - 5	10/20/05	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)
	5 - 7	10/20/05	ND(0.036)	ND(0.036)	0.014 J	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.014 J
	7 - 9	10/20/05	ND(0.037)	ND(0.037)	0.018 J	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.018 J
MSSB-D05	1 - 2	4/28/2004	ND(0.12)	ND(0.12)	ND(0.12)	ND(0.12)	0.28	ND(0.12)	ND(0.12)	0.28
MSSB-D06	1 - 3	7/21/2004	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	3.3	ND(0.24)	ND(0.24)	3.3
	3 - 5	7/21/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
MSSB-D07	1 - 3	2/13/2004	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	5.0	ND(0.24)	ND(0.24)	5.0
	3 - 5	2/13/2004	ND(0.23)	ND(0.23)	ND(0.23)	0.66	ND(0.23)	ND(0.23)	ND(0.23)	0.66
	5 - 7	2/13/2004	5.0 JN	ND(0.44)	ND(0.44)	ND(0.44)	ND(0.44)	ND(0.44)	ND(0.44)	5.0 JN
	7 - 9	2/13/2004	ND(0.57)	ND(0.57)	ND(0.57)	ND(0.57)	5.8	ND(0.57)	ND(0.57)	5.8
	9 - 11	2/13/2004	ND(0.21)	ND(0.21)	ND(0.21)	ND(0.21)	2.1	ND(0.21)	ND(0.21)	2.1
	11 - 13	2/13/2004	ND(0.28)	ND(0.28)	ND(0.28)	1.5 J	ND(0.28)	ND(0.28)	ND(0.28)	1.5 J
	13 - 15	2/13/2004	0.48	ND(0.045)	ND(0.045)	ND(0.045)	ND(0.045)	ND(0.045)	ND(0.045)	0.48
	15 - 17	2/13/2004	ND(0.26)	ND(0.26)	ND(0.26)	0.92	ND(0.26)	ND(0.26)	ND(0.26)	0.92
	17 - 19	2/13/2004	ND(0.24)	ND(0.24)	ND(0.24)	0.79	ND(0.24)	ND(0.24)	ND(0.24)	0.79
	19 - 21	2/13/2004	ND(0.26)	ND(0.26)	ND(0.26)	1.1	ND(0.26)	ND(0.26)	ND(0.26)	1.1

TABLE 5
SUMMARY OF PDI PCB SAMPLE DATA - MILL STREET AREA SUBSURFACE SOILS

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
MSSB-D07SE	1 - 3	7/22/2004	ND(0.51)	ND(0.51)	ND(0.51)	ND(0.51)	8.6	ND(0.51)	ND(0.51)	8.6
	3 - 5	7/22/2004	ND(0.41)	ND(0.41)	ND(0.41)	ND(0.41)	1.4	ND(0.41)	ND(0.41)	1.4
	5 - 7	7/22/2004	ND(230)	ND(230)	ND(230)	ND(230)	560	ND(230)	ND(230)	560
	7 - 9	7/22/2004	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	6.0	ND(0.24)	ND(0.24)	6.0
	9 - 11	7/22/2004	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	3.1	ND(0.24)	ND(0.24)	3.1
	11 - 13	7/22/2004	ND(0.043)	ND(0.043)	ND(0.043)	ND(0.043)	0.22	ND(0.043)	ND(0.043)	0.22
	13 - 15	7/22/2004	ND(0.043)	ND(0.043)	ND(0.043)	ND(0.043)	0.58	0.22	ND(0.043)	0.80
	15 - 17	7/22/2004	ND(0.043)	ND(0.043)	ND(0.043)	ND(0.043)	0.034 J	ND(0.043)	ND(0.043)	0.034 J
	17 - 19	7/22/2004	ND(0.27)	ND(0.27)	ND(0.27)	ND(0.27)	0.91	0.28	ND(0.27)	1.2
	19 - 21	7/22/2004	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	0.53	0.20	ND(0.042)	0.73
	21 - 21.5	7/22/2004	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	0.38	0.14	ND(0.041)	0.52
MSSB-D07W	1 - 3	7/28/2004	ND(460) [ND(530)]	ND(460) [ND(530)]	ND(460) [ND(530)]	ND(460) [ND(530)]	800 [830]	ND(460) [ND(530)]	ND(460) [ND(530)]	800 [830]
	3 - 5	7/28/2004	ND(4.2)	ND(4.2)	ND(4.2)	ND(4.2)	20	ND(4.2)	ND(4.2)	20
	5 - 7	7/28/2004	ND(0.18)	ND(0.18)	ND(0.18)	ND(0.18)	3.6 J	ND(0.18)	ND(0.18)	3.6 J
	7 - 9	7/28/2004	ND(0.22)	ND(0.22)	ND(0.22)	ND(0.22)	4.2	ND(0.22)	ND(0.22)	4.2
	9 - 11	7/28/2004	ND(0.20)	ND(0.20)	ND(0.20)	ND(0.20)	1.3	ND(0.20)	ND(0.20)	1.3
	11 - 13	7/28/2004	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	0.058	ND(0.040)	ND(0.040)	0.058
	13 - 15	7/28/2004	ND(0.25)	ND(0.25)	ND(0.25)	ND(0.25)	0.69	ND(0.25)	ND(0.25)	0.69
	15 - 17	7/28/2004	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	0.28	ND(0.042)	ND(0.042)	0.28
	17 - 19	7/28/2004	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	0.074	ND(0.040)	ND(0.040)	0.074
	19 - 21	7/28/2004	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	0.12	ND(0.040)	ND(0.040)	0.12
	21 - 21.5	7/28/2004	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	0.19	ND(0.039)	ND(0.039)	0.19
MSSB-D08	1 - 3	7/1/2004	ND(220)	ND(220)	ND(220)	ND(220)	380	ND(220)	ND(220)	380
	3 - 5	7/1/2004	ND(200)	ND(200)	ND(200)	ND(200)	720	ND(200)	ND(200)	720
	5 - 7	7/1/2004	ND(3.7)	ND(3.7)	ND(3.7)	ND(3.7)	26	ND(3.7)	ND(3.7)	26
	7 - 8	7/1/2004	ND(0.22)	ND(0.22)	ND(0.22)	ND(0.22)	0.90	ND(0.22)	ND(0.22)	0.90
	8 - 10	7/1/2004	ND(0.046)	ND(0.046)	ND(0.046)	ND(0.046)	0.087	ND(0.046)	ND(0.046)	0.087
MSSB-D09	1 - 3	7/21/2004	0.24	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.24
	3 - 5	7/21/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.016 J	ND(0.034)	ND(0.034)	0.016 J
	5 - 7	7/21/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.022 J	ND(0.034)	ND(0.034)	0.022 J
	7 - 8	7/21/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.047 J	ND(0.034)	ND(0.034)	0.047 J
	8 - 10	7/21/2004	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)
MSSB-D10	1 - 2	4/29/2004	ND(0.40)	ND(0.40)	ND(0.40)	ND(0.40)	5.4	ND(0.40)	ND(0.40)	5.4
	2 - 3	4/29/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.036	ND(0.034)	ND(0.034)	0.036
MSSB-D11	1 - 3	7/6/2004	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	1.4	ND(0.24)	ND(0.24)	1.4
	3 - 5	7/6/2004	ND(24) [ND(250)]	ND(24) [ND(250)]	ND(24) [ND(250)]	ND(24) [ND(250)]	330 J [880 J]	ND(24) [ND(250)]	ND(24) [ND(250)]	330 J [880 J]
	5 - 7	7/6/2004	ND(0.21)	ND(0.21)	ND(0.21)	ND(0.21)	0.52	ND(0.21)	ND(0.21)	0.52
	7 - 9	7/6/2004	ND(0.14)	ND(0.14)	ND(0.14)	ND(0.14)	0.10 J	ND(0.14)	ND(0.14)	0.10 J
	9 - 11	7/6/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)
	11 - 13	7/6/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)
	13 - 15	7/6/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.15	ND(0.038)	ND(0.038)	0.15
	15 - 17	7/6/2004	ND(0.31)	ND(0.31)	ND(0.31)	ND(0.31)	1.1	ND(0.31)	ND(0.31)	1.1
	17 - 19	7/6/2004	ND(0.27)	ND(0.27)	ND(0.27)	ND(0.27)	0.84	ND(0.27)	ND(0.27)	0.84
	19 - 20	7/6/2004	ND(0.034)	ND(0.034)	ND(0.034)	0.074	ND(0.034)	ND(0.034)	ND(0.034)	0.074
MSSB-D13	1 - 3	2/13/2004	ND(460)	ND(460)	ND(460)	10000	ND(460)	ND(460)	ND(460)	10000
	3 - 5	2/13/2004	ND(400) [ND(550)]	ND(400) [ND(550)]	ND(400) [ND(550)]	20000 [20000]	ND(400) [ND(550)]	ND(400) [ND(550)]	ND(400) [ND(550)]	20000 [20000]
	5 - 7	2/13/2004	ND(500)	ND(500)	ND(500)	7800	ND(500)	ND(500)	ND(500)	7800
	7 - 9	2/13/2004	ND(260)	ND(260)	ND(260)	1900	ND(260)	ND(260)	ND(260)	1900
	9 - 11	2/13/2004	ND(120)	ND(120)	ND(120)	3400	ND(120)	ND(120)	ND(120)	3400
	11 - 13	2/13/2004	ND(4.7)	ND(4.7)	ND(4.7)	56	ND(4.7)	ND(4.7)	ND(4.7)	56
	13 - 15	2/13/2004	ND(48)	ND(48)	ND(48)	620	ND(48)	460	ND(48)	1100
	15 - 17	2/13/2004	ND(4.0)	ND(4.0)	ND(4.0)	ND(22)	ND(4.0)	12	ND(4.0)	ND(34)
	17 - 19	2/13/2004	ND(0.44)	ND(0.44)	ND(0.44)	ND(5.0)	ND(0.44)	ND(0.44)	ND(0.44)	ND(5.0)
	19 - 21	2/13/2004	ND(100)	ND(100)	ND(100)	ND(650)	ND(100)	ND(100)	ND(100)	ND(650)
	21 - 22	2/13/2004	ND(220)	ND(220)	ND(220)	4300	ND(220)	ND(220)	ND(220)	4300

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GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
MSSB-D13E	1 - 3	7/6/2004	ND(2600)	ND(2600)	ND(2600)	26000	ND(2600)	ND(2600)	ND(2600)	26000
	3 - 5	7/6/2004	ND(1100)	ND(1100)	ND(1100)	10000	ND(1100)	ND(1100)	ND(1100)	10000
	5 - 7	7/6/2004	ND(43)	ND(43)	ND(43)	56 J	ND(43)	ND(43)	ND(43)	56 J
	7 - 9	7/6/2004	ND(1300)	ND(1300)	ND(1300)	4000	ND(1300)	ND(1300)	ND(1300)	4000
	9 - 11	7/6/2004	ND(570)	ND(570)	ND(570)	1500	ND(570)	ND(570)	ND(570)	1500
	11 - 13	7/6/2004	ND(100)	ND(100)	ND(100)	200	ND(100)	ND(100)	ND(100)	200
	13 - 15	7/6/2004	ND(0.52)	ND(0.52)	ND(0.52)	5.8	ND(0.52)	ND(0.52)	ND(0.52)	5.8
	15 - 16	7/6/2004	ND(0.25)	ND(0.25)	ND(0.25)	1.6	ND(0.25)	ND(0.25)	ND(0.25)	1.6
MSSB-D15	1 - 3	7/1/2004	ND(1300)	ND(1300)	ND(1300)	ND(1300)	3700	ND(1300)	ND(1300)	3700
	3 - 5	7/1/2004	ND(0.20)	ND(0.20)	ND(0.20)	0.30	ND(0.20)	ND(0.20)	ND(0.20)	0.30
	5 - 7	8/25/2004	ND(0.96) [ND(0.85)]	ND(0.96) [ND(0.85)]	ND(0.96) [ND(0.85)]	ND(0.96) [ND(0.85)]	10 [8.8]	ND(0.96) [ND(0.85)]	ND(0.96) [ND(0.85)]	10 [8.8]
	7 - 9	8/25/2004	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	2.8	ND(0.24)	ND(0.24)	2.8
	9 - 11	8/25/2004	ND(0.19)	ND(0.19)	ND(0.19)	ND(0.19)	1.4	ND(0.19)	ND(0.19)	1.4
	11 - 12	8/25/2004	ND(0.22)	ND(0.22)	ND(0.22)	ND(0.22)	1.3	ND(0.22)	ND(0.22)	1.3
MSSB-D17	1 - 3	12/17/2003	ND(0.036) [ND(0.036)]	ND(0.036) [ND(0.036)]	ND(0.036) [ND(0.036)]	ND(0.036) [ND(0.036)]	0.032 J [0.033 J]	ND(0.036) [ND(0.036)]	ND(0.036) [ND(0.036)]	0.032 J [0.033 J]
	3 - 5	12/17/2003	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.042	ND(0.035)	ND(0.035)	0.042
	5 - 7	12/17/2003	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	0.029 J	ND(0.040)	ND(0.040)	0.029 J
	7 - 9	12/17/2003	ND(0.072)	ND(0.072)	ND(0.072)	0.17	ND(0.072)	ND(0.072)	ND(0.072)	0.17
	9 - 11	12/17/2003	ND(0.037)	ND(0.037)	ND(0.037)	0.056 J	ND(0.037)	ND(0.037)	ND(0.037)	0.056 J
	11 - 13	12/17/2003	ND(0.038)	ND(0.038)	ND(0.038)	0.023 J	ND(0.038)	ND(0.038)	ND(0.038)	0.023 J
	13 - 14.5	12/17/2003	ND(0.036)	ND(0.036)	ND(0.036)	0.17	ND(0.036)	ND(0.036)	ND(0.036)	0.17
MSSB-E01	1 - 3	12/19/2003	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	0.018 J	ND(0.039)	ND(0.039)	0.018 J
	3 - 5	12/19/2003	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	0.024 J	ND(0.042)	ND(0.042)	0.024 J
	5 - 7	12/19/2003	ND(0.037) [ND(0.036)]	ND(0.037) [ND(0.036)]	ND(0.037) [ND(0.036)]	ND(0.037) [ND(0.036)]	0.031 J [0.090]	ND(0.037) [ND(0.036)]	ND(0.037) [ND(0.036)]	0.031 J [0.090]
	7 - 9	12/19/2003	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.061)	ND(0.038)	ND(0.038)	ND(0.061)
	9 - 11	12/19/2003	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.055)	ND(0.037)	ND(0.037)	ND(0.055)
	11 - 13	12/19/2003	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.048)	ND(0.042)	ND(0.042)	ND(0.048)
	13 - 15	12/19/2003	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.043)	ND(0.039)	ND(0.039)	ND(0.043)
	15 - 17	12/19/2003	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.054)	ND(0.039)	ND(0.039)	ND(0.054)
	17 - 19	12/19/2003	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.054)	ND(0.041)	ND(0.041)	ND(0.054)
	19 - 21	12/19/2003	ND(0.043)	ND(0.043)	ND(0.043)	ND(0.043)	0.026 J	ND(0.043)	ND(0.043)	0.026 J
	21 - 23	12/19/2003	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.026 J	ND(0.038)	ND(0.038)	0.026 J
	23 - 24.1	12/19/2003	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.025 J	ND(0.038)	ND(0.038)	0.025 J
MSSB-E03	1 - 3	12/23/2003	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.021 J	ND(0.035)	ND(0.035)	0.021 J
	3 - 5	12/23/2003	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.024 J	ND(0.035)	ND(0.035)	0.024 J
	5 - 7	12/23/2003	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)
	7 - 9	12/23/2003	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	0.039	ND(0.039)	ND(0.039)	0.039
	9 - 11	12/23/2003	ND(0.036) [ND(0.036)]	ND(0.036) [ND(0.036)]	ND(0.036) [ND(0.036)]	ND(0.036) [ND(0.036)]	ND(0.036) [0.019 J]	ND(0.036) [ND(0.036)]	ND(0.036) [ND(0.036)]	ND(0.036) [0.019 J]
	11 - 13	12/23/2003	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.022 J	ND(0.038)	ND(0.038)	0.022 J
	13 - 15	12/23/2003	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	0.020 J	0.014 J	ND(0.039)	0.034 J
	15 - 17	12/23/2003	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	0.021 J	0.018 J	ND(0.039)	0.039
	17 - 19	12/23/2003	ND(0.043)	ND(0.043)	ND(0.043)	ND(0.043)	0.022 J	ND(0.043)	ND(0.043)	0.022 J
	19 - 21	12/23/2003	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.027 J	ND(0.035)	ND(0.035)	0.027 J
	21 - 21.4	12/23/2003	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.053)	ND(0.035)	ND(0.035)	ND(0.053)
MSSB-E05	1 - 3	12/4/2003	ND(3.6)	ND(3.6)	ND(3.6)	ND(3.6)	3.7	2.7 J	ND(3.6)	6.4
	3 - 5	12/4/2003	ND(0.70)	ND(0.70)	ND(0.70)	ND(0.70)	3.9	3.2	ND(0.70)	7.1
	5 - 7	12/4/2003	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.097	0.088	ND(0.037)	0.18
	7 - 9	12/4/2003	ND(0.039)	ND(0.039)	ND(0.039)	0.040	ND(0.039)	ND(0.039)	ND(0.039)	0.040
	9 - 11	12/11/2003	ND(0.041) [ND(0.040)]	ND(0.041) [ND(0.040)]	ND(0.041) [ND(0.040)]	ND(0.041) [ND(0.040)]	0.020 J [0.029 J]	ND(0.041) [ND(0.040)]	ND(0.041) [ND(0.040)]	0.020 J [0.029 J]
	11 - 13	12/11/2003	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.025 J	0.021 J	ND(0.036)	0.046
MSSB-E05E	1 - 3	7/21/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.23 J	ND(0.037)	ND(0.037)	0.23 J
	3 - 5	7/21/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
	5 - 7	7/21/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)

TABLE 5
SUMMARY OF PDI PCB SAMPLE DATA - MILL STREET AREA SUBSURFACE SOILS

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
MSSB-E05N	1 - 3	7/21/2004	ND(0.91) [ND(0.84)]	ND(0.91) [ND(0.84)]	ND(0.91) [ND(0.84)]	ND(0.91) [ND(0.84)]	12 [11]	ND(0.91) [ND(0.84)]	ND(0.91) [ND(0.84)]	12 [11]
	3 - 5	7/21/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)
	5 - 7	7/21/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)
	7 - 9	10/20/05	ND(0.036)	ND(0.036)	0.26	ND(0.036)	ND(0.036)	0.032 J	ND(0.036)	0.29
MSSB-E05W	1 - 3	7/21/2004	ND(0.43)	ND(0.43)	ND(0.43)	ND(0.43)	6.4	ND(0.43)	ND(0.43)	6.4
	3 - 5	7/21/2004	ND(0.52)	ND(0.52)	ND(0.52)	ND(0.52)	11	ND(0.52)	ND(0.52)	11
	5 - 7	7/21/2004	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	5.7	ND(0.24)	ND(0.24)	5.7
	7 - 9	10/20/05	ND(1.9)	ND(1.9)	25	ND(1.9)	ND(1.9)	2.9	ND(1.9)	28
	9 - 11	10/20/05	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)
MSSB-E07	1 - 3	12/9/2003	ND(0.70)	ND(0.70)	ND(0.70)	ND(0.70)	8.4	ND(0.70)	ND(0.70)	8.4
	3 - 5	12/9/2003	ND(0.13)	ND(0.13)	ND(0.13)	ND(0.13)	1.7	ND(0.13)	ND(0.13)	1.7
	5 - 7	12/9/2003	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.21	ND(0.036)	ND(0.036)	0.21
	7 - 9	12/9/2003	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.29	ND(0.036)	ND(0.036)	0.29
	9 - 11	12/9/2003	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	0.067	0.029 J	ND(0.039)	0.096
	11 - 13	12/9/2003	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)
	13 - 15	12/9/2003	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)
	15 - 17	12/9/2003	ND(0.043)	ND(0.043)	ND(0.043)	ND(0.043)	0.047	ND(0.043)	ND(0.043)	0.047
	17 - 19	12/9/2003	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	0.025 J	ND(0.042)	ND(0.042)	0.025 J
	19 - 20.4	12/9/2003	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	0.22	ND(0.042)	ND(0.042)	0.22
MSSB-E07W	1 - 3	7/21/2004	ND(0.21)	ND(0.21)	ND(0.21)	ND(0.21)	1.4	ND(0.21)	ND(0.21)	1.4
	3 - 5	7/21/2004	ND(0.046)	ND(0.046)	ND(0.046)	ND(0.046)	0.19 J	ND(0.046)	ND(0.046)	0.19 J
	5 - 7	7/21/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.011 J	ND(0.035)	ND(0.035)	0.011 J
MSSB-E08	1 - 3	7/22/2004	ND(4300) [ND(2500)]	ND(4300) [ND(2500)]	ND(4300) [ND(2500)]	ND(4300) [ND(2500)]	17000 [14000]	ND(4300) [ND(2500)]	ND(4300) [ND(2500)]	17000 [14000]
	3 - 5	7/22/2004	ND(0.23)	ND(0.23)	ND(0.23)	ND(0.23)	2.8	ND(0.23)	ND(0.23)	2.8
	5 - 6	7/22/2004	ND(0.22)	ND(0.22)	ND(0.22)	ND(0.22)	1.2	ND(0.22)	ND(0.22)	1.2
	6 - 8	7/22/2004	ND(0.29)	ND(0.29)	ND(0.29)	ND(0.29)	1.4	ND(0.29)	ND(0.29)	1.4
MSSB-E09	1 - 3	12/9/2003	ND(3.5)	ND(3.5)	ND(3.5)	ND(3.5)	33	ND(3.5)	ND(3.5)	33
	3 - 5	12/9/2003	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.082	ND(0.037)	ND(0.037)	0.082
	5 - 7	12/9/2003	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.020 J	ND(0.037)	ND(0.037)	0.020 J
	7 - 9	12/9/2003	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	0.11	ND(0.039)	ND(0.039)	0.11
	9 - 11	12/9/2003	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	0.012 J	ND(0.040)	ND(0.040)	0.012 J
	11 - 13	12/9/2003	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)
	13 - 15	12/9/2003	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)
	15 - 17	12/9/2003	ND(0.039)	ND(0.039)	ND(0.039)	0.016 J	ND(0.039)	ND(0.039)	ND(0.039)	0.016 J
	17 - 19	12/9/2003	ND(0.038)	ND(0.038)	ND(0.038)	0.037 J	ND(0.038)	ND(0.038)	ND(0.038)	0.037 J
	19 - 21	12/11/2003	ND(0.038)	ND(0.038)	ND(0.038)	0.042	ND(0.038)	ND(0.038)	ND(0.038)	0.042
MSSB-E09N	1 - 3	7/20/2004	ND(0.25)	ND(0.25)	ND(0.25)	ND(0.25)	3.5	ND(0.25)	ND(0.25)	3.5
	3 - 5	7/20/2004	ND(0.25)	ND(0.25)	ND(0.25)	ND(0.25)	1.0	ND(0.25)	ND(0.25)	1.0
MSSB-E09W	1 - 3	7/1/2004	ND(11) [ND(12)]	ND(11) [ND(12)]	ND(11) [ND(12)]	ND(11) [ND(12)]	210 [150]	ND(11) [ND(12)]	ND(11) [ND(12)]	210 [150]
	3 - 5	7/1/2004	ND(0.17)	ND(0.17)	ND(0.17)	0.40	ND(0.17)	ND(0.17)	ND(0.17)	0.40
MSSB-E10	1 - 3	7/20/2004	ND(4.5)	ND(4.5)	ND(4.5)	ND(4.5)	46	ND(4.5)	ND(4.5)	46
	3 - 5	7/20/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.11	ND(0.034)	ND(0.034)	0.11
MSSB-E11	1 - 3	12/18/2003	ND(35) [ND(18)]	ND(35) [ND(18)]	ND(35) [ND(18)]	ND(35) [ND(18)]	280 [290]	ND(35) [ND(18)]	ND(35) [ND(18)]	280 [290]
	3 - 5	12/18/2003	ND(0.74)	ND(0.74)	ND(0.74)	ND(0.74)	3.6	ND(0.74)	ND(0.74)	3.6
	5 - 7	12/18/2003	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)
	7 - 9	12/18/2003	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.039)	ND(0.034)	ND(0.034)	ND(0.039)
	9 - 11	12/18/2003	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)
	11 - 13	12/18/2003	ND(0.20)	ND(0.20)	ND(0.20)	ND(0.20)	0.79	ND(0.20)	ND(0.20)	0.79
	13 - 15	12/18/2003	ND(0.16)	ND(0.16)	ND(0.16)	ND(0.16)	0.55	ND(0.16)	ND(0.16)	0.55
	15 - 17	12/18/2003	ND(0.082)	ND(0.082)	ND(0.082)	ND(0.082)	0.31	ND(0.082)	ND(0.082)	0.31
	17 - 19	12/18/2003	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	0.29	ND(0.042)	ND(0.042)	0.29
	19 - 21	12/18/2003	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	0.073	ND(0.042)	ND(0.042)	0.073
	21 - 21.8	12/18/2003	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)

TABLE 5
SUMMARY OF PDI PCB SAMPLE DATA - MILL STREET AREA SUBSURFACE SOILS

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
MSSB-E12	1 - 3	7/7/2004	ND(13)	ND(13)	ND(13)	61	ND(13)	ND(13)	ND(13)	61
	3 - 4	7/7/2004	ND(42)	ND(42)	ND(42)	270	ND(42)	ND(42)	ND(42)	270
	4 - 6	7/1/2004	ND(0.26)	ND(0.26)	ND(0.26)	0.16 J	ND(0.26)	ND(0.26)	ND(0.26)	0.16 J
	6 - 8	7/1/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.12	ND(0.035)	ND(0.035)	0.12
	8 - 10	7/7/2004	ND(0.22)	ND(0.22)	ND(0.22)	0.86	ND(0.22)	ND(0.22)	ND(0.22)	0.86
	10 - 12	7/1/2004	ND(0.20)	ND(0.20)	ND(0.20)	0.13 J	ND(0.20)	ND(0.20)	ND(0.20)	0.13 J
	12 - 14	7/7/2004	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	0.021 J	ND(0.040)	ND(0.040)	0.021 J
	14 - 16	7/1/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.032 J	ND(0.037)	ND(0.037)	0.032 J
MSSB-E13	1 - 3	12/17/2003	ND(1800)	ND(1800)	ND(1800)	12000	ND(1800)	ND(1800)	ND(1800)	12000
	3 - 5	12/17/2003	ND(2.0)	ND(2.0)	ND(2.0)	15	ND(2.0)	ND(2.0)	ND(2.0)	15
	5 - 7	12/17/2003	ND(0.039)	ND(0.039)	ND(0.039)	0.22	ND(0.039)	ND(0.039)	ND(0.039)	0.22
	7 - 9	12/17/2003	ND(8.6)	ND(8.6)	ND(8.6)	36	ND(8.6)	ND(8.6)	ND(8.6)	36
	9 - 11	12/17/2003	ND(0.74)	ND(0.74)	ND(0.74)	5.6	ND(0.74)	ND(0.74)	ND(0.74)	5.6
	11 - 13	12/17/2003	ND(0.19)	ND(0.19)	ND(0.19)	2.0	ND(0.19)	ND(0.19)	ND(0.19)	2.0
	13 - 15	12/17/2003	ND(0.15)	ND(0.15)	ND(0.15)	0.44	ND(0.15)	ND(0.15)	ND(0.15)	0.44
	15 - 17	12/17/2003	ND(0.15)	ND(0.15)	ND(0.15)	0.82	ND(0.15)	ND(0.15)	ND(0.15)	0.82
	17 - 19	12/17/2003	ND(0.083)	ND(0.083)	ND(0.083)	0.27	ND(0.083)	ND(0.083)	ND(0.083)	0.27
	19 - 21	12/18/2003	ND(0.17)	ND(0.17)	ND(0.17)	0.92	ND(0.17)	ND(0.17)	ND(0.17)	0.92
	21 - 21.3	12/18/2003	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)
MSSB-E13E	1 - 3	7/27/2004	ND(810)	ND(810)	ND(810)	17000	ND(810)	ND(810)	ND(810)	17000
	3 - 5	7/27/2004	ND(210)	ND(210)	ND(210)	1600	ND(210)	ND(210)	ND(210)	1600
	5 - 7	7/27/2004	ND(0.049) [ND(0.043)]	ND(0.049) [ND(0.043)]	ND(0.049) [ND(0.043)]	0.11 J [0.057 J]	ND(0.049) [ND(0.043)]	ND(0.049) [ND(0.043)]	ND(0.049) [ND(0.043)]	0.11 J [0.057 J]
	7 - 9	7/27/2004	ND(0.78)	ND(0.78)	ND(0.78)	ND(0.78)	2.3	0.82	ND(0.78)	3.2
	9 - 11	7/27/2004	ND(0.040)	ND(0.040)	ND(0.040)	0.011 J	ND(0.040)	ND(0.040)	ND(0.040)	0.011 J
	11 - 13	7/27/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.12 JN	ND(0.036)	ND(0.036)	0.12 JN
	13 - 15	7/27/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.032 J	ND(0.037)	ND(0.037)	0.032 J
MSSB-E13S	1 - 2	4/22/2004	ND(0.035)	ND(0.035)	ND(0.035)	0.044	ND(0.035)	ND(0.035)	ND(0.035)	0.044
	2 - 3	4/22/2004	ND(0.034)	ND(0.034)	ND(0.034)	0.045	ND(0.034)	ND(0.034)	ND(0.034)	0.045
	3 - 5	4/22/2004	ND(0.048)	ND(0.048)	ND(0.048)	0.036 J	ND(0.048)	ND(0.048)	ND(0.048)	0.036 J
	5 - 7	4/22/2004	ND(0.038) [ND(0.035)]	ND(0.038) [ND(0.035)]	ND(0.038) [ND(0.035)]	ND(0.038) [ND(0.035)]	ND(0.038) [ND(0.035)]	ND(0.038) [ND(0.035)]	ND(0.038) [ND(0.035)]	ND(0.038) [ND(0.035)]
	7 - 9	4/22/2004	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)
	9 - 11	4/22/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)
	11 - 13	4/22/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)
	13 - 15	4/22/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)
MSSB-E13SS	1 - 2	4/22/2004	ND(0.034)	ND(0.034)	ND(0.034)	0.024 J	ND(0.034)	ND(0.034)	ND(0.034)	0.024 J
	2 - 3	4/22/2004	ND(0.033)	ND(0.033)	ND(0.033)	0.011 J	ND(0.033)	ND(0.033)	ND(0.033)	0.011 J
MSSB-E13W	1 - 3	7/27/2004	ND(0.26)	ND(0.26)	ND(0.26)	2.6	ND(0.26)	ND(0.26)	ND(0.26)	2.6
	3 - 5	7/27/2004	ND(0.40)	ND(0.40)	ND(0.40)	1.8	ND(0.40)	ND(0.40)	ND(0.40)	1.8
	5 - 7	7/27/2004	ND(0.037)	ND(0.037)	ND(0.037)	0.27	ND(0.037)	ND(0.037)	ND(0.037)	0.27
	7 - 9	7/27/2004	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	0.21	0.20	ND(0.040)	0.41
	9 - 11	7/27/2004	ND(0.036)	ND(0.036)	ND(0.036)	0.043	ND(0.036)	ND(0.036)	ND(0.036)	0.043
	11 - 13	7/27/2004	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.23	ND(0.037)	ND(0.037)	0.23
	13 - 15	7/27/2004	ND(0.036)	ND(0.036)	ND(0.036)	0.051	ND(0.036)	ND(0.036)	ND(0.036)	0.051
MSSB-E14	1 - 2	4/29/2004	ND(1400)	ND(1400)	ND(1400)	15000	ND(1400)	ND(1400)	ND(1400)	15000
	2 - 3	4/29/2004	ND(430)	ND(430)	ND(430)	ND(430)	14000	ND(430)	ND(430)	14000
	3 - 5	7/27/2004	ND(12)	ND(12)	ND(12)	ND(12)	98	ND(12)	ND(12)	98
	5 - 7	7/27/2004	ND(0.27)	ND(0.27)	ND(0.27)	2.1	ND(0.27)	ND(0.27)	ND(0.27)	2.1
MSSB-E14S	1 - 3	7/27/2004	ND(2.1)	ND(2.1)	ND(2.1)	ND(2.1)	16	ND(2.1)	ND(2.1)	16
	3 - 5	7/27/2004	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	0.024 J	ND(0.039)	ND(0.039)	0.024 J
	5 - 7	7/27/2004	ND(0.077)	ND(0.077)	ND(0.077)	ND(0.077)	ND(0.077)	ND(0.077)	ND(0.077)	ND(0.077)
MSSB-E14SE	1 - 2	4/22/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)
	2 - 3	4/22/2004	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	0.015 J	ND(0.033)	ND(0.033)	0.015 J
MSSB-E14SW	1 - 2	4/22/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)
	2 - 3	4/22/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)

TABLE 5
SUMMARY OF PDI PCB SAMPLE DATA - MILL STREET AREA SUBSURFACE SOILS

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
MSSB-E15	1 - 3	12/17/2003	ND(18)	ND(18)	ND(18)	ND(18)	64	ND(18)	ND(18)	64
	3 - 5	12/17/2003	ND(0.18)	ND(0.18)	ND(0.18)	ND(0.18)	0.71	ND(0.18)	ND(0.18)	0.71
	5 - 7	12/17/2003	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.12	ND(0.035)	0.025 J	0.15
	7 - 9	12/17/2003	ND(0.076)	ND(0.076)	ND(0.076)	ND(0.076)	0.15	0.22	ND(0.076)	0.36
	9 - 11	12/17/2003	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.016 J	0.016 J	ND(0.038)	0.032 J
	11 - 13	12/17/2003	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.014 J	ND(0.037)	ND(0.037)	0.014 J
	13 - 13.6	12/17/2003	ND(0.038)	ND(0.038)	ND(0.038)	0.15	ND(0.038)	ND(0.038)	ND(0.038)	0.15
MSSB-E15S	1 - 3	4/22/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.40	ND(0.035)	ND(0.035)	0.40
MSSB-F05	1 - 3	7/21/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.011 J	ND(0.034)	ND(0.034)	0.011 J
	3 - 5	7/21/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.019 J	ND(0.034)	ND(0.034)	0.019 J
	5 - 7	7/21/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.020 J	ND(0.036)	ND(0.036)	0.020 J
	7 - 9	10/20/05	ND(0.038)	ND(0.038)	0.083	ND(0.038)	ND(0.038)	0.014 J	ND(0.038)	0.097
MSSB-F06	1 - 2	4/28/2004	ND(0.21) [ND(0.24)]	ND(0.21) [ND(0.24)]	ND(0.21) [ND(0.24)]	1.8 J [0.68 J]	ND(0.21) [ND(0.24)]	ND(0.21) [ND(0.24)]	ND(0.21) [ND(0.24)]	1.8 J [0.68 J]
	2 - 3	4/28/2004	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	0.035 J	ND(0.039)	ND(0.039)	0.035 J
MSSB-F07	1 - 3	12/12/2003	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.062	ND(0.034)	ND(0.034)	0.062
	3 - 5	12/12/2003	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	0.014 J	ND(0.033)	ND(0.033)	0.014 J
	5 - 7	12/12/2003	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)
	7 - 9	12/12/2003	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.066	ND(0.034)	ND(0.034)	0.066
	9 - 11	12/12/2003	ND(0.038)	ND(0.038)	ND(0.038)	0.081	ND(0.038)	ND(0.038)	ND(0.038)	0.081
	11 - 13	12/12/2003	ND(0.039)	ND(0.039)	ND(0.039)	0.011 J	ND(0.039)	ND(0.039)	ND(0.039)	0.011 J
	13 - 15	12/12/2003	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)
	15 - 17	12/12/2003	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)
MSSB-F08	1 - 2	4/29/2004	ND(1.0)	ND(1.0)	ND(1.0)	ND(1.0)	11	ND(1.0)	ND(1.0)	11
	2 - 3	4/29/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.15	ND(0.035)	ND(0.035)	0.15
MSSB-F09	1 - 2	7/1/2004	ND(4.6)	ND(4.6)	ND(4.6)	ND(4.6)	24	ND(4.6)	ND(4.6)	24
	2 - 3	7/1/2004	ND(0.22)	ND(0.22)	ND(0.22)	ND(0.22)	0.20 J	ND(0.22)	ND(0.22)	0.20 J
	3 - 5	7/1/2004	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	0.49	ND(0.042)	ND(0.042)	0.49
MSSB-F10	1 - 2	4/29/2004	ND(4.2) [ND(11)]	ND(4.2) [ND(11)]	ND(4.2) [ND(11)]	ND(4.2) [ND(11)]	65 [88]	ND(4.2) [ND(11)]	ND(4.2) [ND(11)]	65 [88]
	2 - 3	4/29/2004	ND(0.21)	ND(0.21)	ND(0.21)	ND(0.21)	0.52 J	ND(0.21)	ND(0.21)	0.52 J
MSSB-G01	1 - 3	12/11/2003	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.013 J	ND(0.036)	ND(0.036)	0.013 J
	3 - 5	12/11/2003	ND(0.046) [ND(0.044)]	ND(0.046) [ND(0.044)]	ND(0.046) [ND(0.044)]	ND(0.046) [ND(0.044)]	0.066 [0.036 J]	ND(0.046) [ND(0.044)]	ND(0.046) [ND(0.044)]	0.066 [0.036 J]
	5 - 7	12/11/2003	ND(0.075)	ND(0.075)	ND(0.075)	ND(0.075)	0.33	ND(0.075)	ND(0.075)	0.33
	7 - 9	12/11/2003	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.014 J	ND(0.037)	ND(0.037)	0.014 J
	9 - 11	12/11/2003	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)
	11 - 13	12/11/2003	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)
	13 - 15	12/11/2003	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)
	15 - 17	12/11/2003	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.013 J	ND(0.036)	ND(0.036)	0.013 J
	17 - 19	12/11/2003	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
	19 - 21	12/11/2003	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.033 J	ND(0.037)	ND(0.037)	0.033 J
	21 - 23	12/11/2003	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)
	23 - 25	12/11/2003	ND(0.042)	ND(0.042)	ND(0.042)	ND(0.042)	0.016 J	ND(0.042)	ND(0.042)	0.016 J
	25 - 27	12/11/2003	ND(0.043)	ND(0.043)	ND(0.043)	ND(0.043)	0.097	ND(0.043)	ND(0.043)	0.097
	27 - 29	12/12/2003	ND(0.038) [ND(0.037)]	ND(0.038) [ND(0.037)]	ND(0.038) [ND(0.037)]	ND(0.038) [ND(0.037)]	0.028 J [ND(0.037)]	ND(0.038) [ND(0.037)]	ND(0.038) [ND(0.037)]	0.028 J [ND(0.037)]
	29 - 31	12/12/2003	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	0.031 J	ND(0.040)	ND(0.040)	0.031 J
	31 - 31.5	12/12/2003	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	0.012 J	ND(0.040)	ND(0.040)	0.012 J

TABLE 5
SUMMARY OF PDI PCB SAMPLE DATA - MILL STREET AREA SUBSURFACE SOILS

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
MSSB-G03	1 - 3	12/16/2003	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.025 J	ND(0.036)	ND(0.036)	0.025 J
	3 - 5	12/16/2003	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	0.079	ND(0.036)	ND(0.036)	0.079
	5 - 7	12/16/2003	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.048	ND(0.035)	ND(0.035)	0.048
	7 - 9	12/16/2003	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.036 J	ND(0.037)	ND(0.037)	0.036 J
	9 - 11	12/16/2003	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	0.026 J	ND(0.040)	ND(0.040)	0.026 J
	11 - 13	12/16/2003	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.050	ND(0.037)	ND(0.037)	0.050
	13 - 15	12/16/2003	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.029 J	ND(0.037)	ND(0.037)	0.029 J
	20 - 21	12/16/2003	ND(0.078)	ND(0.078)	ND(0.078)	ND(0.078)	0.26	ND(0.078)	ND(0.078)	0.26
	21 - 23	12/16/2003	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	0.11	ND(0.041)	ND(0.041)	0.11
	23 - 25	12/16/2003	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)
	25 - 26	12/16/2003	ND(0.037)	ND(0.037)	ND(0.037)	ND(0.037)	0.075	ND(0.037)	ND(0.037)	ND(0.075)
MSSB-G05	1 - 3	12/16/2003	ND(0.000035)	ND(0.000035)	ND(0.000035)	ND(0.000035)	ND(0.000035)	ND(0.000035)	ND(0.000035)	ND(0.000035)
	3 - 5	12/16/2003	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
	5 - 7	12/16/2003	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
	7 - 9	12/16/2003	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)
	9 - 11	12/16/2003	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.040)	ND(0.048)	ND(0.040)	ND(0.040)	ND(0.048)
	11 - 12	12/16/2003	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.013 J	ND(0.038)	0.013 J
MW-22A	10 - 11	1/14/2004	ND(0.043)	ND(0.043)	ND(0.043)	0.013 J	ND(0.043)	ND(0.043)	ND(0.043)	0.013 J
	13 - 15	1/27/2004	ND(0.036)	ND(0.036)	ND(0.036)	0.068	ND(0.036)	ND(0.036)	ND(0.036)	0.068
	15 - 17	1/27/2004	ND(0.037)	ND(0.037)	ND(0.037)	0.11	ND(0.037)	ND(0.037)	ND(0.037)	0.11
	17 - 19	1/27/2004	ND(0.036)	ND(0.036)	ND(0.036)	0.070	ND(0.036)	ND(0.036)	ND(0.036)	0.070
MW-22B	3 - 4	1/28/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.071)	ND(0.035)	ND(0.035)	ND(0.071)
	4 - 6	1/28/2004	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	0.48	ND(0.041)	ND(0.041)	0.48
	6 - 8	1/28/2004	ND(0.27)	ND(0.27)	ND(0.27)	ND(0.27)	1.8	ND(0.27)	ND(0.27)	1.8
	8 - 10	1/28/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.057	ND(0.035)	ND(0.035)	0.057
MW-23A	17 - 19	1/22/2004	ND(0.037)	ND(0.037)	ND(0.037)	0.051	ND(0.037)	ND(0.037)	ND(0.037)	0.051
	19 - 21	1/22/2004	ND(0.038)	ND(0.038)	ND(0.038)	0.046	ND(0.038)	ND(0.038)	ND(0.038)	0.046
	21 - 23	1/22/2004	ND(0.039)	ND(0.039)	ND(0.039)	0.071	ND(0.039)	ND(0.039)	ND(0.039)	0.071
MW-23B	9 - 11	1/26/2004	ND(0.039)	ND(0.039)	ND(0.039)	0.062	ND(0.039)	ND(0.039)	ND(0.039)	0.062
	11 - 13	1/26/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)
	13 - 15	1/26/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.022 J	ND(0.038)	ND(0.038)	0.022 J
MW-23C	1 - 3	1/20/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.017 J	ND(0.034)	ND(0.034)	0.017 J
	3 - 5	1/20/2004	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]	ND(0.034) [ND(0.034)]
	5 - 7	1/20/2004	ND(0.038)	ND(0.038)	ND(0.038)	0.013 J	ND(0.038)	ND(0.038)	ND(0.038)	0.013 J
	7 - 9	1/20/2004	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)
	15 - 17	1/20/2004	ND(0.038)	ND(0.038)	ND(0.038)	0.11	ND(0.038)	ND(0.038)	ND(0.038)	0.11
MW-24A	17 - 19	1/6/2004	ND(0.037)	ND(0.037)	ND(0.037)	0.56	ND(0.037)	ND(0.037)	ND(0.037)	0.56
	19 - 21	1/6/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.056)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.056)
	21 - 23	1/6/2004	ND(0.035)	ND(0.035)	ND(0.035)	0.088	ND(0.035)	ND(0.035)	ND(0.035)	0.088
MW-24B	1 - 3	1/7/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.12	ND(0.038)	ND(0.038)	0.12
	9 - 11	1/7/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)
	11 - 13	1/7/2004	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)	ND(0.041)
	13 - 15	1/8/2004	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.015 J	ND(0.035)	ND(0.035)	0.015 J
MW-24C	3 - 5	1/5/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.084	ND(0.038)	ND(0.038)	0.084
	5 - 7	1/5/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.057)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.057)
	7 - 9	1/5/2004	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.041)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.041)
	15 - 17	1/5/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.055)	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.055)
SB-05	1 - 2	4/29/2004	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	2.1	ND(0.24)	ND(0.24)	2.1
	2 - 3	4/29/2004	ND(0.038)	ND(0.038)	ND(0.038)	ND(0.038)	0.035 J	ND(0.038)	ND(0.038)	0.035 J
SB-12	1 - 2	4/29/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)

TABLE 5
SUMMARY OF PDI PCB SAMPLE DATA - MILL STREET AREA SUBSURFACE SOILS

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs
SB-12 (ESE)	1 - 2	7/12/2004	ND(440)	ND(440)	ND(440)	ND(440)	610	620	ND(440)	1200
	2 - 3	7/12/2004	ND(45)	ND(45)	ND(45)	ND(45)	260	300	ND(45)	560
	3 - 5	7/12/2004	ND(0.26)	ND(0.26)	ND(0.26)	ND(0.26)	1.3	1.6	ND(0.26)	3.0
SB-13	1 - 2	4/28/2004	ND(0.035) [ND(0.034)]	ND(0.035) [ND(0.034)]	ND(0.035) [ND(0.034)]	ND(0.035) [ND(0.034)]	0.029 J [0.021 J]	ND(0.035) [ND(0.034)]	ND(0.035) [ND(0.034)]	0.029 J [0.021 J]
	2 - 3	10/20/05	ND(0.035)	ND(0.035)	ND(0.035)	ND(0.035)	0.012 J	ND(0.035)	ND(0.035)	0.012 J
	3 - 5	10/20/05	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)	ND(0.036)
	5 - 7	10/20/05	ND(0.033)	ND(0.033)	0.021 J	ND(0.033)	ND(0.033)	ND(0.033)	ND(0.033)	0.021 J
	7 - 9	10/20/05	ND(0.039)	ND(0.039)	0.048	ND(0.039)	ND(0.039)	ND(0.039)	ND(0.039)	0.048
SB-14	1 - 2	4/28/2004	ND(0.035) [ND(0.39)]	ND(0.035) [ND(0.39)]	ND(0.035) [ND(0.39)]	ND(0.035) [ND(0.39)]	0.020 J [5.3]	ND(0.035) [ND(0.39)]	ND(0.035) [ND(0.39)]	0.020 J [5.3]
	2 - 3	4/28/2004	ND(0.034)	ND(0.034)	ND(0.034)	ND(0.034)	0.011 J	ND(0.034)	ND(0.034)	0.011 J
SF-01g-I	1 - 3	7/12/2004	ND(23)	ND(23)	ND(23)	ND(23)	240	130	ND(23)	370
	3 - 5	7/12/2004	ND(0.27)	ND(0.27)	ND(0.27)	ND(0.27)	1.2	ND(0.27)	ND(0.27)	1.2
SF-04g-I	1 - 2	4/29/2004	ND(190)	ND(190)	ND(190)	ND(190)	4300	ND(190)	ND(190)	4300
	2 - 3	4/29/2004	ND(0.83)	ND(0.83)	ND(0.83)	ND(0.83)	6.7 JN	ND(0.83)	ND(0.83)	6.7 JN

TABLE 5
SUMMARY OF PDI PCB SAMPLE DATA - MILL STREET AREA SUBSURFACE SOILS

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in dry weight parts per million, ppm)

Notes:

1. Samples were collected by Blasland, Bouck & Lee, Inc., and submitted to Severn Trent Laboratories, Inc. for analysis of PCBs.
2. ND - Analyte was not detected. The number in parentheses is the associated detection limit.
3. Field duplicate sample results are presented in brackets.
4. In the areas where temporary cover materials have been placed (e.g., geotextile and soil cover), the 0- to 1-foot surface soil sampling interval began at the depth of the geotextile installed by EPA, which is considered to represent the boundary between clean barrier soils and native Site soils.

Data Qualifiers:

J - The compound was positively identified; however, the associated numerical value is an estimated concentration only.
N - The analysis indicates the presence of a compound for which there is presumptive evidence to make a tentative identification. The associated numerical value is an estimated concentration only.

TABLE 6
SUMMARY OF PRE-CONSTRUCTION VERIFICATION PCB SOIL SAMPLE DATA- ELM STREET AREA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

Location ID: Sample Depth(Feet): Date Collected:	Units	SW-D1-D2 4 - 6 05/01/12	SW-D1-D2 8 - 10 05/01/12	SW-D3-D4 4 - 6 04/26/12	SW-D3-D4 8 - 10 05/01/12	SW-D5-D6 4 - 6 04/26/12	SW-D5-D6 8 - 10 04/27/12	SW-G1-G2 7 - 9 04/20/12	SW-G1-G2 12 - 14 04/20/12	SW-G3-G4 7 - 9 04/18/12	SW-G3-G4 12 - 14 04/18/12	SW-G5-G6 5 - 7 10/05/12
PCBs												
Aroclor 1016	mg/kg	ND(0.23)	ND(0.26)	ND(24)	ND(1.5)	ND(24)	ND(5.0) [ND(57)]	ND(19)	ND(110)	ND(120)	ND(120)	ND(0.22)
Aroclor 1221	mg/kg	ND(0.23)	ND(0.26)	ND(24)	ND(1.5)	ND(24)	ND(5.0) [ND(57)]	ND(19)	ND(110)	ND(120)	ND(120)	ND(0.22)
Aroclor 1232	mg/kg	ND(0.23)	ND(0.26)	ND(24)	ND(1.5)	ND(24)	ND(5.0) [ND(57)]	ND(19)	ND(110)	ND(120)	ND(120)	ND(0.22)
Aroclor 1242	mg/kg	ND(0.23)	0.53 J	ND(24)	21 J	ND(24)	ND(5.0) [42 J]	ND(19)	ND(110)	3,400 J	720 J	1.4
Aroclor 1248	mg/kg	ND(0.23)	ND(0.26)	47 J	ND(1.5)	10 J	50 J [ND(57)]	720 J	150 J	ND(120)	ND(120)	ND(0.22)
Aroclor 1254	mg/kg	ND(0.23)	ND(0.26)	ND(24)	ND(1.5)	ND(24)	ND(5.0) [ND(57)]	ND(19)	ND(110)	ND(120)	ND(120)	ND(0.22)
Aroclor 1260	mg/kg	ND(0.23)	ND(0.26)	ND(24)	ND(1.5)	ND(24)	ND(5.0) [ND(57)]	ND(19)	ND(110)	ND(120)	ND(120)	ND(0.22)
Total PCBs	mg/kg	ND(0.23)	0.53 J	47 J	21 J	10 J	50 J [42 J]	720 J	150 J	3,400 J	720 J	1.4
Miscellaneous Parameters												
% Moisture	%	10.0	12.0	13.0	26.0	9.40	15.0 [17.0]	7.60	18.0	13.0	17.0	5.00
% Solids	%	90.0	88.0	87.0	74.0	91.0	85.0 [83.0]	92.0	82.0	87.0	83.0	95.0

TABLE 6
SUMMARY OF PRE-CONSTRUCTION VERIFICATION PCB SOIL SAMPLE DATA- ELM STREET AREA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

Location ID: Sample Depth(Feet): Date Collected:	Units	SW-G5-G6 7 - 9 10/05/12	SW-G5-G6 9 - 11 10/05/12	SW-G5-G6 11 - 12 10/05/12	SW-G5-G6 12 - 14 10/05/12	SW-G5-G6 14 - 16 10/05/12	SW-G7-G8 5 - 7 10/01/12	SW-G7-G8 7 - 9 10/01/12	SW-G7-G8 9 - 11 10/01/12	SW-G7-G8 11 - 12 10/01/12	SW-G7-G8 12 - 14 10/01/12	SW-G7-G8 14 - 16 10/01/12
PCBs												
Aroclor 1016	mg/kg	ND(43)	ND(2.3)	ND(0.24)	ND(1.1)	ND(0.27)	ND(55) [ND(49)]	ND(1,100)	ND(0.27)	ND(0.27)	ND(0.31)	ND(0.27)
Aroclor 1221	mg/kg	ND(43)	ND(2.3)	ND(0.24)	ND(1.1)	ND(0.27)	ND(55) [ND(49)]	ND(1,100)	ND(0.27)	ND(0.27)	ND(0.31)	ND(0.27)
Aroclor 1232	mg/kg	ND(43)	ND(2.3)	ND(0.24)	ND(1.1)	ND(0.27)	ND(55) [ND(49)]	ND(1,100)	ND(0.27)	ND(0.27)	ND(0.31)	ND(0.27)
Aroclor 1242	mg/kg	98 J	20 J	1.0	7.3 J	ND(0.27)	75 JN [350 J]	31,000 J	ND(0.27)	ND(0.27)	7.0	ND(0.27)
Aroclor 1248	mg/kg	ND(43)	ND(2.3)	ND(0.24)	ND(1.1)	ND(0.27)	ND(55) [ND(49)]	ND(1,100)	ND(0.27)	ND(0.27)	ND(0.31)	ND(0.27)
Aroclor 1254	mg/kg	ND(43)	ND(2.3)	ND(0.24)	ND(1.1)	ND(0.27)	ND(55) [ND(49)]	ND(1,100)	ND(0.27)	ND(0.27)	ND(0.31)	ND(0.27)
Aroclor 1260	mg/kg	ND(43)	ND(2.3)	ND(0.24)	ND(1.1)	ND(0.27)	ND(55) [ND(49)]	ND(1,100)	ND(0.27)	ND(0.27)	ND(0.31)	ND(0.27)
Total PCBs	mg/kg	98 J	20 J	1.0	7.3 J	ND(0.27)	75 JN [350 J]	31,000 J	ND(0.27)	ND(0.27)	7.0	ND(0.27)
Miscellaneous Parameters												
% Moisture	%	6.20	4.50	6.30	11.0	15.0	14.0 [16.0]	8.60	12.0	11.0	21.0	14.0
% Solids	%	94.0	95.0	94.0	89.0	85.0	86.0 [84.0]	91.0	88.0	89.0	79.0	86.0

TABLE 6
SUMMARY OF PRE-CONSTRUCTION VERIFICATION PCB SOIL SAMPLE DATA- ELM STREET AREA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

Location ID: Sample Depth(Feet): Date Collected:	Units	SW-G9-G10 4 - 6 10/09/12	SW-G9-G10 6 - 8 10/09/12	SW-G9-G10 8 - 10 10/09/12	SW-G9-G10 10 - 12 10/09/12	SW-G11-G12 3 - 5 10/09/12	SW-G11-G12 5 - 7 10/09/12	SW-G11-G12 7 - 9 10/09/12	SW-G11-G12 9 - 11 10/09/12	SW-K1-K2 7 - 9 04/18/12	SW-K1-K2 11 - 13 04/18/12	SW-K3-K4 7 - 9 04/18/12
PCBs												
Aroclor 1016	mg/kg	ND(55)	ND(0.24)	ND(52)	ND(0.21)	ND(0.20)	ND(0.20)	ND(0.22)	ND(0.20)	ND(4.7)	ND(110)	ND(21)
Aroclor 1221	mg/kg	ND(55)	ND(0.24)	ND(52)	ND(0.21)	ND(0.20)	ND(0.20)	ND(0.22)	ND(0.20)	ND(4.7)	ND(110)	ND(21)
Aroclor 1232	mg/kg	ND(55)	ND(0.24)	ND(52)	ND(0.21)	ND(0.20)	ND(0.20)	ND(0.22)	ND(0.20)	ND(4.7)	ND(110)	ND(21)
Aroclor 1242	mg/kg	670 J	ND(0.24)	1,100 J	0.32 J	ND(0.20)	ND(0.20)	ND(0.22)	ND(0.20)	ND(4.7)	4,200 J	ND(21)
Aroclor 1248	mg/kg	ND(55)	9.5	ND(52)	ND(0.21)	0.19 J	ND(0.20)	0.097 J	0.16 J	38 J	ND(110)	100 J
Aroclor 1254	mg/kg	ND(55)	ND(0.24)	ND(52)	ND(0.21)	ND(0.20)	ND(0.20)	ND(0.22)	ND(0.20)	ND(4.7)	ND(110)	ND(21)
Aroclor 1260	mg/kg	ND(55)	ND(0.24)	ND(52)	ND(0.21)	ND(0.20)	ND(0.20)	ND(0.22)	ND(0.20)	ND(4.7)	ND(110)	ND(21)
Total PCBs	mg/kg	670 J	9.5	1,100 J	0.32 J	0.19 J	ND(0.20)	0.097 J	0.16 J	38 J	4,200 J	100 J
Miscellaneous Parameters												
% Moisture	%	11.0	4.20	26.0	3.10	9.30	7.00	8.00	8.20	13.0	16.0	15.0
% Solids	%	89.0	96.0	74.0	97.0	91.0	93.0	92.0	92.0	87.0	84.0	85.0

TABLE 6
SUMMARY OF PRE-CONSTRUCTION VERIFICATION PCB SOIL SAMPLE DATA- ELM STREET AREA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

Location ID: Sample Depth(Feet): Date Collected:	Units	SW-K3-K4 11 - 13 04/18/12	SW-K5-K6 3 - 5 10/02/12	SW-K5-K6 7 - 9 10/02/12	SW-K5-K6 9 - 11 10/02/12	SW-K5-K6 11 - 13 10/02/12	SW-K5-K6 13 - 15 10/02/12	SW-Q1-Q2 10 - 12 04/24/12	SW-Q1-Q2 16 - 18 04/24/12	SW-Q3-Q4 7 - 9 04/25/12	SW-Q3-Q4 12 - 14 04/25/12	SW-Q3-Q4 17 - 19 04/25/12
PCBs												
Aroclor 1016	mg/kg	ND(0.28) [ND(2.4)]	ND(0.24) [ND(0.19)]	ND(0.20)	ND(0.27)	ND(0.20)	ND(0.25)	ND(230)	ND(0.24)	ND(2.2)	ND(12)	ND(48)
Aroclor 1221	mg/kg	ND(0.28) [ND(2.4)]	ND(0.24) [ND(0.19)]	ND(0.20)	ND(0.27)	ND(0.20)	ND(0.25)	ND(230)	ND(0.24)	ND(2.2)	ND(12)	ND(48)
Aroclor 1232	mg/kg	ND(0.28) [ND(2.4)]	ND(0.24) [ND(0.19)]	ND(0.20)	ND(0.27)	ND(0.20)	ND(0.25)	ND(230)	ND(0.24)	ND(2.2)	ND(12)	ND(48)
Aroclor 1242	mg/kg	ND(0.28) [ND(2.4)]	1.1 J [ND(0.19)]	0.65 J	ND(0.27)	ND(0.20)	ND(0.25)	9,100 J	5.0	ND(2.2)	ND(12)	ND(48)
Aroclor 1248	mg/kg	10 J [19 J]	ND(0.24) [2.4 J]	ND(0.20)	ND(0.27)	ND(0.20)	ND(0.25)	ND(230)	ND(0.24)	8.3	180	56
Aroclor 1254	mg/kg	ND(0.28) [ND(2.4)]	ND(0.24) [ND(0.19)]	ND(0.20)	ND(0.27)	ND(0.20)	ND(0.25)	ND(230)	ND(0.24)	16	ND(12)	ND(48)
Aroclor 1260	mg/kg	0.68 JN [ND(2.4)]	ND(0.24) [ND(0.19)]	ND(0.20)	ND(0.27)	0.26 J	ND(0.25)	ND(230)	ND(0.24)	ND(2.2)	8.5 J	ND(48)
Total PCBs	mg/kg	11 JN [19 J]	1.1 J [2.4 J]	0.65 J	ND(0.27)	0.26 J	ND(0.25)	9,100 J	5.0	24	190 J	56
Miscellaneous Parameters												
% Moisture	%	29.0 [16.0]	8.40 [9.90]	13.0	12.0	6.60	15.0	7.00	18.0	18.0	15.0	12.0
% Solids	%	71.0 [84.0]	92.0 [90.0]	87.0	88.0	93.0	85.0	93.0	82.0	82.0	85.0	88.0

TABLE 6
SUMMARY OF PRE-CONSTRUCTION VERIFICATION PCB SOIL SAMPLE DATA- ELM STREET AREA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

Location ID: Sample Depth(Feet): Date Collected:	Units	SW-Q5 11 - 13 04/25/12	SW-Q5 14 - 16 04/25/12	SW-Q5 18 - 20 04/25/12	SW-Q6-Q7 10 - 12 04/24/12	SW-Q6-Q7 16 - 18 04/24/12	SW-Q8-Q9 8 - 10 10/02/12	SW-Q8-Q9 10 - 12 10/02/12	SW-Q8-Q9 12 - 14 10/02/12	SW-Q8-Q9 16 - 18 10/02/12	SW-Q10 6 - 8 10/02/12	SW-Q10 9 - 11 10/02/12
PCBs												
Aroclor 1016	mg/kg	ND(1.2)	ND(2.3)	ND(0.26)	ND(1.3)	ND(14)	ND(1.2)	ND(0.21)	ND(4.2)	ND(4.7)	ND(0.20)	ND(0.24)
Aroclor 1221	mg/kg	ND(1.2)	ND(2.3)	ND(0.26)	ND(1.3)	ND(14)	ND(1.2)	ND(0.21)	ND(4.2)	ND(4.7)	ND(0.20)	ND(0.24)
Aroclor 1232	mg/kg	ND(1.2)	ND(2.3)	ND(0.26)	ND(1.3)	ND(14)	ND(1.2)	ND(0.21)	ND(4.2)	ND(4.7)	ND(0.20)	ND(0.24)
Aroclor 1242	mg/kg	5.5 J	22 J	0.85 J	ND(1.3)	ND(14)	8.7 J	ND(0.21)	33 J	32 J	ND(0.20)	ND(0.24)
Aroclor 1248	mg/kg	ND(1.2)	ND(2.3)	ND(0.26)	24	38	ND(1.2)	0.43 J	ND(4.2)	ND(4.7)	ND(0.20)	ND(0.24)
Aroclor 1254	mg/kg	ND(1.2)	ND(2.3)	ND(0.26)	ND(1.3)	ND(14)	ND(1.2)	0.29 J	ND(4.2)	ND(4.7)	ND(0.20)	ND(0.24)
Aroclor 1260	mg/kg	ND(1.2)	ND(2.3)	ND(0.26)	ND(1.3)	ND(14)	ND(1.2)	ND(0.21)	ND(4.2)	ND(4.7)	ND(0.20)	ND(0.24)
Total PCBs	mg/kg	5.5 J	22 J	0.85 J	24	38	8.7 J	0.72 J	33 J	32 J	ND(0.20)	ND(0.24)
Miscellaneous Parameters												
% Moisture	%	16.0	14.0	13.0	22.0	19.0	8.20	6.40	8.20	12.0	2.30	3.00
% Solids	%	84.0	86.0	87.0	78.0	81.0	92.0	94.0	92.0	88.0	98.0	97.0

TABLE 6
SUMMARY OF PRE-CONSTRUCTION VERIFICATION PCB SOIL SAMPLE DATA- ELM STREET AREA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

Location ID: Sample Depth(Feet): Date Collected:	Units	SW-Q10 11 - 13 10/02/12	SW-Q10 13 - 15 10/02/12	SW-Q10 16 - 18 10/02/12	SW-V3-V4 18 - 20 05/02/12	SW-V3-V4 21 - 23 05/02/12	SW-V5-V6 14 - 16 04/30/12	SW-V5-V6 19 - 21 05/01/12	SW-V5-V6 22 - 24 05/01/12	SW-V7 17 - 19 04/30/12	SW-V7 21 - 23 04/30/12	SW-V8-V9 13 - 15 10/04/12
PCBs												
Aroclor 1016	mg/kg	ND(0.22)	ND(0.19)	ND(0.23)	ND(54)	ND(0.25)	ND(110)	ND(43)	ND(58)	ND(110)	ND(33)	ND(0.26)
Aroclor 1221	mg/kg	ND(0.22)	ND(0.19)	ND(0.23)	680 J	8.9 JN	ND(110)	ND(43)	ND(58)	ND(110)	ND(33)	ND(0.26)
Aroclor 1232	mg/kg	ND(0.22)	ND(0.19)	ND(0.23)	ND(54)	ND(0.25)	ND(110)	ND(43)	ND(58)	ND(110)	95 J	ND(0.26)
Aroclor 1242	mg/kg	ND(0.22)	2.0 J	ND(0.23)	ND(54)	1.1 J	720	910 J	270	1,000	ND(33)	0.33
Aroclor 1248	mg/kg	1.6	ND(0.19)	ND(0.23)	ND(54)	ND(0.25)	ND(110)	ND(43)	ND(58)	ND(110)	ND(33)	ND(0.26)
Aroclor 1254	mg/kg	1.4	2.3	ND(0.23)	27 J	ND(0.25)	ND(110)	ND(43)	ND(58)	ND(110)	13 J	ND(0.26)
Aroclor 1260	mg/kg	ND(0.22)	ND(0.19)	ND(0.23)	ND(54)	ND(0.25)	ND(110)	ND(43)	70	ND(110)	ND(33)	ND(0.26)
Total PCBs	mg/kg	3.0	4.3 J	ND(0.23)	710 J	10 JN	720	910 J	340	1,000	110 J	0.33
Miscellaneous Parameters												
% Moisture	%	3.60	3.60	5.70	23.0	29.0	12.0	17.0	24.0	13.0	28.0	9.30
% Solids	%	96.0	96.0	94.0	77.0	71.0	88.0	83.0	76.0	87.0	72.0	91.0

TABLE 6
SUMMARY OF PRE-CONSTRUCTION VERIFICATION PCB SOIL SAMPLE DATA- ELM STREET AREA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

Location ID: Sample Depth(Feet): Date Collected:	Units	SW-V8-V9 17 - 19 10/04/12	SW-V8-V9 19 - 21 10/04/12	SW-V8-V9 21 - 23 10/04/12	SW-V8-V9 23 - 24 10/04/12	SW-V10-V11 13 - 15 10/03/12	SW-V10-V11 15 - 17 10/03/12	SW-V10-V11 17 - 19 10/03/12	SW-V10-V11 19 - 20 10/03/12	SW-V10-V11 20 - 22 10/03/12	SW-V10-V11 22 - 23 10/03/12	SW-V10-V11 23 - 25 10/03/12
PCBs												
Aroclor 1016	mg/kg	ND(0.28)	ND(0.27)	ND(0.33)	ND(0.35)	ND(13)	ND(1.3)	ND(0.22)	ND(0.23) [ND(0.23)]	ND(2.2)	ND(0.24)	ND(0.23)
Aroclor 1221	mg/kg	ND(0.28)	ND(0.27)	ND(0.33)	ND(0.35)	ND(13)	ND(1.3)	ND(0.22)	ND(0.23) [ND(0.23)]	ND(2.2)	ND(0.24)	ND(0.23)
Aroclor 1232	mg/kg	ND(0.28)	ND(0.27)	ND(0.33)	ND(0.35)	ND(13)	ND(1.3)	ND(0.22)	ND(0.23) [ND(0.23)]	ND(2.2)	ND(0.24)	ND(0.23)
Aroclor 1242	mg/kg	5.1	3.5 J	0.74 J	ND(0.35)	37 J	15	0.12 J	0.058 J [0.065 J]	17 J	ND(0.24)	ND(0.23)
Aroclor 1248	mg/kg	ND(0.28)	ND(0.27)	ND(0.33)	ND(0.35)	ND(13)	ND(1.3)	ND(0.22)	ND(0.23) [ND(0.23)]	ND(2.2)	1.2	0.22 J
Aroclor 1254	mg/kg	8.2	ND(0.27)	ND(0.33)	ND(0.35)	ND(13)	ND(1.3)	ND(0.22)	ND(0.23) [ND(0.23)]	ND(2.2)	ND(0.24)	0.52
Aroclor 1260	mg/kg	ND(0.28)	ND(0.27)	ND(0.33)	ND(0.35)	ND(13)	ND(1.3)	ND(0.22)	ND(0.23) [ND(0.23)]	ND(2.2)	ND(0.24)	ND(0.23)
Total PCBs	mg/kg	13	3.5 J	0.74 J	ND(0.35)	37 J	15	0.12 J	0.058 J [0.065 J]	17 J	1.2	0.74 J
Miscellaneous Parameters												
% Moisture	%	17.0	16.0	30.0	32.0	12.0	12.0	12.0	13.0 [11.0]	11.0	17.0	16.0
% Solids	%	83.0	84.0	70.0	68.0	88.0	88.0	88.0	87.0 [89.0]	89.0	83.0	84.0

TABLE 6
SUMMARY OF PRE-CONSTRUCTION VERIFICATION PCB SOIL SAMPLE DATA- ELM STREET AREA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

Location ID: Sample Depth(Feet): Date Collected:	Units	SW-V10-V11 25 - 27 10/03/12	SW-V12 15 - 17 10/03/12	SW-V12 17 - 19 10/03/12	SW-V12 19 - 21 10/03/12	SW-V12 21 - 23 10/03/12	SW-V12 23 - 25 10/03/12	SW-V13 14 - 16 10/02/12	SW-V13 16 - 18 10/02/12	SW-V13 18 - 20 10/02/12	SW-V13 20 - 21 10/02/12	SW-V13 21 - 23 10/02/12
PCBs												
Aroclor 1016	mg/kg	ND(0.39)	ND(48)	ND(0.26)	ND(51)	ND(55)	ND(0.38)	ND(0.25)	ND(0.24)	ND(0.29)	ND(0.22)	ND(0.28)
Aroclor 1221	mg/kg	ND(0.39)	ND(48)	ND(0.26)	ND(51)	ND(55)	ND(0.38)	ND(0.25)	ND(0.24)	ND(0.29)	ND(0.22)	ND(0.28)
Aroclor 1232	mg/kg	ND(0.39)	ND(48)	ND(0.26)	ND(51)	ND(55)	ND(0.38)	ND(0.25)	ND(0.24)	ND(0.29)	ND(0.22)	ND(0.28)
Aroclor 1242	mg/kg	5.0 J	300 J	0.67 J	570	260 J	ND(0.38)	ND(0.25)	ND(0.24)	ND(0.29)	ND(0.22)	ND(0.28)
Aroclor 1248	mg/kg	ND(0.39)	ND(48)	ND(0.26)	ND(51)	ND(55)	0.46 J	ND(0.25)	6.7	ND(0.29)	0.086 J	ND(0.28)
Aroclor 1254	mg/kg	ND(0.39)	ND(48)	ND(0.26)	ND(51)	ND(55)	1.4 J	ND(0.25)	ND(0.24)	ND(0.29)	ND(0.22)	ND(0.28)
Aroclor 1260	mg/kg	ND(0.39)	ND(48)	ND(0.26)	ND(51)	ND(55)	1.2	ND(0.25)	ND(0.24)	ND(0.29)	ND(0.22)	ND(0.28)
Total PCBs	mg/kg	5.0 J	300 J	0.67 J	570	260 J	3.1 J	ND(0.25)	6.7	ND(0.29)	0.086 J	ND(0.28)
Miscellaneous Parameters												
% Moisture	%	44.0	7.70	14.0	10.0	17.0	43.0	10.0	7.30	21.0	9.00	13.0
% Solids	%	56.0	92.0	86.0	90.0	83.0	57.0	90.0	93.0	79.0	91.0	87.0

TABLE 6
SUMMARY OF PRE-CONSTRUCTION VERIFICATION PCB SOIL SAMPLE DATA- ELM STREET AREA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

Location ID: Sample Depth(Feet): Date Collected:	Units	SW-V13 23 - 24 10/02/12	SW-V13 24 - 26 10/02/12	SW-V13 26 - 28 10/02/12	SW-Z1-Z2 6 - 8 05/04/12	SW-Z1-Z2 11 - 13 05/04/12	SW-Z3-Z4 6 - 8 10/04/12	SW-Z3-Z4 9 - 11 10/04/12	SW-Z3-Z4 11 - 13 10/04/12	SW-Z3-Z4 13 - 15 10/04/12
PCBs										
Aroclor 1016	mg/kg	ND(0.29)	ND(0.45)	ND(0.33)	ND(0.26)	ND(25)	ND(0.22)	ND(0.22)	ND(0.23)	ND(0.23)
Aroclor 1221	mg/kg	ND(0.29)	ND(0.45)	ND(0.33)	ND(0.26)	ND(25)	ND(0.22)	ND(0.22)	ND(0.23)	ND(0.23)
Aroclor 1232	mg/kg	ND(0.29)	ND(0.45)	ND(0.33)	ND(0.26)	ND(25)	ND(0.22)	ND(0.22)	ND(0.23)	ND(0.23)
Aroclor 1242	mg/kg	ND(0.29)	ND(0.45)	ND(0.33)	ND(0.26)	ND(25)	ND(0.22)	ND(0.22)	ND(0.23)	ND(0.23)
Aroclor 1248	mg/kg	ND(0.29)	ND(0.45)	ND(0.33)	0.20 J	250	0.17 J	0.067 J	ND(0.23)	ND(0.23)
Aroclor 1254	mg/kg	ND(0.29)	ND(0.45)	ND(0.33)	ND(0.26)	ND(25)	ND(0.22)	ND(0.22)	ND(0.23)	ND(0.23)
Aroclor 1260	mg/kg	ND(0.29)	ND(0.45)	ND(0.33)	ND(0.26)	ND(25)	ND(0.22)	ND(0.22)	ND(0.23)	ND(0.23)
Total PCBs	mg/kg	ND(0.29)	ND(0.45)	ND(0.33)	0.20 J	250	0.17 J	0.067 J	ND(0.23)	ND(0.23)
Miscellaneous Parameters										
% Moisture	%	20.0	53.0	39.0	5.80	5.70	3.20	1.60	1.30	1.40
% Solids	%	80.0	47.0	61.0	94.0	94.0	97.0	98.0	99.0	99.0

Notes:
1. Samples were collected by ARCADIS and submitted to TestAmerica (formerly Severn Trent Laboratories) for analysis.
2. Field duplicate sample results are presented in brackets.
3. ND - Compound was not detected. The number in parentheses is the associated detection limit.

Data Qualifiers:

J - The compound was positively identified; however, the associated numerical value is an estimated concentration.

N - The analysis indicates the presence of a compound for which there is presumptive evidence to make a tentative identification. The associated numerical value is an estimated concentration only.

TABLE 7
SUMMARY OF SOIL CHARACTERIZATION SAMPLE DATA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

			Elm Street Area						
Location ID:			**SC-1**	**SC-2**	**SC-3**	**SC-4**	**SC-5**	**SC-6**	**SC-6**
Sample Depth(feet):		**TCLP Regulatory**	**0 - 2**	**0 - 2**	**0 - 2**	**0 - 2**	**5 - 7**	**0 - 2**	**3 - 4.5**
Date Collected:	**Units**	**Level**	**04/17/12**	**04/17/12**	**04/26/12**	**05/01/12**	**05/01/12**	**05/03/12**	**05/03/12**
Volatile Organics-TCLP									
1,1-Dichloroethene	mg/L	0.7	NA	NA	NA	NA	ND(0.010)	NA	ND(0.010)
1,2-Dichloroethane	mg/L	0.5	NA	NA	NA	NA	ND(0.010)	NA	ND(0.010)
2-Butanone	mg/L	200	NA	NA	NA	NA	ND(0.050)	NA	ND(0.050)
Benzene	mg/L	0.5	NA	NA	NA	NA	ND(0.010)	NA	ND(0.010)
Carbon Tetrachloride	mg/L	0.5	NA	NA	NA	NA	ND(0.010)	NA	ND(0.010)
Chlorobenzene	mg/L	100	NA	NA	NA	NA	ND(0.010)	NA	ND(0.010)
Chloroform	mg/L	6.0	NA	NA	NA	NA	ND(0.010)	NA	ND(0.010)
Tetrachloroethene	mg/L	0.7	NA	NA	NA	NA	ND(0.010)	NA	ND(0.010)
Trichloroethene	mg/L	0.5	NA	NA	NA	NA	ND(0.010)	NA	ND(0.010)
Vinyl chloride	mg/L	0.2	NA	NA	NA	NA	ND(0.010)	NA	ND(0.010)
Semivolatile Organics-TCLP									
1,4-Dichlorobenzene	mg/L	7.5	NA	NA	NA	NA	ND(0.010)	NA	ND(0.010)
2,4,5-Trichlorophenol	mg/L	400	NA	NA	NA	NA	ND(0.0050)	NA	ND(0.0050)
2,4,6-Trichlorophenol	mg/L	2.0	NA	NA	NA	NA	ND(0.0050)	NA	ND(0.0050)
2,4-Dinitrotoluene	mg/L	0.13	NA	NA	NA	NA	ND(0.0050)	NA	ND(0.0050)
2-Methylphenol	mg/L	200	NA	NA	NA	NA	ND(0.0050)	NA	0.0046 J
3-Methylphenol	mg/L	200	NA	NA	NA	NA	ND(0.010)	NA	ND(0.010)
4-Methylphenol	mg/L	200	NA	NA	NA	NA	ND(0.010)	NA	ND(0.010)
Hexachlorobenzene	mg/L	0.13	NA	NA	NA	NA	ND(0.0050)	NA	ND(0.0050)
Hexachlorobutadiene	mg/L	0.5	NA	NA	NA	NA	ND(0.0050)	NA	ND(0.0050)
Hexachloroethane	mg/L	3.0	NA	NA	NA	NA	ND(0.0050)	NA	ND(0.0050)
Nitrobenzene	mg/L	2.0	NA	NA	NA	NA	ND(0.0050)	NA	ND(0.0050)
Pentachlorophenol	mg/L	100	NA	NA	NA	NA	ND(0.010)	NA	ND(0.010)
Pyridine	mg/L	5.0	NA	NA	NA	NA	ND(0.025)	NA	ND(0.025)
Pesticides-TCLP									
Heptachlor Epoxide	mg/L	- -	NA	NA	NA	NA	ND(0.00020)	NA	ND(0.00020)
Chlordane	mg/L	0.03	NA	NA	NA	NA	ND(0.0020)	NA	ND(0.0020)
Endrin	mg/L	0.02	NA	NA	NA	NA	ND(0.00020)	NA	ND(0.00020)
Heptachlor	mg/L	0.008	NA	NA	NA	NA	ND(0.00020)	NA	ND(0.00020)
Gamma-BHC	mg/L	0.4	NA	NA	NA	NA	0.000065 Jp	NA	ND(0.00020)
Methoxychlor	mg/L	10	NA	NA	NA	NA	ND(0.00020)	NA	ND(0.00020)
Toxaphene	mg/L	0.5	NA	NA	NA	NA	ND(0.0020)	NA	ND(0.0020)
Herbicides-TCLP									
2,4-D	mg/L	10	NA	NA	NA	NA	ND(0.0020)	NA	ND(0.0020)
2,4,5-TP (Silvex)	mg/L	1.0	NA	NA	NA	NA	ND(0.0020)	NA	ND(0.0020)
PCBs									
Aroclor 1016	mg/kg	- -	ND(0.22)	ND(1.0)	ND(24)	ND(56)	ND(2.1)	ND(230)	ND(17)
Aroclor 1221	mg/kg	- -	ND(0.22)	ND(1.0)	ND(24)	ND(56)	ND(2.1)	ND(230)	ND(17)
Aroclor 1232	mg/kg	- -	ND(0.22)	ND(1.0)	ND(24)	ND(56)	ND(2.1)	ND(230)	ND(17)
Aroclor 1242	mg/kg	- -	ND(0.22)	ND(1.0)	ND(24)	ND(56)	ND(2.1)	ND(230)	ND(17)
Aroclor 1248	mg/kg	- -	2.5 p	30 p	210	790 p	25 p	1,300	46
Aroclor 1254	mg/kg	- -	ND(0.22)	ND(1.0)	ND(24)	ND(56)	ND(2.1)	ND(230)	ND(17)
Aroclor 1260	mg/kg	- -	0.14 Jp	ND(1.0)	ND(24)	ND(56)	ND(2.1)	ND(230)	ND(17)
Total PCBs	mg/kg	- -	2.6 Jp	30 p	210	790 p	25 p	1,300	46
Inorganics-TCLP									
Arsenic	mg/L	5.0	ND(0.01)	0.0058 J	0.011	ND(0.01)	ND(0.01)	ND(0.01)	ND(0.01)
Barium	mg/L	100	0.2 B	0.26 B	0.39 B	0.29 B	0.11 B	0.31 B	0.52 B
Cadmium	mg/L	1.0	0.0012 B	0.0018 B	0.002	0.0011	0.00074 J	0.00073 J	0.0008 J
Chromium	mg/L	5.0	0.0028 JB	0.0092 B	0.017 B	0.0019 JB	0.0029 JB	0.0042 B	0.14 B
Lead	mg/L	5.0	0.18	0.15	0.41	0.15	0.017	0.3	2.4
Mercury	mg/L	0.2	ND(0.0002)	ND(0.0002)	ND(0.0002 *)	ND(0.0002)	ND(0.0002)	0.019 B	0.00059 B
Selenium	mg/L	1.0	ND(0.015)	ND(0.015)	ND(0.015)	ND(0.015)	ND(0.015)	ND(0.015)	ND(0.015)
Silver	mg/L	5.0	ND(0.003)	ND(0.003)	ND(0.003)	ND(0.003)	ND(0.003)	ND(0.003)	ND(0.003)
Miscellaneous Parameters									
% Moisture	%	- -	7.60	7.10	13.0	16.0	4.10	7.60	28.0
% Solids	%	- -	92.0	93.0	87.0	84.0	96.0	92.0	72.0
Cyanide, Reactive	mg/kg	- -	NA	NA	NA	NA	NA	NA	NA
Flashpoint	Degrees F	- -	NA	NA	NA	NA	NA	NA	NA
pH	SU	- -	NA	NA	NA	NA	NA	NA	NA
Sulfide, Reactive	mg/kg	- -	NA	NA	NA	NA	NA	NA	NA

TABLE 7
SUMMARY OF SOIL CHARACTERIZATION SAMPLE DATA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

			Elm Street Area							
Location ID:			**SC-6**	**SC-6**	**SC-7**	**SC-7**	**SC-7**	**SC-8**	**SC-8**	**SC-8**
Sample Depth(feet):		**TCLP Regulatory**	**7 - 9**	**12 - 14**	**0 - 2**	**7 - 9**	**12 - 14**	**0 - 2**	**7 - 9**	**12 - 14**
Date Collected:	**Units**	**Level**	**05/03/12**	**05/03/12**	**05/03/12**	**05/03/12**	**05/03/12**	**05/03/12**	**05/03/12**	**05/03/12**
Volatile Organics-TCLP										
1,1-Dichloroethene	mg/L	0.7	NA	NA	ND(0.010)	ND(0.010)	ND(0.010)	NA	NA	NA
1,2-Dichloroethane	mg/L	0.5	NA	NA	ND(0.010)	ND(0.010)	ND(0.010)	NA	NA	NA
2-Butanone	mg/L	200	NA	NA	ND(0.050)	ND(0.050)	ND(0.050)	NA	NA	NA
Benzene	mg/L	0.5	NA	NA	ND(0.010)	ND(0.010)	ND(0.010)	NA	NA	NA
Carbon Tetrachloride	mg/L	0.5	NA	NA	ND(0.010)	ND(0.010)	ND(0.010)	NA	NA	NA
Chlorobenzene	mg/L	100	NA	NA	ND(0.010)	ND(0.010)	ND(0.010)	NA	NA	NA
Chloroform	mg/L	6.0	NA	NA	ND(0.010)	ND(0.010)	ND(0.010)	NA	NA	NA
Tetrachloroethene	mg/L	0.7	NA	NA	ND(0.010)	ND(0.010)	ND(0.010)	NA	NA	NA
Trichloroethene	mg/L	0.5	NA	NA	ND(0.010)	ND(0.010)	ND(0.010)	NA	NA	NA
Vinyl chloride	mg/L	0.2	NA	NA	ND(0.010)	ND(0.010)	ND(0.010)	NA	NA	NA
Semivolatile Organics-TCLP										
1,4-Dichlorobenzene	mg/L	7.5	NA	NA	ND(0.010)	ND(0.010)	ND(0.010)	NA	NA	NA
2,4,5-Trichlorophenol	mg/L	400	NA	NA	ND(0.0050)	ND(0.0050)	ND(0.0050)	NA	NA	NA
2,4,6-Trichlorophenol	mg/L	2.0	NA	NA	ND(0.0050)	ND(0.0050)	ND(0.0050)	NA	NA	NA
2,4-Dinitrotoluene	mg/L	0.13	NA	NA	ND(0.0050)	ND(0.0050)	ND(0.0050)	NA	NA	NA
2-Methylphenol	mg/L	200	NA	NA	ND(0.0050)	ND(0.0050)	0.0058	NA	NA	NA
3-Methylphenol	mg/L	200	NA	NA	ND(0.010)	ND(0.010)	0.0020 J	NA	NA	NA
4-Methylphenol	mg/L	200	NA	NA	ND(0.010)	ND(0.010)	0.0020 J	NA	NA	NA
Hexachlorobenzene	mg/L	0.13	NA	NA	ND(0.0050)	ND(0.0050)	ND(0.0050)	NA	NA	NA
Hexachlorobutadiene	mg/L	0.5	NA	NA	ND(0.0050)	ND(0.0050)	ND(0.0050)	NA	NA	NA
Hexachloroethane	mg/L	3.0	NA	NA	ND(0.0050)	ND(0.0050)	ND(0.0050)	NA	NA	NA
Nitrobenzene	mg/L	2.0	NA	NA	ND(0.0050)	ND(0.0050)	ND(0.0050)	NA	NA	NA
Pentachlorophenol	mg/L	100	NA	NA	ND(0.010)	ND(0.010)	ND(0.010)	NA	NA	NA
Pyridine	mg/L	5.0	NA	NA	ND(0.025)	ND(0.025)	ND(0.025)	NA	NA	NA
Pesticides-TCLP										
Heptachlor Epoxide	mg/L	- -	NA	NA	ND(0.00020)	ND(0.00020)	ND(0.0040)	NA	NA	NA
Chlordane	mg/L	0.03	NA	NA	ND(0.0020)	ND(0.0020)	ND(0.040)	NA	NA	NA
Endrin	mg/L	0.02	NA	NA	ND(0.00020)	ND(0.00020)	ND(0.0040)	NA	NA	NA
Heptachlor	mg/L	0.008	NA	NA	0.000063 J	ND(0.00020)	ND(0.0040)	NA	NA	NA
Gamma-BHC	mg/L	0.4	NA	NA	0.000064 Jp	ND(0.00020)	ND(0.0040)	NA	NA	NA
Methoxychlor	mg/L	10	NA	NA	ND(0.00020)	ND(0.00020)	ND(0.0040)	NA	NA	NA
Toxaphene	mg/L	0.5	NA	NA	ND(0.0020)	ND(0.0020)	ND(0.040)	NA	NA	NA
Herbicides-TCLP										
2,4-D	mg/L	10	NA	NA	NA	ND(0.0020)	ND(0.0020)	NA	NA	NA
2,4,5-TP (Silvex)	mg/L	1.0	NA	NA	NA	ND(0.0020)	ND(0.0020)	NA	NA	NA
PCBs										
Aroclor 1016	mg/kg	- -	ND(23)	ND(2.1)	ND(120)	ND(0.22)	ND(28)	ND(300)	ND(20)	ND(2.5)
Aroclor 1221	mg/kg	- -	ND(23)	ND(2.1)	ND(120)	ND(0.22)	ND(28)	ND(300)	ND(20)	ND(2.5)
Aroclor 1232	mg/kg	- -	ND(23)	ND(2.1)	ND(120)	ND(0.22)	ND(28)	ND(300)	ND(20)	ND(2.5)
Aroclor 1242	mg/kg	- -	ND(23)	5.6	ND(120)	ND(0.22)	ND(28)	ND(300)	ND(20)	ND(2.5)
Aroclor 1248	mg/kg	- -	79	ND(2.1)	120	0.83	64	1,200	84	8.7
Aroclor 1254	mg/kg	- -	ND(23)	ND(2.1)	ND(120)	ND(0.22)	ND(28)	ND(300)	ND(20)	ND(2.5)
Aroclor 1260	mg/kg	- -	ND(23)	ND(2.1)	ND(120)	ND(0.22)	ND(28)	ND(300)	ND(20)	ND(2.5)
Total PCBs	mg/kg	- -	79	5.6	120	0.83	64	1,200	84	8.7
Inorganics-TCLP										
Arsenic	mg/L	5.0	ND(0.01)	0.029	0.0084 J	ND(0.01)	ND(0.01)	0.0086 J	ND(0.01)	0.017
Barium	mg/L	100	2.5 B	0.17 B	0.27 B	0.15 B	0.13 B	0.73 B	0.56 B	0.34 B
Cadmium	mg/L	1.0	0.0019	0.0029	0.0014	0.00053 J	0.00063 J	0.0048	0.0032	0.0041
Chromium	mg/L	5.0	0.031 B	0.032 B	0.009 B	0.0024 JB	0.0042 B	0.19 B	0.055 B	0.034 B
Lead	mg/L	5.0	0.47	0.053	0.19	0.039	0.0065	**5.3**	2.5	0.16
Mercury	mg/L	0.2	0.00021 B	0.00012 JB	ND(0.0002)	ND(0.0002)	0.00013 JB	0.00025 B	ND(0.0002)	0.002 B
Selenium	mg/L	1.0	ND(0.015)	ND(0.015)	ND(0.015)	ND(0.015)	ND(0.015)	ND(0.015)	ND(0.015)	ND(0.015)
Silver	mg/L	5.0	ND(0.003)	ND(0.003)	ND(0.003)	ND(0.003)	ND(0.003)	ND(0.003)	ND(0.003)	ND(0.003)
Miscellaneous Parameters										
% Moisture	%	- -	13.0	9.30	12.0	5.50	12.0	18.0	15.0	19.0
% Solids	%	- -	87.0	91.0	88.0	94.0	88.0	82.0	85.0	81.0
Cyanide, Reactive	mg/kg	- -	NA	NA	NA	NA	NA	NA	NA	NA
Flashpoint	Degrees F	- -	NA	NA	NA	NA	NA	NA	NA	NA
pH	SU	- -	NA	NA	NA	NA	NA	NA	NA	NA
Sulfide, Reactive	mg/kg	- -	NA	NA	NA	NA	NA	NA	NA	NA

TABLE 7
SUMMARY OF SOIL CHARACTERIZATION SAMPLE DATA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

			Elm Street Area						
Location ID:			**SC-9**	**SC-10**	**SC-11**	**SC-12**	**SC-13**	**SC-14**	**SC-15 (RESIN)**
Sample Depth(feet):		**TCLP Regulatory**	**0 - 2**	**0 - 2**	**1 - 3**	**0 - 2**	**0 - 2**	**4 - 6**	**1 - 1.5**
Date Collected:	**Units**	**Level**	**04/17/12**	**04/18/12**	**04/25/12**	**04/18/12**	**04/26/12**	**04/26/12**	**04/20/12**
Volatile Organics-TCLP									
1,1-Dichloroethene	mg/L	0.7	NA	NA	NA	NA	NA	ND(0.010)	ND(0.010)
1,2-Dichloroethane	mg/L	0.5	NA	NA	NA	NA	NA	ND(0.010)	ND(0.010)
2-Butanone	mg/L	200	NA	NA	NA	NA	NA	ND(0.050)	ND(0.050)
Benzene	mg/L	0.5	NA	NA	NA	NA	NA	ND(0.010)	ND(0.010)
Carbon Tetrachloride	mg/L	0.5	NA	NA	NA	NA	NA	ND(0.010)	ND(0.010)
Chlorobenzene	mg/L	100	NA	NA	NA	NA	NA	ND(0.010)	ND(0.010)
Chloroform	mg/L	6.0	NA	NA	NA	NA	NA	ND(0.010)	ND(0.010)
Tetrachloroethene	mg/L	0.7	NA	NA	NA	NA	NA	ND(0.010)	ND(0.010)
Trichloroethene	mg/L	0.5	NA	NA	NA	NA	NA	0.0052 J	ND(0.010)
Vinyl chloride	mg/L	0.2	NA	NA	NA	NA	NA	ND(0.010)	ND(0.010)
Semivolatile Organics-TCLP									
1,4-Dichlorobenzene	mg/L	7.5	NA	NA	NA	NA	NA	ND(0.010)	NA
2,4,5-Trichlorophenol	mg/L	400	NA	NA	NA	NA	NA	ND(0.0050)	NA
2,4,6-Trichlorophenol	mg/L	2.0	NA	NA	NA	NA	NA	ND(0.0050)	NA
2,4-Dinitrotoluene	mg/L	0.13	NA	NA	NA	NA	NA	ND(0.0050)	NA
2-Methylphenol	mg/L	200	NA	NA	NA	NA	NA	ND(0.0050)	NA
3-Methylphenol	mg/L	200	NA	NA	NA	NA	NA	ND(0.010)	NA
4-Methylphenol	mg/L	200	NA	NA	NA	NA	NA	ND(0.010)	NA
Hexachlorobenzene	mg/L	0.13	NA	NA	NA	NA	NA	ND(0.0050)	NA
Hexachlorobutadiene	mg/L	0.5	NA	NA	NA	NA	NA	ND(0.0050)	NA
Hexachloroethane	mg/L	3.0	NA	NA	NA	NA	NA	ND(0.0050)	NA
Nitrobenzene	mg/L	2.0	NA	NA	NA	NA	NA	ND(0.0050)	NA
Pentachlorophenol	mg/L	100	NA	NA	NA	NA	NA	ND(0.010)	NA
Pyridine	mg/L	5.0	NA	NA	NA	NA	NA	ND(0.025)	NA
Pesticides-TCLP									
Heptachlor Epoxide	mg/L	- -	NA	NA	NA	NA	NA	ND(0.010)	NA
Chlordane	mg/L	0.03	NA	NA	NA	NA	NA	ND(0.10)	NA
Endrin	mg/L	0.02	NA	NA	NA	NA	NA	ND(0.010)	NA
Heptachlor	mg/L	0.008	NA	NA	NA	NA	NA	ND(0.010)	NA
Gamma-BHC	mg/L	0.4	NA	NA	NA	NA	NA	0.011	NA
Methoxychlor	mg/L	10	NA	NA	NA	NA	NA	ND(0.010)	NA
Toxaphene	mg/L	0.5	NA	NA	NA	NA	NA	ND(0.10)	NA
Herbicides-TCLP									
2,4-D	mg/L	10	NA	NA	NA	NA	NA	ND(0.0020)	NA
2,4,5-TP (Silvex)	mg/L	1.0	NA	NA	NA	NA	NA	ND(0.0020)	NA
PCBs									
Aroclor 1016	mg/kg	- -	ND(110)	ND(110)	ND(1,100)	ND(0.21)	ND(25)	ND(21)	ND(1,200)
Aroclor 1221	mg/kg	- -	ND(110)	ND(110)	ND(1,100)	ND(0.21)	ND(25)	ND(21)	ND(1,200)
Aroclor 1232	mg/kg	- -	ND(110)	ND(110)	ND(1,100)	ND(0.21)	ND(25)	ND(21)	ND(1,200)
Aroclor 1242	mg/kg	- -	ND(110)	ND(110)	9,000	4.2 p	ND(25)	ND(21)	7,200 p
Aroclor 1248	mg/kg	- -	420 p	810	ND(1,100)	ND(0.21)	55	440	ND(1,200)
Aroclor 1254	mg/kg	- -	ND(110)	ND(110)	ND(1,100)	ND(0.21)	ND(25)	ND(21)	ND(1,200)
Aroclor 1260	mg/kg	- -	ND(110)	ND(110)	ND(1,100)	ND(0.21)	ND(25)	ND(21)	ND(1,200)
Total PCBs	mg/kg	- -	420 p	810	9,000	4.2 p	55	440	7,200 p
Inorganics-TCLP									
Arsenic	mg/L	5.0	ND(0.01)	ND(0.01)	ND(0.01)	ND(0.01)	0.01	ND(0.01)	0.006 J
Barium	mg/L	100	2 B	1.2 B	0.42 B	0.16 B	0.31 B	0.41 B	0.22 B
Cadmium	mg/L	1.0	0.0013 B	0.0015 B	0.0024	0.0006 JB	0.0017	0.0014	0.0018 B
Chromium	mg/L	5.0	0.033 B	0.022 B	0.14 B	ND(0.004)	0.0067 B	0.015 B	0.0029 JB
Lead	mg/L	5.0	**10.4**	0.59	1.7	0.007	0.11	0.22	0.41
Mercury	mg/L	0.2	ND(0.0002)	ND(0.0002)	ND(0.0002)	ND(0.0002)	ND(0.0002 *)	ND(0.0002 *)	ND(0.0002)
Selenium	mg/L	1.0	ND(0.015)	ND(0.015)	ND(0.015)	ND(0.015)	ND(0.015)	ND(0.015)	ND(0.015)
Silver	mg/L	5.0	ND(0.003)	ND(0.003)	ND(0.003)	ND(0.003)	ND(0.003)	ND(0.003)	ND(0.003)
Miscellaneous Parameters									
% Moisture	%	- -	6.10	5.80	6.60	3.40	8.40	11.0	5.90
% Solids	%	- -	94.0	94.0	93.0	97.0	92.0	89.0	94.0
Cyanide, Reactive	mg/kg	- -	ND(10.0)	NA	NA	NA	NA	NA	NA
Flashpoint	Degrees F	- -	>50.0	NA	NA	NA	NA	NA	NA
pH	SU	- -	6.86	NA	NA	NA	NA	NA	NA
Sulfide, Reactive	mg/kg	- -	2.00 JB	NA	NA	NA	NA	NA	NA

TABLE 7
SUMMARY OF SOIL CHARACTERIZATION SAMPLE DATA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

			Elm Street Area						
Location ID:			**SC-15**	**SC-16**	**SC-17**	**SC-18**	**SC-19**	**SC-19**	**SC-19**
Sample Depth(feet):		**TCLP Regulatory**	**3 - 5**	**9 - 11**	**0 - 2**	**0 - 2**	**5 - 7**	**5 - 7**	**5 - 7**
Date Collected:	**Units**	**Level**	**04/20/12**	**04/25/12**	**05/01/12**	**04/23/12**	**04/24/12**	**05/02/12**	**06/28/12**
Volatile Organics-TCLP									
1,1-Dichloroethene	mg/L	0.7	NA	NA	NA	NA	NA	NA	ND(0.010)
1,2-Dichloroethane	mg/L	0.5	NA	NA	NA	NA	NA	NA	ND(0.010)
2-Butanone	mg/L	200	NA	NA	NA	NA	NA	NA	ND(0.050)
Benzene	mg/L	0.5	NA	NA	NA	NA	NA	NA	ND(0.010)
Carbon Tetrachloride	mg/L	0.5	NA	NA	NA	NA	NA	NA	ND(0.010)
Chlorobenzene	mg/L	100	NA	NA	NA	NA	NA	NA	ND(0.010)
Chloroform	mg/L	6.0	NA	NA	NA	NA	NA	NA	ND(0.010)
Tetrachloroethene	mg/L	0.7	NA	NA	NA	NA	NA	NA	ND(0.010)
Trichloroethene	mg/L	0.5	NA	NA	NA	NA	NA	NA	ND(0.010)
Vinyl chloride	mg/L	0.2	NA	NA	NA	NA	NA	NA	ND(0.010)
Semivolatile Organics-TCLP									
1,4-Dichlorobenzene	mg/L	7.5	NA	NA	NA	NA	NA	NA	ND(0.010)
2,4,5-Trichlorophenol	mg/L	400	NA	NA	NA	NA	NA	NA	ND(0.0050)
2,4,6-Trichlorophenol	mg/L	2.0	NA	NA	NA	NA	NA	NA	ND(0.0050 *)
2,4-Dinitrotoluene	mg/L	0.13	NA	NA	NA	NA	NA	NA	ND(0.0050 *)
2-Methylphenol	mg/L	200	NA	NA	NA	NA	NA	NA	ND(0.0050)
3-Methylphenol	mg/L	200	NA	NA	NA	NA	NA	NA	ND(0.010)
4-Methylphenol	mg/L	200	NA	NA	NA	NA	NA	NA	ND(0.010)
Hexachlorobenzene	mg/L	0.13	NA	NA	NA	NA	NA	NA	ND(0.0050)
Hexachlorobutadiene	mg/L	0.5	NA	NA	NA	NA	NA	NA	ND(0.0050)
Hexachloroethane	mg/L	3.0	NA	NA	NA	NA	NA	NA	ND(0.0050)
Nitrobenzene	mg/L	2.0	NA	NA	NA	NA	NA	NA	ND(0.0050)
Pentachlorophenol	mg/L	100	NA	NA	NA	NA	NA	NA	ND(0.010)
Pyridine	mg/L	5.0	NA	NA	NA	NA	NA	NA	ND(0.025)
Pesticides-TCLP									
Heptachlor Epoxide	mg/L	- -	NA	NA	NA	NA	NA	NA	NA
Chlordane	mg/L	0.03	NA	NA	NA	NA	NA	NA	NA
Endrin	mg/L	0.02	NA	NA	NA	NA	NA	NA	NA
Heptachlor	mg/L	0.008	NA	NA	NA	NA	NA	NA	NA
Gamma-BHC	mg/L	0.4	NA	NA	NA	NA	NA	NA	NA
Methoxychlor	mg/L	10	NA	NA	NA	NA	NA	NA	NA
Toxaphene	mg/L	0.5	NA	NA	NA	NA	NA	NA	NA
Herbicides-TCLP									
2,4-D	mg/L	10	NA	NA	NA	NA	NA	NA	NA
2,4,5-TP (Silvex)	mg/L	1.0	NA	NA	NA	NA	NA	NA	NA
PCBs									
Aroclor 1016	mg/kg	- -	ND(100)	ND(0.26)	ND(44)	ND(47)	ND(1.1)	ND(2.2)	NA
Aroclor 1221	mg/kg	- -	ND(100)	ND(0.26)	ND(44)	ND(47)	ND(1.1)	ND(2.2)	NA
Aroclor 1232	mg/kg	- -	ND(100)	ND(0.26)	ND(44)	ND(47)	ND(1.1)	ND(2.2)	NA
Aroclor 1242	mg/kg	- -	490 p	ND(0.26)	ND(44)	ND(47)	ND(1.1)	ND(2.2)	NA
Aroclor 1248	mg/kg	- -	ND(100)	1.0	770 p	65	10	36 p	NA
Aroclor 1254	mg/kg	- -	ND(100)	ND(0.26)	ND(44)	ND(47)	ND(1.1)	ND(2.2)	NA
Aroclor 1260	mg/kg	- -	ND(100)	ND(0.26)	ND(44)	ND(47)	ND(1.1)	ND(2.2)	NA
Total PCBs	mg/kg	- -	490 p	1.0	770 p	65	10	36 p	NA
Inorganics-TCLP									
Arsenic	mg/L	5.0	ND(0.01)	0.0073 J	ND(0.01)	ND(0.01)	ND(0.01)	ND(0.01)	NA
Barium	mg/L	100	0.43 B	0.65 B	0.29 B	0.25 B	0.34 B	0.29 B	NA
Cadmium	mg/L	1.0	0.00077 JB	0.0076	0.0018	0.00082 J	0.00077 J	0.00098 J	NA
Chromium	mg/L	5.0	0.0012 JB	0.0026 JB	0.002 JB	0.0024 JB	0.0097 B	0.0014 JB	NA
Lead	mg/L	5.0	0.28	0.26	0.019	0.03	0.032	0.022	NA
Mercury	mg/L	0.2	ND(0.0002)	ND(0.0002 *)	ND(0.0002)	ND(0.0002)	ND(0.0002)	ND(0.0002)	NA
Selenium	mg/L	1.0	ND(0.015)	ND(0.015)	ND(0.015)	ND(0.015)	ND(0.015)	ND(0.015)	NA
Silver	mg/L	5.0	ND(0.003)	ND(0.003)	ND(0.003)	ND(0.003)	ND(0.003)	ND(0.003)	NA
Miscellaneous Parameters									
% Moisture	%	- -	9.80	21.0	5.20	9.90	6.70	7.10	NA
% Solids	%	- -	90.0	79.0	95.0	90.0	93.0	93.0	NA
Cyanide, Reactive	mg/kg	- -	NA	NA	NA	NA	NA	NA	NA
Flashpoint	Degrees F	- -	NA	NA	NA	NA	NA	NA	NA
pH	SU	- -	NA	NA	NA	NA	NA	NA	NA
Sulfide, Reactive	mg/kg	- -	NA	NA	NA	NA	NA	NA	NA

TABLE 7
SUMMARY OF SOIL CHARACTERIZATION SAMPLE DATA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

			Elm Street Area						
Location ID:			**SC-20**	**SC-21**	**SC-22**	**SC-23**	**SC-24**	**SC-25**	**SC-26**
Sample Depth(feet):		**TCLP Regulatory**	**6 - 8**	**0 - 2**	**5 - 7**	**0 - 2**	**0 - 2**	**7 - 9**	**7 - 9**
Date Collected:	**Units**	**Level**	**04/24/12**	**04/27/12**	**04/27/12**	**04/26/12**	**04/27/12**	**04/30/12**	**04/24/12**
Volatile Organics-TCLP									
1,1-Dichloroethene	mg/L	0.7	NA	NA	ND(0.010)	NA	NA	NA	NA
1,2-Dichloroethane	mg/L	0.5	NA	NA	ND(0.010)	NA	NA	NA	NA
2-Butanone	mg/L	200	NA	NA	ND(0.050)	NA	NA	NA	NA
Benzene	mg/L	0.5	NA	NA	ND(0.010)	NA	NA	NA	NA
Carbon Tetrachloride	mg/L	0.5	NA	NA	ND(0.010)	NA	NA	NA	NA
Chlorobenzene	mg/L	100	NA	NA	ND(0.010)	NA	NA	NA	NA
Chloroform	mg/L	6.0	NA	NA	ND(0.010)	NA	NA	NA	NA
Tetrachloroethene	mg/L	0.7	NA	NA	ND(0.010)	NA	NA	NA	NA
Trichloroethene	mg/L	0.5	NA	NA	ND(0.010)	NA	NA	NA	NA
Vinyl chloride	mg/L	0.2	NA	NA	ND(0.010)	NA	NA	NA	NA
Semivolatile Organics-TCLP									
1,4-Dichlorobenzene	mg/L	7.5	NA	NA	ND(0.010)	NA	NA	NA	NA
2,4,5-Trichlorophenol	mg/L	400	NA	NA	ND(0.0050)	NA	NA	NA	NA
2,4,6-Trichlorophenol	mg/L	2.0	NA	NA	ND(0.0050)	NA	NA	NA	NA
2,4-Dinitrotoluene	mg/L	0.13	NA	NA	ND(0.0050)	NA	NA	NA	NA
2-Methylphenol	mg/L	200	NA	NA	ND(0.0050)	NA	NA	NA	NA
3-Methylphenol	mg/L	200	NA	NA	ND(0.010)	NA	NA	NA	NA
4-Methylphenol	mg/L	200	NA	NA	ND(0.010)	NA	NA	NA	NA
Hexachlorobenzene	mg/L	0.13	NA	NA	ND(0.0050)	NA	NA	NA	NA
Hexachlorobutadiene	mg/L	0.5	NA	NA	ND(0.0050)	NA	NA	NA	NA
Hexachloroethane	mg/L	3.0	NA	NA	ND(0.0050)	NA	NA	NA	NA
Nitrobenzene	mg/L	2.0	NA	NA	ND(0.0050)	NA	NA	NA	NA
Pentachlorophenol	mg/L	100	NA	NA	ND(0.010)	NA	NA	NA	NA
Pyridine	mg/L	5.0	NA	NA	ND(0.025)	NA	NA	NA	NA
Pesticides-TCLP									
Heptachlor Epoxide	mg/L	- -	NA	NA	ND(0.00020)	NA	NA	NA	NA
Chlordane	mg/L	0.03	NA	NA	ND(0.0020)	NA	NA	NA	NA
Endrin	mg/L	0.02	NA	NA	ND(0.00020)	NA	NA	NA	NA
Heptachlor	mg/L	0.008	NA	NA	0.00015 Jp	NA	NA	NA	NA
Gamma-BHC	mg/L	0.4	NA	NA	0.00026 p	NA	NA	NA	NA
Methoxychlor	mg/L	10	NA	NA	ND(0.00020)	NA	NA	NA	NA
Toxaphene	mg/L	0.5	NA	NA	ND(0.0020)	NA	NA	NA	NA
Herbicides-TCLP									
2,4-D	mg/L	10	NA	NA	ND(0.0020)	NA	NA	NA	NA
2,4,5-TP (Silvex)	mg/L	1.0	NA	NA	ND(0.0020)	NA	NA	NA	NA
PCBs									
Aroclor 1016	mg/kg	- -	ND(54)	ND(0.24)	ND(20)	ND(25)	ND(1,300) [ND(2.0)]	ND(220)	ND(12)
Aroclor 1221	mg/kg	- -	ND(54)	ND(0.24)	ND(20)	ND(25)	ND(1,300) [ND(2.0)]	ND(220)	ND(12)
Aroclor 1232	mg/kg	- -	ND(54)	ND(0.24)	ND(20)	ND(25)	ND(1,300) [ND(2.0)]	ND(220)	ND(12)
Aroclor 1242	mg/kg	- -	54	ND(0.24)	ND(20)	ND(25)	ND(1,300) [ND(2.0)]	2,400	46
Aroclor 1248	mg/kg	- -	ND(54)	1.3	670	360	1,900 [16]	ND(220)	ND(12)
Aroclor 1254	mg/kg	- -	ND(54)	ND(0.24)	ND(20)	ND(25)	ND(1,300) [ND(2.0)]	ND(220)	ND(12)
Aroclor 1260	mg/kg	- -	ND(54)	ND(0.24)	ND(20)	ND(25)	ND(1,300) [ND(2.0)]	ND(220)	ND(12)
Total PCBs	mg/kg	- -	54	1.3	670	360	1,900 [16]	2,400	46
Inorganics-TCLP									
Arsenic	mg/L	5.0	ND(0.01)	ND(0.01)	ND(0.01)	ND(0.01)	ND(0.01) [ND(0.01)]	0.0066 J	ND(0.01)
Barium	mg/L	100	0.27 B	0.55 B	0.65 B	0.37 B	0.33 B [0.44 B]	0.28 B	2.3 B
Cadmium	mg/L	1.0	0.00085 J	0.00091 J	0.0019	0.0011	0.0021 [0.003]	ND(0.001)	0.11
Chromium	mg/L	5.0	0.0025 JB	0.014 B	0.013 B	0.022 B	0.23 B [0.31 B]	0.017 B	0.0068 B
Lead	mg/L	5.0	0.084	0.13	0.34	0.064	1.5 [2.2]	0.43	**26.5**
Mercury	mg/L	0.2	ND(0.0002)	ND(0.0002 *)	ND(0.0002 *)	ND(0.0002 *)	0.015 [0.0027]	0.006	ND(0.0002)
Selenium	mg/L	1.0	ND(0.015)	ND(0.015)	ND(0.015)	ND(0.015)	ND(0.015) [ND(0.015)]	ND(0.015)	0.0093 J
Silver	mg/L	5.0	ND(0.003)	ND(0.003)	ND(0.003)	ND(0.003)	ND(0.003) [ND(0.003)]	ND(0.003)	ND(0.003)
Miscellaneous Parameters									
% Moisture	%	- -	11.0	7.80	6.40	11.0	9.10 [11.0]	8.90	13.0
% Solids	%	- -	89.0	92.0	94.0	89.0	91.0 [89.0]	91.0	87.0
Cyanide, Reactive	mg/kg	- -	NA	NA	NA	NA	NA	NA	NA
Flashpoint	Degrees F	- -	NA	NA	NA	NA	NA	NA	NA
pH	SU	- -	NA	NA	NA	NA	NA	NA	NA
Sulfide, Reactive	mg/kg	- -	NA	NA	NA	NA	NA	NA	NA

TABLE 7
SUMMARY OF SOIL CHARACTERIZATION SAMPLE DATA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

			Elm Street Area					
Location ID:			**SC-27**	**SC-28**	**SC-29**	**SC-30**	**SC-31**	**SC-32**
Sample Depth(feet):		**TCLP Regulatory**	**12 - 14**	**0 - 2**	**0 - 2**	**0 - 2**	**7 - 9**	**0 - 2**
Date Collected:	**Units**	**Level**	**04/24/12**	**04/25/12**	**04/26/12**	**04/26/12**	**05/02/12**	**04/26/12**
Volatile Organics-TCLP								
1,1-Dichloroethene	mg/L	0.7	ND(0.010)	NA	NA	NA	NA	NA
1,2-Dichloroethane	mg/L	0.5	ND(0.010)	NA	NA	NA	NA	NA
2-Butanone	mg/L	200	ND(0.050)	NA	NA	NA	NA	NA
Benzene	mg/L	0.5	ND(0.010)	NA	NA	NA	NA	NA
Carbon Tetrachloride	mg/L	0.5	ND(0.010)	NA	NA	NA	NA	NA
Chlorobenzene	mg/L	100	ND(0.010)	NA	NA	NA	NA	NA
Chloroform	mg/L	6.0	ND(0.010)	NA	NA	NA	NA	NA
Tetrachloroethene	mg/L	0.7	ND(0.010)	NA	NA	NA	NA	NA
Trichloroethene	mg/L	0.5	0.014	NA	NA	NA	NA	NA
Vinyl chloride	mg/L	0.2	ND(0.010)	NA	NA	NA	NA	NA
Semivolatile Organics-TCLP								
1,4-Dichlorobenzene	mg/L	7.5	ND(0.010)	NA	NA	NA	NA	NA
2,4,5-Trichlorophenol	mg/L	400	ND(0.0050)	NA	NA	NA	NA	NA
2,4,6-Trichlorophenol	mg/L	2.0	ND(0.0050)	NA	NA	NA	NA	NA
2,4-Dinitrotoluene	mg/L	0.13	ND(0.0050)	NA	NA	NA	NA	NA
2-Methylphenol	mg/L	200	ND(0.0050)	NA	NA	NA	NA	NA
3-Methylphenol	mg/L	200	ND(0.010)	NA	NA	NA	NA	NA
4-Methylphenol	mg/L	200	ND(0.010)	NA	NA	NA	NA	NA
Hexachlorobenzene	mg/L	0.13	ND(0.0050)	NA	NA	NA	NA	NA
Hexachlorobutadiene	mg/L	0.5	ND(0.0050)	NA	NA	NA	NA	NA
Hexachloroethane	mg/L	3.0	ND(0.0050)	NA	NA	NA	NA	NA
Nitrobenzene	mg/L	2.0	ND(0.0050)	NA	NA	NA	NA	NA
Pentachlorophenol	mg/L	100	ND(0.010 *)	NA	NA	NA	NA	NA
Pyridine	mg/L	5.0	ND(0.025)	NA	NA	NA	NA	NA
Pesticides-TCLP								
Heptachlor Epoxide	mg/L	- -	ND(0.00020)	NA	NA	NA	NA	NA
Chlordane	mg/L	0.03	ND(0.0020)	NA	NA	NA	NA	NA
Endrin	mg/L	0.02	ND(0.00020)	NA	NA	NA	NA	NA
Heptachlor	mg/L	0.008	ND(0.00020)	NA	NA	NA	NA	NA
Gamma-BHC	mg/L	0.4	ND(0.00020)	NA	NA	NA	NA	NA
Methoxychlor	mg/L	10	ND(0.00020)	NA	NA	NA	NA	NA
Toxaphene	mg/L	0.5	ND(0.0020)	NA	NA	NA	NA	NA
Herbicides-TCLP								
2,4-D	mg/L	10	ND(0.0020)	NA	NA	NA	NA	NA
2,4,5-TP (Silvex)	mg/L	1.0	ND(0.0020)	NA	NA	NA	NA	NA
PCBs								
Aroclor 1016	mg/kg	- -	ND(0.26)	ND(190) [ND(120)]	ND(2.1)	ND(130)	ND(2.6)	ND(1.2)
Aroclor 1221	mg/kg	- -	ND(0.26)	ND(190) [ND(120)]	ND(2.1)	ND(130)	ND(2.6)	ND(1.2)
Aroclor 1232	mg/kg	- -	ND(0.26)	ND(190) [ND(120)]	ND(2.1)	ND(130)	ND(2.6)	ND(1.2)
Aroclor 1242	mg/kg	- -	4.4	ND(190) [ND(120)]	ND(2.1)	ND(130)	15	ND(1.2)
Aroclor 1248	mg/kg	- -	ND(0.26)	490 [280]	10	130	ND(2.6)	4.3
Aroclor 1254	mg/kg	- -	ND(0.26)	ND(190) [ND(120)]	ND(2.1)	ND(130)	ND(2.6)	8.5
Aroclor 1260	mg/kg	- -	ND(0.26)	ND(190) [ND(120)]	ND(2.1)	ND(130)	ND(2.6)	3.7
Total PCBs	mg/kg	- -	4.4	490 [280]	10	130	15	17
Inorganics-TCLP								
Arsenic	mg/L	5.0	0.011	ND(0.01) [ND(0.01)]	ND(0.01)	ND(0.01)	0.0074 J	ND(0.01)
Barium	mg/L	100	1.7 B	0.52 B [0.59 B]	0.5 B	0.17 B	0.43 B	0.95 B
Cadmium	mg/L	1.0	0.07	0.0075 [0.0045]	0.0054	ND(0.001)	0.0012	0.0076
Chromium	mg/L	5.0	0.017 B	0.0031 JB [0.0027 JB]	0.0083 B	0.0027 JB	0.0026 JB	0.017 B
Lead	mg/L	5.0	2.8	1.1 [2]	0.41	0.019	0.21	1.1
Mercury	mg/L	0.2	0.00039	ND(0.0002) [ND(0.0002)]	ND(0.0002 *)	ND(0.0002 *)	ND(0.0002)	ND(0.0002 *)
Selenium	mg/L	1.0	ND(0.015)	ND(0.015) [ND(0.015)]	ND(0.015)	ND(0.015)	ND(0.015)	ND(0.015)
Silver	mg/L	5.0	ND(0.003)	ND(0.003) [ND(0.003)]	ND(0.003)	ND(0.003)	ND(0.003)	ND(0.003)
Miscellaneous Parameters								
% Moisture	%	- -	13.0	8.20 [9.00]	6.20	8.70	11.0	9.90
% Solids	%	- -	87.0	92.0 [91.0]	94.0	91.0	89.0	90.0
Cyanide, Reactive	mg/kg	- -	ND(10.0)	NA	NA	NA	NA	NA
Flashpoint	Degrees F	- -	>50.0	NA	NA	NA	NA	NA
pH	SU	- -	7.63	NA	NA	NA	NA	NA
Sulfide, Reactive	mg/kg	- -	ND(10.0)	NA	NA	NA	NA	NA

TABLE 7
SUMMARY OF SOIL CHARACTERIZATION SAMPLE DATA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

			Elm Street Area						
Location ID:			**SC-33**	**SC-34**	**SC-35**	**SC-36**	**SC-37**	**SC-38**	**SC-39**
Sample Depth(feet):		**TCLP Regulatory**	**5 - 7**	**12 - 14**	**20 - 22**	**0 - 2**	**3 - 5**	**0 - 2**	**0 - 2**
Date Collected:	**Units**	**Level**	**05/02/12**	**05/02/12**	**05/02/12**	**04/26/12**	**04/26/12**	**04/25/12**	**04/26/12**
Volatile Organics-TCLP									
1,1-Dichloroethene	mg/L	0.7	NA	ND(0.010)	NA	NA	ND(0.010)	NA	NA
1,2-Dichloroethane	mg/L	0.5	NA	ND(0.010)	NA	NA	ND(0.010)	NA	NA
2-Butanone	mg/L	200	NA	ND(0.050)	NA	NA	ND(0.050)	NA	NA
Benzene	mg/L	0.5	NA	ND(0.010)	NA	NA	ND(0.010)	NA	NA
Carbon Tetrachloride	mg/L	0.5	NA	ND(0.010)	NA	NA	ND(0.010)	NA	NA
Chlorobenzene	mg/L	100	NA	ND(0.010)	NA	NA	ND(0.010)	NA	NA
Chloroform	mg/L	6.0	NA	ND(0.010)	NA	NA	ND(0.010)	NA	NA
Tetrachloroethene	mg/L	0.7	NA	ND(0.010)	NA	NA	ND(0.010)	NA	NA
Trichloroethene	mg/L	0.5	NA	ND(0.010)	NA	NA	ND(0.010)	NA	NA
Vinyl chloride	mg/L	0.2	NA	ND(0.010)	NA	NA	ND(0.010)	NA	NA
Semivolatile Organics-TCLP									
1,4-Dichlorobenzene	mg/L	7.5	NA	ND(0.010)	NA	NA	ND(0.010)	NA	NA
2,4,5-Trichlorophenol	mg/L	400	NA	ND(0.0050)	NA	NA	ND(0.0050)	NA	NA
2,4,6-Trichlorophenol	mg/L	2.0	NA	ND(0.0050)	NA	NA	ND(0.0050)	NA	NA
2,4-Dinitrotoluene	mg/L	0.13	NA	ND(0.0050)	NA	NA	ND(0.0050)	NA	NA
2-Methylphenol	mg/L	200	NA	ND(0.0050)	NA	NA	ND(0.0050)	NA	NA
3-Methylphenol	mg/L	200	NA	ND(0.010)	NA	NA	ND(0.010)	NA	NA
4-Methylphenol	mg/L	200	NA	ND(0.010)	NA	NA	ND(0.010)	NA	NA
Hexachlorobenzene	mg/L	0.13	NA	ND(0.0050)	NA	NA	ND(0.0050)	NA	NA
Hexachlorobutadiene	mg/L	0.5	NA	ND(0.0050)	NA	NA	ND(0.0050)	NA	NA
Hexachloroethane	mg/L	3.0	NA	ND(0.0050)	NA	NA	ND(0.0050)	NA	NA
Nitrobenzene	mg/L	2.0	NA	ND(0.0050)	NA	NA	ND(0.0050)	NA	NA
Pentachlorophenol	mg/L	100	NA	ND(0.010)	NA	NA	ND(0.010)	NA	NA
Pyridine	mg/L	5.0	NA	ND(0.025)	NA	NA	ND(0.025)	NA	NA
Pesticides-TCLP									
Heptachlor Epoxide	mg/L	- -	NA	ND(0.00020)	NA	NA	ND(0.00020)	NA	NA
Chlordane	mg/L	0.03	NA	ND(0.0020)	NA	NA	ND(0.0020)	NA	NA
Endrin	mg/L	0.02	NA	ND(0.00020)	NA	NA	ND(0.00020)	NA	NA
Heptachlor	mg/L	0.008	NA	ND(0.00020)	NA	NA	ND(0.00020)	NA	NA
Gamma-BHC	mg/L	0.4	NA	ND(0.00020)	NA	NA	0.000083 Jp	NA	NA
Methoxychlor	mg/L	10	NA	ND(0.00020)	NA	NA	ND(0.00020)	NA	NA
Toxaphene	mg/L	0.5	NA	ND(0.0020)	NA	NA	ND(0.0020)	NA	NA
Herbicides-TCLP									
2,4-D	mg/L	10	NA	ND(0.0020)	NA	NA	ND(0.0020)	NA	NA
2,4,5-TP (Silvex)	mg/L	1.0	NA	ND(0.0020)	NA	NA	ND(0.0020)	NA	NA
PCBs									
Aroclor 1016	mg/kg	- -	ND(3.8)	ND(0.24)	ND(160)	ND(2.4)	ND(18)	ND(42)	ND(2.1)
Aroclor 1221	mg/kg	- -	ND(3.8)	ND(0.24)	ND(160)	ND(2.4)	ND(18)	ND(42)	ND(2.1)
Aroclor 1232	mg/kg	- -	ND(3.8)	ND(0.24)	ND(160)	ND(2.4)	ND(18)	ND(42)	ND(2.1)
Aroclor 1242	mg/kg	- -	ND(3.8)	ND(0.24)	4,100 p	ND(2.4)	ND(18)	960 p	ND(2.1)
Aroclor 1248	mg/kg	- -	69 p	3.6 p	ND(160)	5.9	15 J	ND(42)	8.3
Aroclor 1254	mg/kg	- -	ND(3.8)	ND(0.24)	ND(160)	ND(2.4)	ND(18)	ND(42)	ND(2.1)
Aroclor 1260	mg/kg	- -	ND(3.8)	ND(0.24)	ND(160)	ND(2.4)	ND(18)	ND(42)	ND(2.1)
Total PCBs	mg/kg	- -	69 p	3.6 p	4,100 p	5.9	15 J	960 p	8.3
Inorganics-TCLP									
Arsenic	mg/L	5.0	ND(0.01)	ND(0.01)	0.071	ND(0.01)	0.017	ND(0.01)	0.0068 J
Barium	mg/L	100	0.21 B	0.38 B	0.36 B	0.47 B	0.48 B	0.23 B	0.4 B
Cadmium	mg/L	1.0	0.0011	0.0021	0.0034	0.0023	0.0045	0.0016	0.0012
Chromium	mg/L	5.0	0.0069 B	0.002 JB	0.073 B	0.01 B	0.32 B	0.0092 B	0.012 B
Lead	mg/L	5.0	0.037	0.78	0.06	0.14	3.6	0.16	0.22
Mercury	mg/L	0.2	0.00015 J	ND(0.0002)	0.00073	ND(0.0002 *)	ND(0.0002 *)	ND(0.0002)	ND(0.0002 *)
Selenium	mg/L	1.0	ND(0.015)	ND(0.015)	ND(0.015)	ND(0.015)	ND(0.015)	ND(0.015)	ND(0.015)
Silver	mg/L	5.0	ND(0.003)	ND(0.003)	ND(0.003)	ND(0.003)	ND(0.003)	ND(0.003)	ND(0.003)
Miscellaneous Parameters									
% Moisture	%	- -	7.80	10.0	27.0	4.80	4.80	4.90	6.50
% Solids	%	- -	92.0	90.0	73.0	95.0	95.0	95.0	93.0
Cyanide, Reactive	mg/kg	- -	NA	NA	NA	NA	NA	NA	NA
Flashpoint	Degrees F	- -	NA	NA	NA	NA	NA	NA	NA
pH	SU	- -	NA	NA	NA	NA	NA	NA	NA
Sulfide, Reactive	mg/kg	- -	NA	NA	NA	NA	NA	NA	NA

TABLE 7
SUMMARY OF SOIL CHARACTERIZATION SAMPLE DATA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

			Elm Street Area			Mill Street Area				
Location ID:			**SC-D3-D4**	**SC-D5-D6**	**SC-G2 (RESIN)**	**SC-40**	**SC-41**	**SC-42**	**SC-43**	**SC-44**
Sample Depth(feet):		**TCLP Regulatory**	**0 - 2**	**0 - 2**	**11 - 13**	**0 - 2**	**4 - 6**	**7 - 9**	**0 - 2**	**5 - 7**
Date Collected:	**Units**	**Level**	**04/26/12**	**04/26/12**	**04/19/12**	**05/14/12**	**05/14/12**	**05/15/12**	**05/14/12**	**05/14/12**
Volatile Organics-TCLP										
1,1-Dichloroethene	mg/L	0.7	NA	NA	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
1,2-Dichloroethane	mg/L	0.5	NA	NA	0.013	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
2-Butanone	mg/L	200	NA	NA	ND(0.050)	ND(0.050)	ND(0.050)	ND(0.050)	ND(0.050)	ND(0.050)
Benzene	mg/L	0.5	NA	NA	0.0071 J	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Carbon Tetrachloride	mg/L	0.5	NA	NA	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Chlorobenzene	mg/L	100	NA	NA	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Chloroform	mg/L	6.0	NA	NA	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Tetrachloroethene	mg/L	0.7	NA	NA	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Trichloroethene	mg/L	0.5	NA	NA	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Vinyl chloride	mg/L	0.2	NA	NA	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Semivolatile Organics-TCLP										
1,4-Dichlorobenzene	mg/L	7.5	NA	NA	NA	NA	NA	NA	NA	NA
2,4,5-Trichlorophenol	mg/L	400	NA	NA	NA	NA	NA	NA	NA	NA
2,4,6-Trichlorophenol	mg/L	2.0	NA	NA	NA	NA	NA	NA	NA	NA
2,4-Dinitrotoluene	mg/L	0.13	NA	NA	NA	NA	NA	NA	NA	NA
2-Methylphenol	mg/L	200	NA	NA	NA	NA	NA	NA	NA	NA
3-Methylphenol	mg/L	200	NA	NA	NA	NA	NA	NA	NA	NA
4-Methylphenol	mg/L	200	NA	NA	NA	NA	NA	NA	NA	NA
Hexachlorobenzene	mg/L	0.13	NA	NA	NA	NA	NA	NA	NA	NA
Hexachlorobutadiene	mg/L	0.5	NA	NA	NA	NA	NA	NA	NA	NA
Hexachloroethane	mg/L	3.0	NA	NA	NA	NA	NA	NA	NA	NA
Nitrobenzene	mg/L	2.0	NA	NA	NA	NA	NA	NA	NA	NA
Pentachlorophenol	mg/L	100	NA	NA	NA	NA	NA	NA	NA	NA
Pyridine	mg/L	5.0	NA	NA	NA	NA	NA	NA	NA	NA
Pesticides-TCLP										
Heptachlor Epoxide	mg/L	- -	NA	NA	NA	NA	NA	NA	NA	NA
Chlordane	mg/L	0.03	NA	NA	NA	NA	NA	NA	NA	NA
Endrin	mg/L	0.02	NA	NA	NA	NA	NA	NA	NA	NA
Heptachlor	mg/L	0.008	NA	NA	NA	NA	NA	NA	NA	NA
Gamma-BHC	mg/L	0.4	NA	NA	NA	NA	NA	NA	NA	NA
Methoxychlor	mg/L	10	NA	NA	NA	NA	NA	NA	NA	NA
Toxaphene	mg/L	0.5	NA	NA	NA	NA	NA	NA	NA	NA
Herbicides-TCLP										
2,4-D	mg/L	10	NA	NA	NA	NA	NA	NA	NA	NA
2,4,5-TP (Silvex)	mg/L	1.0	NA	NA	NA	NA	NA	NA	NA	NA
PCBs										
Aroclor 1016	mg/kg	- -	ND(20)	ND(21)	ND(140)	ND(13)	ND(0.25)	ND(0.26)	ND(0.23)	ND(0.25)
Aroclor 1221	mg/kg	- -	ND(20)	ND(21)	ND(140)	ND(13)	ND(0.25)	ND(0.26)	ND(0.23)	ND(0.25)
Aroclor 1232	mg/kg	- -	ND(20)	ND(21)	ND(140)	ND(13)	ND(0.25)	ND(0.26)	ND(0.23)	ND(0.25)
Aroclor 1242	mg/kg	- -	ND(20)	ND(21)	1,700	ND(13)	ND(0.25)	0.18 J	ND(0.23)	ND(0.25)
Aroclor 1248	mg/kg	- -	240	140	ND(140)	37	0.44	ND(0.26)	0.77	0.81
Aroclor 1254	mg/kg	- -	ND(20)	ND(21)	ND(140)	ND(13)	ND(0.25)	ND(0.26)	ND(0.23)	ND(0.25)
Aroclor 1260	mg/kg	- -	ND(20)	ND(21)	ND(140)	ND(13)	ND(0.25)	ND(0.26)	ND(0.23)	ND(0.25)
Total PCBs	mg/kg	- -	240	140	1,700	37	0.44	0.18 J	0.77	0.81
Inorganics-TCLP										
Arsenic	mg/L	5.0	NA	NA	NA	NA	NA	NA	ND(0.01)	NA
Barium	mg/L	100	NA	NA	NA	NA	NA	NA	0.066 B	NA
Cadmium	mg/L	1.0	NA	NA	NA	NA	NA	NA	ND(0.001)	NA
Chromium	mg/L	5.0	NA	NA	NA	NA	NA	NA	0.0025 JB	NA
Lead	mg/L	5.0	NA	NA	NA	NA	NA	NA	0.0045 J	NA
Mercury	mg/L	0.2	NA	NA	NA	NA	NA	NA	ND(0.0002)	NA
Selenium	mg/L	1.0	NA	NA	NA	NA	NA	NA	ND(0.015)	NA
Silver	mg/L	5.0	NA	NA	NA	NA	NA	NA	ND(0.003)	NA
Miscellaneous Parameters										
% Moisture	%	- -	14.0	9.80	14.0	9.60	9.40	17.0	8.10	6.60
% Solids	%	- -	86.0	90.0	86.0	90.0	91.0	83.0	92.0	93.0
Cyanide, Reactive	mg/kg	- -	NA	NA	NA	NA	NA	NA	NA	NA
Flashpoint	Degrees F	- -	NA	NA	NA	NA	NA	NA	NA	NA
pH	SU	- -	NA	NA	NA	NA	NA	NA	NA	NA
Sulfide, Reactive	mg/kg	- -	NA	NA	NA	NA	NA	NA	NA	NA

TABLE 7
SUMMARY OF SOIL CHARACTERIZATION SAMPLE DATA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

			Mill Street Area						
Location ID:			**SC-45**	**SC-46**	**SC-47**	**SC-48**	**SC-49**	**SC-50**	**SC-51**
Sample Depth(feet):		**TCLP Regulatory**	**13 - 15**	**17 - 19**	**20 - 22**	**0 - 2**	**3 - 5**	**7 - 9**	**0 - 2**
Date Collected:	**Units**	**Level**	**05/15/12**	**05/15/12**	**05/15/12**	**05/14/12**	**05/14/12**	**05/15/12**	**05/07/12**
Volatile Organics-TCLP									
1,1-Dichloroethene	mg/L	0.7	ND(0.010)	ND(0.010) [ND(0.010)]	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
1,2-Dichloroethane	mg/L	0.5	ND(0.010)	ND(0.010) [ND(0.010)]	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
2-Butanone	mg/L	200	ND(0.050)	ND(0.050) [ND(0.050)]	ND(0.050)	ND(0.050)	ND(0.050)	ND(0.050)	ND(0.050)
Benzene	mg/L	0.5	ND(0.010)	ND(0.010) [ND(0.010)]	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Carbon Tetrachloride	mg/L	0.5	ND(0.010)	ND(0.010) [ND(0.010)]	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Chlorobenzene	mg/L	100	ND(0.010)	ND(0.010) [ND(0.010)]	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Chloroform	mg/L	6.0	ND(0.010)	ND(0.010) [ND(0.010)]	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Tetrachloroethene	mg/L	0.7	ND(0.010)	ND(0.010) [ND(0.010)]	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Trichloroethene	mg/L	0.5	ND(0.010)	ND(0.010) [ND(0.010)]	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Vinyl chloride	mg/L	0.2	ND(0.010)	ND(0.010) [ND(0.010)]	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Semivolatile Organics-TCLP									
1,4-Dichlorobenzene	mg/L	7.5	ND(0.010)	NA	NA	NA	NA	NA	NA
2,4,5-Trichlorophenol	mg/L	400	ND(0.0050)	NA	NA	NA	NA	NA	NA
2,4,6-Trichlorophenol	mg/L	2.0	ND(0.0050)	NA	NA	NA	NA	NA	NA
2,4-Dinitrotoluene	mg/L	0.13	ND(0.0050)	NA	NA	NA	NA	NA	NA
2-Methylphenol	mg/L	200	ND(0.0050)	NA	NA	NA	NA	NA	NA
3-Methylphenol	mg/L	200	ND(0.010)	NA	NA	NA	NA	NA	NA
4-Methylphenol	mg/L	200	ND(0.010)	NA	NA	NA	NA	NA	NA
Hexachlorobenzene	mg/L	0.13	ND(0.0050)	NA	NA	NA	NA	NA	NA
Hexachlorobutadiene	mg/L	0.5	ND(0.0050)	NA	NA	NA	NA	NA	NA
Hexachloroethane	mg/L	3.0	ND(0.0050)	NA	NA	NA	NA	NA	NA
Nitrobenzene	mg/L	2.0	ND(0.0050)	NA	NA	NA	NA	NA	NA
Pentachlorophenol	mg/L	100	ND(0.010)	NA	NA	NA	NA	NA	NA
Pyridine	mg/L	5.0	ND(0.025)	NA	NA	NA	NA	NA	NA
Pesticides-TCLP									
Heptachlor Epoxide	mg/L	- -	ND(0.0040)	NA	NA	NA	NA	NA	NA
Chlordane	mg/L	0.03	ND(0.040)	NA	NA	NA	NA	NA	NA
Endrin	mg/L	0.02	ND(0.0040)	NA	NA	NA	NA	NA	NA
Heptachlor	mg/L	0.008	0.0057	NA	NA	NA	NA	NA	NA
Gamma-BHC	mg/L	0.4	ND(0.0040)	NA	NA	NA	NA	NA	NA
Methoxychlor	mg/L	10	ND(0.0040)	NA	NA	NA	NA	NA	NA
Toxaphene	mg/L	0.5	ND(0.040)	NA	NA	NA	NA	NA	NA
Herbicides-TCLP									
2,4-D	mg/L	10	ND(0.0020)	NA	NA	NA	NA	NA	NA
2,4,5-TP (Silvex)	mg/L	1.0	ND(0.0020)	NA	NA	NA	NA	NA	NA
PCBs									
Aroclor 1016	mg/kg	- -	ND(46)	ND(25) [ND(120)]	ND(12)	ND(10)	ND(2.4)	ND(11)	ND(1,200)
Aroclor 1221	mg/kg	- -	ND(46)	ND(25) [ND(120)]	ND(12)	ND(10)	ND(2.4)	ND(11)	ND(1,200)
Aroclor 1232	mg/kg	- -	ND(46)	ND(25) [ND(120)]	ND(12)	ND(10)	ND(2.4)	ND(11)	ND(1,200)
Aroclor 1242	mg/kg	- -	450	320 [400]	31	ND(10)	ND(2.4)	92	17,000
Aroclor 1248	mg/kg	- -	ND(46)	ND(25) [ND(120)]	ND(12)	29	41	ND(11)	ND(1,200)
Aroclor 1254	mg/kg	- -	ND(46)	ND(25) [ND(120)]	ND(12)	ND(10)	ND(2.4)	ND(11)	ND(1,200)
Aroclor 1260	mg/kg	- -	ND(46)	ND(25) [ND(120)]	ND(12)	ND(10)	ND(2.4)	ND(11)	ND(1,200)
Total PCBs	mg/kg	- -	450	320 [400]	31	29	41	92	17,000
Inorganics-TCLP									
Arsenic	mg/L	5.0	ND(0.01)	NA	NA	NA	NA	NA	0.0071 J
Barium	mg/L	100	0.071 B	NA	NA	NA	NA	NA	1.1 B
Cadmium	mg/L	1.0	ND(0.001)	NA	NA	NA	NA	NA	0.0021
Chromium	mg/L	5.0	0.0042 B	NA	NA	NA	NA	NA	0.19 B
Lead	mg/L	5.0	0.0084	NA	NA	NA	NA	NA	1.7 B
Mercury	mg/L	0.2	ND(0.0002)	NA	NA	NA	NA	NA	ND(0.0002)
Selenium	mg/L	1.0	ND(0.015)	NA	NA	NA	NA	NA	ND(0.015)
Silver	mg/L	5.0	ND(0.003)	NA	NA	NA	NA	NA	ND(0.003)
Miscellaneous Parameters									
% Moisture	%	- -	19.0	21.0 [22.0]	22.0	6.40	18.0	12.0	6.10
% Solids	%	- -	81.0	79.0 [78.0]	78.0	94.0	82.0	88.0	94.0
Cyanide, Reactive	mg/kg	- -	NA	NA	NA	NA	NA	NA	NA
Flashpoint	Degrees F	- -	NA	NA	NA	NA	NA	NA	NA
pH	SU	- -	NA	NA	NA	NA	NA	NA	NA
Sulfide, Reactive	mg/kg	- -	NA	NA	NA	NA	NA	NA	NA

TABLE 7
SUMMARY OF SOIL CHARACTERIZATION SAMPLE DATA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

			Mill Street Area						
Location ID:			**SC-52**	**SC-53**	**SC-54**	**SC-55**	**SC-56**	**SC-57**	**SC-58**
Sample Depth(feet):		**TCLP Regulatory**	**3 - 5**	**7 - 9**	**0 - 2**	**0 - 2**	**3 - 5**	**6 - 8**	**0 - 2**
Date Collected:	**Units**	**Level**	**05/07/12**	**05/10/12**	**05/09/12**	**05/07/12**	**05/07/12**	**05/07/12**	**05/09/12**
Volatile Organics-TCLP									
1,1-Dichloroethene	mg/L	0.7	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010) [ND(0.010)]	ND(0.010)	ND(0.010)	ND(0.010)
1,2-Dichloroethane	mg/L	0.5	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010) [ND(0.010)]	ND(0.010)	ND(0.010)	ND(0.010)
2-Butanone	mg/L	200	ND(0.050)	ND(0.050)	ND(0.050)	ND(0.050) [ND(0.050)]	ND(0.050)	ND(0.050)	ND(0.050)
Benzene	mg/L	0.5	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010) [0.0095 J]	0.015	ND(0.010)	ND(0.010)
Carbon Tetrachloride	mg/L	0.5	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010) [ND(0.010)]	ND(0.010)	ND(0.010)	ND(0.010)
Chlorobenzene	mg/L	100	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010) [ND(0.010)]	ND(0.010)	ND(0.010)	ND(0.010)
Chloroform	mg/L	6.0	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010) [ND(0.010)]	ND(0.010)	ND(0.010)	ND(0.010)
Tetrachloroethene	mg/L	0.7	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010) [ND(0.010)]	ND(0.010)	ND(0.010)	ND(0.010)
Trichloroethene	mg/L	0.5	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010) [ND(0.010)]	ND(0.010)	ND(0.010)	ND(0.010)
Vinyl chloride	mg/L	0.2	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010) [ND(0.010)]	ND(0.010)	ND(0.010)	ND(0.010)
Semivolatile Organics-TCLP									
1,4-Dichlorobenzene	mg/L	7.5	NA	NA	NA	NA	NA	NA	ND(0.010)
2,4,5-Trichlorophenol	mg/L	400	NA	NA	NA	NA	NA	NA	ND(0.0050)
2,4,6-Trichlorophenol	mg/L	2.0	NA	NA	NA	NA	NA	NA	ND(0.0050)
2,4-Dinitrotoluene	mg/L	0.13	NA	NA	NA	NA	NA	NA	ND(0.0050)
2-Methylphenol	mg/L	200	NA	NA	NA	NA	NA	NA	ND(0.0050)
3-Methylphenol	mg/L	200	NA	NA	NA	NA	NA	NA	ND(0.010)
4-Methylphenol	mg/L	200	NA	NA	NA	NA	NA	NA	ND(0.010)
Hexachlorobenzene	mg/L	0.13	NA	NA	NA	NA	NA	NA	ND(0.0050)
Hexachlorobutadiene	mg/L	0.5	NA	NA	NA	NA	NA	NA	ND(0.0050)
Hexachloroethane	mg/L	3.0	NA	NA	NA	NA	NA	NA	ND(0.0050)
Nitrobenzene	mg/L	2.0	NA	NA	NA	NA	NA	NA	ND(0.0050)
Pentachlorophenol	mg/L	100	NA	NA	NA	NA	NA	NA	ND(0.010)
Pyridine	mg/L	5.0	NA	NA	NA	NA	NA	NA	ND(0.025)
Pesticides-TCLP									
Heptachlor Epoxide	mg/L	- -	NA	NA	NA	NA	NA	NA	ND(0.00020)
Chlordane	mg/L	0.03	NA	NA	NA	NA	NA	NA	ND(0.0020)
Endrin	mg/L	0.02	NA	NA	NA	NA	NA	NA	ND(0.00020)
Heptachlor	mg/L	0.008	NA	NA	NA	NA	NA	NA	0.000061 J
Gamma-BHC	mg/L	0.4	NA	NA	NA	NA	NA	NA	0.000061 J
Methoxychlor	mg/L	10	NA	NA	NA	NA	NA	NA	ND(0.00020)
Toxaphene	mg/L	0.5	NA	NA	NA	NA	NA	NA	ND(0.0020)
Herbicides-TCLP									
2,4-D	mg/L	10	NA	NA	NA	NA	NA	NA	ND(0.0020)
2,4,5-TP (Silvex)	mg/L	1.0	NA	NA	NA	NA	NA	NA	ND(0.0020)
PCBs									
Aroclor 1016	mg/kg	- -	ND(46)	ND(1.4)	ND(41)	ND(54) [ND(130)]	ND(0.96)	ND(0.24)	ND(1.1)
Aroclor 1221	mg/kg	- -	ND(46)	ND(1.4)	ND(41)	ND(54) [ND(130)]	ND(0.96)	ND(0.24)	ND(1.1)
Aroclor 1232	mg/kg	- -	ND(46)	ND(1.4)	ND(41)	ND(54) [ND(130)]	ND(0.96)	ND(0.24)	ND(1.1)
Aroclor 1242	mg/kg	- -	450	3.5	73	ND(54) [ND(130)]	ND(0.96)	ND(0.24)	9.0
Aroclor 1248	mg/kg	- -	ND(46)	ND(1.4)	ND(41)	350 [390]	5.2	1.3	ND(1.1)
Aroclor 1254	mg/kg	- -	ND(46)	ND(1.4)	ND(41)	ND(54) [ND(130)]	ND(0.96)	ND(0.24)	ND(1.1)
Aroclor 1260	mg/kg	- -	ND(46)	ND(1.4)	ND(41)	ND(54) [ND(130)]	ND(0.96)	ND(0.24)	ND(1.1)
Total PCBs	mg/kg	- -	450	3.5	73	350 [390]	5.2	1.3	9.0
Inorganics-TCLP									
Arsenic	mg/L	5.0	NA	NA	NA	0.011 [0.012]	NA	NA	0.008 J
Barium	mg/L	100	NA	NA	NA	0.32 B [0.38 B]	NA	NA	0.11 B
Cadmium	mg/L	1.0	NA	NA	NA	0.0021 [0.002]	NA	NA	0.00072 J
Chromium	mg/L	5.0	NA	NA	NA	0.013 B [0.017 B]	NA	NA	0.0054 B
Lead	mg/L	5.0	NA	NA	NA	0.24 B [0.27 B]	NA	NA	0.041
Mercury	mg/L	0.2	NA	NA	NA	0.00012 J [ND(0.0002)]	NA	NA	0.00012 J
Selenium	mg/L	1.0	NA	NA	NA	0.011 J [ND(0.015)]	NA	NA	ND(0.015)
Silver	mg/L	5.0	NA	NA	NA	ND(0.003) [ND(0.003)]	NA	NA	ND(0.003)
Miscellaneous Parameters									
% Moisture	%	- -	5.30	22.0	4.90	20.0 [14.0]	5.30	18.0	5.80
% Solids	%	- -	95.0	78.0	95.0	80.0 [86.0]	95.0	82.0	94.0
Cyanide, Reactive	mg/kg	- -	NA	NA	NA	NA	NA	NA	ND(10.0)
Flashpoint	Degrees F	- -	NA	NA	NA	NA	NA	NA	>50.0
pH	SU	- -	NA	NA	NA	NA	NA	NA	6.87
Sulfide, Reactive	mg/kg	- -	NA	NA	NA	NA	NA	NA	2.00 JB

TABLE 7
SUMMARY OF SOIL CHARACTERIZATION SAMPLE DATA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

			Mill Street Area							
Location ID:			**SC-59**	**SC-60**	**SC-61**	**SC-62**	**SC-62**	**SC-63**	**SC-63**	**SC-64**
Sample Depth(feet):		**TCLP Regulatory**	**3 - 5**	**0 - 2**	**3 - 5**	**0 - 2**	**0 - 2**	**5 - 7**	**5 - 7**	**13 - 15**
Date Collected:	**Units**	**Level**	**05/09/12**	**05/07/12**	**05/07/12**	**05/08/12**	**06/14/12**	**05/08/12**	**06/14/12**	**05/16/12**
Volatile Organics-TCLP										
1,1-Dichloroethene	mg/L	0.7	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
1,2-Dichloroethane	mg/L	0.5	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
2-Butanone	mg/L	200	ND(0.050)	ND(0.050)	ND(0.050)	ND(0.050)	ND(0.050)	ND(0.050)	0.013 J	ND(0.050)
Benzene	mg/L	0.5	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Carbon Tetrachloride	mg/L	0.5	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Chlorobenzene	mg/L	100	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	0.0089 J	ND(0.010)
Chloroform	mg/L	6.0	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Tetrachloroethene	mg/L	0.7	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Trichloroethene	mg/L	0.5	ND(0.010)	ND(0.010)	ND(0.010)	0.013	0.011	ND(0.010)	ND(0.010)	ND(0.010)
Vinyl chloride	mg/L	0.2	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Semivolatile Organics-TCLP										
1,4-Dichlorobenzene	mg/L	7.5	NA	NA	NA	NA	NA	NA	NA	ND(0.010)
2,4,5-Trichlorophenol	mg/L	400	NA	NA	NA	NA	NA	NA	NA	ND(0.0050)
2,4,6-Trichlorophenol	mg/L	2.0	NA	NA	NA	NA	NA	NA	NA	ND(0.0050)
2,4-Dinitrotoluene	mg/L	0.13	NA	NA	NA	NA	NA	NA	NA	ND(0.0050)
2-Methylphenol	mg/L	200	NA	NA	NA	NA	NA	NA	NA	ND(0.0050)
3-Methylphenol	mg/L	200	NA	NA	NA	NA	NA	NA	NA	ND(0.010)
4-Methylphenol	mg/L	200	NA	NA	NA	NA	NA	NA	NA	ND(0.010)
Hexachlorobenzene	mg/L	0.13	NA	NA	NA	NA	NA	NA	NA	ND(0.0050)
Hexachlorobutadiene	mg/L	0.5	NA	NA	NA	NA	NA	NA	NA	ND(0.0050)
Hexachloroethane	mg/L	3.0	NA	NA	NA	NA	NA	NA	NA	ND(0.0050)
Nitrobenzene	mg/L	2.0	NA	NA	NA	NA	NA	NA	NA	ND(0.0050)
Pentachlorophenol	mg/L	100	NA	NA	NA	NA	NA	NA	NA	ND(0.010)
Pyridine	mg/L	5.0	NA	NA	NA	NA	NA	NA	NA	ND(0.025)
Pesticides-TCLP										
Heptachlor Epoxide	mg/L	- -	NA	NA	NA	NA	NA	NA	NA	ND(0.010)
Chlordane	mg/L	0.03	NA	NA	NA	NA	NA	NA	NA	ND(0.10)
Endrin	mg/L	0.02	NA	NA	NA	NA	NA	NA	NA	ND(0.010)
Heptachlor	mg/L	0.008	NA	NA	NA	NA	NA	NA	NA	0.0032 J
Gamma-BHC	mg/L	0.4	NA	NA	NA	NA	NA	NA	NA	ND(0.010)
Methoxychlor	mg/L	10	NA	NA	NA	NA	NA	NA	NA	ND(0.010)
Toxaphene	mg/L	0.5	NA	NA	NA	NA	NA	NA	NA	ND(0.10)
Herbicides-TCLP										
2,4-D	mg/L	10	NA	NA	NA	NA	NA	NA	NA	ND(0.0020)
2,4,5-TP (Silvex)	mg/L	1.0	NA	NA	NA	NA	NA	NA	NA	ND(0.0020)
PCBs										
Aroclor 1016	mg/kg	- -	ND(1.3)	ND(500)	ND(110)	ND(1,100)	NA	ND(1,200)	NA	ND(130)
Aroclor 1221	mg/kg	- -	ND(1.3)	ND(500)	ND(110)	ND(1,100)	NA	ND(1,200)	NA	ND(130)
Aroclor 1232	mg/kg	- -	ND(1.3)	ND(500)	ND(110)	ND(1,100)	NA	ND(1,200)	NA	ND(130)
Aroclor 1242	mg/kg	- -	2.5	ND(500)	ND(110)	15,000	NA	6,900	NA	300
Aroclor 1248	mg/kg	- -	ND(1.3)	2,000	170	ND(1,100)	NA	ND(1,200)	NA	ND(130)
Aroclor 1254	mg/kg	- -	ND(1.3)	ND(500)	ND(110)	ND(1,100)	NA	ND(1,200)	NA	ND(130)
Aroclor 1260	mg/kg	- -	ND(1.3)	ND(500)	ND(110)	ND(1,100)	NA	ND(1,200)	NA	ND(130)
Total PCBs	mg/kg	- -	2.5	2,000	170	15,000	NA	6,900	NA	300
Inorganics-TCLP										
Arsenic	mg/L	5.0	NA	0.008 J	NA	0.13	NA	NA	NA	ND(0.01)
Barium	mg/L	100	NA	1.1 B	NA	0.29 B	NA	NA	NA	0.2 B
Cadmium	mg/L	1.0	NA	0.0043	NA	ND(0.001)	NA	NA	NA	ND(0.001)
Chromium	mg/L	5.0	NA	0.16 B	NA	0.036 B	NA	NA	NA	0.0064 B
Lead	mg/L	5.0	NA	2 B	NA	0.5 B	NA	NA	NA	0.026
Mercury	mg/L	0.2	NA	0.00033	NA	0.00033	NA	NA	NA	ND(0.0002)
Selenium	mg/L	1.0	NA	ND(0.015)	NA	ND(0.015)	NA	NA	NA	ND(0.015)
Silver	mg/L	5.0	NA	ND(0.003)	NA	ND(0.003)	NA	NA	NA	ND(0.003)
Miscellaneous Parameters										
% Moisture	%	- -	5.40	19.0	5.70	15.0	NA	17.0	NA	21.0
% Solids	%	- -	95.0	81.0	94.0	85.0	NA	83.0	NA	79.0
Cyanide, Reactive	mg/kg	- -	NA	NA	NA	NA	NA	NA	NA	ND(10.0)
Flashpoint	Degrees F	- -	NA	NA	NA	NA	NA	NA	NA	>50.0
pH	SU	- -	NA	NA	NA	NA	NA	NA	NA	7.05
Sulfide, Reactive	mg/kg	- -	NA	NA	NA	NA	NA	NA	NA	4.00 JB

TABLE 7
SUMMARY OF SOIL CHARACTERIZATION SAMPLE DATA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

			Mill Street Area							
Location ID:			**SC-65**	**SC-66**	**SC-67**	**SC-67**	**SC-68**	**SC-68**	**SC-69**	**SC-70**
Sample Depth(feet):		**TCLP Regulatory**	**17 - 19**	**20 - 21.3**	**0 - 2**	**0 - 2**	**5 - 7**	**5 - 7**	**13 - 15**	**17 - 19**
Date Collected:	**Units**	**Level**	**05/16/12**	**05/16/12**	**05/08/12**	**06/13/12**	**05/08/12**	**06/13/12**	**06/13/12**	**06/14/12**
Volatile Organics-TCLP										
1,1-Dichloroethene	mg/L	0.7	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
1,2-Dichloroethane	mg/L	0.5	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
2-Butanone	mg/L	200	ND(0.050)	ND(0.050)	ND(0.050)	ND(0.050)	ND(0.050)	ND(0.050)	ND(0.050)	ND(0.050)
Benzene	mg/L	0.5	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Carbon Tetrachloride	mg/L	0.5	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Chlorobenzene	mg/L	100	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Chloroform	mg/L	6.0	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Tetrachloroethene	mg/L	0.7	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Trichloroethene	mg/L	0.5	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	0.0062 J	ND(0.010)	ND(0.010)	ND(0.010)
Vinyl chloride	mg/L	0.2	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Semivolatile Organics-TCLP										
1,4-Dichlorobenzene	mg/L	7.5	NA	NA	NA	NA	NA	NA	NA	NA
2,4,5-Trichlorophenol	mg/L	400	NA	NA	NA	NA	NA	NA	NA	NA
2,4,6-Trichlorophenol	mg/L	2.0	NA	NA	NA	NA	NA	NA	NA	NA
2,4-Dinitrotoluene	mg/L	0.13	NA	NA	NA	NA	NA	NA	NA	NA
2-Methylphenol	mg/L	200	NA	NA	NA	NA	NA	NA	NA	NA
3-Methylphenol	mg/L	200	NA	NA	NA	NA	NA	NA	NA	NA
4-Methylphenol	mg/L	200	NA	NA	NA	NA	NA	NA	NA	NA
Hexachlorobenzene	mg/L	0.13	NA	NA	NA	NA	NA	NA	NA	NA
Hexachlorobutadiene	mg/L	0.5	NA	NA	NA	NA	NA	NA	NA	NA
Hexachloroethane	mg/L	3.0	NA	NA	NA	NA	NA	NA	NA	NA
Nitrobenzene	mg/L	2.0	NA	NA	NA	NA	NA	NA	NA	NA
Pentachlorophenol	mg/L	100	NA	NA	NA	NA	NA	NA	NA	NA
Pyridine	mg/L	5.0	NA	NA	NA	NA	NA	NA	NA	NA
Pesticides-TCLP										
Heptachlor Epoxide	mg/L	- -	NA	NA	NA	NA	NA	NA	NA	NA
Chlordane	mg/L	0.03	NA	NA	NA	NA	NA	NA	NA	NA
Endrin	mg/L	0.02	NA	NA	NA	NA	NA	NA	NA	NA
Heptachlor	mg/L	0.008	NA	NA	NA	NA	NA	NA	NA	NA
Gamma-BHC	mg/L	0.4	NA	NA	NA	NA	NA	NA	NA	NA
Methoxychlor	mg/L	10	NA	NA	NA	NA	NA	NA	NA	NA
Toxaphene	mg/L	0.5	NA	NA	NA	NA	NA	NA	NA	NA
Herbicides-TCLP										
2,4-D	mg/L	10	NA	NA	NA	NA	NA	NA	NA	NA
2,4,5-TP (Silvex)	mg/L	1.0	NA	NA	NA	NA	NA	NA	NA	NA
PCBs										
Aroclor 1016	mg/kg	- -	ND(2.0)	ND(290)	ND(2,400)	NA	ND(49)	NA	ND(1.2)	ND(120)
Aroclor 1221	mg/kg	- -	ND(2.0)	ND(290)	ND(2,400)	NA	ND(49)	NA	ND(1.2)	ND(120)
Aroclor 1232	mg/kg	- -	ND(2.0)	ND(290)	ND(2,400)	NA	ND(49)	NA	ND(1.2)	ND(120)
Aroclor 1242	mg/kg	- -	68	1,800	42,000	NA	880	NA	27	400
Aroclor 1248	mg/kg	- -	ND(2.0)	ND(290)	ND(2,400)	NA	ND(49)	NA	ND(1.2)	ND(120)
Aroclor 1254	mg/kg	- -	ND(2.0)	ND(290)	ND(2,400)	NA	ND(49)	NA	ND(1.2)	ND(120)
Aroclor 1260	mg/kg	- -	ND(2.0)	ND(290)	ND(2,400)	NA	ND(49)	NA	ND(1.2)	ND(120)
Total PCBs	mg/kg	- -	68	1,800	42,000	NA	880	NA	27	400
Inorganics-TCLP										
Arsenic	mg/L	5.0	NA	NA	NA	NA	NA	NA	NA	NA
Barium	mg/L	100	NA	NA	NA	NA	NA	NA	NA	NA
Cadmium	mg/L	1.0	NA	NA	NA	NA	NA	NA	NA	NA
Chromium	mg/L	5.0	NA	NA	NA	NA	NA	NA	NA	NA
Lead	mg/L	5.0	NA	NA	NA	NA	NA	NA	NA	NA
Mercury	mg/L	0.2	NA	NA	NA	NA	NA	NA	NA	NA
Selenium	mg/L	1.0	NA	NA	NA	NA	NA	NA	NA	NA
Silver	mg/L	5.0	NA	NA	NA	NA	NA	NA	NA	NA
Miscellaneous Parameters										
% Moisture	%	- -	9.00	19.0	13.0	NA	21.0	NA	14.0	18.0
% Solids	%	- -	91.0	81.0	87.0	NA	79.0	NA	86.0	82.0
Cyanide, Reactive	mg/kg	- -	NA	NA	NA	NA	NA	NA	NA	NA
Flashpoint	Degrees F	- -	NA	NA	NA	NA	NA	NA	NA	NA
pH	SU	- -	NA	NA	NA	NA	NA	NA	NA	NA
Sulfide, Reactive	mg/kg	- -	NA	NA	NA	NA	NA	NA	NA	NA

TABLE 7
SUMMARY OF SOIL CHARACTERIZATION SAMPLE DATA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

			Mill Street Area						
Location ID:			**SC-72**	**SC-73**	**SC-74**	**SC-75**	**SC-76**	**SC-77**	**SC-78**
Sample Depth(feet):		**TCLP Regulatory**	**0 - 2**	**5 - 7**	**13 - 15**	**17 - 19**	**20 - 22**	**0 - 2**	**5 - 7**
Date Collected:	**Units**	**Level**	**05/09/12**	**05/09/12**	**05/14/12**	**05/14/12**	**05/14/12**	**05/08/12**	**05/08/12**
Volatile Organics-TCLP									
1,1-Dichloroethene	mg/L	0.7	ND(0.010)	ND(0.010) [ND(0.010)]	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
1,2-Dichloroethane	mg/L	0.5	ND(0.010)	ND(0.010) [ND(0.010)]	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
2-Butanone	mg/L	200	ND(0.050)	ND(0.050) [ND(0.050)]	ND(0.050)	ND(0.050)	ND(0.050)	ND(0.050)	ND(0.050)
Benzene	mg/L	0.5	ND(0.010)	ND(0.010) [ND(0.010)]	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Carbon Tetrachloride	mg/L	0.5	ND(0.010)	ND(0.010) [ND(0.010)]	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Chlorobenzene	mg/L	100	ND(0.010)	0.026 [0.017]	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Chloroform	mg/L	6.0	ND(0.010)	ND(0.010) [ND(0.010)]	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Tetrachloroethene	mg/L	0.7	ND(0.010)	ND(0.010) [ND(0.010)]	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Trichloroethene	mg/L	0.5	0.048	ND(0.010) [ND(0.010)]	ND(0.010)	ND(0.010)	ND(0.010)	0.028	0.24
Vinyl chloride	mg/L	0.2	ND(0.010)	ND(0.010) [ND(0.010)]	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Semivolatile Organics-TCLP									
1,4-Dichlorobenzene	mg/L	7.5	NA	NA	NA	NA	NA	NA	NA
2,4,5-Trichlorophenol	mg/L	400	NA	NA	NA	NA	NA	NA	NA
2,4,6-Trichlorophenol	mg/L	2.0	NA	NA	NA	NA	NA	NA	NA
2,4-Dinitrotoluene	mg/L	0.13	NA	NA	NA	NA	NA	NA	NA
2-Methylphenol	mg/L	200	NA	NA	NA	NA	NA	NA	NA
3-Methylphenol	mg/L	200	NA	NA	NA	NA	NA	NA	NA
4-Methylphenol	mg/L	200	NA	NA	NA	NA	NA	NA	NA
Hexachlorobenzene	mg/L	0.13	NA	NA	NA	NA	NA	NA	NA
Hexachlorobutadiene	mg/L	0.5	NA	NA	NA	NA	NA	NA	NA
Hexachloroethane	mg/L	3.0	NA	NA	NA	NA	NA	NA	NA
Nitrobenzene	mg/L	2.0	NA	NA	NA	NA	NA	NA	NA
Pentachlorophenol	mg/L	100	NA	NA	NA	NA	NA	NA	NA
Pyridine	mg/L	5.0	NA	NA	NA	NA	NA	NA	NA
Pesticides-TCLP									
Heptachlor Epoxide	mg/L	- -	NA	NA	NA	NA	NA	NA	NA
Chlordane	mg/L	0.03	NA	NA	NA	NA	NA	NA	NA
Endrin	mg/L	0.02	NA	NA	NA	NA	NA	NA	NA
Heptachlor	mg/L	0.008	NA	NA	NA	NA	NA	NA	NA
Gamma-BHC	mg/L	0.4	NA	NA	NA	NA	NA	NA	NA
Methoxychlor	mg/L	10	NA	NA	NA	NA	NA	NA	NA
Toxaphene	mg/L	0.5	NA	NA	NA	NA	NA	NA	NA
Herbicides-TCLP									
2,4-D	mg/L	10	NA	NA	NA	NA	NA	NA	NA
2,4,5-TP (Silvex)	mg/L	1.0	NA	NA	NA	NA	NA	NA	NA
PCBs									
Aroclor 1016	mg/kg	- -	ND(2,900)	ND(420) [ND(1,700)]	ND(14)	ND(120)	ND(140)	ND(2,800)	ND(300)
Aroclor 1221	mg/kg	- -	ND(2,900)	ND(420) [ND(1,700)]	ND(14)	ND(120)	ND(140)	ND(2,800)	ND(300)
Aroclor 1232	mg/kg	- -	ND(2,900)	ND(420) [ND(1,700)]	ND(14)	ND(120)	ND(140)	ND(2,800)	ND(300)
Aroclor 1242	mg/kg	- -	53,000	4,900 [6,900]	160	470	3,000	30,000	6,000
Aroclor 1248	mg/kg	- -	ND(2,900)	ND(420) [ND(1,700)]	ND(14)	ND(120)	ND(140)	ND(2,800)	ND(300)
Aroclor 1254	mg/kg	- -	ND(2,900)	ND(420) [ND(1,700)]	ND(14)	ND(120)	ND(140)	ND(2,800)	ND(300)
Aroclor 1260	mg/kg	- -	ND(2,900)	ND(420) [ND(1,700)]	ND(14)	ND(120)	ND(140)	ND(2,800)	ND(300)
Total PCBs	mg/kg	- -	53,000	4,900 [6,900]	160	470	3,000	30,000	6,000
Inorganics-TCLP									
Arsenic	mg/L	5.0	0.0066 J	NA	NA	NA	NA	NA	NA
Barium	mg/L	100	0.56 B	NA	NA	NA	NA	NA	NA
Cadmium	mg/L	1.0	0.0024	NA	NA	NA	NA	NA	NA
Chromium	mg/L	5.0	0.0026 JB	NA	NA	NA	NA	NA	NA
Lead	mg/L	5.0	0.56	NA	NA	NA	NA	NA	NA
Mercury	mg/L	0.2	0.0016	NA	NA	NA	NA	NA	NA
Selenium	mg/L	1.0	ND(0.015)	NA	NA	NA	NA	NA	NA
Silver	mg/L	5.0	ND(0.003)	NA	NA	NA	NA	NA	NA
Miscellaneous Parameters									
% Moisture	%	- -	15.0	43.0 [46.0]	20.0	21.0	16.0	19.0	27.0
% Solids	%	- -	85.0	57.0 [54.0]	80.0	79.0	84.0	81.0	73.0
Cyanide, Reactive	mg/kg	- -	NA	NA	NA	NA	NA	NA	NA
Flashpoint	Degrees F	- -	NA	NA	NA	NA	NA	NA	NA
pH	SU	- -	NA	NA	NA	NA	NA	NA	NA
Sulfide, Reactive	mg/kg	- -	NA	NA	NA	NA	NA	NA	NA

TABLE 7
SUMMARY OF SOIL CHARACTERIZATION SAMPLE DATA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

			Mill Street Area							
Location ID:			**SC-79**	**SC-80**	**SC-81**	**SC-82**	**SC-82**	**SC-83**	**SC-83**	**SC-84**
Sample Depth(feet):		**TCLP Regulatory**	**13 - 15**	**17 - 19**	**19.7 - 20.2**	**0 - 2**	**0 - 2**	**5 - 7**	**5 - 7**	**9 - 11**
Date Collected:	**Units**	**Level**	**05/11/12**	**05/11/12**	**05/11/12**	**05/09/12**	**06/13/12**	**05/09/12**	**06/13/12**	**05/21/12**
Volatile Organics-TCLP										
1,1-Dichloroethene	mg/L	0.7	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
1,2-Dichloroethane	mg/L	0.5	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
2-Butanone	mg/L	200	ND(0.050)	ND(0.050)	ND(0.050)	ND(0.050)	ND(0.050)	ND(0.050)	ND(0.050)	ND(0.050)
Benzene	mg/L	0.5	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Carbon Tetrachloride	mg/L	0.5	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Chlorobenzene	mg/L	100	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Chloroform	mg/L	6.0	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Tetrachloroethene	mg/L	0.7	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Trichloroethene	mg/L	0.5	ND(0.010)	ND(0.010)	ND(0.010)	0.020	0.037	0.019	0.14	ND(0.010)
Vinyl chloride	mg/L	0.2	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Semivolatile Organics-TCLP										
1,4-Dichlorobenzene	mg/L	7.5	ND(0.010 *)	NA	NA	NA	NA	ND(0.010)	NA	NA
2,4,5-Trichlorophenol	mg/L	400	ND(0.0050)	NA	NA	NA	NA	ND(0.0050)	NA	NA
2,4,6-Trichlorophenol	mg/L	2.0	ND(0.0050)	NA	NA	NA	NA	ND(0.0050)	NA	NA
2,4-Dinitrotoluene	mg/L	0.13	ND(0.0050)	NA	NA	NA	NA	ND(0.0050)	NA	NA
2-Methylphenol	mg/L	200	ND(0.0050)	NA	NA	NA	NA	ND(0.0050)	NA	NA
3-Methylphenol	mg/L	200	ND(0.010)	NA	NA	NA	NA	ND(0.010)	NA	NA
4-Methylphenol	mg/L	200	ND(0.010)	NA	NA	NA	NA	ND(0.010)	NA	NA
Hexachlorobenzene	mg/L	0.13	ND(0.0050)	NA	NA	NA	NA	ND(0.0050)	NA	NA
Hexachlorobutadiene	mg/L	0.5	ND(0.0050 *)	NA	NA	NA	NA	ND(0.0050)	NA	NA
Hexachloroethane	mg/L	3.0	ND(0.0050 *)	NA	NA	NA	NA	ND(0.0050)	NA	NA
Nitrobenzene	mg/L	2.0	ND(0.0050)	NA	NA	NA	NA	ND(0.0050)	NA	NA
Pentachlorophenol	mg/L	100	ND(0.010)	NA	NA	NA	NA	ND(0.010)	NA	NA
Pyridine	mg/L	5.0	ND(0.025)	NA	NA	NA	NA	ND(0.025)	NA	NA
Pesticides-TCLP										
Heptachlor Epoxide	mg/L	- -	ND(0.0020)	NA	NA	NA	NA	ND(0.020)	NA	NA
Chlordane	mg/L	0.03	ND(0.020)	NA	NA	NA	NA	ND(0.20)	NA	NA
Endrin	mg/L	0.02	ND(0.0020)	NA	NA	NA	NA	ND(0.020)	NA	NA
Heptachlor	mg/L	0.008	**0.0094**	NA	NA	NA	NA	ND(0.020)	NA	NA
Gamma-BHC	mg/L	0.4	0.0018 J	NA	NA	NA	NA	ND(0.020)	NA	NA
Methoxychlor	mg/L	10	ND(0.0020)	NA	NA	NA	NA	ND(0.020)	NA	NA
Toxaphene	mg/L	0.5	ND(0.020)	NA	NA	NA	NA	ND(0.20)	NA	NA
Herbicides-TCLP										
2,4-D	mg/L	10	ND(0.0020)	NA	NA	NA	NA	ND(0.0020)	NA	NA
2,4,5-TP (Silvex)	mg/L	1.0	ND(0.0020)	NA	NA	NA	NA	ND(0.0020)	NA	NA
PCBs										
Aroclor 1016	mg/kg	- -	ND(110)	ND(50)	ND(12)	ND(5,700)	NA	ND(430)	NA	ND(14)
Aroclor 1221	mg/kg	- -	ND(110)	ND(50)	ND(12)	ND(5,700)	NA	ND(430)	NA	ND(14)
Aroclor 1232	mg/kg	- -	ND(110)	ND(50)	ND(12)	ND(5,700)	NA	ND(430)	NA	ND(14)
Aroclor 1242	mg/kg	- -	1,100	310	200	22,000	NA	3,000	NA	310
Aroclor 1248	mg/kg	- -	ND(110)	ND(50)	ND(12)	ND(5,700)	NA	ND(430)	NA	ND(14)
Aroclor 1254	mg/kg	- -	ND(110)	ND(50)	ND(12)	ND(5,700)	NA	ND(430)	NA	ND(14)
Aroclor 1260	mg/kg	- -	ND(110)	ND(50)	ND(12)	ND(5,700)	NA	ND(430)	NA	ND(14)
Total PCBs	mg/kg	- -	1,100	310	200	22,000	NA	3,000	NA	310
Inorganics-TCLP										
Arsenic	mg/L	5.0	ND(0.01)	NA	NA	NA	NA	ND(0.01)	NA	NA
Barium	mg/L	100	0.086 B	NA	NA	NA	NA	0.12 B	NA	NA
Cadmium	mg/L	1.0	ND(0.001)	NA	NA	NA	NA	0.00083 J	NA	NA
Chromium	mg/L	5.0	0.0034 JB	NA	NA	NA	NA	0.0065 B	NA	NA
Lead	mg/L	5.0	0.038	NA	NA	NA	NA	0.036	NA	NA
Mercury	mg/L	0.2	ND(0.0002)	NA	NA	NA	NA	ND(0.0002)	NA	NA
Selenium	mg/L	1.0	ND(0.015)	NA	NA	NA	NA	ND(0.015)	NA	NA
Silver	mg/L	5.0	ND(0.003)	NA	NA	NA	NA	ND(0.003)	NA	NA
Miscellaneous Parameters										
% Moisture	%	- -	14.0	8.70	7.80	11.0	NA	14.0	NA	14.0
% Solids	%	- -	86.0	91.0	92.0	89.0	NA	86.0	NA	86.0
Cyanide, Reactive	mg/kg	- -	NA	NA	NA	NA	NA	NA	NA	NA
Flashpoint	Degrees F	- -	NA	NA	NA	NA	NA	NA	NA	NA
pH	SU	- -	NA	NA	NA	NA	NA	NA	NA	NA
Sulfide, Reactive	mg/kg	- -	NA	NA	NA	NA	NA	NA	NA	NA

TABLE 7
SUMMARY OF SOIL CHARACTERIZATION SAMPLE DATA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

			Mill Street Area				
Location ID:			**SC-85**	**SC-86**	**SC-87**	**SC-88**	**SC-89**
Sample Depth(feet):		**TCLP Regulatory**	**13 - 15**	**0 - 2**	**3 - 5**	**0 - 2**	**4 - 6**
Date Collected:	**Units**	**Level**	**06/13/12**	**05/09/12**	**05/09/12**	**05/09/12**	**05/09/12**
Volatile Organics-TCLP							
1,1-Dichloroethene	mg/L	0.7	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
1,2-Dichloroethane	mg/L	0.5	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
2-Butanone	mg/L	200	ND(0.050)	ND(0.050)	ND(0.050)	ND(0.050)	ND(0.050)
Benzene	mg/L	0.5	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Carbon Tetrachloride	mg/L	0.5	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Chlorobenzene	mg/L	100	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Chloroform	mg/L	6.0	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Tetrachloroethene	mg/L	0.7	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Trichloroethene	mg/L	0.5	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Vinyl chloride	mg/L	0.2	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)	ND(0.010)
Semivolatile Organics-TCLP							
1,4-Dichlorobenzene	mg/L	7.5	NA	NA	NA	NA	NA
2,4,5-Trichlorophenol	mg/L	400	NA	NA	NA	NA	NA
2,4,6-Trichlorophenol	mg/L	2.0	NA	NA	NA	NA	NA
2,4-Dinitrotoluene	mg/L	0.13	NA	NA	NA	NA	NA
2-Methylphenol	mg/L	200	NA	NA	NA	NA	NA
3-Methylphenol	mg/L	200	NA	NA	NA	NA	NA
4-Methylphenol	mg/L	200	NA	NA	NA	NA	NA
Hexachlorobenzene	mg/L	0.13	NA	NA	NA	NA	NA
Hexachlorobutadiene	mg/L	0.5	NA	NA	NA	NA	NA
Hexachloroethane	mg/L	3.0	NA	NA	NA	NA	NA
Nitrobenzene	mg/L	2.0	NA	NA	NA	NA	NA
Pentachlorophenol	mg/L	100	NA	NA	NA	NA	NA
Pyridine	mg/L	5.0	NA	NA	NA	NA	NA
Pesticides-TCLP							
Heptachlor Epoxide	mg/L	- -	NA	NA	NA	NA	NA
Chlordane	mg/L	0.03	NA	NA	NA	NA	NA
Endrin	mg/L	0.02	NA	NA	NA	NA	NA
Heptachlor	mg/L	0.008	NA	NA	NA	NA	NA
Gamma-BHC	mg/L	0.4	NA	NA	NA	NA	NA
Methoxychlor	mg/L	10	NA	NA	NA	NA	NA
Toxaphene	mg/L	0.5	NA	NA	NA	NA	NA
Herbicides-TCLP							
2,4-D	mg/L	10	NA	NA	NA	NA	NA
2,4,5-TP (Silvex)	mg/L	1.0	NA	NA	NA	NA	NA
PCBs							
Aroclor 1016	mg/kg	- -	ND(25)	ND(13,000)	ND(1,100)	ND(6.6)	ND(0.24)
Aroclor 1221	mg/kg	- -	ND(25)	ND(13,000)	ND(1,100)	ND(6.6)	ND(0.24)
Aroclor 1232	mg/kg	- -	ND(25)	ND(13,000)	12,000	ND(6.6)	ND(0.24)
Aroclor 1242	mg/kg	- -	520	82,000	5,900	ND(6.6)	1.5
Aroclor 1248	mg/kg	- -	ND(25)	ND(13,000)	ND(1,100)	15	ND(0.24)
Aroclor 1254	mg/kg	- -	ND(25)	ND(13,000)	ND(1,100)	ND(6.6)	ND(0.24)
Aroclor 1260	mg/kg	- -	ND(25)	ND(13,000)	ND(1,100)	ND(6.6)	ND(0.24)
Total PCBs	mg/kg	- -	520	82,000	18,000	15	1.5
Inorganics-TCLP							
Arsenic	mg/L	5.0	NA	NA	NA	NA	NA
Barium	mg/L	100	NA	NA	NA	NA	NA
Cadmium	mg/L	1.0	NA	NA	NA	NA	NA
Chromium	mg/L	5.0	NA	NA	NA	NA	NA
Lead	mg/L	5.0	NA	NA	NA	NA	NA
Mercury	mg/L	0.2	NA	NA	NA	NA	NA
Selenium	mg/L	1.0	NA	NA	NA	NA	NA
Silver	mg/L	5.0	NA	NA	NA	NA	NA
Miscellaneous Parameters							
% Moisture	%	- -	16.0	13.0	22.0	17.0	12.0
% Solids	%	- -	84.0	87.0	78.0	83.0	88.0
Cyanide, Reactive	mg/kg	- -	NA	NA	NA	NA	NA
Flashpoint	Degrees F	- -	NA	NA	NA	NA	NA
pH	SU	- -	NA	NA	NA	NA	NA
Sulfide, Reactive	mg/kg	- -	NA	NA	NA	NA	NA

TABLE 7
SUMMARY OF SOIL CHARACTERIZATION SAMPLE DATA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

Notes:
1. Samples were collected by ARCADIS and submitted to TestAmerica (formerly Severn Trent Laboratories) for analysis.
2. Field duplicate sample results are presented in brackets.
3. ND - The analyte/compound was not detected. The number in parentheses is the associated detection limit.
4. NA - Not analyzed.
5. All results are preliminary; data validation has not been performed.
6. Bolded and shaded values indicate a TCLP Regulatory Level exceedance.

Data Qualifiers:
B - Compound was found in the blank and sample.
J - The analyte/compound was positively identified; however, the associated numerical value is an estimated concentration only.
p - This flag is used for a pesticide/Aroclor target analyte when there is greater than 25% difference for detected concentrations between the two GC columns. The greater of the two values is reported on the data page and flagged with a "p".
* - The compound was analyzed for, but not detected. LCS or LCSD exceeds the control limits

TABLE 8
ELM STREET AREA EXCEEDANCES OF 1 mg/kg SURFACE SCL NOT ADDRESSED BY LIMITS OF SOIL REMOVAL

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in units milligram per kilogram, mg/kg)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs	Property Location
Surface Soil Samples											
ESSS-R18E	0 - 1	4/23/2004	ND(0.18) [ND(0.21)]	ND(0.18) [ND(0.21)]	ND(0.18) [ND(0.21)]	ND(0.18) [ND(0.21)]	0.45 J [0.85 J]	0.54 [0.82]	ND(0.18) [ND(0.21)]	0.98 J [1.7 J]	Cemetery
ESSS-R20N	0 - 1	4/23/2004	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	0.86	1.5	ND(0.24)	2.4	Cemetery

Note:
1. See Table 6 of the Pre-Design Report dated January 2005 for the notes associated with the original table from which this table was created.

TABLE 9
MILL STREET AREA EXCEEDANCES OF 1 mg/kg SCLs
NOT FULLY ADDRESSED WHEN USING BACKHOE FOR GUIDE WALLS OF SPTC WALL
AND FOCUSED EXCAVATION PERFORMED NORTH OF SPTC WALL,
OR OTHERWISE ALREADY APPROVED BY USEPA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in units milligram per kilogram, mg/kg)

Sample ID	Depth (Feet)	Date Collected	Aroclor 1016	Aroclor 1221	Aroclor 1232	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Total PCBs	Property
Surface Soil Samples											
MSSB-B13	0 - 1	2/12/2004	ND(0.23)	ND(0.23)	ND(0.23)	ND(0.23)	1.2	0.45	ND(0.23)	1.6	Railroad
MSSB-B17	0 - 1	2/12/2004	ND(0.24)	ND(0.24)	ND(0.24)	2.4	ND(0.24)	ND(0.24)	ND(0.24)	2.4	Railroad
MSSS-B13E	0 - 1	4/19/2004	ND(0.21)	ND(0.21)	ND(0.21)	ND(0.21)	1.3	ND(0.21)	ND(0.21)	1.3	Railroad
MSSS-C18N	0 - 1	4/19/2004	ND(2.1)	ND(2.1)	ND(2.1)	ND(2.1)	8.6	ND(2.1)	ND(2.1)	8.6	Railroad
Subsurface Soil Samples											
EB-13	9 - 11	6/30/2004	ND(0.23) [ND(0.27)]	ND(0.23) [ND(0.27)]	ND(0.23) [ND(0.27)]	1.2 [0.93]	ND(0.23) [ND(0.27)]	ND(0.23) [ND(0.27)]	ND(0.23) [ND(0.27)]	1.2 [0.93]	Town
	15 - 16.5	11/13/1991	--	--	--	--	--	--	--	1.4 J	
MSSB-C07NW	17-19	7/8/2004	ND(4.2)	ND(4.2)	ND(4.2)	ND(4.2)	ND(4.2)	28	ND(4.2)	28	Railroad
	19-21	7/8/2004	ND(5.7)	ND(5.7)	ND(5.7)	ND(5.7)	ND(5.7)	39	ND(5.7)	39	
	21-23	7/8/2004	ND(4.4)	ND(4.4)	ND(4.4)	ND(4.4)	ND(4.4)	30	ND(4.4)	30	
MSSB-C07W	9 - 11	7/28/2004	1.1	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	1.1	Draper
MSSB-C11	5 - 7	1/8/2004	ND(0.37)	ND(0.37)	ND(0.37)	ND(0.37)	2.1	ND(0.37)	ND(0.37)	2.1	Border
	11 - 13	1/8/2004	ND(0.76)	ND(0.76)	ND(0.76)	ND(0.76)	3.7	ND(0.76)	ND(0.76)	3.7	(Town/Railroad)
MSSB-C11W	5 - 7	7/22/2004	ND(0.21)	ND(0.21)	ND(0.21)	ND(0.21)	1.4	ND(0.21)	ND(0.21)	1.4	Border
	7 - 9	7/22/2004	ND(0.25)	ND(0.25)	ND(0.25)	ND(0.25)	1.5	ND(0.25)	ND(0.25)	1.5	(Town/Railroad)
	9 - 11	7/22/2004	ND(0.27)	ND(0.27)	ND(0.27)	ND(0.27)	2.1	ND(0.27)	ND(0.27)	2.1	
MSSB-D07	9 - 11	2/13/2004	ND(0.21)	ND(0.21)	ND(0.21)	ND(0.21)	2.1	ND(0.21)	ND(0.21)	2.1	Border
	11 - 13	2/13/2004	ND(0.28)	ND(0.28)	ND(0.28)	1.5 J	ND(0.28)	ND(0.28)	ND(0.28)	1.5 J	(Town/Draper)
	19 - 21	2/13/2004	ND(0.26)	ND(0.26)	ND(0.26)	1.1	ND(0.26)	ND(0.26)	ND(0.26)	1.1	
MSSB-D07SE	9 - 11	7/22/2004	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	3.1	ND(0.24)	ND(0.24)	3.1	Border
	17 - 19	7/22/2004	ND(0.27)	ND(0.27)	ND(0.27)	ND(0.27)	0.91	0.28	ND(0.27)	1.2	(Town/Draper)
MSSB-D07W	9 - 11	7/28/2004	ND(0.20)	ND(0.20)	ND(0.20)	ND(0.20)	1.3	ND(0.20)	ND(0.20)	1.3	Draper
MSSB-D11	15 - 17	7/6/2004	ND(0.31)	ND(0.31)	ND(0.31)	ND(0.31)	1.1	ND(0.31)	ND(0.31)	1.1	Town
MSSB-D13E	15 - 16	7/6/2004	ND(0.25)	ND(0.25)	ND(0.25)	1.6	ND(0.25)	ND(0.25)	ND(0.25)	1.6	Town
MSSB-D15	7 - 9	8/25/2004	ND(0.24)	ND(0.24)	ND(0.24)	ND(0.24)	2.8	ND(0.24)	ND(0.24)	2.8	Town
	9 - 11	8/25/2004	ND(0.19)	ND(0.19)	ND(0.19)	ND(0.19)	1.4	ND(0.19)	ND(0.19)	1.4	
	11 - 12	8/25/2004	ND(0.22)	ND(0.22)	ND(0.22)	ND(0.22)	1.3	ND(0.22)	ND(0.22)	1.3	
MSSB-E07	3 - 5	12/9/2003	ND(0.13)	ND(0.13)	ND(0.13)	ND(0.13)	1.7	ND(0.13)	ND(0.13)	1.7	Draper
MSSB-E13	11 - 13	12/17/2003	ND(0.19)	ND(0.19)	ND(0.19)	2.0	ND(0.19)	ND(0.19)	ND(0.19)	2.0	Town
MSSB-E13E	7 - 9	7/27/2004	ND(0.78)	ND(0.78)	ND(0.78)	ND(0.78)	2.3	0.82	ND(0.78)	3.2	Town
MSSB-E14	5 - 7	7/27/2004	ND(0.27)	ND(0.27)	ND(0.27)	2.1	ND(0.27)	ND(0.27)	ND(0.27)	2.1	Town

Notes:
1. See Tables 9 and 11 of the Pre-Design Report dated January 2005 for the notes associated with the original tables from which this table was created.
2. Excludes two samples from boring MSSB-C01 (11-13' and 23-25') that EPA has determined do not need to be addressed by the cleanup.
3. Excludes 11 samples from borings MSSB-B12 (15-17'), -B13 (9-11'), -B17 (1-3' and 3-5'), -C14 (13-15'), -C15 (7-9', 11-13', and 15-17') and -C17 (3-5', 7-9', and 15-17').
EPA's February 13, 2007 letter approved GE's technical justification for not addressing the soils associated with these samples.

TABLE 10
ESTIMATED VOLUME OF MATERIAL SUBJECT TO REMEDIAL ACTION TO ACHIEVE NON-CORRIDOR SCLs

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

Area	Excavation Cell Identifier	Approximate Excavation Depth (feet bgs)	Elevation of Excavation Bottom (feet)	Approximate Surface Area (square feet)	Approximate In-Situ Volume (cubic feet)	Approximate In-Situ Volume (cubic yards)	Approximate In-Situ Volume (cubic yards)	
							TSCA	Non-TSCA
Elm Street Area	A	1	--	18,153.04	18,150	670	500	170
	B	--	244	459.50	1,150	40	40	--
	C	3	--	1,338.94	4,020	150	--	150
	D	--	238	1,247.28	13,100	490	490	--
	E	--	244	617.66	2,470	90	90	--
	F	--	238	918.96	7,730	290	290	--
	G	1	--	1,209.75	1,210	40	10	30
	H	--	241	2,548.23	28,880	1,070	1,070	--
	I	1	--	12,489.58	12,490	460	290	170
	J	--	236	4,708.03	56,270	2,080	2,080	--
	K	--	240	2,225.14	32,260	1,190	1,190	--
	L	--	249	2,492.54	12,410	460	460	--
	M	3	--	3,729.85	11,190	410	410	--
	N	--	263	889.91	1,780	70	70	--
	O	--	262	926.97	2,940	110	110	--
	P	--	256	1,189.24	8,320	310	310	--
	Q	--	258	2,102.54	9,460	350	350	--
	R	--	251	4,097.52	40,980	1,520	1,520	--
	S	--	239	1,018.08	19,340	720	720	--
	T	--	244	665.10	9,640	360	360	--
	U	--	253	380.80	1,140	40	40	--
	V	--	247	3,001.02	32,510	1,200	1,200	--
	W	--	234.5	6,571.17	117,800	4,360	4,360	--
	X	--	250	2,960.37	31,820	1,180	1,180	--
	Y	--	252.5	2,300.45	19,550	720	720	--
	Z	--	255	861.20	5,600	210	210	--
	AA	1	--	11,928.37	22,340	830	380	460
	BB	--	251	2,043.60	22,750	840	840	--
	CC	--	248	1,143.12	12,570	470	470	--
	DD	--	245	650.26	8,450	310	310	
	EE	1	--	4,931.80	4,930	180	--	180
			Subtotal:	**99,800**	**573,250**	**21,220**	**20,070**	**1,160**
Mill Street Area	A	1	--	1,623.45	1,620	60	--	60
	B	--	256	315.59	630	20	--	20
	C	1	--	731.98	730	30	--	30
	D	--	257	929.68	1,860	70	10	60
	E	--	250	803.70	7,230	270	--	270
	F	--	254	159.29	800	30	--	30
	G	--	254	155.43	890	30	--	30
	H	--	238	831.54	19,960	740	740	--
	I	--	249	2,123.17	23,350	860	660	200
	J	3	--	5,111.68	15,340	570	310	260
	K	--	251	2,162.23	22,000	810	400	410
	L	--	258	276.51	1,660	60	60	--
	M	--	254	2,367.63	15,260	570	470	100
	N	--	251	284.30	2,560	90	90	--
	O	--	238	3,471.58	77,420	2,870	2,870	--
	P	--	254	308.91	1,850	70	70	--
	Q	--	248	88.76	1,070	40	40	--
	R	--	245	907.13	13,790	510	510	--
	S	--	255	1,602.11	9,250	340	240	100
	T	--	254	1,323.03	11,090	410	240	170
	U	1	--	4,809.87	4,810	180	--	180
	V	1	--	1,405.95	1,410	50	30	20
	1	1.5	--	408.64	610	20	--	20
	2	2.125	--	184.53	390	10	--	10
	3	2	--	1,211.42	2,420	90	60	10
	4	3	--	81.89	250	5	5	--
	5	4	--	351.42	1,410	50	50	--
	6	3	--	938.67	2,820	100	60	50
			Subtotal:	**34,970**	**242,480**	**8,955**	**6,915**	**2,030**
			Total:	**134,770**	**815,730**	**30,175**	**26,985**	**3,190**

Notes:
1. Refer to Figure 9 for Elm Street Area excavation cell identifiers.
2. Refer to Figure 12 for Mill Street Area excavation cell identifiers.
3. Approximate volumes were rounded using computer software.
4. TSCA - Toxic Substances Control Act.

TABLE 11
ADDITIONAL SOIL REMOVAL REQUIRED FOR REPLACEMENT
STORM SEWER, COVER SYSTEM, STORM WATER RETENTION AREA, AND GABION WALL

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

Area	Excavation Cell Identifier	Excavation Depth Below Remedial Excavation (feet)	Approximate Surface Area (square feet)	Approximate In-Situ Volume (cubic feet)	Approximate In-Situ Volume (cubic yards)
Elm Street Area	A	0.3	3,722.27	1,240	50
	B	0.3	380.80	130	5
	C	2.3	1,226.63	2,860	105
	D	2.3	512.42	1,200	40
	E	2.3	71.20	170	10
	F	1.3	501.11	670	20
	G	0.3	135.11	50	5
	H	0.3	1,373.27	460	20
	I	2.3	2,515.57	5,870	220
	J	3.3	15.97	50	5
	K	12	180.15	2,160	80
	L	12	588.78	7,070	260
	M	7.5	44.36	330	10
	N	5.25	124.16	650	20
	O	4	180.64	720	30
	P	5	225.01	1,130	40
	Q	2.5	1,374.44	3,440	130
	R	2.3	507.13	1,180	40
	S	3.5	1,670.47	5,850	220
Subtotal:			**15,349**	**35,230**	**1,310**

Notes:
1. Refer to Figure 10 for excavation cell identifiers.
2. Approximate volumes were rounded using computer software.
3. Volume calculations for Excavation Cells K, L, M, N, O, and P are based on assumed excavation depth to the bedding for the replacement storm sewer as illustrated on Technical Drawing G-20.

TABLE 12
ESTIMATED TOTAL VOLUME OF MATERIAL SUBJECT TO REMEDIAL ACTION

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

Area	Excavation Cell Identifier	Approximate Excavation Depth (feet bgs)	Elevation of Excavation Bottom (feet)	Approximate Surface Area (square feet)	Approximate In-Situ Volume (cubic feet)	Approximate In-Situ Volume (cubic yards)
Elm Street Area	A1	1	--	16,482.57	16,480	610
	A2	--	241	1,670.47	7,520	280
	B	--	244	459.50	1,150	40
	C	3	--	1,338.94	4,020	150
	D	--	238	1,247.28	13,100	490
	E	--	244	617.66	2,470	90
	F	--	238	918.96	7,730	290
	G	1	--	1,209.75	1,210	40
	H	--	241	2,548.23	28,880	1,070
	I	1	--	10,672.59	10,670	400
	J	--	236	4,708.03	56,270	2,080
	K	--	240	2,225.14	32,260	1,190
	L	--	249	2,492.54	12,410	460
	M	3.3	--	6,175.49	20,380	750
	N	--	263	388.79	780	30
	O	--	262	791.86	2,770	100
	P	--	256	1,189.24	8,320	310
	Q	--	258	734.50	3,310	120
	R	--	251	4,097.52	40,980	1,520
	S	--	239	1,018.08	19,340	720
	T	--	244	665.10	9,640	360
	U	--	253	380.80	1,140	40
	V	--	247	3,001.02	32,510	1,200
	W	--	234.5	6,571.17	117,800	4,360
	X1	--	250	2,509.51	26,980	1,000
	X2	--	250	170.54	1,830	70
	Y1	--	252.5	2,084.93	17,720	660
	Y2	--	252.5	91.26	780	30
	Z1	--	255	789.28	5,130	180
	Z2	--	255	31.46	200	10
	AA	1	--	1,570.00	1,570	60
	BB	3.3	--	3,918.32	14,570	550
	CC	1	--	307.24	310	10
	DD	12	--	180.15	2,160	80
	EE	13	--	588.78	7,650	290
	FF	1	--	6,927.01	17,340	660
	GG	13	--	44.36	580	30
	HH	13.5	--	124.16	1,680	50
	II	13.5	--	180.64	2,440	90
	JJ1	--	251	85.96	860	30
	JJ2	--	251	1,777.77	20,080	750
	KK	12.5	--	280.32	3,500	150
	LL	--	248	1,143.12	12,570	470
	MM	--	245	650.26	8,450	310
	NN	2.3	--	555.89	1,280	50
	OO	1	--	1,615.12	1,620	60
	PP	1	--	2,402.73	2,400	100
	QQ	1	--	294.13	290	10
	RR	2.5	--	--	3,460	130
	Pavement Removal		--	695.12	30	30
	Additional volume associated with sloping			--	--	1,840
			Subtotal:	**100,623.29**	**606,620**	**24,400**

TABLE 12
ESTIMATED TOTAL VOLUME OF MATERIAL SUBJECT TO REMEDIAL ACTION

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

Area	Excavation Cell Identifier	Approximate Excavation Depth (feet bgs)	Elevation of Excavation Bottom (feet)	Approximate Surface Area (square feet)	Approximate In-Situ Volume (cubic feet)	Approximate In-Situ Volume (cubic yards)
Mill Street Area	A	1	--	1,623.45	1,620	60
	B	--	256	315.59	630	20
	C	1	--	731.98	730	30
	D	--	257	929.68	1,860	70
	E	--	250	803.70	7,230	270
	F	--	254	159.29	800	30
	G	--	254	155.43	890	30
	H	--	238	831.54	19,960	740
	I	--	249	2,123.17	23,350	860
	J	3	--	5,111.68	15,340	570
	K	--	251	2,162.23	22,000	810
	L	--	258	276.51	1,660	60
	M	--	254	2,367.63	15,260	570
	N	--	251	284.30	2,560	90
	O	--	238	3,471.58	77,420	2,870
	P	--	254	308.91	1,850	70
	Q	--	248	88.76	1,070	40
	R	--	245	907.13	13,790	510
	S	--	255	1,602.11	9,250	340
	T	--	254	1,323.03	11,090	410
	U	1	--	4,809.87	4,810	180
	V	1	--	1,405.95	1,410	50
	1	1.5	--	408.64	610	20
	2	2.125	--	184.53	390	10
	3	2	--	1,211.42	2,420	90
	4	3	--	81.89	250	5
	5	4	--	351.42	1,410	50
	6	3	--	938.67	2,820	100
	Slurry material associated with installation of SPTC walls			--	--	2,000
	Additional volume associated with sloping			--	--	950
			Subtotal:	**34,970**	**242,480**	**11,905**
			Total:	**135,593**	**849,100**	**36,305**

Notes:
1. Refer to Figure 11 for Elm Street Area excavation cell identifiers.
2. Refer to Figure 12 for Mill Street Area excavation cell identifiers.
3. Approximate volumes were rounded using computer software.
4. Based on the support of excavation (SOE) design performed by Haley & Aldrich, the sloping of excavations shown on Technical Drawings S-2 and S-9 will require the excavation of an additional approximately 2,790 cy of material. This includes approximately 1,840 cy from the Elm Street Area and approximately 950 cy from the Mill Street Area.

TABLE 13
GROUNDWATER ELEVATION MONITORING DATA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in feet above mean sea level)

Monitoring Well	January/February 2004		March 18, 2004	April 19 & 20, 2004	May 21, 2004	June 23, 2004	July 13, 2004	August 18, 2004	September 14, 2004	October 19, 2004	November 17, 2004	December 13, 2004
	Elevation	Date										
Elm Street Area Monitoring Wells												
MW-01A	236.80	1/22/04	236.30	237.81	237.01	236.36	236.12	235.92	235.86	236.17	235.99	237.24
MW-01B	237.76	1/22/04	236.06	238.63	237.96	236.75	235.82	235.57	235.53	236.00	235.65	237.90
MW-02AR	235.43	2/4/04	235.45	236.95	236.01	235.32	235.15	235.13	235.10	235.38	235.20	236.61
MW-02B	235.55	2/4/04	235.47	237.02	236.05	235.39	235.26	235.18	235.17	235.42	235.26	236.62
MW-03A	235.66	2/4/04	235.62	236.70	236.07	235.45	235.28	235.22	235.17	235.51	235.29	236.63
MW-03B	235.26	2/5/04	235.25	236.18	235.61	235.00	234.82	234.87	234.83	235.20	234.96	236.39
MW-04A	235.70	1/27/04	235.62	236.72	236.09	235.47	235.33	235.23	235.17	235.53	235.29	236.64
MW-04B	235.26	1/27/04	235.25	236.12	235.58	234.98	234.88	234.86	234.82	235.18	234.96	236.36
MW-04C	235.76	2/4/04	235.73	236.89	236.24	235.63	235.46	235.34	235.28	235.60	235.39	236.71
MW-18B	235.54	2/3/04	235.52	236.70	235.98	235.37	235.19	235.12	235.08	235.45	235.22	236.60
MW-26A	235.77	1/22/04	235.40	236.41	235.79	235.18	235.05	235.01	234.98	235.36	235.13	236.50
MW-26B	235.22	2/4/04	235.24	236.21	235.60	235.00	234.85	234.87	234.83	235.21	235.04	236.39
MW-27A	239.92	2/5/04	239.73	241.96	240.78	240.06	239.63	239.30	239.24	239.59	239.39	240.39
MW-27B	241.79	2/5/04	242.21	246.39	244.22	243.60	243.46	242.50	242.24	242.75	241.87	244.53
MW-28A	243.41	1/26/04	242.93	244.92	243.93	243.36	242.98	242.63	242.56	242.87	242.71	243.35
MW-28B	248.16	1/26/04	248.15	249.32	248.64	248.41	248.27	248.05	248.04	248.17	248.10	248.70
MW-29B	235.48	2/4/04	235.50	236.61	235.94	235.34	235.17	235.13	235.09	235.46	235.24	236.61
Mill Street Area Monitoring Wells												
MW-07A	252.74	2/2/04	252.93	261.62	253.35	252.97	252.50	252.08	252.07	252.80	252.55	253.67
MW-09A	251.66	1/27/04	251.38	252.54	251.98	251.44	250.71	250.05	250.03	251.11	250.88	251.95
MW-09B	252.99	1/27/04	-	253.65	253.13	252.45	251.51	250.91	250.90	252.44	252.25	253.46
MW-21C	252.65	1/21/04	252.52	253.57	252.97	252.57	252.04	251.66	251.67	252.43	252.22	253.33
MW-22A	252.91	2/3/04	253.10	254.15	253.44	252.93	252.32	251.85	251.89	252.80	252.62	253.95
MW-22B	252.93	2/3/04	253.11	254.15	253.44	252.93	252.31	251.85	251.89	252.81	252.62	253.96
MW-22C	255.22	1/30/04	252.31	253.32	252.73	252.25	251.56	251.14	251.16	252.08	251.89	253.01
MW-23A	252.99	1/28/04	253.05	254.24	253.40	252.91	252.35	251.92	251.95	252.78	252.59	253.92
MW-23B	252.95	1/28/04	252.97	254.18	253.32	252.86	252.34	251.96	251.94	252.70	252.52	253.85
MW-23C	252.42	1/28/04	252.57	253.68	252.95	252.52	252.02	251.62	251.62	252.37	252.18	253.30
MW-24A	252.61*	1/23/04	252.83	253.90	253.20	252.84	252.31	252.01	251.95	252.66	252.46	253.54
MW-24B	252.87	1/23/04	252.83	253.92	253.19	252.83	252.38	252.01	251.96	252.65	252.45	253.57
MW-24C	251.94	1/29/04	252.30	253.44	252.70	252.28	251.80	251.34	251.35	252.10	251.90	252.99
Other Monitoring Wells												
MW-05A	236.19	1/19/04	235.35	236.41	235.59	235.08	234.93	234.92	234.88	235.29	235.01	236.51
MW-05BR	235.31	2/3/04	235.25	236.22	235.50	234.93	234.78	234.82	234.76	235.21	234.91	236.45
MW-06A	-	-	-	-	-	-	-	-	-	-	-	-
MW-06B	-	-	-	-	-	-	-	-	-	-	-	-
MW-06C	-	-	-	-	-	-	-	-	-	-	-	-
MW-08A	252.63	1/30/04	252.62	253.39	252.85	252.72	251.52	251.39	251.53	252.32	252.36	252.82
MW-08B	252.85	1/30/04	253.10	253.84	253.41	252.59	252.01	251.82	251.79	252.93	252.61	253.91
MW-10A	251.26	1/20/04	251.04	252.39	251.71	251.16	250.50	249.93	249.90	250.66	250.46	251.61
MW-10B	252.79	1/20/04	250.56	253.30	252.73	252.37	249.17	251.84	251.95	252.38	251.95	252.86
MW-10C	251.71	1/21/04	251.05	252.41	251.80	251.25	250.61	250.04	250.01	250.74	250.58	251.71
MW-11A	240.49	2/2/04	239.98	242.31	241.55	240.92	240.34	239.71	239.52	239.77	239.59	240.39
MW-11B	239.76	2/2/04	239.35	241.67	240.89	240.22	239.61	238.01	238.82	239.05	238.88	239.67
MW-11C	-	-	-	-	-	-	-	-	-	-	-	-
MW-25B	253.93	1/21/04	253.89	255.06	254.27	253.77	253.27	252.87	252.91	253.65	253.47	254.63
MW-25C	253.85	1/21/04	253.77	254.99	254.17	253.68	253.16	252.78	252.82	253.55	253.36	254.53
MW-30B	-	-	-	-	-	-	-	-	-	-	-	-
MW-30C	-	-	-	-	-	-	-	-	-	-	-	-
MW-31C	-	-	-	-	-	-	-	-	-	-	-	-
Gas Station Monitoring Wells												
GULF-02R	-	-	-	-	-	-	-	-	-	-	-	-
GULF-03	-	-	-	-	-	-	-	-	-	-	-	-
MOBIL-02R	-	-	-	-	-	-	-	-	-	-	-	-
MOBIL-04	-	-	-	-	-	-	-	-	-	-	-	-
Staff Gauges												
SG-1	See Note 6	See Note 6	See Note 6	237.18	See Note 7	See Note 7	See Note 7	See Note 7	See Note 7	See Note 7	See Note 7	See Note 7
SG-2	See Note 6	See Note 6	See Note 6	235.04	235.26	234.79	234.92	235.94	234.69	235.12	234.80	236.23

TABLE 13
GROUNDWATER ELEVATION MONITORING DATA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in feet above mean sea level)

Monitoring Well	January 11, 2005	July 31, 2007	October 8, 2007	January 22, 2008	April 16, 2008	July 29, 2008	October 17, 2008	January 20, 2009	April 21, 2009	July 23, 2009	October 7, 2009
Elm Street Area Monitoring Wells											
MW-01A	236.58	236.20	235.84	236.65	238.38	237.59	236.62	237.24	237.37	237.29	236.30
MW-01B	236.60	235.95	235.46	237.01	238.49	238.48	236.21	236.88	237.10	237.09	235.83
MW-02AR	235.70	235.22	235.15	235.79	237.29	236.54	235.46	235.98	236.20	236.10	235.33
MW-02B	235.73	235.35	235.25	235.85	237.35	236.59	235.54	236.05	236.27	236.17	235.41
MW-03A	235.83	235.34	235.20	236.02	237.34	236.79	235.66	236.26	236.53	236.28	235.49
MW-03B	235.47	234.94	234.89	235.68	236.68	236.42	235.15	235.70	236.05	235.74	235.05
MW-04A	235.83	235.32	235.36	235.99	237.30	236.76	235.64	236.22	236.54	236.24	235.43
MW-04B	235.44	234.89	234.87	235.66	236.64	236.38	235.13	235.66	236.03	235.72	235.02
MW-04C	235.96	235.51	235.08	236.13	237.32	236.89	235.83	236.42	236.75	236.44	235.58
MW-18B	235.77	235.29	235.11	235.87	237.12	236.72	235.53	236.15	236.31	236.17	235.39
MW-26A	235.63	235.15	234.80	235.86	236.84	236.61	235.35	235.95	236.30	236.02	235.28
MW-26B	235.47	234.99	235.21	235.72	236.64	236.50	235.22	235.76	236.14	235.82	235.09
MW-27A	240.03	239.80	239.18	240.35	242.06	241.33	240.59	241.07	241.15	241.47	239.89
MW-27B	243.55	243.89	243.17	245.33	245.25	246.42	244.70	245.39	245.60	245.59	244.39
MW-28A	243.26	243.20	242.48	243.48	245.01	244.22	244.04	244.32	244.31	244.67	243.28
MW-28B	248.33	248.72	248.43	249.33	249.54	250.15	249.13	249.46	249.53	249.73	248.82
MW-29B	235.74	235.30	235.17	235.96	237.88	237.88	235.54	236.09	236.43	236.18	235.39
Mill Street Area Monitoring Wells											
MW-07A	253.06	252.57	251.38	253.14	253.90	254.19	253.20	253.24	253.62	253.57	252.42
MW-09A	251.46	251.11	249.04	251.46	252.84	252.83	250.85	252.13	252.46	252.35	250.63
MW-09B	252.84	252.16	249.80	252.81	253.63	253.98	251.76	253.16	253.46	253.21	251.42
MW-21C	252.74	252.24	250.88	252.81	253.63	253.85	252.82	253.02	253.37	253.24	252.05
MW-22A	253.15	252.58	251.04	253.23	254.04	254.41	253.17	253.41	253.78	253.56	252.22
MW-22B	253.16	252.59	251.07	253.24	254.05	254.39	253.16	253.42	253.76	253.57	252.22
MW-22C	252.46	251.92	250.29	252.50	253.45	253.54	252.58	252.86	253.14	253.01	251.61
MW-23A	253.12	252.56	251.15	253.23	254.01	254.47	253.12	253.34	253.88	253.55	252.29
MW-23B	253.03	252.51	251.20	253.20	253.92	254.53	253.04	253.24	253.87	253.49	252.30
MW-23C	252.70	252.22	250.83	252.82	253.60	253.85	252.77	252.97	253.36	253.20	251.99
MW-24A	252.96	252.49	251.29	253.07	253.62	254.05	252.98	253.11	253.42	253.36	252.32
MW-24B	252.93	252.48	251.29	253.08	253.64	254.12	252.97	253.10	253.44	253.35	252.33
MW-24C	252.41	251.97	250.61	252.62	253.34	253.63	252.56	252.80	253.16	253.06	251.85
Other Monitoring Wells											
MW-05A	235.58	234.96	234.89	235.85	236.88	236.55	235.26	235.76	236.17	236.88	235.05
MW-05BR	235.45	234.80	234.79	235.79	236.70	236.50	235.09	235.65	236.00	235.67	234.94
MW-06A	-	-	-	235.57 (See Note 3)	236.39 (See Note 3)	236.21 (See Note 3)	234.91 (See Note 3)	NA (See Note 4)	NA (See Note 4)	NA (See Note 4)	234.84
MW-06B	-	-	-	235.63 (See Note 3)	236.53 (See Note 3)	236.36 (See Note 3)	234.93 (See Note 3)	NA (See Note 4)	NA (See Note 4)	NA (See Note 4)	234.85
MW-06C	-	-	-	235.60 (See Note 3)	236.54 (See Note 3)	236.32 (See Note 3)	234.97 (See Note 3)	NA (See Note 4)	NA (See Note 4)	NA (See Note 4)	234.90
MW-08A	253.04	251.90	250.01	252.70	253.52	253.75	252.70	253.02	253.21	253.12	251.36
MW-08B	253.09	252.25	250.70	253.36	253.91	254.38	252.95	253.28	254.11	253.57	251.85
MW-10A	251.16	250.68	248.92	250.94	252.71	252.30	251.50	251.79	252.11	252.29 (See Note 8)	250.48
MW-10B	252.48	252.35	249.21	252.80	253.47	253.32	252.38	252.71	253.03	252.73 (See Note 8)	250.75
MW-10C	251.31	250.88	248.89	250.85	252.64	252.21	251.42	251.73	252.02	252.21 (See Note 8)	250.43
MW-11A	240.49	240.44	239.24	240.06	243.71	241.29	241.27	241.95	241.89	242.05	240.32
MW-11B	239.75	239.77	238.53	239.30	243.00	240.80	240.70	241.37	241.30	241.46	239.75
MW-11C	-	-	-	-	-	241.12	241.22	241.96	241.82	242.02	240.25
MW-25B	254.05	253.36	252.05	253.97	254.92	255.06	254.03	254.15	254.62	254.36	253.26
MW-25C	253.95	253.27	251.99	253.88	254.85	254.99	254.05	254.06	254.56	254.32	253.17
MW-30B	-	-	-	-	-	252.99	252.50	252.56	252.66	252.74	252.04
MW-30C	-	-	-	-	-	253.02	252.42	252.52	252.63	252.76	251.83
MW-31C	-	-	-	-	-	-	-	-	-	-	-
Gas Station Monitoring Wells											
GULF-02R	-	249.26	248.98	249.88	250.32	250.53	249.78	250.20	250.57	250.64	249.57
GULF-03	-	249.19	248.56	250.28	250.24	251.45	249.58	249.91	250.29	250.36	249.22
MOBIL-02R	-	248.04	247.55	249.53	249.82	250.20	251.85	249.37	249.66 (See Note 5)	249.64 (See Note 5)	247.81 (See Note 5)
MOBIL-04	-	248.69	248.59 (See Note 5)	249.65	249.92	250.52 (See Note 5)	249.22	249.80	249.94 (See Note 5)	250.06	248.86
Staff Gauges											
SG-1	See Note 7	Dry	Dry	Frozen	See Note 7	See Note 7	See Note 7	See Note 7	See Note 7	See Note 7	See Note 7
SG-2	235.19	235.19	235.21	Frozen	235.74	235.02	234.24	234.74	235.99	236.29	235.14

TABLE 13
GROUNDWATER ELEVATION MONITORING DATA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in feet above mean sea level)

Monitoring Well	January 12, 2010	April 20, 2010	July 20, 2010	October 19, 2010	January 18, 2011	April 19, 2011	July 19, 2011	October 11, 2011	January 19, 2012	April 17, 2012	July 24, 2012
Elm Street Area											
MW-01A	236.72	237.89	235.52	235.87	236.36	237.91	235.89	237.00	236.82	236.32	235.30
MW-01B	236.55	238.15	235.00	235.53	236.06	238.15	237.82	238.26	237.94	236.50	234.84
MW-02AR	235.71	236.53	234.89	235.15	235.58	236.86	235.98	235.68	235.64	235.28	234.66
MW-02B	235.76	236.58	234.98	235.25	235.65	236.87	235.05	235.79	235.73	235.37	234.72
MW-03A	235.77	236.64	234.65	235.23	235.64	237.07	234.89	235.98	235.86	235.41	234.27
MW-03B	235.45	235.95	234.23	234.94	235.40	236.77	234.43	235.46	235.34	234.98	233.76
MW-04A	236.52	236.56	234.63	235.30	235.61	237.05	234.94	235.97	235.89	235.40	234.26
MW-04B	235.97	235.88	234.18	234.92	235.28	236.63	234.33	235.44	235.34	234.93	233.78
MW-04C	236.75	236.86	234.81	235.31	235.72	237.20	235.09	236.15	236.08	235.55	234.39
MW-18B	235.75	236.50	234.55	235.14	235.55	237.03	234.83	236.00	235.73	235.32	234.16
MW-26A	235.65	236.27	234.45	235.12	235.53	236.87	234.70	235.82	235.62	235.19	234.05
MW-26B	235.48	235.99	234.25	234.97	235.38	236.72	234.50	235.61	235.42	235.02	233.81
MW-27A	240.40	241.79	239.13	239.36	239.91	241.46	239.84	241.52	240.63	244.51	239.47
MW-27B	245.01	245.68	243.72	244.37	244.54	245.84	244.07	245.75	244.71	240.16	244.54
MW-28A	243.72	244.89	242.69	242.72	243.22	244.41	243.37	244.89	243.89	243.39	243.16
MW-28B	249.12	249.46	248.60	248.68	248.62	249.74	248.66	249.89	249.09	248.87	248.62
MW-29B	235.79	236.43	234.61	235.22	235.64	237.05	234.86	237.01	238.17	235.39	234.25
Mill Street Area											
MW-07A	253.04	253.71	251.82	251.62	252.68	254.01	252.67	253.90	253.20	252.83	252.08
MW-09A	251.60	252.85	249.72	249.36	250.94	NA (See Note 10)	250.81	252.43	252.02	252.14 (See Note 11)	250.20
MW-09B	252.73	253.59	250.46	250.16	252.33	NA (See Note 10)	251.74	253.41	252.07	253.37 (See Note 11)	251.03
MW-21C	252.74	253.51	251.29	251.17	252.29	253.66	252.25	253.53	252.95	252.54	252.03
MW-22A	253.16	253.93	251.48	251.38	252.71	254.22	252.52	253.95	253.31	252.89	251.90
MW-22B	253.15	253.94	251.48	251.39	252.72	254.21	252.51	253.97	253.29	252.91	251.91
MW-22C	252.52	253.41	250.80	250.61	253.03	253.42	251.83	253.24	252.75	252.29	251.37
MW-23A	253.06	253.84	251.60	251.10	252.52	254.25	252.62	253.90	253.29	252.91	252.02
MW-23B	253.00	253.73	251.64	251.60	252.45	254.20	252.59	253.81	253.23	252.82	252.02
MW-23C	252.70	253.43	251.30	251.24	252.13	253.67	252.27	253.47	252.96	252.53	251.94
MW-24A	253.00	253.52	251.75	251.59	252.42	253.83	252.72	253.71	253.06	252.83	252.16
MW-24B	253.00	253.53	251.74	251.59	252.41	253.88	252.71	253.73	253.07	252.84	252.18
MW-24C	252.66	253.35	251.12	251.02	251.92	253.51	252.19	253.45	252.87	252.67	251.98
Other Wells											
MW-05A	235.59	236.14	234.25	235.06	235.36	236.84	234.53	235.65	235.52	235.03	233.82
MW-05BR	235.45	235.94	234.10	234.95	235.25	236.75	234.36	235.54	235.38	234.90	233.67
MW-06A	NA (See Note 4)	NA (See Note 4)	NA (See Note 4)	234.82	NA (See Note 4)	NA (See Note 4)	NA (See Note 4)	235.27	NA (See Note 4)	NA (See Note 4)	NA (See Note 4)
MW-06B	NA (See Note 4)	NA (See Note 4)	NA (See Note 4)	234.87	NA (See Note 4)	NA (See Note 4)	NA (See Note 4)	235.36	NA (See Note 4)	NA (See Note 4)	NA (See Note 4)
MW-06C	NA (See Note 4)	NA (See Note 4)	NA (See Note 4)	234.87	NA (See Note 4)	NA (See Note 4)	NA (See Note 4)	235.37	NA (See Note 4)	NA (See Note 4)	NA (See Note 4)
MW-08A	252.77	253.36	250.49	250.61	252.17	253.42	251.63	253.32	252.93	252.46	251.03
MW-08B	252.97	253.79	251.16	251.74	252.64	253.86	252.11	253.69	253.28	252.85	251.55
MW-10A	251.20	252.72	249.42	249.14	250.36	252.21	251.53	--	251.67	250.90	249.93
MW-10B	252.38	253.28	249.78	250.67	252.83	253.05	251.93	252.71	252.60	252.27	250.33
MW-10C	251.15	252.66	249.40	249.11	250.27	252.16	250.50	252.01	251.62	250.96	250.00
MW-11A	240.73	243.59	239.69	238.84	239.13	241.89	240.43	241.48	241.57	240.59	239.92
MW-11B	240.12	243.10	239.11	238.30	239.71	241.30	239.77	240.82	240.91	239.91	239.26
MW-11C	240.72	243.55	239.67	238.82	239.65	241.82	240.37	241.44	241.52	240.41	239.89
MW-25B	254.06	254.78	252.47	252.49	253.43	255.31	253.41	254.76	254.10	253.76	252.98
MW-25C	253.94	254.71	252.41	252.40	253.39	254.86	253.34	254.69	254.04	253.65	252.91
MW-30B	252.43	252.77	251.56	251.36	252.27	252.90	252.30	253.06	252.50	252.34	252.06
MW-30C	252.33	252.87	251.34	251.13	252.04	252.89	252.06	253.12	252.43	252.15	251.77
MW-31C	-	-	-	-	-	-	-	-	-	-	234.57
Gas Station Wells											
GULF-02R	249.77	250.19	248.79	249.13	NA (See Note 4)	NA (See Note 4)	NA (See Note 4)	249.70	NA (See Note 4)	NA (See Note 4)	NA (See Note 4)
GULF-03	249.60	250.12	248.69	248.99	NA (See Note 4)	NA (See Note 4)	NA (See Note 4)	250.57	NA (See Note 4)	NA (See Note 4)	NA (See Note 4)
MOBIL-02R	NA (See Note 9)	249.29 (See Note 5)	247.43 (See Note 5)	247.81 (See Note 5)	247.81 (See Note 5)	249.56	247.66	249.61	248.54	248.10	247.64
MOBIL-04	NA (See Note 9)	249.73	248.47	248.76	248.67	250.14	248.72	249.30 (See Note 5)	249.36	249.00	248.73
Staff Gauges											
SG-1	See Note 7	See Note 7	See Note 7	See Note 7	See Note 7	See Note 7	See Note 7	See Note 7	See Note 7	See Note 7	233.59
SG-2	Frozen	235.55	Dry	See Note 7	Frozen	See Note 7	233.28	234.18	234.28	233.63	Dry

TABLE 13
GROUNDWATER ELEVATION MONITORING DATA

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in feet above mean sea level)

Notes:

1. * = Measured from top of casing before the coupling was added for the locking cap.
2. - = Not measured.
3. The groundwater elevation data for the MW-06 well cluster during the 2008 monitoring events presented in Water Monitoring Reports prior to April 2009 was calculated using survey information provided by EPA in the *Final Remedial Investigation Report for Fletcher's Paint Site, Milford, NH* (July 1, 1994). ARCADIS surveyed the location, ground, and measuring point elevation data for the MW-06 well cluster (as well as the MW-05 and MW-30 clusters and the Gulf and Mobil monitoring wells) following the April 2009 monitoring event. The groundwater elevation data presented in this table were revised based upon the ARCADIS survey data.
4. In accordance with EPA approval letter dated December 9, 2010, groundwater elevations at the MW-06 monitoring well cluster, GULF-02R and GULF-03 are only collected annually during the September quarterly monitoring event.
5. Groundwater elevation corrected for thickness of free product. Specific gravity of free product assumed to be 0.74 (see, http://ww2.ramapo.edu/libfiles/HR/Environmental_Health_and_Safety/MSDS/Facilities/Plumbing/gasoline.pdf). The depth to free product at MOBIL-02R on April 21, 2009, July 23, 2009, October 7, 2009, April 20, 2010, July 20, 2010, October 19, 2010, and January 18, 2011 was 11.65 feet, 11.76 feet, 13.57 feet, 12.25 feet, 13.99 feet, 13.20 feet, and 13.75 feet, respectively with free product thickness of 0.98 feet, 0.62 feet, 0.69 feet, 0.06 feet, 0.53 feet, 0.01 feet, and 0.01 feet, respectively. The depth to free product at MOBIL-04 on October 8, 2007, July 29, 2008, April 21, 2009, and October 11, 2011 was 11.51 feet, 9.56 feet, 10.19 feet and 10.81 feet, respectively with free product thickness of 0.14 feet, 0.24 feet, 0.02 feet and 0.13 feet, respectively.
6. Staff gauges SG-1 and SG-2 were not installed until April 2004. In addition, staff gauge SG-2 has been replaced three times (on June 24, 2009, July 5, 2011, and July 6, 2012) after being displaced by ice during the preceding winter.
7. SG-1 either could not be located or was inaccessible for measurement. SG-1 was re-surveyed on April 11, 2012. The corresponding ground elevation and measuring point elevation have been updated to reflect the new survey data. However, SG-2 was used to record the elevation measurement for the April 2012 quarterly monitoring event.
8. The groundwater elevations for the MW-10 monitoring well cluster during the July 2009 quarterly monitoring event were not collected on the same day as the measurements at the other wells in the network and may have been impacted by dewatering associated with sample collection.
9. The Shack Corner Mobil property changed ownership prior to the January 2010 quarterly monitoring event. GE/ARCADIS was unable to obtain access from the new owner prior to completing the monitoring event. Therefore, groundwater elevations were not collected at MOBIL-02R and MOBIL-04 during the January 2010 quarterly monitoring event.
10. GE/ARCADIS was unable to obtain access from the property owner for the MW-09 monitoring well cluster prior to the completion of the April 2011 monitoring event; therefore, groundwater elevations were not collected at the MW-09 monitoring well cluster during the April 2011 quarterly monitoring event.
11. ARCADIS was unable to obtain access from the property owner for the MW-09 monitoring well cluster prior to April 17, 2012; therefore, groundwater elevations were not collected until May 16, 2012.

TABLE 14
UST CHARACTERIZATION DATA - WASTEWATER

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in parts per million, ppm, unless otherwise noted)

Parameter / Sample ID: / Date Collected:	TCLP Regulatory Level	M12 (WATER) 08/12/03	M14N (WATER) 08/12/03
Volatile Organics			
1,1-Dichloroethene	0.7	ND(0.0050)	ND(180)
1,2 Dichloroethane	0.5	ND(0.0050)	ND(180)
2-Butanone	200	ND(0.025)	ND(360)
Benzene	0.5	ND(0.0050)	ND(180)
Carbon Tetrachloride	0.5	ND(0.0050)	ND(180)
Chlorobenzene	100	ND(0.0050)	ND(180)
Chloroform	6.0	ND(0.0050)	ND(180)
Tetrachloroethene	0.7	ND(0.0050)	ND(180)
Trichloroethene	0.5	ND(0.0050)	ND(180)
Vinyl chloride	0.2	ND(0.0050)	ND(180)
Semivolatile Organics			
1,4-Dichlorobenzene	7.5	ND(0.040)	NA
2,4,5-Trichlorophenol	400	ND(0.040)	NA
2,4,6-Trichlorophenol	2.0	ND(0.040)	NA
2,4-Dinitrotoluene	0.13	ND(0.040)	NA
2-Methylphenol	200	ND(0.040)	NA
3-Methylphenol	200	ND(0.040)	NA
4-Methylphenol	200	ND(0.040)	NA
Hexachlorobenzene	0.13	ND(0.040)	NA
Hexachlorobutadiene	0.5	ND(0.040)	NA
Hexachloroethane	3.0	ND(0.040)	NA
Nitrobenzene	2.0	ND(0.040)	NA
Pentachlorophenol	100	ND(0.20)	NA
Pyridine	5.0	ND(0.10)	NA
PCBs			
Aroclor 1016	- -	ND(0.00047)	NA
Aroclor 1221	- -	ND(0.00047)	NA
Aroclor 1232	- -	ND(0.00047)	NA
Aroclor 1242	- -	ND(0.00047)	NA
Aroclor 1248	- -	0.0028	NA
Aroclor 1254	- -	0.00073	NA
Aroclor 1260	- -	ND(0.00047)	NA
Inorganics			
Arsenic	5.0	ND(0.0070)	NA
Barium - Total	100	0.102	NA
Cadmium - Total	1.0	ND(0.0010)	NA
Chromium - Total	5.0	0.0028	NA
Lead - Total	5.0	ND(0.010)	NA
Mercury - Total	0.2	ND(0.00020)	NA
Selenium - Total	1.0	ND(0.010)	NA
Silver - Total	5.0	ND(0.0030)	NA
Miscellaneous Parameters			
Corrosivity (pH) (SU)	- -	6.72	NA
H2S Released From Waste	- -	ND(10.0)	NA
HCN Released From Waste	- -	ND(10.0)	NA
Heat of Combustion (BTU/LB)	- -	ND(1000)	NA
Percent Chlorine (%)	- -	0.0110	NA

Notes:
1. Samples were collected by Blasland, Bouck & Lee, Inc., and submitted to Severn Trent Laboratories, Inc. for analysis of TCLP VOCs, TCLP SVOCs, PCBs, TCLP metals, and miscellaneous parameters.
2. ND - Analyte was not detected. The number in parentheses is the associated reporting limit.
3. NA - Not analyzed.

TABLE 15
UST CHARACTERIZATION DATA - NON-WASTEWATER

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE
(Results are presented in parts per million, ppm, unless otherwise noted)

Parameter / Sample ID: / Date Collected:	TCLP Regulatory Level	20x TCLP Regulatory Level	M12 (SOIL) 08/12/03	M14N (SLUDGE) 08/12/03
Volatile Organics				
1,1-Dichloroethene	0.7	14	ND(0.050)	ND(18)
1,2 Dichloroethane	0.5	10	ND(0.050)	ND(18)
2-Butanone	200	4,000	ND(0.25)	ND(36)
Benzene	0.5	10	ND(0.050)	ND(18)
Carbon Tetrachloride	0.5	10	ND(0.050)	ND(18)
Chlorobenzene	100	2,000	ND(0.050)	ND(18)
Chloroform	6.0	120	0.044 J	ND(18)
Tetrachloroethene	0.7	14	ND(0.050)	ND(18)
Trichloroethene	0.5	10	ND(0.050)	ND(18)
Vinyl chloride	0.2	4.0	ND(0.050)	ND(18)
Semivolatile Organics				
1,4-Dichlorobenzene	7.5	150	ND(0.040)	ND(62)
2,4,5-Trichlorophenol	400	8,000	ND(0.040)	ND(62)
2,4,6-Trichlorophenol	2.0	40	ND(0.040)	ND(62)
2,4-Dinitrotoluene	0.13	2.6	ND(0.040)	ND(62)
2-Methylphenol	200	4,000	ND(0.040)	ND(62)
3-Methylphenol	200	4,000	ND(0.040)	ND(62)
4-Methylphenol	200	4,000	ND(0.040)	ND(62)
Hexachlorobenzene	0.13	2.6	ND(0.040)	ND(62)
Hexachlorobutadiene	0.5	10	ND(0.040)	ND(62)
Hexachloroethane	3.0	60	ND(0.040)	ND(62)
Nitrobenzene	2.0	40	ND(0.040)	ND(62)
Pentachlorophenol	100	2,000	ND(0.20)	ND(310)
Pyridine	5.0	100	ND(0.10)	ND(160)
PCBs				
Aroclor 1016	- -	- -	ND(1.4)	ND(2.4)
Aroclor 1221	- -	- -	ND(1.4)	ND(2.4)
Aroclor 1232	- -	- -	ND(1.4)	ND(2.4)
Aroclor 1242	- -	- -	ND(1.4)	ND(2.4)
Aroclor 1248	- -	- -	11	ND(2.4)
Aroclor 1254	- -	- -	4.3	ND(2.4)
Aroclor 1260	- -	- -	ND(1.4)	ND(2.4)
Inorganics				
Arsenic	5.0	100	0.0467	ND(0.530)
Barium - Total	100	2,000	0.563	0.308
Cadmium - Total	1.0	20	ND(0.00100)	ND(0.0758)
Chromium - Total	5.0	100	0.0244	0.245
Lead - Total	5.0	100	0.0670	ND(0.758)
Mercury - Total	0.2	4.0	ND(0.000200)	ND(0.00680)
Selenium - Total	1.0	20	0.0138	ND(0.758)
Silver - Total	5.0	100	ND(0.00300)	ND(0.227)
Miscellaneous Parameters				
Corrosivity (pH) (SU)	- -	- -	6.75	6.54
H2S Released From Waste	- -	- -	ND(10.0)	ND(10.0)
HCN Released From Waste	- -	- -	ND(10.0)	ND(10.0)
Heat of Combustion (BTU/LB)	- -	- -	ND(1,000)	16,800
Percent Chlorine (%)	- -	- -	0.0570	0.00460

Notes:
1. Samples were collected by Blasland, Bouck & Lee, Inc., and submitted to Severn Trent Laboratories, Inc. for analysis of TCLP VOCs, TCLP SVOCs, PCBs, TCLP metals, and miscellaneous parameters.
2. ND - Analyte was not detected. The number in parentheses is the associated reporting limit.

Data Qualifier:
J - Indicates an estimated value less than the practical quantitation limit (PQL).

TABLE 16
SUMMARY OF EXISTING WELL CONSTRUCTION

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

WELL ID	NORTHING	EASTING	GROUND ELEVATION (Feet AMSL)	MEASURING POINT ELEVATION (Feet AMSL)	WELL DIAMETER (Inches)	FLUSH-MOUNT/ STICK-UP	TOTAL DEPTH (TIC)	TOP OF SCREEN ELEVATION (Feet AMSL)	BASE OF SCREEN ELEVATION (Feet AMSL)	WELL MATERIAL
Elm St										
MW-01A	122264.8	987377.5	265.78	264.77	2	FLUSH	52.00	222.68	212.68	PVC
MW-01B	122263.3	987384.8	265.6	264.85	2	FLUSH	32.25	242.6	232.6	PVC
MW-02A	See MW-02AR	See MW-02AR	259.13	257.37	2	FLUSH	34.20	226.93	224.93	PVC
MW-02AR	122449.0	987561.4	258.6	261.18	2	STICK-UP	32.61	233.6	228.6	PVC
MW-02B	122443.8	987561.7	258.36	257.87	2	FLUSH	29.05	243.36	228.36	PVC
MW-03A	122441.0	987317.8	250.53	249.64	2	FLUSH	44.90	214.53	204.53	PVC
MW-03B	122446.2	987312.0	250.37	249.85	2	FLUSH	20.11	239.37	229.37	PVC
MW-04A	122540.3	987233.0	247.53	246.54	2	FLUSH	49.75	207.53	197.53	PVC
MW-04B	122533.7	987233.8	247.38	246.43	2	FLUSH	16.48	240.38	230.38	PVC
MW-04C	122532.1	987220.9	247.18	246.46	2	FLUSH	55.35	196.68	191.68	PVC
MW-18B	122342.6	987312.2	257.95	257.25	2	FLUSH	28.33	238.95	228.95	PVC
MW-26A	122390.2	987467.0	256.2	259.35	2	STICK-UP	45.00	223.72	213.92	PVC
MW-26B	122386.8	987464.4	256.5	259.50	2	STICK-UP	32.13	237.65	227.85	PVC
MW-27A	122225.5	987532.6	261.4	264.46	2	STICK-UP	39.25	234.9	225.1	PVC
MW-27B	122227.8	987537.9	261.4	264.6	2	STICK-UP	28.15	245.3	235.44	stainless steel
MW-28A	122239.7	987630.9	260.9	263.98	2	STICK-UP	34.80	238.96	229.16	PVC
MW-28B	122239.0	987624.1	260.7	264.07	2	STICK-UP	22.86	250.8	241	PVC
MW-29B	122338.4	987449.0	258.5	261.49	2	STICK-UP	32.93	238.5	228.7	PVC
MW-31C	122626.0	987083.8	246.62	246.26	4	FLUSH	74.14	N/A	N/A	stainless steel
Mill St										
MW-07A	121555.7	987530.9	259.9	261.59	2	STICK-UP	18.87	254.7	242.8	PVC
PZ-07B	121555.5	987536.2	260.0	262.69	2	STICK-UP	13.37	254.5	249.5	PVC
PZ-07C	121558.5	987526.9	260.2	263.22	4	STICK-UP	37.02	N/A	N/A	PVC
MW-09A	121602.1	987263.8	257.85	257.25	2	FLUSH	22.18	242.89	234.89	PVC
MW-09B	121600.7	987268.1	258.06	257.86	2	FLUSH	13.45	254.73	243.23	PVC
PZ-21A	121577.4	987465.4	259.2	261.86	2	STICK-UP	24.27	242.7	237.7	PVC
PZ-21B	121577.3	987472.1	259.3	262.08	2	STICK-UP	12.89	254.3	249.3	PVC
MW-21C	121601.3	987391.6	259.2	261.72	2	STICK-UP	30.05	N/A	N/A	PVC
MW-22A	121601.3	987391.6	259.5	262.57	2	STICK-UP	21.51	246	241.2	PVC
MW-22B	121601.1	987385.6	259.4	262.36	2	STICK-UP	12.40	255	250.2	PVC
MW-22C	121602.4	987396.1	259.4	262.66	2	STICK-UP	42.70	229.4	219.6	PVC
PW-1	121583.7	987479.3	259.0	261.27	6	STICK-UP	27.80	248.55	239.0	stainless steel
PW-2	121583.1	987484.5	259.1	261.41	6	STICK-UP	46.31	N/A	N/A	stainless steel

Notes:
1. This table only presents information for monitoring wells impacted or potentially impacted by the implementation of the remedial action.
2. AMSL - Above mean sea level.
3. TIC - Top of inside casing.

TABLE 17
CHEMICAL-SPECIFIC ARARs

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

Medium	Potential Federal Requirement	Status	Requirement Synopsis	Action to be Taken to Attain ARAR
Groundwater	Safe Drinking Water Act (SDWA) Maximum Contaminant Levels (MCLs) (40 CFR 141.11, 141.13, 141.61, 141.62)	Relevant and Appropriate	Provides enforceable drinking water supply and cleanup standards for turbidity and certain inorganic and organic contaminants.	1998 SDWA MCLs (which are equal to the Interim Clean-Up Levels (ICLs) referenced by the 1998 ROD) will be attained through source control (i.e., soil removal) and subsequent monitored natural attenuation.
Surface Water/ Groundwater	SDWA Non-Zero MCL Goals (MCLGs) (40 CFR 141.50, 141.51)	Relevant and Appropriate	Provides non-enforceable zero and non-zero health goals for specific organic and inorganic contaminants in public water systems.	1998 SDWA Non-Zero MCLGs (which are equal to the ICLs referenced by the 1998 ROD) will be attained through source control (i.e., soil removal) and subsequent monitored natural attenuation.
Surface Water	Clean Water Act (CWA) s. 304(a), Ambient Water Quality Criteria (AWQC) for Protection of Human Health and Aquatic Life, 40 CFR 131	Relevant and Appropriate	AWQCs are developed under the CWA as guidelines from which states develop water quality standards for protection of human health and aquatic organisms.	AWQCs will be attained in adjacent surface waters through source control (i.e., soil removal) and subsequent monitored natural attenuation.
Soil/ Groundwater	Toxic Substance Control Act (TSCA) PCB "Mega-Rule" (40 CFR 761) and PCB Spill Cleanup Policy (40 CFR Part 761, Subpart G)	To Be Considered	Applicable to cleanup of PCB remediation waste -- sediments/soils containing PCBs at a concentration of 50 ppm or greater released from an original source containing PCBs at a concentration greater than 500 ppm prior to 4/18/78, or a concentration of 50 ppm or greater after 7/2/79 (40 CFR 761.3); and PCB liquids at concentrations of 50 ppm or greater (40 CFR 761.60.) Includes standards for cleanup of spills resulting from the release during remediation of materials containing PCBs at a concentration of 50 ppm or greater for spills which occur after May 4, 1987. 40 CFR 761.120(a).	Should any spill/release of PCBs at a concentration of 50 ppm or greater occur during the course of the remedial action, such releases will be addressed in compliance with these requirements.

TABLE 17
CHEMICAL-SPECIFIC ARARs

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

Medium	Potential Federal Requirement	Status	Requirement Synopsis	Action to be Taken to Attain ARAR
Groundwater	EPA Final Groundwater Use and Value Determination Guidance	To Be Considered	Provides a rating system for the State to establish restoration goals for a groundwater aquifer based on its vulnerability, use and value.	This guidance was considered in conjunction with the federal SDWA and the New Hampshire Groundwater protection Rules in the development of the 1998 ROD remedy for source control. The aquifer was classified as medium value, drinking water levels are expected to be attained at the completion of the remedial action and limited action and institutional control actions described in the 1998 ROD are consistent with this.
Groundwater	New Hampshire Groundwater Protection Regulations; Ambient Groundwater Quality Standards (AGQS). Env-Wq 402.04	Applicable	Groundwater shall be suitable for drinking water; shall not contain contaminants above the concentrations set in 402.06; shall not cause violation of surface water quality standards when naturally discharged to surface waters.	Source control (i.e., soil removal of OU-1 soils) will limit discharges to groundwater that could result in a violation of surface water quality of adjacent surface waters or rendering groundwater unsuitable for use as drinking water.
Groundwater	New Hampshire Groundwater Protection Regulations. Env-Wq 402.10	Applicable	Table 1 established maximum contaminant levels (Ambient Groundwater Quality Standards), which at the time were the same as EPA MCLs.	Source control (i.e., soil removal of OU-1 soils) will limit discharge of VOCs, PCBs, and inorganics at concentrations above state MCL and MCLG levels.
Surface Water	Clean Water Act (CWA) Ambient Water Quality Criteria (WQC) for Protection of Human Health and Aquatic Life. Env-Ws 1700	Relevant and Appropriate	Establishes water quality standards for protection of human health and aquatic organisms. Standards include dissolved oxygen, pH, bacteria, toxic substances, etc.	Discharges into surface waters from the temporary water treatment system will meet Surface Water Quality Regulations. Erosion/sedimentation controls will be installed and maintained around the exclusion zones to eliminate discharges of soils/sediments to surface waters.
Soil	EPA Guidance on Remedial Actions for Superfund Sites with PCB Contamination (1990)	To Be Considered	Describes the recommended approach to evaluating and remediating Superfund Sites with PCB contamination.	The guidance will be considered when establishing remediation goals for PCB contaminated media.

TABLE 18
ACTION-SPECIFIC ARARs

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

Medium	Potential Federal Requirement	Status	Requirement Synopsis	Project Component	Action to be Taken to Attain ARAR
Air	RCRA (40 CFR 264, Subpart AA)	Applicable	Air emission standards for process vents and closed-vent systems and control devices associated with air or steam stripping operations that manage hazardous wastes with organic concentrations of at least 10 ppmw.	Air emissions from temporary water treatment system.	Should air stripping operations manage hazardous wastes with organic concentrations of at least 10 ppm by weight, vents operated as part of the air stripper system will comply with Sections 1032 through 1036 of this Subpart.
Air	RCRA (40 CFR 264, Subpart BB)	Applicable	Air emission standards for equipment that contains or contacts hazardous wastes with organic concentrations of at least 10 percent by weight.	Air emissions from temporary water treatment system.	Should equipment come into contact with hazardous wastes containing organic concentrations of at least 10 percent by weight, the equipment will be equipped and monitored for leaks as specified in Sections 1052 through 1065 of this Subpart.
Surface Water	Clean Water Act (CWA), Section 402, National Pollutant Discharge Elimination System (NPDES), 33 USC 1342; 40 CFR 122-125, 129, 131 NPDES General Permit for Remediation in NH and MA; 40 CFR 122.3(d)	Applicable	Standards for the discharge of pollutants into surface waters. Remediation General Permit imposes effluent limitations, standards, prohibitions and best management practices for discharges from construction dewatering of contaminated sites.	Excavation/ Dewatering	Discharges associated with dewatering of Mill Street soils will meet requirements through onsite treatment, or treatment at offsite plant, and/or under GP, if applicable. Discharge activities shall meet the substantive requirements of these regulations.

TABLE 18
ACTION-SPECIFIC ARARs

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

Medium	Potential Federal Requirement	Status	Requirement Synopsis	Project Component	Action to be Taken to Attain ARAR
Soil	40 CFR 122.26(C)(1)(ii)(C); 40 CFR 122.44(i); NPDES General Permit for Construction Stormwater Management	Applicable	Discharges of stormwater associated with construction activities must implement best management practices and other measures, to control pollutants in stormwater discharges during and after construction activities.	Earth Disturbance	Erosion and sedimentation controls will be installed and maintained around the perimeter of the exclusion zones during the remedial actions until surface covers are restored, and, for vegetative covers, established. Also, waters from impacted equipment/material staging/handling areas will be contained and routed to a temporary water treatment facility for treatment prior to discharge.
Soil	Toxic Substance Control Act (TSCA) (40 CFR 761), 40 CFR 761.50, 40 CFR 761.61, 40 CFR 761.65(c)(9) Storage and Disposal of Bulk PCB Remediation Waste	Applicable	General requirements (761.50) and specific technical requirements and options (761.61, 761.65) for cleanup, storage and disposal of PCB Remediation waste. Includes specific provisions for storage of PCB remediation waste in piles for up to 180 days (761.65(c)(9)). Section 761.61(a)(5)(i)(B)(2)(ii) of TSCA provides that soil or debris contaminated with PCB concentrations less than 50 mg/kg shall be disposed of in accordance with the disposal options of 761.(a)(5)(v)(A) and Section 761(a)(5)(i)(B)(2)(iii) of TSCA provides that soil and debris with PCB concentrations greater than 50 mg/kg shall be disposed of in a permitted hazardous waste landfill or disposal facility.	Storage/Pre-Transportation Handling of Waste	Excavated materials and/or other residuals subject to these regulations will be disposed of within 180 days at an appropriate/approved off-site disposal facility. Remediation waste soils stored on-site will meet these requirements.

TABLE 18
ACTION-SPECIFIC ARARs

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

Medium	Potential Federal Requirement	Status	Requirement Synopsis	Project Component	Action to be Taken to Attain ARAR
Soil/ Groundwater	TSCA - 761.61(a) and (c) and 40 CFR 761.65(c)(1) Storage and Disposal of Liquid PCB Remediation Waste	Applicable	These regulations address the use, cleanup, storage and disposal of PCBs including PCB remediation waste. PCB remediation waste is waste containing PCBs as a results of a spill or release of PCB containing oil. Provides options for cleanup and disposal of liquid PCB remediation waste, allowing for temporary storage of certain PCB containers containing PCB liquids at concentrations of 50 ppm or greater, normally for no more than 30 days but time period may be extended by Regional Administrator. (761.65(c)(1)).	Storage/Transportation/ Disposal of Waste	Liquid Remediation wastes subject to these regulations will be disposed of within 30 days, or grounds for a waiver will be met consistent with the Record of Decision. Remediation waste liquids will be stored in containers suitable for offsite transport/disposal and managed according to a SPCC Plan. Water treatment system will be operated on concrete/asphalt surface that is bermed/curbed and equipped with a sump pump. Treatment residuals will be routed to an approved off-site treatment/disposal facility. Compliant with TSCA requirements by excavation and off-site treatment/disposal of soil with >50 ppm PCB.

TABLE 18
ACTION-SPECIFIC ARARs

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

Medium	Potential Federal Requirement	Status	Requirement Synopsis	Project Component	Action to be Taken to Attain ARAR
Soil	RCRA - 40 CFR Part 261.11 40 CFR, 261.24	Applicable	Generators must characterize their wastes to determine if the waste is hazardous by listing (40 CFR 261, Subpart D), by Characteristic (40 CFR 261, Subpart C), or excluded from regulation 940 CFR 261.4) Testing procedure (TCLP) to assess materials for potential hazardous characteristics including toxicity.	Generation, management, Storage/ Transportation/ Disposal of Waste	Excavated soils may be classified as characteristic. By products and residues from the treatment of contaminated groundwater must also be characterized. Waste characterization samples will be collected prior to/during implementation of the remedial action to determine whether any material to be excavated is a RCRA hazardous waste. TCLP testing may also be considered.

TABLE 18
ACTION-SPECIFIC ARARs

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

Medium	Potential Federal Requirement	Status	Requirement Synopsis	Project Component	Action to be Taken to Attain ARAR
Soil/ Groundwater	RCRA - 40 CFR 262.30-33, 262.34; 40 CFR 264 Subparts J and L Land Disposal Restrictions 40 CFR Subpart E, 40 CFR 268.50; 40 CFR 264.554	Applicable	Pre-transport requirements for generators of hazardous waste (packaging, labeling, marking, placarding). Allows on-site accumulation of hazardous waste for 90 days or less in containers, tanks, drip pads, or containment buildings, provided generator complies with specified requirements, including referenced requirements of 40 CFR Part 265. 40 CFR 262.34. Also includes requirements for storage for more than 90 days, 40 CFR 262.34(b). Design, operating, closure, and (if necessary) post-closure requirements for storage of hazardous waste in tanks. (Subpart J). Design, operating, closure, and (if necessary) post-closure requirements for storage of hazardous waste in waste piles outside structures. (Subpart L). Prohibits storage of hazardous wastes that are prohibited from land disposal under Part 268, Subpart C, unless on-site storage of such wastes are in containers, tanks, or containment buildings to facilitate recovery, treatment, or disposal and the generator meets the applicable requirements for such storage. 40 CFR 268.50. This prohibition and requirements do not apply to hazardous remediation wastes stored in a staging pile approved pursuant to 40 CFR 264.554.	Storage of Waste	Any hazardous waste generated and stockpiled onsite over 90 days will be stored in accordance with these requirements. Excavated soil identified as a hazardous waste will be managed in accordance with these regulations prior to disposal. Wastes exhibiting a hazardous characteristic would need to be treated to meet the Universal Treatment Standards (UTS) for all hazardous constituents present in the residuals prior to disposal, in accordance with these regulations. PCB materials that are also characteristic for metals would comply with the deferred LDR policy for these wastes. Characteristic hazardous soils can be treated to meet the UTS standard or the alternative treatment standards for RCRA hazardous soils.

TABLE 18
ACTION-SPECIFIC ARARs

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

Medium	Potential Federal Requirement	Status	Requirement Synopsis	Project Component	Action to be Taken to Attain ARAR
Soil/ Groundwater (continued)	RCRA - 40 CFR 262.30-33, 262.34; 40 CFR 264 Subparts J and L Land Disposal Restrictions 40 CFR Subpart E, 40 CFR 268.50; 40 CFR 264.554	Applicable	Restricts land disposal of hazardous wastes that exceed specific criteria. Establishes UTS, which hazardous wastes must be treated to prior to land disposal. Phase IV Rule rev. establishes Alternative Treatment Standards for soils containing hazardous wastes.	Storage of Waste	
Soil	TSCA/RCRA Storage Requirements	Applicable		Storage of Investigation Derived Waste	1998 ROD: Waiver issued by EPA, pursuant to CERCLA 121(d)(4)(A), of time limits for interim storage of investigation-derived waste.
Air/ Groundwater	Requirements for Owners and Operators of Hazardous Waste Facilities/ Hazardous Waste Transfer Facilities. Env-Hw 702.11	Applicable	Requires monitoring pursuant to plan to address potential for migration.	Source Control and Natural Attenuation	Groundwater and air emissions monitoring will be conducted as required during remediation.

TABLE 18
ACTION-SPECIFIC ARARs

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

Medium	Potential Federal Requirement	Status	Requirement Synopsis	Project Component	Action to be Taken to Attain ARAR
Groundwater	Non-degradation of Groundwater to Protect Surface Water. Env-Wq 402.04	Applicable	Groundwater shall be suitable for drinking water; shall not contain contaminants above the concentrations set in 402.06; shall not cause violation of surface water quality standards when naturally discharged to surface waters.	Source Control and Natural Attenuation	Remedial action will limit discharges to groundwater that would result in a violation of surface water quality at adjacent surface waters or render groundwater unsuitable for drinking water.
Groundwater	Groundwater Management Zone (GMZ). Env-Or 607.05	Applicable	Regulations relating to delineation of GMZ boundaries and limited circumstance in which the use of groundwater must be restricted by easement or ownership.	Monitored Natural Attenuation, Institutional Controls	GMZ boundaries will be delineated in accordance with the substantive requirements of this regulation by implementing the WMP, as revised and/or modified during the remedial design and the IC/AR Plan and EMP following the remedial action.
Groundwater	Water Quality Sampling, Analysis, and Monitoring. Env-Wq 402.08	Applicable	Provides general standards for the implementation of a groundwater monitoring program.	Monitored Natural Attenuation	Groundwater sampling, monitoring and analysis under the revised WMP (during remedial action) and the EMP (following the remedial action), will comply with the substantive requirements of this regulation.

TABLE 18
ACTION-SPECIFIC ARARs

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

Medium	Potential Federal Requirement	Status	Requirement Synopsis	Project Component	Action to be Taken to Attain ARAR
Groundwater	Groundwater Monitoring Wells. Env-Wq 402.09	Applicable	Specifies standards for the design, installation and decommissioning of monitoring wells.	Monitored Natural Attenuation	Monitoring wells will be designed, installed and decommissioned consistent with this regulation.
Groundwater	Groundwater discharges and groundwater discharge zone. Env-Wq 402.22 - Prohibited Discharges; Env-Wq 402.07 - Groundwater Discharge Zone; and Env-Wq 402.21 - Groundwater Discharge Permit Compliance Criteria.	Applicable	Discharges to groundwater must receive treatment by BAT; discharges shall not contain a regulated contaminant that exceeds AGQS; a permit is required to discharge to groundwater; information must delineate the groundwater discharge zone under the permit. Groundwater treatment and discharges at the site must meet the substantive requirements of this regulation.	Discharges of Dewatering Liquids to Groundwater (if any)	Temporary water treatment system was designed with BAT. Remedial actions involving discharges to groundwater will comply with the substantive requirements of these regulations. Remedial actions involving discharges to the Souhegan River will comply with the substantive requirements of these regulations.
Air	Env-A 1002	Applicable	Establishes prevention, abatement and control procedures for fugitive dust emissions due to construction and excavation.	Source Control	These procedures shall be followed to maintain dust control during remediation activities
Air	Env-A 1305 Env-A 606	Applicable	Establishes requirements for technology and for air impact analysis with respect to devises emitting regulated substances.	Discharge of Dewatering Liquids to drainage ditch (culvert).	Discharges from any new or modified facility will comply with these requirements.

TABLE 18
ACTION-SPECIFIC ARARs

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

Medium	Potential Federal Requirement	Status	Requirement Synopsis	Project Component	Action to be Taken to Attain ARAR
Surface Water	Standards for Classifications of Surface Waters of the State. NH Water Quality Criteria Standards, RSA 485-A; Env-Wq 1700 – Surface Water Quality Regulations. (1998 ROD incorrectly cited Chapter 149-3, Ws 400, Parts 430-439)	Applicable	Disposal of wastes that will lower the quality of surface waters below classification standards is prohibited; the regulations provide standards for contamination associated with specific classes of waters including dissolved oxygen, bacteria, pH, contaminants, etc.	Discharge of Dewatering Liquids to drainage ditch (culvert).	Dewatered liquids will be routed to a temporary water treatment system. Discharges to surface waters from the temporary water treatment system will meet applicable standards.
Surface Water	Water Quality Standards and NH Antidegradation Policy. Env-Wq 1708	Applicable	No person shall place or discharge pollutants into any waters of the state unless the discharge complies with effluent standards and limitations and will not degrade existing water quality.	Discharge of dewatering liquids to drainage ditch (culvert).	Dewatered liquids will be routed to a temporary water treatment system. Discharges to surface waters from the temporary water treatment system will meet applicable standards.

TABLE 18
ACTION-SPECIFIC ARARs

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

Medium	Potential Federal Requirement	Status	Requirement Synopsis	Project Component	Action to be Taken to Attain ARAR
Soil	New Hampshire Hazardous Waste Management Act and Hazardous Waste Rules. RSA Chapter 147-A – Hazardous Waste Management, and Env-Hw 100-1114 - Division of Hazardous Waste Rules.	Applicable	State Hazardous Waste Management Standards operated in lieu of federal RCRA Subtitle C requirements. Establishes hazardous waste management guidelines including ID of HW (400); requirements for handling, storing, transporting (500-700).	Excavation, storage and transport of hazardous wastes.	The actions to be taken to comply with the substantive requirements of the regulations specified in the ROD are discussed below.
Soil	Siting Requirements and Variances. Env-Wm 353.09 – Siting Requirements for New Facilities.	Applicable	Establishes siting requirements and variances for HW facilities near geologic fault areas and flood plains and sets forth state procedures for identifying the boundaries of the flood plains. Applies to new facilities, which include a location at which hazardous waste is subjected to treatment, storage or disposal.	Dewatering system, possibly excavation and storage.	Waiver of siting requirements (Env-Wm 353.09(b)(2) and 353.09(d)) issued by EPA.
Soil	Requirements for Facilities with a Standard Permit and/or a Transfer Facility Permit. Env-Wm 708.03(d) and 708.03(d)(1).	Applicable	Includes standards for owners and operators of hazardous waste facilities that store containers. Provides requirements for types, management, and inspection of containers.	Storage/Disposal of Waste	The remedial action will comply with the substantive requirements of those regulations relating to the proper and safe usage of tanks and containers.

TABLE 18
ACTION-SPECIFIC ARARs

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

Medium	Potential Federal Requirement	Status	Requirement Synopsis	Project Component	Action to be Taken to Attain ARAR
Soil	Hazardous Waste Regulations – General Requirements. Env-Hw 702.09 – General Design Requirements.	Applicable	All facilities must be designed to control fugitive emissions, prevent unplanned releases, divert surface water run-off.	Dewatering	The temporary water treatment system was designed in accordance with these requirements.
Soil	Requirements for Facilities with a Standard Permit and/or a Transfer Facility Permit. Env-Hw 708.02 – Operation Requirements.	Applicable	Facility must comply with 40 CFR Part 264. §§12-19 (Notices, general waste analysis, security, inspection requirements, personnel training, location standards) and 40 CFR 264 Subparts C, D, F, G and H (preparedness and prevention, contingency plan and emergency procedures, closure and post-closure, financial requirements)	Dewatering and Soil cover	The temporary water treatment system will be operated in accordance with these requirements. The restored soil cover will meet all requirements except where waived for equivalence performance.
Soil	UST Regulations and Guidelines. Env-Wm 1401.18 – Underground Storage Facilities. ROD incorrectly cited Env-Ws 411.18, which expired in 1997.	Applicable	DES must be notified prior to the removal or closure of a UST. The person closing a UST must be certified by International Code Council.	UST Removal/Disposal	Removal of the three remaining USTs will comply with the substantive requirements of these regulations.

TABLE 19
LOCATION-SPECIFIC ARARs

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

Medium	Potential Federal Requirement	Status	Requirement Synopsis	Action to be Taken to Attain ARAR
Sediment	Clean Water Act (CWA) Section 404(b) and Rivers and Harbors Act Section 10 (33 U.S.C. 403).	Applicable	No discharge of dredged or fill material shall be permitted if there is a practicable alternative that has less adverse impact on aquatic ecosystem provided the alternative does not have other significant adverse environmental consequences.	Soil erosion/sedimentation control measures will be installed and maintained during remediation to minimize impacts. There is no practical alternative to conducting work in the wetlands.
Wetlands	Protection of Wetlands (Executive Order No. 11990) 40 CFR 6, Appendix A (Policy on Implementing E.O. 11990) CWA Section 404(b) (40 CFR 230; 33 CFR 323) and Rivers and Harbors Act Section 10 (33 U.S.C. 403)	Applicable	Requires that federal agencies' activities avoid, to the extent possible, adverse impacts on wetlands if there is a practicable alternative, and minimize adverse impacts on wetlands if no practicable alternative exists. See preceding item for CWA provisions.	The alternative will be implemented with control of wetlands excavation to the greatest extent possible. Excavation in wetlands will meet the requirements of this Executive Order and applicable regulatory requirements. Restoration and, if required, mitigation will follow any such excavations. There is no practical alternative to conducting work in the wetlands.
Floodplains	Floodplain Management (Executive Order No. 11988) 40 CFR 6.302(b) and 40 CFR 6, Appendix A (Policy on Implementing E.O. 11988)	Applicable	Requires that federal agencies evaluate the effects of their actions (including actions undertaken by other entities pursuant to Federal permit or license) on floodplain to avoid or minimize adverse effects on floodplain.	The remedial action was designed to restore current grades. As such, the remedial action will be implemented in such a manner as to minimize the impacts to the risk of flood loss to the greatest extent possible. Because the contamination is located in the floodplain there is no practical alternative to conducting work within the floodplain.

TABLE 19
LOCATION-SPECIFIC ARARs

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

Medium	Potential Federal Requirement	Status	Requirement Synopsis	Action to be Taken to Attain ARAR
Surface Water	Rivers and Harbors Act (Section 10 [33 U.S.C. 401]) and CWA (Section 404 [33 U.S.C. 1344]), 33 CFR 323; See PGP for NH	Applicable	Regulates the discharge of dredged or fill material into waters of the United States. No discharge shall be permitted if there is a practicable alternative that has less adverse impact on resource area. See prior synopsis regarding wetlands medium.	Erosion and sedimentation controls will be installed and maintained during the remedial action to mitigate potential discharges of dredged or fill materials.
Surface Water	Fish and Wildlife Coordination Act (16 USC 661-666)	Applicable	Federal agencies or public or private entities under Federal permit or license, proposing to undertake an action that will control or modify a water body must consult U.S. Fish and Wildlife Service regarding measures to prevent loss of or damage to fish and wildlife resources and to provide for the development and improvement of such resources.	Implementation of remedy will be in compliance with this regulation since the EPA will consult with the U.S. Fish and Wildlife Service.
Water Resources	Water Management and Protection - Water Pollution and Waste Disposal. RSA 485-A:17 – Terrain Alteration, and Env-Wq 1500 – Permits for RSA 485-A:17 Activities.	Applicable	Criteria for alteration of terrain near state surface waters that may affect water quality. Includes activities in or on the border of surface water if 50,000 sq. ft. within protected shoreline or 100,000 sq. ft. in all other areas will be disturbed. Must include protective measures to prevent soil erosion and compliance with Env-Wq 1507 (permanent methods for protecting water quality).	Excavations near the Souhegan River will comply with the substantive requirements of these regulations. Work within the Elm Street Area (contiguous area of more than 50,000 square feet adjacent to river) will comply with the substantive requirements of the regulations.

TABLE 19
LOCATION-SPECIFIC ARARs

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

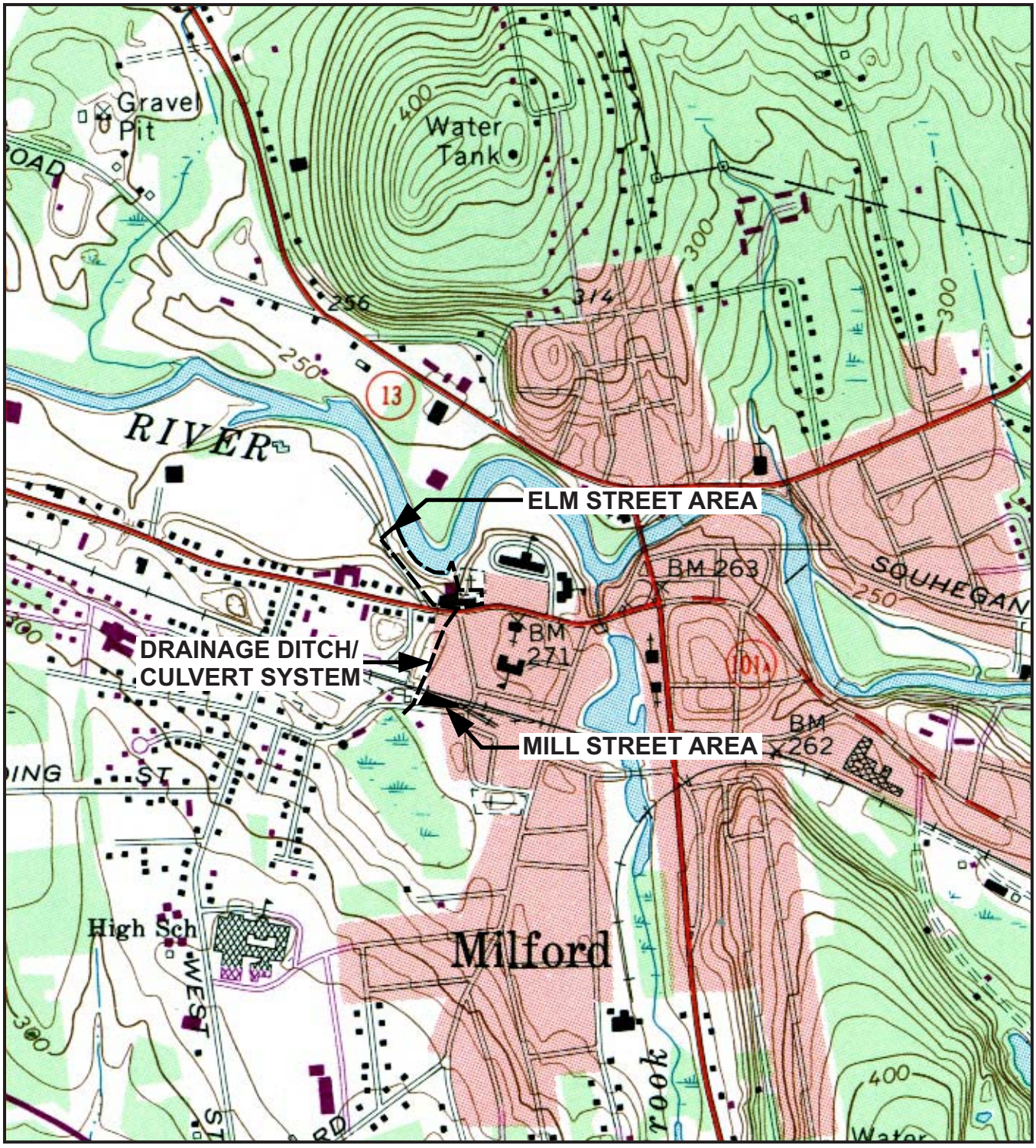
Medium	Potential Federal Requirement	Status	Requirement Synopsis	Action to be Taken to Attain ARAR
Wetlands	New Hampshire Wetlands Act. RSA 482-A – Dredge and Fill in Wetlands; Env-Wt 100-900; ROD incorrectly cited regulations as Env-Ws 300-400, 600, 700.	Applicable	Requires minimal alterations to wetlands to preserve beneficial functions.	Remedial activities in wetlands located in or adjacent to the Site will avoid or minimize impacts to the greatest extent possible. Any excavation in wetlands will meet applicable substantive requirements. Because contamination is located in the wetland adjacent to the site, there is no practical alternative to conducting work in or near wetland.
Water Resources	Section 401 Water Quality Certificate. RSA 485-A – Water Pollution and Waste Disposal: specifically RSA 485-A:8 – Classification of Surface Waters, and RSA 485-A:13 – Water Discharge Permits; and Env-Wq 1700 - Water Quality Regulations.	Applicable	Remedial Action must adequately protect the environment, public health and state's surface waters; must not violate state's surface water quality standards. All discharges to surface waters must be in compliance with these requirements.	Any discharge to the State's surface waters will be in compliance with the substantive components of these regulations.
Wetlands/ Water Resources	RSA 483-B – Shoreland Water Quality Protection Act.	Applicable	Protected shoreland is defined as all land located within 250 feet of ordinary high water mark. The act prohibits alteration of river bank and activity within protected shoreland without approval under RSA 482-A (Wetlands Act) and RSA 485-A:17 (Alteration of Terrain; prohibits fertilizer other than limestone within 50 feet of high water mark; requires natural woodland buffer within 150 feet of high water mark).	The remedial action, which includes alteration of the riverbank along the Elm Street Area, is subject to EPA approval (after consultation with the State). Work shall be conducted in accordance with the substantive requirements of these regulations. Fertilizer will not be utilized within 50 feet of the high water mark.

TABLE 19
LOCATION-SPECIFIC ARARs

FINAL (100%) DESIGN REPORT
FLETCHER'S PAINT WORKS AND STORAGE FACILITY SUPERFUND SITE
GENERAL ELECTRIC COMPANY - MILFORD, NEW HAMPSHIRE

Medium	Potential Federal Requirement	Status	Requirement Synopsis	Action to be Taken to Attain ARAR
Habitat	Endangered Species. Fis 1000 - Conservation of Endangered Species.	Applicable	Identifies, by list, the endangered species throughout the state. If any species are identified on-site, then need to comply with RSA 212-A. Taking, possessing and transporting of endangered species is prohibited.	The NH Fish and Game Department will be consulted prior to implementation of the remedial action. If endangered/threatened species/habitat exists, applicable requirements will be met.

Figures



REFERENCE: Base Map Source USGS 7.5 Minute Quads. Series Milford, New Hampshire, Photorevised 1985.

1000' 0 1000'

Approximate Scale: 1" = 1000'

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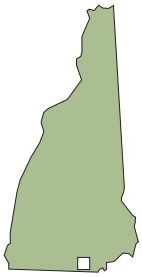


AREA LOCATION

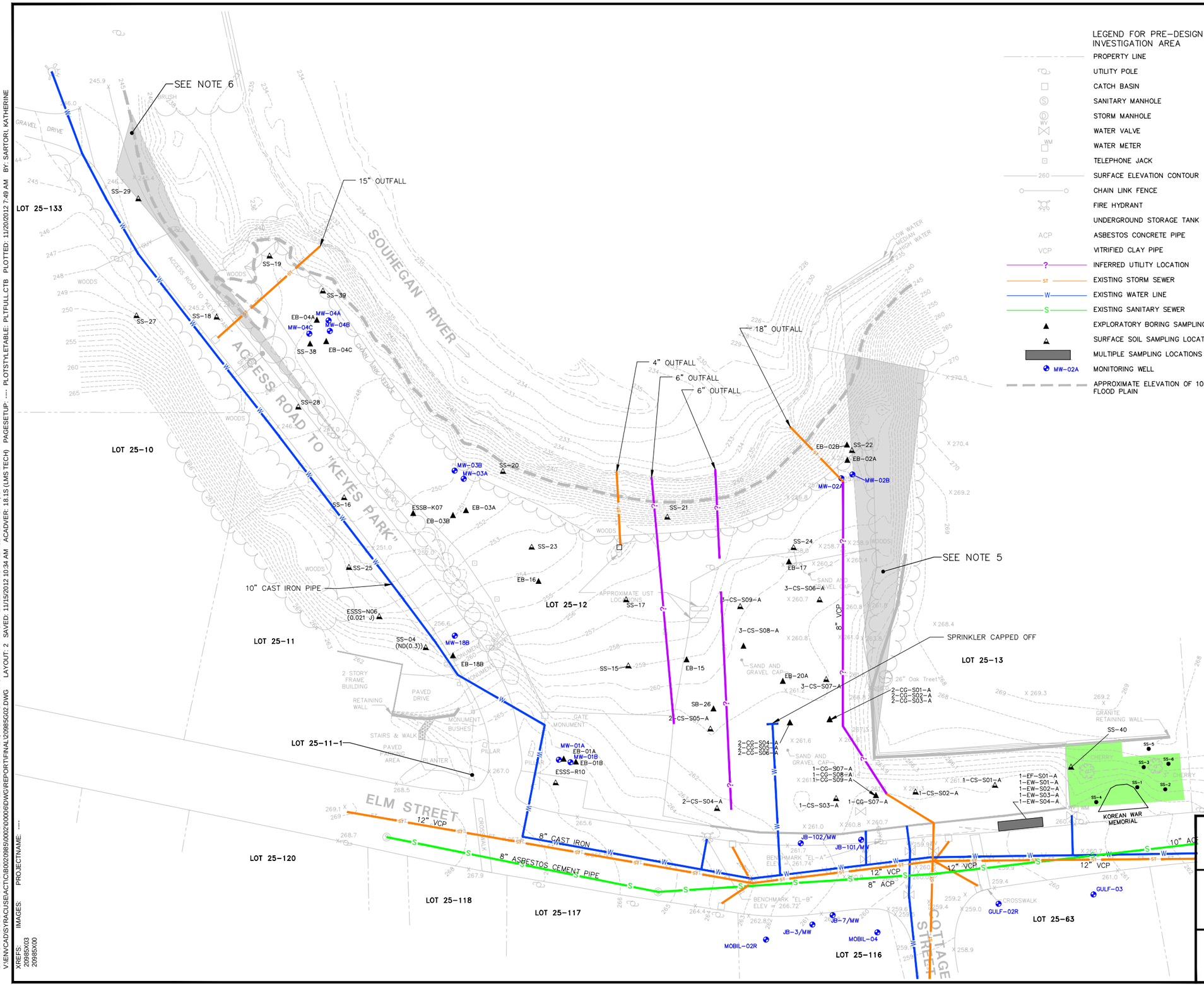
GENERAL ELECTRIC COMPANY
FLETCHER'S PAINT WORKS AND STORAGE FACILITY
SUPERFUND SITE - MILFORD, NEW HAMPSHIRE
FINAL (100%) DESIGN REPORT

SITE LOCATION MAP

ARCADIS

FIGURE
1

11/14/2012 SYRACUSE-141ENV-DJHOWES, K.SARTORI
C:B0020985/0002/00006/REPORT/CDR/20985N02.CDR



LEGEND FOR PRE-DESIGN INVESTIGATION AREA

- PROPERTY LINE
- UTILITY POLE
- CATCH BASIN
- SANITARY MANHOLE
- STORM MANHOLE
- WATER VALVE
- WATER METER
- TELEPHONE JACK
- SURFACE ELEVATION CONTOUR
- CHAIN LINK FENCE
- FIRE HYDRANT
- UNDERGROUND STORAGE TANK
- ASBESTOS CONCRETE PIPE
- VITRIFIED CLAY PIPE
- INFERRED UTILITY LOCATION
- EXISTING STORM SEWER
- EXISTING WATER LINE
- EXISTING SANITARY SEWER
- EXPLORATORY BORING SAMPLING LOCATION
- SURFACE SOIL SAMPLING LOCATION
- MULTIPLE SAMPLING LOCATIONS
- MONITORING WELL
- APPROXIMATE ELEVATION OF 100-YEAR FLOOD PLAIN

LEGEND FOR HISTORIC SOIL REMEDIATION AREA

- ESE GRAB SAMPLE LOCATION
- 1-FOOT REMOVAL

NOTES:

1. ELEVATIONS BASED ON NORTH AMERICAN VERTICAL DATUM OF 1988.
2. HORIZONTAL DATUM BASED ON NEW HAMPSHIRE STATE PLANE COORDINATE SYSTEM OF 1983.
3. CONTOUR INTERVAL = 1 FEET.
4. MAP COMPILED FROM ACTUAL FIELD SURVEY PERFORMED BY BBL, INC. FROM JULY 16, 2003 THROUGH AUGUST 14, 2003, BY MERIDAN LAND SERVICES, INC. JANUARY 22, 2004, AND BY ARCADIS ON MAY 24, 2007.
5. TITLE TO SHADED AREA IS UNCERTAIN AT THIS TIME. NO BOUNDARY LINE AGREEMENT (REFERRED TO IN THE CHAIN OF TITLE) HAS BEEN FOUND.
6. SHADED AREA AT THE NORTHWEST CORNER OF THE LOT DEPICTS AREA WHICH IS PART OF THE ROAD TO THE KEYES FIELD PARCEL. NO CONVEYANCE TO THE TOWN FOR THIS AREA HAS BEED FOUND.
7. LOCATION OF UNDERGROUND UTILITIES AND OTHER UNDERGROUND STRUCTURES OBTAINED FROM TOWN OF MILFORD DEPARTMENT OF PUBLIC WORKS RECORDS AND OTHER SOURCES AND MAY BE APPROXIMATE ONLY.
8. THE EXACT TERMINUS OF THE CAPPED OFF SPRINKLER IS UNKNOWN. DISTANCE ONTO THE SITE IS SHOWN AS SUSPECTED BY GEOPHYSICAL INVESTIGATION.
9. LOCATION AND PRESENCE OF BUILDING DRAINAGE FEATURES BASED ON USEPA 1994 RI.
10. LOCATION OF UNDERGROUND UTILITIES AND OTHER UNDERGROUND STRUCTURES OBTAINED BY FIELD MEASUREMENTS WHERE POSSIBLE. LOCATION OF WATER, SEWER, AND DRAINAGE UTILITIES OBTAINED FROM TOWN OF MILFORD DEPARTMENT OF PUBLIC WORKS RECORDS.
11. ELM STREET SITE PROPERTY LINE SHOWN WAS ESTABLISHED FROM DEEDS OF RECORD, SURVEY, AND EXISTING MONUMENTATION. OTHER PROPERTY LINES SHOWN WERE OBTAINED FROM TOWN OF MILFORD TAX MAP 25.

DRAFT
FOR EPA REVIEW

GENERAL ELECTRIC COMPANY
FLETCHER'S PAINT WORKS AND STORAGE FACILITY
SUPERFUND SITE - MILFORD, NEW HAMPSHIRE
FINAL (100%) DESIGN REPORT

ELM STREET AREA - EXISTING UTILITIES AND HISTORIC SAMPLING LOCATIONS

ARCADIS

FIGURE
2

CITY: SYRACUSE DIV/GROUP: ENVCAD DB: A. SCHILLING L: FORAKER, K.SARTORI PIC: P. FARR PM: C. AVERILL TM: C. AVERILL LYR: ON=*; OFF=*REF*
V:\ENVCAD\SYRACUSE\ACT\CIB\0020985\00020\00006\DWG\REPORT\FINAL\20985G02.DWG LAYOUT: 2 SAVED: 11/15/2012 10:34 AM ACADVER: 18.1S (LMS TECH) PAGESETUP: ---- PLOTSTYLETABLE: PLTFULL.CTB PLOTTED: 11/20/2012 7:49 AM BY: SARTORI, KATHERINE
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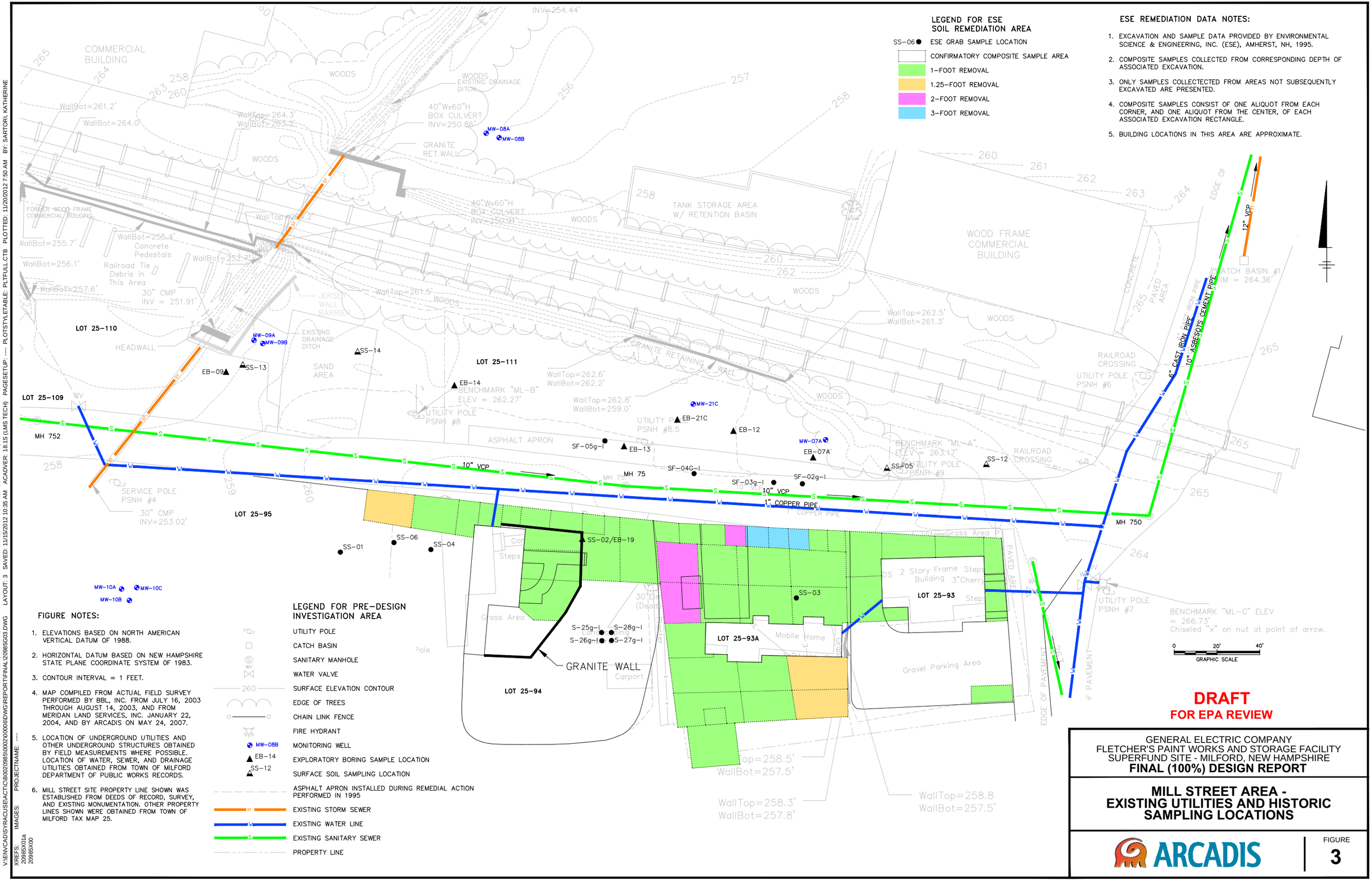

LEGEND FOR ESE SOIL REMEDIATION AREA

- SS-06● ESE GRAB SAMPLE LOCATION
- CONFIRMATORY COMPOSITE SAMPLE AREA
- 1-FOOT REMOVAL
- 1.25-FOOT REMOVAL
- 2-FOOT REMOVAL
- 3-FOOT REMOVAL

ESE REMEDIATION DATA NOTES:

1. EXCAVATION AND SAMPLE DATA PROVIDED BY ENVIRONMENTAL SCIENCE & ENGINEERING, INC. (ESE), AMHERST, NH, 1995.
2. COMPOSITE SAMPLES COLLECTED FROM CORRESPONDING DEPTH OF ASSOCIATED EXCAVATION.
3. ONLY SAMPLES COLLECTECTED FROM AREAS NOT SUBSEQUENTLY EXCAVATED ARE PRESENTED.
4. COMPOSITE SAMPLES CONSIST OF ONE ALIQUOT FROM EACH CORNER, AND ONE ALIQUOT FROM THE CENTER, OF EACH ASSOCIATED EXCAVATION RECTANGLE.
5. BUILDING LOCATIONS IN THIS AREA ARE APPROXIMATE.

FIGURE NOTES:

1. ELEVATIONS BASED ON NORTH AMERICAN VERTICAL DATUM OF 1988.
2. HORIZONTAL DATUM BASED ON NEW HAMPSHIRE STATE PLANE COORDINATE SYSTEM OF 1983.
3. CONTOUR INTERVAL = 1 FEET.
4. MAP COMPILED FROM ACTUAL FIELD SURVEY PERFORMED BY BBL, INC. FROM JULY 16, 2003 THROUGH AUGUST 14, 2003, AND FROM MERIDAN LAND SERVICES, INC. JANUARY 22, 2004, AND BY ARCADIS ON MAY 24, 2007.
5. LOCATION OF UNDERGROUND UTILITIES AND OTHER UNDERGROUND STRUCTURES OBTAINED BY FIELD MEASUREMENTS WHERE POSSIBLE. LOCATION OF WATER, SEWER, AND DRAINAGE UTILITIES OBTAINED FROM TOWN OF MILFORD DEPARTMENT OF PUBLIC WORKS RECORDS.
6. MILL STREET SITE PROPERTY LINE SHOWN WAS ESTABLISHED FROM DEEDS OF RECORD, SURVEY, AND EXISTING MONUMENTATION. OTHER PROPERTY LINES SHOWN WERE OBTAINED FROM TOWN OF MILFORD TAX MAP 25.

LEGEND FOR PRE-DESIGN INVESTIGATION AREA

- UTILITY POLE
- CATCH BASIN
- SANITARY MANHOLE
- WATER VALVE
- 260 SURFACE ELEVATION CONTOUR
- EDGE OF TREES
- CHAIN LINK FENCE
- FIRE HYDRANT
- MW-08B MONITORING WELL
- EB-14 EXPLORATORY BORING SAMPLE LOCATION
- SS-12 SURFACE SOIL SAMPLING LOCATION
- ASPHALT APRON INSTALLED DURING REMEDIAL ACTION PERFORMED IN 1995
- ST EXISTING STORM SEWER
- W EXISTING WATER LINE
- S EXISTING SANITARY SEWER
- PROPERTY LINE

DRAFT
FOR EPA REVIEW

GENERAL ELECTRIC COMPANY
FLETCHER'S PAINT WORKS AND STORAGE FACILITY
SUPERFUND SITE - MILFORD, NEW HAMPSHIRE
FINAL (100%) DESIGN REPORT

MILL STREET AREA - EXISTING UTILITIES AND HISTORIC SAMPLING LOCATIONS

ARCADIS

FIGURE
3

CITY: SYRACUSE DIV/GROUP: ENVCAD DB: A. SCHILLING L: FORAKER, K.SARTORI PIC: P. FARR PM: C. AVERILL TM: C. AVERILL LYR: ON=*; OFF=*REF*
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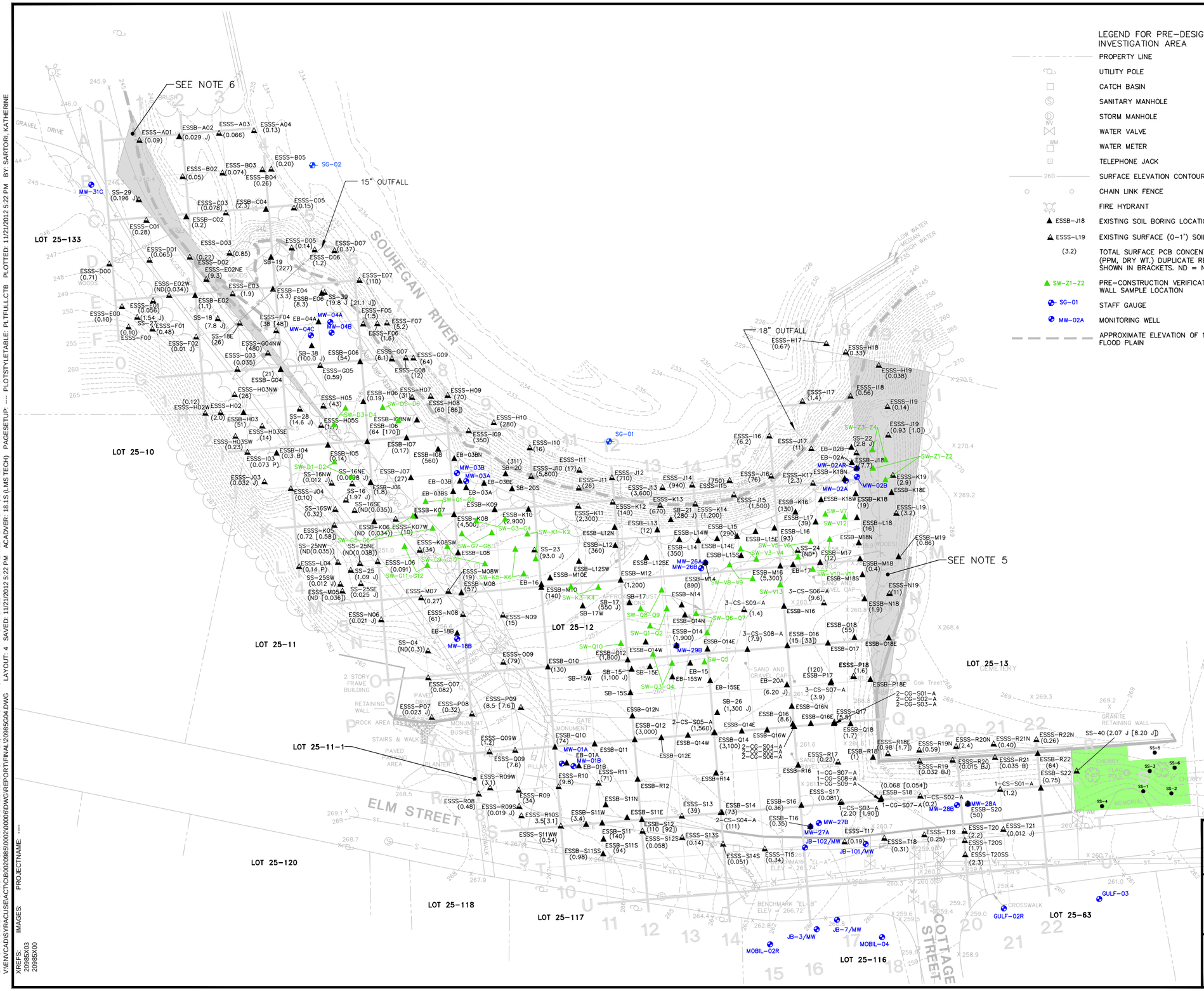

LEGEND FOR PRE-DESIGN INVESTIGATION AREA

- PROPERTY LINE
- UTILITY POLE
- CATCH BASIN
- SANITARY MANHOLE
- STORM MANHOLE
- WV — WATER VALVE
- WM — WATER METER
- TELEPHONE JACK
- 260 — SURFACE ELEVATION CONTOUR
- CHAIN LINK FENCE
- FIRE HYDRANT
- ESSB-J18 — EXISTING SOIL BORING LOCATION
- ESSS-L19 — EXISTING SURFACE (0-1') SOIL LOCATION
- (3.2) — TOTAL SURFACE PCB CONCENTRATION (PPM, DRY WT.) DUPLICATE RESULTS SHOWN IN BRACKETS. ND = NON-DETECT.
- SW-Z1-Z2 — PRE-CONSTRUCTION VERIFICATION SIDE WALL SAMPLE LOCATION
- SG-01 — STAFF GAUGE
- MW-02A — MONITORING WELL
- APPROXIMATE ELEVATION OF 100-YEAR FLOOD PLAIN

LEGEND FOR HISTORIC SOIL REMEDIATION AREA

- SS-1 — ESE GRAB SAMPLE LOCATION
- 1-FOOT REMOVAL

NOTES:

1. ELEVATIONS BASED ON NORTH AMERICAN VERTICAL DATUM OF 1988.
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6. SHADED AREA AT THE NORTHWEST CORNER OF THE LOT DEPICTS AREA WHICH IS PART OF THE ROAD TO THE KEYES FIELD PARCEL. NO CONVEYANCE TO THE TOWN FOR THIS AREA HAS BEED FOUND.
7. A SAND AND GRAVEL CAP WAS PREVIOUSLY INSTALLED OVER THE MAJORITY OF THE ELM STREET AREA BY USEPA. DURING THE PDI, THE CAP WAS OBSERVED TO BE APPROXIMATELY ONE FOOT THICK AT MOST LOCATIONS ACROSS THE PROPERTY. AT OTHER LOCATIONS, APPROXIMATE CAP THICKNESSES WERE MEASURED AS FOLLOWS: 1.5 FEET AT EB-15SE, G06, M12, N18, O16, Q10, Q12E, Q16N, Q18, AND S14; TWO FEET AT O14, O18, AND Q12; FOUR FEET AT M16; FIVE FEET AT S18; AND UP TO SIX FEET ALONG THE CEMETERY WALL AS MEASURED AT P18E. THE SAND AND GRAVEL CAP WILL BE REMOVED DURING THE SITE PREPARATION PHASE.
8. ELM STREET SITE PROPERTY LINE SHOWN WAS ESTABLISHED FROM DEEDS OF RECORD, SURVEY, AND EXISTING MONUMENTATION. OTHER PROPERTY LINES SHOWN WERE OBTAINED FROM TOWN OF MILFORD TAX MAP 25.

0 30' 60'
GRAPHIC SCALE

DRAFT
FOR EPA REVIEW

GENERAL ELECTRIC COMPANY
FLETCHER'S PAINT WORKS AND STORAGE FACILITY
SUPERFUND SITE - MILFORD, NEW HAMPSHIRE
FINAL (100%) DESIGN REPORT

ELM STREET AREA - SOIL SAMPLING LOCATIONS AND SURFACE SOIL PCB SAMPLE DATA

ARCADIS

FIGURE
4

CITY: SYRACUSE DIV/GROUP: ENVCAD DB: A. SCHILLING L: FORAKER, K.SARTORI PIC: P. FARR PM: C. AVERILL TM: C. AVERILL LYR: ON=*; OFF=*REF*
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XREFS: 20985X03 20985X00 IMAGES: PROJECTNAME: ----

CITY: SYRACUSE DIV/GROUP: ENVCAD DB: A. SCHILLING L. FORAKER, K.SARTORI PIC: P. FARR PM: C. AVERILL TM: C. AVERILL LYR: ON=*; OFF=*REF* PAGESETUP: ---- PLOTSTYLETABLE: PLTFULL.CTB PLOTTED: 11/21/2012 11:32 AM BY: POSENAUER, LISA
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XREFS: 20985X00 IMAGES: PROJECTNAME: ----

SUMMARY OF PRE-DESIGN INVESTIGATION PCB SOIL SAMPLING DATA (ppm, DRY WT.) (SAMPLE INCREMENTS IN FEET BELOW CAP)

SampleID	ESSB-A02	ESSB-C02	ESSB-C04	ESSB-E02	ESSB-E04	ESSB-E06	ESSB-G04	ESSB-G06	ESSB-H03	ESSB-H06	ESSB-I04	ESSB-I05	ESSB-I06	ESSB-I07	ESSB-I08	ESSB-I08NW	ESSB-J06	ESSB-J07	ESSB-J18	ESSB-K06	ESSB-K07	ESSB-K08	ESSB-K09	ESSB-K10	ESSB-K16	ESSB-K18	ESSB-K18E	ESSB-K18N	ESSB-K18W	ESSB-L08	ESSB-L12	SampleID
1-2	--	--	--	--	--	--	--	--	46	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	6	--	--	--	--	--	1-2
1-3	0.18	ND (0.034)	4.4 [3.2]	0.011 J	0.36 [0.44]	12	ND (0.034)	58	--	220	1.6	ND (0.035)	1,300	91	58	--	1.2	46	8.6	0.042 B	2,100	1,000	4,300	50	62	--	75 [120]	45 [73]	22 [38]	110	140	1-3
2-4	--	--	--	--	--	--	--	--	0.30 (2-3')	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	6.1	--	--	--	--	--	2-4
3-5	0.022 J [0.018 J]	ND (0.044)	2.8	0.084	6	36	0.055	52	--	6.8 [5.4]	0.068 B	ND (0.035)	17	16	0.89	--	2	0.36	1.6	0.026 BJ [0.031 BJ]	2.8	68 [48]	68	7.4	2.4	--	29	0.11 B	280	0.94	40	3-5
4-6	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	490	--	--	--	--	--	4-6
5-7	ND (0.046)	--	3.1	0.1	2.1	6.1	ND (0.034) [ND (0.034)]	34	--	85	0.017 BJ	ND (0.035)	21	6.6	3.4 [3.1]	--	0.033 J	0.13	0.67	0.013 BJ	--	2.3	--	0.064	4.3	--	1.6	0.098 B	0.22	--	44	5-7
6-8	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	110	--	--	--	--	--	6-8
7-9	--	--	--	0.021 J	26	11	0.024 J	17	--	8.8	0.38 B	0.016 J [0.025 J]	310	88	0.12	11	0.014 J	--	1.1	0.0094 BJ	--	1.4	--	4.6	1.7	--	1.5	0.14 J	50	--	0.42	7-9
8-10	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	28	--	--	--	--	--	8-10
9-11	--	--	--	ND (0.042)	0.29	47	ND (0.041)	0.58	--	2.7	0.044 B	ND (0.038)	0.18	5.9	120	17	ND (0.041)	0.43	--	ND (0.035)	--	0.76	--	0.037	190	--	0.23	2.6	300	--	52	9-11
10-12	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	150	--	--	--	--	--	10-12
11-13	--	--	--	ND (0.042)	--	0.046	ND (0.043)	0.054	--	--	0.035 BJ	--	1.4	0.063	15	9.9	--	0.028 J	73	0.1 B	--	0.24	--	2.1	2.7	--	0.1	1.3	720	--	58	11-13
12-14	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	70	--	--	--	--	--	12-14
13-15	--	--	--	--	--	--	ND (0.04)	--	--	--	0.037 BJ	--	0.15	--	0.071	--	--	0.045	0.24	ND (0.041)	--	0.044	--	0.051	0.14	--	ND (0.033)	0.18 B	0.098	--	40	13-15
14-16	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	94	--	--	--	--	--	14-16
15-17	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	46 [30 B]	0.016 BJ	--	ND (0.19)	--	0.25	0.64	--	2.7	7.7	0.020 J	--	0.23	15-17
16-18	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	16-18
17-19	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	0.33	--	--	0.14	--	0.036 J	0.048	--	ND (0.033)	7.7	ND (0.038)	--	0.23	17-19
18-20	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	18-20
19-21	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	0.074	--	--	--	--	--	24	--	ND (0.035)	56	0.21	--	--	19-21
20-22	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	20-22
21-23	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	0.069	--	--	--	--	--	140	--	0.018 J	2.2	--	--	--	21-23
23-25	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	0.030 J (24')	--	--	--	--	23-25

SampleID	ESSB-L12N	ESSB-L12SE	ESSB-L12SW	ESSB-L13	ESSB-L14	ESSB-L14E	ESSB-L14W	ESSB-L15	ESSB-L15E	ESSB-L15S	ESSB-L16	ESSB-L17	ESSB-L18	ESSB-M08	ESSB-M10	ESSB-M10E	ESSB-M12	ESSB-M14	ESSB-M16	ESSB-M17	ESSB-M18	ESSB-M18N	ESSB-M18S	ESSB-M19	ESSB-N14	ESSB-N16	ESSB-N18	ESSB-O10	ESSB-O12	ESSB-O14	ESSB-O14E	SampleID
1-2	--	--	--	--	--	--	--	1,100	520	40	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	1-2
1-3	240	0.26 B	10,000	--	7,200	420	3,200 [3,300]	--	--	--	--	--	3.5	7.2	2.9	740 B [450 B]	78 [110]	84 J	31	5.5	96	2.1 [2.5]	2.8	2	6,900	0.076	0.16	23	92	17,000 [12,000]	21,000	1-3
2-4	--	--	--	--	--	--	--	10 (2-3')	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	2-4
3-5	140	0.81	19,000	150 [120] (4-5')	23	200	2.3	--	470	--	--	--	1.8	0.079	2.5	46 B	0.5	9.4	11	11,000	580	240	16	5.2	7,800	0.18	120	7.8	14	16,000	8,500	3-5
4-6	--	--	--	230 (5-6')	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	4-6
5-7	--	--	4,100	--	0.44	51 B	--	--	32	--	--	--	4.8	0.08	--	6.6 B	0.31	80	86	180	0.4	140	0.24	0.084	810	900	18	14 [34]	0.052 B	40,000	15,000 [17,000]	5-7
6-8	--	--	--	220 (6-7')	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	6-8
7-9	--	--	8,800	--	10	200	--	--	--	--	5.6 [4.0]	890	0.52	0.035 J	--	16 B	0.45	21	42	--	0.12	--	--	--	360	1,700	8.3 (7-8')	46	11	240	34	7-9
8-10	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	2.7	--	--	--	--	8-10
9-11	--	--	2,800	--	6.7	3,900 B	--	--	--	--	0.32 B	19	10	ND (0.035)	--	--	0.45	0.74 [19]	0.25	--	0.024 J	--	--	--	1.5	0.15	--	0.022 J	2.2 [0.23 B]	490	4.4	9-11
10-12	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	10-12
11-13	--	--	240	--	--	--	--	--	--	--	0.16	8.1	3.6	ND (0.035)	--	--	0.034 J	0.39	0.47	--	2.8	--	--	--	4	--	--	0.15	0.2 B	19	2.4	11-13
12-14	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	12-14
13-15	--	--	--	--	--	--	--	--	--	--	--	--	2.1	ND (0.037)	--	--	ND (0.036)	2.8	0.12	--	1.7	--	--	--	0.91	--	--	0.044	ND (0.034)	--	2.3	13-15
14-16	--	--	--	--	--	--	--	--	--	--	--	--	--	ND (0.04) (15-16')	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	14-16
15-17	--	--	--	--	--	--	--	--	--	--	--	--	1.2	--	--	--	1.8	--	1.4	--	0.014 J	--	--	--	1.4	--	--	0.03 J	0.33 B	150	0.51	15-17
16-18	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	0.24	--	--	--	--	--	--	--	--	--	--	--	--	--	16-18
17-19	--	--	--	--	--	--	--	--	--	--	--	--	0.26	--	--	--	ND (0.28)	--	0.75	--	0.0096 J	--	--	--	6	--	--	0.024 J	0.09 B	19	0.23	17-19
18-20	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	0.25	--	--	--	--	--	--	--	--	--	--	--	--	--	18-20
19-21	--	--	--	--	--	--	--	--	7,100	--	3.6	1.1	0.76	--	--	--	0.38	--	--	--	ND (0.047)	--	--	--	0.13 B	--	--	0.051	1.2 B	1.2	0.1	19-21
20-22	--	--	--	--	--	--	--	--	--	--	--	--	--	0.024 J	--	--	--	0.051	--	--	--	--	--	--	--	--	--	--	--	--	--	20-22
21-23	--	--	--	--	--	--	--	--	11,000	--	1,200	0.31 B	--	--	--	--	2.7	--	--	--	ND (0.041)	--	--	--	0.061 B	--	--	ND (0.039)	--	1.2	0.28	21-23

SampleID	ESSB-O14N	ESSB-O14W	ESSB-O16	ESSB-O17	ESSB-O18	ESSB-O18E	ESSB-P17	ESSB-P18E	ESSB-Q10	ESSB-Q11	ESSB-Q12	ESSB-Q12E	ESSB-Q12N	ESSB-Q14	ESSB-Q14E	ESSB-Q14W	ESSB-Q16	ESSB-Q16E	ESSB-Q16N	ESSB-Q16W	ESSB-Q18	ESSB-R12	ESSB-R14	ESSB-R16	ESSB-R18	ESSB-R22	ESSB-S11	ESSB-S11E	ESSB-S11N	ESSB-S11S	SampleID
1-2	--	--	--	--	1,800	--	9.1	--	--	--	240	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	0.08	1,000	170	1,000	1-2
1-3	24,000	640	4,600	18	--	1.6	--	0.08	1.5	0.25	--	200	300	9,100	15,000	35	24	--	--	15	0.073 B	4,200	1,400	--	0.12	6.9	--	87 (2-3')	0.60 (2-3')	330 (2-3')	1-3
2-4	--	--	--	--	2,700	--	--	--	--	--	130	--	--	--	--	--	--	75	--	--	--	--	--	1.2	--	--	--	--	--	--	2-4
3-5	14,000	0.2	540	37	--	0.021 J [1.5]	--	ND (0.034)	0.22 B	0.011 J (3-4')	--	0.27 (3-4')	2.4 (3-4')	0.16	7,700	4.2	22 [31]	--	120 [140]	--	0.024 BJ [ND (0.036)]	340 (3-4')	2.6	--	--	--	--	--	--	0.091 [0.31]	3-5
4-6	--	--	--	--	2,100	--	--	--	--	0.047	0.076	0.058	5.2 [5.3]	--	--	--	--	1	0.6	0.097	--	0.92	--	0.023 BJ	--	--	--	--	--	--	4-6
5-7	25	0.052	1.3	150	--	ND (0.033)	--	ND (0.035)	0.19 B	--	--	--	--	0.1 [0.079]	--	--	56	--	--	--	ND (0.035)	--	--	--	--	--	--	--	--	--	5-7
6-8	--	--	--	--	450	--	--	--	--	--	2.6	--	--	--	--	--	--	1.2	4.4	0.91	--	--	--	0.21 B	--	--	--	--	--	--	6-8
7-9	220	0.032 J	190	2.4	--	0.11 (7-8')	--	ND (0.034) (7-8')	0.011 BJ	--	--	--	--	--	--	--	--	--	--	--	0.030 BJ	--	--	--	--	--	--	--	--	--	7-9
8-10	--	--	--	--	2.5	0.12	--	ND (0.039)	--	--	0.19	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	8-10
9-11	2.7	0.022 J	0.87	2.7	--	--	--	--	ND (0.035)	--	--	--	--	--	--	--	--	--	--	--	0.014 BJ	--	--	--	--	--	--	--	--	--	9-11
10-12	--	--	--	--	0.93 B	--	--	--	--	--	0.094	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	10-12
11-13	1.1 (11-11.4')	0.17	0.045	--	--	--	--	--	0.037 BJ	--	--	--	--	44	--	--	--	--	--	--	0.042 B	--	--	--	--	--	--	--	--	--	11-13
12-14	--	--	--	--	0.048 B	--	--	--	--	--	0.012 J	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	12-14
13-15	--	0.65 J	0.020 J	--	--	--	--	--	0.012 BJ	--	--	--	--	5.2	--	--	--	--	--	--	0.012 BJ	--	--	--	--	--	--	--	--	--	13-15
14-16	--	--	--	--	0.086 B	--	--	--	--	--	0.34	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	14-16
15-17	5.3 (15-15.5')	ND (0.43)	0.036 J	--	--	--	--	--	0.72 B	--	--	--	--	--	--	--	--	--	--	--	0.053 B	--	--	--	--	--	--	--	--	--	15-17
16-18	--	--	--	--	ND (0.036)	--	--	--	--	--	0.072	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	16-18
17-19	--	0.25	0.049	--	--	--	--	--	2.5	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	17-19
18-20	--	--	--	--	0.056 B	--	--	--	--	--	0.2	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	18-20
19-21	--	0.040 J	0.4	--	--	--	--	--	0.98	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	19-21
20-22	--	--	--	--	0.01 BJ [ND (0.039)]	--	--	--	--	--	0.020 J	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	20-22
21-23	--	0.020 J	ND (0.046)	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	21-23

SampleID	ESSB-S11SS	ESSB-S11W	ESSB-S12	ESSB-S14	ESSB-S16	ESSB-S18	ESSB-S20	ESSB-S22	ESSB-T16	EB-03B	EB-03E	EB-03BN	EB-03BS	EB-15	EB-15SE	EB-15SW	EB-20A	SB-15	SB-15E	SB-15S	SB-15W	SB-17	SB-17W	SB-19	SB-20	SB-20S	SB-21	SB-26	SB-38	3-CS-S08-A	SampleID
1-2	0.65	3.3	--	--	--	--	--	--	--	200	--	--	--	--	--	--	--	1,300	--	--	--	--	--	4.4	200	--	400	--	7.9 [0.043]	--	1-2
1-3	0.12 (2-3')	ND (0.033) (2-3')	1.3	0.032 J	0.030 J	ND (0.033)	0.088	0.0093 J	0.053	390 [410]	670	34	9	--	540 (1-2.5')	1,500	250	400; 3,000 (2-3')	160	510	660	680	2.4	--	25 (2'-3')	--	3.3 (2-3')	950	--	460	1-3
2-4	--	--	--	--	--	--	--	--	--	--	--	--	--	0.19 [0.20] (2.5-4.5')	880 (2.5-4.5')	--	--	--	--	--	--	--	--	--	--	170 (3-4')	--	--	--	--	2-4
3-5	--	--	0.23	0.0090 J	0.15	ND (0.034)	0.076	0.0095 J	1.4	370	180	6.8	21	--	--	980	17	0.26	7.7	0.56	3.8	2.9	--	--	--	100 (4-5')	--	470	--	1.6	3-5
4-6	--	--	--	--	--	--	--	--	--	--	--	--	--	0.29 (4.5-6.5')	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	4-6
5-7	--	--	0.091	43	0.044	ND (0.035)	0.050 B	ND (0.035)	0.028 J	2,000	140	1.9	890	--	--	1,200	210	0.017 J	5.5	0.049	20	--	--	--	--	71 (5-6')	--	--	--	0.06	5-7
6-8	--	--	--	--	--	--	--	--	--	--	--	--	--	0.15 (6.5-8.5')	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	6-8
7-9	--	--	0.051	0.046	0.21	ND (0.036)	0.042 [0.031 J]	0.097	0.056	--	--	--	--	--	--	69	100	--	--	--	--	--	--	--	--	--	--	--	--	0.57	7-9
8-10	--	--	--	--	--	--	--	--	--	--	--	--	--	0.72 (8.5-10.5')	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	8-10
9-11	--	--	0.05	10	0.37	0.0094 J	0.068	ND (0.035)	0.68	0.055	--	0.094 B	--	--	--	0.69	0.053	--	--	--	--	--	--	--	--	--	--	--	--	ND (0.035)	9-11
10-12	--	--	--	--	--	--	--	--	--	--	--	--	--	0.067 (10.5-12')	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	10-12
11-13	--	--	0.11	ND (0.042)	2.9	0.072 (11-12')	0.11	0.045	6.4	--	--	300	--	--	--	0.11	--	--	--	--	--	--	--	--	--	--	--	--	--	--	11-13
12-14	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	12-14
13-15	--	--	0.089	0.14	2.7	--	0.057	0.13	0.44	0.096 B	--	1	--	--	--	0.19	--	--	--	--	--	--	--	--	--	--	--	--	--	--	13-15
14-16	--	--	--	--	--	--	--	--	--	--	--	--	--	0.28 (14-14.5')	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	14-16
15-17	--	--	0.084	0.022 J	0.29	--	--	0.038 J	0.2	--	--	0.54	--	0.037 J (14.5-16.5')	--	0.011 J	--	--	--	--	--	--	--	--	--	--	--	--	--	--	15-17
16-18	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	16-18
17-19	--	--	0.05	0.051	--	--	--	--	0.034 J	--	--	--	--	0.056 (16.5-18.5')	--	0.053	--	--	--	--	--	--	--	--	--	--	--	--	--	--	17-19
18-20	--	--	--	--	--	--	--	--	--	--	--	--	--	0.027 J (18.5-20.5')	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	18-20
19-21	--	--	--	0.056 (19-20')	--	--	--	--	--	--	--	--	--	--	--	0.036 J	--	--	--	--	--	--	--	--	--	--	--	--	--	--	19-21
20-22	--	--	--	--	--	--	--	--	--	--	--	--	--	0.036 J (20.5-22.5')	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	20-22
21-23	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	0.091	--	--	--	--	--	--	--	--	--	--	--	--	--	--	21-23

SUMMARY OF PRE-CONSTRUCTION VERIFICATION SLIDE WALL SAMPLING DATA (PPM, DRY WT.) (SAMPLE INCREMENTS IN FEET)

SAMPLE ID	SW-D1-D2	SW-D3-D4	SW-D5-D6	SW-G1-G2	SW-G3-G4	SW-G5-G6	SW-G7-G8	SW-G9-G10	SW-G11-G12	SW-K1-K2	SW-K3-K4	SW-K5-K6	SW-Q1-Q2	SW-Q3-Q4	SW-Q5	SW-Q6-Q7	SW-Q8-Q9	SW-Q10	SW-V3-V4	SW-V5-V6	SW-V7	SW-V8-V9	SW-V10-V11	SW-V12	SW-V13	SW-Z1-Z2	SW-Z3-Z4
3-5	--	--	--	--	--	--	--	--	0.19 J	--	--	1.1 J [2.4 J]	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
4-6	ND (0.23)	47 J	10 J	--	--	--	--	670 J	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
5-7	--	--	--	--	--	1.4	75 JN [350 J]	--	ND (0.20)	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
6-8	--	--	--	--	--	--	--	9.5	--	--	--	--	--	--	--	--	--	ND (0.20)	--	--	--	--	--	--	--	0.20 J	0.17 J
7-9	--	--	--	720 J	3,400 J	98 J	31,000 J	--	0.097 J	38 J	100 J	0.65 J	--	24	--	--	--	--	--	--	--	--	--	--	--	--	--
8-10	0.53 J	21 J	50 J [42 J]	--	--	--	--	1,100 J	--	--	--	--	--	--	--	--	8.7 J	--	--	--	--	--	--	--	--	--	--
9-11	--	--	--	--	--	20 J	ND (0.27)	--	0.16 J	--	--	ND (0.27)	--	--	--	--	--	ND (0.24)	--	--	--	--	--	--	--	--	0.067 J
10-12	--	--	--	--	--	--	--	0.32 J	--	--	--	--	9,100 J	--	--	24	0.72 J	--	--	--	--	--	--	--	--	--	--
11-13	--	--	--	--	--	1.0 (11-12')	ND (0.27) (11-12')	--	--	4,200 J	11 JN (19 J)	0.26 J	--	--	5.5 J	--	--	3.0	--	--	--	--	--	--	--	250	ND (0.23)
12-14	--	--	--	150 J	720 J	7.3 J	7.0	--	--	--	--	--	--	190 J	--	--	33 J	--	--	--	--	--	--	--	--	--	--
13-15	--	--	--	--	--	--	--	--	--	--	--	ND (0.25)	--	--	--	--	--	4.3 J	--	--	--	0.33	37 J	--	--	--	ND (0.23)
14-16	--	--	--	--	--	ND (0.27)	ND (0.27)	--	--	--	--	--	--	--	22 J	--	--	--	--	720	--	--	--	--	ND (0.25)	--	--
15-17	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	15	300 J	--	--	--
16-18	--	--	--	--	--	--	--	--	--	--	--	--	5.0	--	--	38	32 J	ND (0.23)	--	--	--	--	--	--	6.7	--	--
17-19	--	--	--	--	--	--	--	--	--	--	--	--	--	56	--	--	--	--	--	--	1,000	13.0	0.12 J	0.67 J	--	--	--
18-20	--	--	--	--	--	--	--	--	--	--	--	--	--	--	0.85 J	--	--	--	710 J	--	--	--	--	--	ND (0.29)	--	--
19-21	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	910 J	--	3.5 J	0.058 J [0.065 J] (19-20')	570	--	--	--
20-22	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	17 J	--	0.086 J (20-21')	--	--
21-23	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	10 JN	--	110 J	0.74 J	--	260 J	ND (0.28)	--	--
22-24	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	340	--	--	1.2 (22-23')	--	ND (0.29)(23-24')	--	--
23-25	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	ND (0.35) (23-24')	0.74 J	3.1 J	--	--	--
24-26	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	ND (0.45)	--	--
25-27	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	5.0 J	--	--	--	--
26-28	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	ND (0.33)	--	--

SUMMARY OF HISTORIC EPA DATA (ppm, DRY WT.) (SAMPLE INCREMENTS IN FEET)

1-CG-S07-A	0.023 J (0-2')		
1-CG-S08-A	ND (0.042) (2-4')		
1-CG-S09-A	ND (0.042) (4-6')		
2-CG-S01-A	3.4 (0-2')		
2-CG-S02-A	ND (0.040) (2-4')		
2-CG-S03-A	ND (0.044) (4-6')		
2-CG-S04-A	4.90 (0-2')		
2-CG-S05-A	27.90 (2-4')		
2-CG-S06-A	218 (4-6')		
EB-01A	ND (40-41.5')		
EB-01B	ND (20-21.5')		
EB-02A	12 (1-3')	1.2 J (24-28')	
EB-02B	0.46 (25-28')		
EB-03A	0.041 (45-46.5')		
EB-03B	20.0 J (7-9')	150 J (11-13')	5.70 J; 3.70 J (15-21')
EB-04A	0.29 (17-19')		
EB-05A	0.027 J (12-14')	ND (0.086) (42-44')	
EB-06C	ND (0.084) (20-22')	ND (0.073) (53-55')	
EB-11A	0.023 J (30-31.5')	ND (0.074) (73-77')	
EB-15	5,000 J (1-2.5')	8.8 J (24-26')	
EB-16	0.069 J (20-21.5')	0.019 J (38-39.5')	
EB-17	11.0 J (10-12')	90.0 J (27-29')	
EB-18B	ND (0.077) (17-18')	ND (0.080) (22-25')	ND (0.077) (55-56.5')
EB-20A	6.20 J; 0.130 (0-4')	2.60 J (12-14')	13.0 J (26-30')
SS-04	0.052 (7-9')		

DRAFT
FOR EPA REVIEW

NOTES:

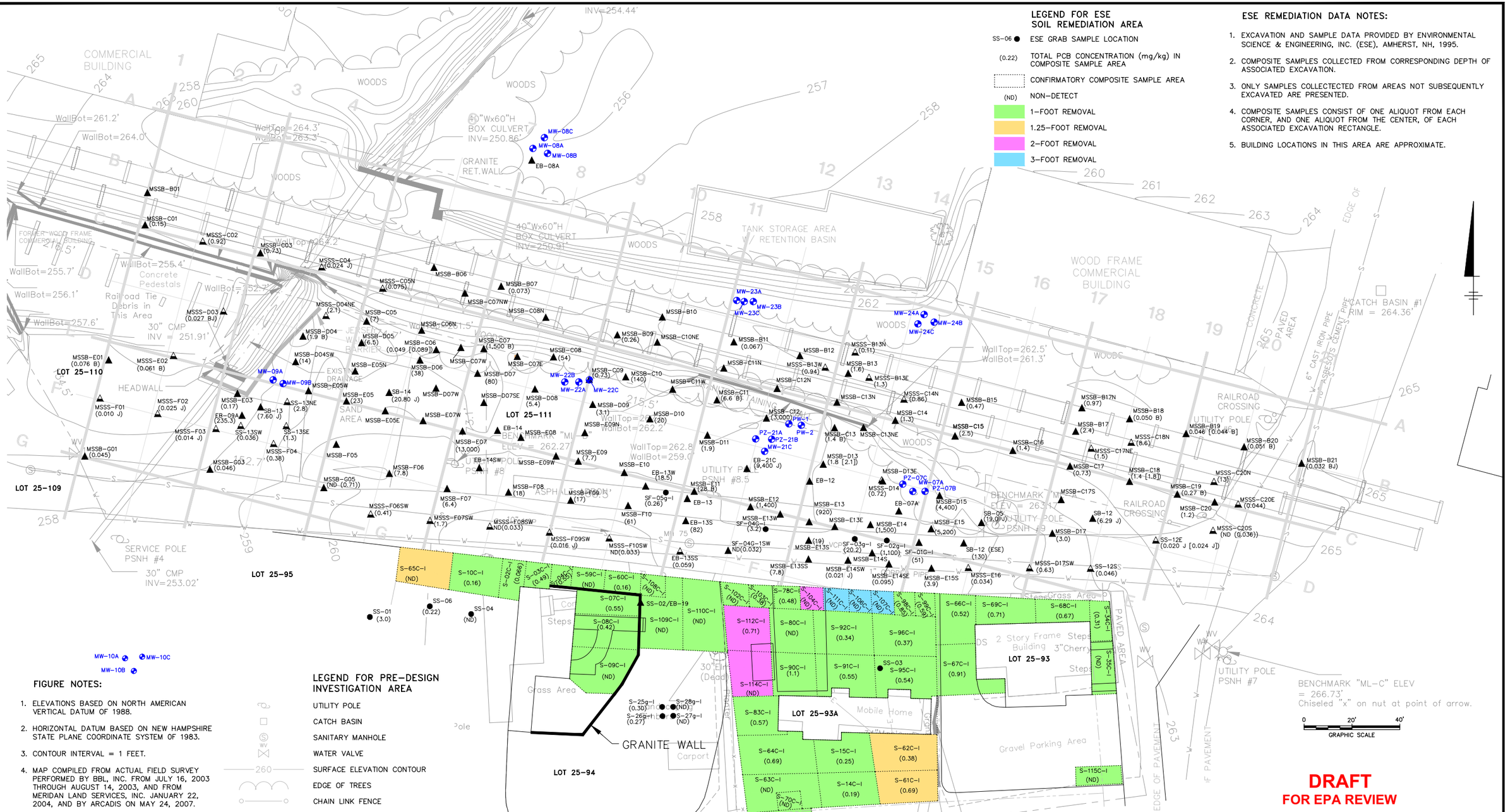
1. ND (0.038) = NOT DETECTED. DETECTION LIMIT IN PARENTHESES, (IF AVAILABLE).
2. [0.067] = DUPLICATE ANALYSIS RESULT SHOWN IN BRACKETS.
3. B = INDICATES THE ANALYTE WAS ALSO DETECTED IN THE ASSOCIATED METHOD BLANK.
4. J = INDICATES THE DETECTED CONCENTRATION IS CONSIDERED AN ESTIMATED VALUE.
5. EPA DATA INCREMENTS ARE HISTORIC, SHOWN AS FEET BELOW PREVIOUSLY EXISTING GRADE.
6. YELLOW SHADING INDICATES SAMPLES CONTAINING PCBs IN EXCESS OF SOIL CLEANUP LEVEL SPECIFIED IN ROD.

GENERAL ELECTRIC COMPANY
FLETCHER'S PAINT WORKS AND STORAGE FACILITY
SUPERFUND SITE - MILFORD, NEW HAMPSHIRE
FINAL (100%) DESIGN REPORT

ELM STREET AREA - SUBSURFACE SOIL PCB SAMPLE DATA

ARCADIS

FIGURE
5



LEGEND FOR ESE SOIL REMEDIATION AREA

- SS-06 ● ESE GRAB SAMPLE LOCATION
- (0.22) TOTAL PCB CONCENTRATION (mg/kg) IN COMPOSITE SAMPLE AREA
- CONFIRMATORY COMPOSITE SAMPLE AREA
- (ND) NON-DETECT
- 1-FOOT REMOVAL
- 1.25-FOOT REMOVAL
- 2-FOOT REMOVAL
- 3-FOOT REMOVAL

ESE REMEDIATION DATA NOTES:

1. EXCAVATION AND SAMPLE DATA PROVIDED BY ENVIRONMENTAL SCIENCE & ENGINEERING, INC. (ESE), AMHERST, NH, 1995.
2. COMPOSITE SAMPLES COLLECTED FROM CORRESPONDING DEPTH OF ASSOCIATED EXCAVATION.
3. ONLY SAMPLES COLLECTECTED FROM AREAS NOT SUBSEQUENTLY EXCAVATED ARE PRESENTED.
4. COMPOSITE SAMPLES CONSIST OF ONE ALIQUOT FROM EACH CORNER, AND ONE ALIQUOT FROM THE CENTER, OF EACH ASSOCIATED EXCAVATION RECTANGLE.
5. BUILDING LOCATIONS IN THIS AREA ARE APPROXIMATE.

FIGURE NOTES:

1. ELEVATIONS BASED ON NORTH AMERICAN VERTICAL DATUM OF 1988.
2. HORIZONTAL DATUM BASED ON NEW HAMPSHIRE STATE PLANE COORDINATE SYSTEM OF 1983.
3. CONTOUR INTERVAL = 1 FEET.
4. MAP COMPILED FROM ACTUAL FIELD SURVEY PERFORMED BY BBL, INC. FROM JULY 16, 2003 THROUGH AUGUST 14, 2003, AND FROM MERIDAN LAND SERVICES, INC. JANUARY 22, 2004, AND BY ARCADIS ON MAY 24, 2007.
5. LOCATION OF UNDERGROUND UTILITIES AND OTHER UNDERGROUND STRUCTURES OBTAINED BY FIELD MEASUREMENTS WHERE POSSIBLE. LOCATIONS OF WATER, SEWER, AND DRAINAGE UTILITIES OBTAINED FROM TOWN OF MILFORD DEPARTMENT OF PUBLIC WORKS RECORDS.
6. THE SAND CAP, INSTALLED FOLLOWING DEMOLITION OF THE FORMER DRAPER COAL TRANSFER BUILDING IN FEBRUARY 2002, WAS OBSERVED TO BE APPROXIMATELY 1.2 FEET THICK AT E05E AND E05W AND APPROXIMATELY 2 FEET THICK AT E05.
7. MILL STREET SITE PROPERTY LINE SHOWN WAS ESTABLISHED FROM DEEDS OF RECORD, SURVEY, AND EXISTING MONUMENTATION. OTHER PROPERTY LINES SHOWN WERE OBTAINED FROM TOWN OF MILFORD TAX MAP 25.

LEGEND FOR PRE-DESIGN INVESTIGATION AREA

- UTILITY POLE
- CATCH BASIN
- SANITARY MANHOLE
- WATER VALVE
- 260 SURFACE ELEVATION CONTOUR
- EDGE OF TREES
- CHAIN LINK FENCE
- FIRE HYDRANT
- ▲ MSSB-D05 EXISTING SOIL BORING LOCATION
- ▲ MSSS-C14N EXISTING SURFACE (0-1') SOIL LOCATION
- (0.86) TOTAL SURFACE PCB CONCENTRATION (PPM, DRY WT.) DUPLICATE RESULTS SHOWN IN BRACKETS. ND = NON-DETECT.
- MW-22B MONITORING WELL/PUMPING WELL/TEMPORARY PIEZOMETER
- ASPHALT APRON INSTALLED DURING REMEDIAL ACTION PERFORMED IN 1995
- PROPERTY LINE

DRAFT
FOR EPA REVIEW

GENERAL ELECTRIC COMPANY
FLETCHER'S PAINT WORKS AND STORAGE FACILITY
SUPERFUND SITE - MILFORD, NEW HAMPSHIRE
FINAL (100%) DESIGN REPORT

MILL STREET AREA - SOIL SAMPLING LOCATIONS AND SURFACE SOIL PCB SAMPLE DATA

ARCADIS

FIGURE
6

CITY: SYRACUSE DIV/GROUP: ENVCAD DB: A. SCHILLING L: FORAKER, K.SARTORI PIC: P. FARR PM: C. AVERILL TM: C. AVERILL LYR: ON=*; OFF=*REF*
V:\ENVCAD\SYRACUSE\ACT\CB0020985\0002\00006\DWG\REPORT\FINAL\20985C06.DWG LAYOUT: 6 SAVED: 11/15/2012 11:22 AM ACADVER: 18.1S (LMS TECH) PAGESETUP: ---- PLOTSTYLETABLE: PLTFULL.CTB PLOTTED: 11/20/2012 8:01 AM BY: SARTORI, KATHERINE
XREFS: 20985X01a 20985X00 IMAGES: PROJECTNAME: ----

SUMMARY OF PRE-DESIGN INVESTIGATION (ppm, DRY WT.) (SAMPLE INCREMENTS IN FEET)

Sample ID	MSMW-22Cluster	MSMW-23Cluster	MSMW-24Cluster	MSSB-B01	MSSB-B06	MSSB-B07	MSSB-B09	MSSB-B10	MSSB-B11	MSSB-B12	MSSB-B13	MSSB-B15	MSSB-B17	MSSB-B17N	MSSB-B18	MSSB-B19	MSSB-B20	MSSB-B21	MSSB-C01	MSSB-C03	MSSB-C05	MSSB-C06	MSSB-C06N	Sample ID
1–2	--	--	--	--	--	--	--	--	--	--	--	--	--	0.026 J [0.022 J]	0.042 B	0.011 BJ	ND (0.038)	0.043 B	--	--	--	--	--	1–2
1–3	--	0.017 J	0.12	--	--	0.1	ND (0.034)	0.14	0.46	--	0.034 J	0.089	2.0	--	--	--	--	--	0.089	0.099	0.022 J	1,500	9.6	1–3
3–5	0.071 B (3–4')	ND (0.034) [ND (0.034)]	0.14 B	--	--	0.18	ND (0.033)	ND (0.036)	ND (0.033)	--	0.053 [0.055]	0.18	2.7	--	--	--	--	--	0.078	0.021 J	0.012 J	0.76	0.038	3–5
4–6	0.48 B	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	4–6
5–7	--	0.013 J	0.057 B	--	--	0.046	0.084	0.050	0.013 J	--	ND (0.034)	0.056	0.088	--	--	--	--	--	0.031 J	ND (0.034) [ND (0.034)]	0.027 J	0.10 [0.14]	--	5–7
6–8	1.8	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	6–8
7–9	--	ND (0.041)	0.041 B	--	--	ND (0.039)	ND (0.040)	--	ND (0.034)	ND (0.034)	0.13	0.26	0.34	--	--	--	--	--	0.05	0.068	0.015 J	0.12	--	7–9
8–10	0.057 B	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	8–10
9–11	0.013 J (10–11')	0.062	ND (0.038)	ND (0.038)	--	ND (0.034)	ND (0.034)	--	0.045	0.021 BJ	2.2	0.032 J	0.098	--	--	--	--	--	0.068	0.012 J	0.28	ND (0.040)	--	9–11
11–13	--	ND (0.035)	ND (0.041)	0.16	--	ND (0.035)	ND (0.036) [ND (0.035)]	--	ND (0.037)	ND (0.036)	0.13	0.086	0.27	--	--	--	--	--	4.4	0.023 J	0.021 J	0.42	--	11–13
13–15	0.068 B	0.022 J	0.027 BJ	0.046	--	ND (0.037)	ND (0.035) (13–14')	--	ND (0.036)	0.97	0.9	0.077	0.062	--	--	--	--	--	0.038	0.016 J	0.018 J	0.024 J	--	13–15
15–17	0.11 B	0.11	0.055 B	--	0.056 B [0.036 BJ]	ND (0.036)	--	--	0.064	5.4	0.36	0.058	0.078	--	--	--	--	--	0.13	0.016 J	0.031 J	0.095	--	15–17
17–19	0.07 B	0.051	0.56 B	--	0.032 BJ	0.041	--	--	0.30 [0.32]	0.14 B	0.054	0.035 J	0.038	--	--	--	--	--	0.03 J	0.016 J	0.042	0.073	--	17–19
19–21	--	0.046	0.056 B	--	0.16 B	0.014 J	--	--	0.4	0.14 B	0.6	0.11	0.044 (19–19.6')	--	--	--	--	--	0.031 J	0.026 J	0.062	0.19	--	19–21
21–23	--	0.071	0.088 B	0.045	0.017 BJ	0.031 J	--	--	0.14	0.54	0.13 (21–21.6')	0.32 (21–21.3')	--	--	--	--	--	--	0.019 J	0.018 J	0.027 J	0.16 (21–22.5')	--	21–23
23–25	--	--	--	0.013 J	0.012 BJ (23–23.5')	0.076	--	--	0.093	--	--	--	--	--	--	--	--	--	9.5	0.028 J	0.021 J (23–23.4')	--	--	23–25
25–27	--	--	--	0.012 J	--	0.016 J	--	--	0.14	--	--	--	--	--	--	--	--	--	0.18	0.015 J	--	--	--	25–27
27–29	--	--	--	--	--	0.045 (27–28')	--	--	0.15 (27–28')	--	--	--	--	--	--	--	--	--	0.49	0.014 J (27 – 27.4')	--	--	--	27–29
29–31	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	0.018 J [0.067]	--	--	--	--	29–31
31–33	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	0.029 J	--	--	--	--	31–33
33–35	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	0.067	--	--	--	--	33–35
35–36.5	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	0.056	--	--	--	--	35–36.5
Sample ID	MSSB-C07	MSSB-C07E	MSSB-C07W	MSSB-C07NW	MSSB-C08	MSSB-C08N	MSSB-C09	MSSB-C10	MSSB-C10NE	MSSB-C11	MSSB-C11N	MSSB-C11W	MSSB-C12	MSSB-C12N	MSSB-C13	MSSB-C13N	MSSB-C13NE	MSSB-C14	MSSB-C15	MSSB-C16	MSSB-C17	MSSB-C17S	MSSB-C18	Sample ID
1–2	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	ND (0.035)	--	--	ND (0.037)	1–2
1–3	12,000 B	0.28	56	--	2.0	--	29 [30]	1.2	0.38	110 B	--	2,100	6,700 B	--	100 B	--	--	0.86	0.86	--	0.018 J	0.047 [0.059 B]	--	1–3
3–5	13	0.086	84	0.020 J	45	0.011 J	--	8.2	880	1,100 B [790 B]	ND (0.034)	36	12,000 B	0.022 J	58 B	0.11	12,000	0.028 J	0.43	--	1.7	0.0099 J	--	3–5
4–6	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	4–6
5–7	320	0.17	0.098 J [0.13 J]	0.47	2.4	0.011 J	--	5.9	0.031 J	2.1 B	ND (0.033)	1.4	4,700	0.020 J	2,300 B	ND (0.035) [ND (0.038)]	120 [37]	ND (0.034)	0.24	--	0.084 [0.11 B]	ND (0.037)	--	5–7
6–8	--	--	--	--	--	--	--	4.9 (7–8')	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	6–8
7–9	420 B	0.034 J [290 J]	3.0	ND (0.040)	0.064	0.011 J	--	--	0.034 J	0.42 B	0.018 J	1.5	2,900	0.13	47 B	ND (0.036)	140	ND (0.041)	2.6	--	1.6	ND (0.035)	--	7–9
8–10	--	0.044 J [0.057 J] (7–9') RE	--	--	--	--	--	0.086	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	8–10
9–11	3,600 B	0.054	1.1	ND (0.034)	0.12	ND (0.035)	--	--	ND (0.036)	0.1 B	0.12	2.1	2,600 [1,900]	690	1.3 B [0.92 B]	ND (0.042)	32	0.051	0.52	--	0.047	ND (0.035)	--	9–11
11–13	8,800 B	0.019 J	0.71	ND (0.034)	0.034 J	0.035 J	0.087	--	0.011 J	3.7 B	0.38	ND (0.037)	5,700	3,600	17 B	ND (0.038)	10	ND (0.036)	1.3	--	0.25	ND (0.035)	--	11–13
13–15	25,000 B	ND (0.046)	ND (0.041)	0.017 J	0.12	0.011 J [0.011 J]	--	--	0.22	0.45 B	0.027 J	ND (0.037)	33	43	2.3 B	1.2	10	1.6 B	0.57	--	0.044	ND (0.038)	--	13–15
15–17	9,400 B	ND (0.040)	0.68	ND (0.035)	0.22	0.1	--	--	--	0.42 B	0.57	--	110	57	160 B	1.3	8.1 (15–16')	0.39	1.1	--	1.5	ND (0.036)	--	15–17
17–19	13	ND (0.034)	0.56	28	0.074	0.2	--	--	--	0.31 B	0.67 [0.37]	--	1,400	18	12 B (17–18.7')	1.2	--	0.29	0.4	--	0.06	0.019 BJ (17–18.5')	--	17–19
19–21	290	0.04	0.36	39	0.086 (19–20')	0.17	0.041	--	--	0.26 B	0.48	--	1,300 (19–19.8')	120	--	0.058 (19–19.9')	--	0.24 (19–20')	0.68 (19–20.4')	--	0.26 J (19–20.2')	--	--	19–21
21–23	13 (21–21.4')	0.033 J (21–22.7')	--	30	--	0.15	--	--	--	--	0.38	--	--	0.41	--	--	--	--	--	--	--	--	--	21–23
23–25	--	--	--	0.016 J	--	--	--	--	--	--	0.35 (23–23.8')	--	--	--	--	--	--	--	--	--	--	--	--	23–25
25–27	--	--	--	0.053	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	25–27
27–29	--	--	--	ND (0.038) (27–27.5')	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	27–29
Sample ID	MSSB-C19	MSSB-C20	MSSB-D04	MSSB-D04SW	MSSB-D05	MSSB-D06	MSSB-D07	MSSB-D07W	MSSB-D07SE	MSSB-D08	MSSB-D09	MSSB-D10	MSSB-D11	MSSB-D13	MSSB-D13E	MSSB-D15	MSSB-D17	MSSB-E01	MSSB-E03	MSSB-E05	MSSB-E05E	MSSB-E05N	MSSB-E05W	Sample ID
1–2	--	0.023 J	ND (0.037)	37	0.28	--	--	--	--	--	--	5.4	--	--	--	--	--	--	--	--	--	--	--	1–2
1–3	0.041 B	--	--	0.054 (2–3')	--	3.3	5.0 B	800	8.6	380	0.24	0.036 (2–3')	1.4	10,000 B	26,000	3,700	0.032 J [0.033 J]	0.018 BJ	0.021 J	6.4	0.23	12 [11]	6.4	1–3
3–5	0.27 B	--	--	ND (0.036)	--	ND (0.035)	0.66	20	1.4	720	0.016 J	--	330 [880]	20,000 B [20,000]	10,000	0.3	0.042	0.024 BJ	0.024 J	7.1	ND (0.035)	ND (0.034)	11	3–5
4–6	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	4–6
5–7	0.042 B	--	--	0.014 J	--	--	5.0	3.6	560	26	0.022 J	--	0.52	7,800 B	56	10 [8.8]	0.029 J	0.031 BJ	ND (0.036)	0.18	ND (0.037)	ND (0.038)	5.7	5–7
6–8	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	6–8
7–9	0.25 B [0.29 B]	--	--	0.018 J	--	--	5.8	4.2	6.0	0.90 (7–8')	0.047 (7–8')	--	0.10 BJ	1,900 B	4,000	2.8	0.17	0.061 B	0.039	0.04	--	0.29	28	7–9
8–10	--	--	--	--	--	--	--	--	--	0.087	ND (0.039)	--	--	--	--	--	--	--	--	--	--	--	--	8–10
9–11	0.093 B	--	--	--	--	--	2.1	1.3	3.1	--	--	--	0.029 BJ	3,400 B	1,500	1.4	0.056	0.055 B	ND (0.036) [0.019 BJ]	0.020 J [0.029 J]	--	--	ND (0.037)	9–11
11–13	0.15 B	--	--	--	--	--	1.5	0.058	0.22	--	--	--	ND (0.038)	56 B	200	1.3 (11–12')	0.023 J	0.048 B	0.022 J	0.046	--	--	--	11–13
13–15	0.14	--	--	--	--	--	0.48	0.69	0.80	--	--	--	0.15 B	1,100 B	5.8	--	0.17 (13–14.5')	0.043 B	0.034 J	--	--	--	--	13–15
15–17	0.1	--	--	--	--	--	0.92	0.28	0.034 J	--	--	--	1.1	34 B	1.6 (15–16')	--	--	0.054 B	0.039	--	--	--	--	15–17
17–19	0.018 J	--	--	--	--	--	0.79	0.074	1.2	--	--	--	0.84	5.0 B	--	--	--	0.054 B	0.022 BJ	--	--	--	--	17–19
19–21	0.032 J (19–20.2')	--	--	--	--	--	1.1	0.12	0.73	--	--	--	0.074 B (19–20')	650 B	--	--	--	0.026 BJ	0.027 BJ	--	--	--	--	19–21
21–23	--	--	--	--	--	--	--	0.19 (21–21.5')	0.52 (21–21.5')	--	--	--	--	4,300 B (21–22')	--	--	--	0.026 BJ	0.053 B (21–21.4')	--	--	--	--	21–23
23–25	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	0.025 BJ (23–24.1')	--	--	--	--	--	23–25
Sample ID	MSSB-E07	MSSB-E07W	MSSB-E08	MSSB-E09	MSSB-E09N	MSSB-E09W	MSSB-E10	MSSB-E11	MSSB-E12	MSSB-E13	MSSB-E13E	MSSB-E13W	MSSB-E13S	MSSB-E13SS	MSSB-E14	MSSB-E14S	MSSB-E14SE	MSSB-E14SW	MSSB-E15	MSSB-E15S	MSSB-F05	MSSB-F06	MSSB-F07	Sample ID
1–2	--	--	--	--	--	--	--	--	--	--	--	--	0.044	0.024 J	15,000	--	ND (0.033)	ND (0.034)	--	--	--	1.8 [0.68]	--	1–2
1–3	8.4	1.4	17,000 B	33	3.5	210 [150]	46	280 B [290]	61	12,000	17,000	2.6	0.045 (2–3')	0.011 J (2–3')	14,000 (2–3')	16	0.015 J (2–3')	ND (0.034) (2–3')	64	0.4	0.011 J	0.035 J (2–3')	0.062	1–3
3–5	1.7	0.19	2.8	0.082	1.0	0.4	0.11	3.6 B	270(3–4')	15	1,600	1.8	0.036 J	--	98	0.024 J	--	--	0.71	--	0.019 J	--	0.014 J	3–5
4–6	--	--	1.2 (5–6')	--	--	--	--	--	0.16 J	--	--	--	--	--	--	--	--	--	--	--	--	--	--	4–6
5–7	0.21	0.011 J	--	0.020 J	--	--	--	0.023 BJ	--	0.22	0.11 [0.057]	0.27	ND (0.038)	--	2.1	ND (0.077)	--	--	0.15	--	0.020 J	--	ND (0.033)	5–7
6–8	--	--	1.4	--	--	--	--	--	0.12	--	--	--	--	--	--	--	--	--	--	--	--	--	--	6–8
7–9	0.29	--	--	0.11	--	--	--	0.039 B	--	36	3.2	0.41	ND (0.039)	--	--	--	--	--	0.36	--	0.097	--	0.066	7–9
8–10	--	--	--	--	--	--	--	--	0.86	--	--	--	--	--	--	--	--	--	--	--	--	--	--	8–10
9–11	0.096	--	--	0.012 J	--	--	--	ND (0.040)	0.13 J (10–12')	5.6	0.011 J	0.043	ND (0.037)	--	--	--	--	--	0.032 J	--	--	--	0.081	9–11
11–13	ND (0.04)	--	--	ND (0.040)	--	--	--	0.79 B	0.021 J (12–14')	2	0.12	0.23	ND (0.037)	--	--	--	--	--	0.014 J	--	--	--	0.011 J	11–13
13–15	ND (0.042)	--	--	ND (0.037)	--	--	--	0.55 B	0.032 J (14–16')	0.44	0.032 J	0.051	ND (0.037)	--	--	--	--	--	0.15 (13 – 13.6')	--	--	--	ND (0.038)	13–15
15–17	0.047	--	--	0.016 J	--	--	--	0.31 B	--	0.82	--	--	--	--	--	--	--	--	--	--	--	--	ND (0.040)	15–17
17–19	0.025 J	--	--	0.037 J	--	--	--	0.29 B	--	0.27	--	--	--	--	--	--	--	--	--	--	--	--	--	17–19
19–21	0.22 (19–20.4')	--	--	0.042	--	--	--	0.073 B	--	0.92 B	--	--	--	--	--	--	--	--	--	--	--	--	--	19–21
21–23	--	--	--	--	--	--	--	0.017 BJ (21–21.8')	--	0.032 BJ (21–21.3')	--	--	--	--	--	--	--	--	--	--	--	--	--	21–23
Sample ID	MSSB-F08	MSSB-F09	MSSB-F10	MSSB-G01	MSSB-G03	MSSB-G05	MSSB-SF-01G-1	MSSB-SF-04G-1	SB-5	SB-12	SB-12 (ESE)	SB-13	SB-14	EB-07A	EB-12	EB-13	EB-13S	EB-13W	EB-14	EB-14SW	EB-21C	Sample ID		
1–2	11	24	65 [88]	--	--	--	--	4,300	2.1	ND (0.034)	1,200	0.029 J [0.021 J]	0.020 J [5.3]	--	--	--	--	--	--	--	--	1–2		
1–3	0.15 (2–3')	0.20 J (2–3')	0.52 (2–3')	0.013 J	0.025 J	ND (0.035)	370	6.7 (2–3')	0.035 J (2–3')	--	560 (2–3')	0.012 J (2–3')	0.011 J (2–3')	11,000	--	5.2	0.029 J	11	--	89	--	1–3		
3–5	--	0.49	--	0.066 [0.036 J]	0.079	ND (0.035)	1.2	--	--	--	3.0	ND (0.036)	--	32,000 (3–4')	40,000	21	ND (0.034)	0.23	--	0.014 J	--	3–5		
4–6	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	0.0096 J (5–6')	5.3	4–6		
5–7	--	--	--	0.33	0.048	ND (0.035)	--	--	--	--	--	0.021 J	--	--	10,000	--	ND (0.035)	0.045	--	--	--	5–7		
6–8	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	0.50	0.13	8.4	6–8		
7–9	--	--	--	0.014 J	0.036 J	ND (0.036)	--	--	--	--	--	0.048	--	--	5,500	--	ND (0.041)	0.037	--	--	--	7–9		
8–10	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	8–10		
9–11	--	--	--	ND (0.036)	0.026 J	ND (0.04)	--	--	--	--	--	--	--	--	330	1.2 [0.93]	ND (0.045)	0.061	--	--	2.9 (10–12')	9–11		
11–13	--	--	--	ND (0.040)	0.05	ND (0.038) (11–12')	--	--	--	--	--	--	--	--	180	0.85	ND (0.037)	0.040	--	--	--	11–13		
13–15	--	--	--	ND (0.037)	0.029 J	--	--	--	--	--	--	--	--	--	8.7	0.85	ND (0.039)	0.11	--	--	1.0 (14–16')	13–15		
15–17	--	--	--	0.013 J	--	--	--	--	--	--	--	--	--	--	1.1	--	ND (0.040) (15–16.5')	0.21	--	--	0.98 (16–18')	15–17		
17–19	--	--	--	ND (0.035)	--	--	--	--	--	--	--	--	--	--	2,000	0.85 (16.5–18.5')	ND (0.039) (16.5–18.5')	0.44 (17–18.5')	--	--	2.2 (18–20')	17–19		
19–21	--	--	--	0.033 J	0.26 (20–21')	--	--	--	--	--	--	--	--	--	33	--	--	--	--	--	0.61 (20–22')	19–21		
21–23	--	--	--	ND (0.036)	0.11	--	--	--	--	--	--	--	--	--	0.90	--	--	--	--	--	--	21–23		
23–25	--	--	--	0.016 J	ND (0.036)	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	23–25		
25–27	--	--	--	0.097	ND (0.037) (25–26')	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	25–27		
27–29	--	--	--	0.028 J [ND (0.037)]	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	27–29		
29–31	--	--	--	0.031 J	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	29–31		
31–33	--	--	--	0.012 J (31–31.5')	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	31–33		

SUMMARY OF HISTORIC EPA DATA (ppm, DRY WT.) (SAMPLE INCREMENTS IN FEET)

EB-07A	0.89 (4–5.5')		
EB-08A	ND (0.076) (4–6')		
EB-09A	0.220 [0.210] (4–8')		
EB-10A	ND (0.080) (8–9.5')	ND (0.075) (17.5–20')	
EB-11A	0.023 J (30–31.5')	ND (0.074) (73–77')	
EB-12	26,700 J (1–3')		
EB-13	13.0 J (5–8.5')	1.40 J (15–16.5')	
EB-14	20.0 (4–6')	0.99 (12–16')	
SS-02/EB-19	0.079 (6.5–8')	ND (0.16) (18–21.5')	
EB-21C	100; 89; 9,400 J [9,600 J] (0–4')	780 J (8–10')	190 J (12–14')
SS-01	0.072 (6–7')		
SS-03	0.32 (5.5–7.5')		

NOTES:

1. ND (0.038) = NOT DETECTED. DETECTION LIMIT IN PARENTHESES, (IF AVAILABLE).
2. [0.067] = DUPLICATE ANALYSIS RESULT SHOWN IN BRACKETS.
3. B = INDICATES THE ANALYTE WAS ALSO DETECTED IN THE ASSOCIATED METHOD BLANK.
4. J = INDICATES THE DETECTED CONCENTRATION IS CONSIDERED AN ESTIMATED VALUE.
5. RE = INDICATES RE-ANALYSIS OF SAMPLE RESULT AND DUPLICATE
6. YELLOW SHADING INDICATES SAMPLES CONTAINING PCBs IN EXCESS OF SOIL CLEANUP LEVEL SPECIFIED IN ROD.

DRAFT
FOR EPA REVIEW

GENERAL ELECTRIC COMPANY
FLETCHER'S PAINT WORKS AND STORAGE FACILITY
SUPERFUND SITE - MILFORD, NEW HAMPSHIRE
FINAL (100%) DESIGN REPORT

MILL STREET AREA - SUBSURFACE SOIL PCB SAMPLE DATA

ARCADIS

FIGURE
7

CITY: SYRACUSE DIV/GROUP: ENVCAD DB: A. SCHILLING L. FORAKER, K.SARTORI PIC: P. FARR PM: C. AVERILL TM: C. AVERILL LYR: ON=*; OFF=*REF*
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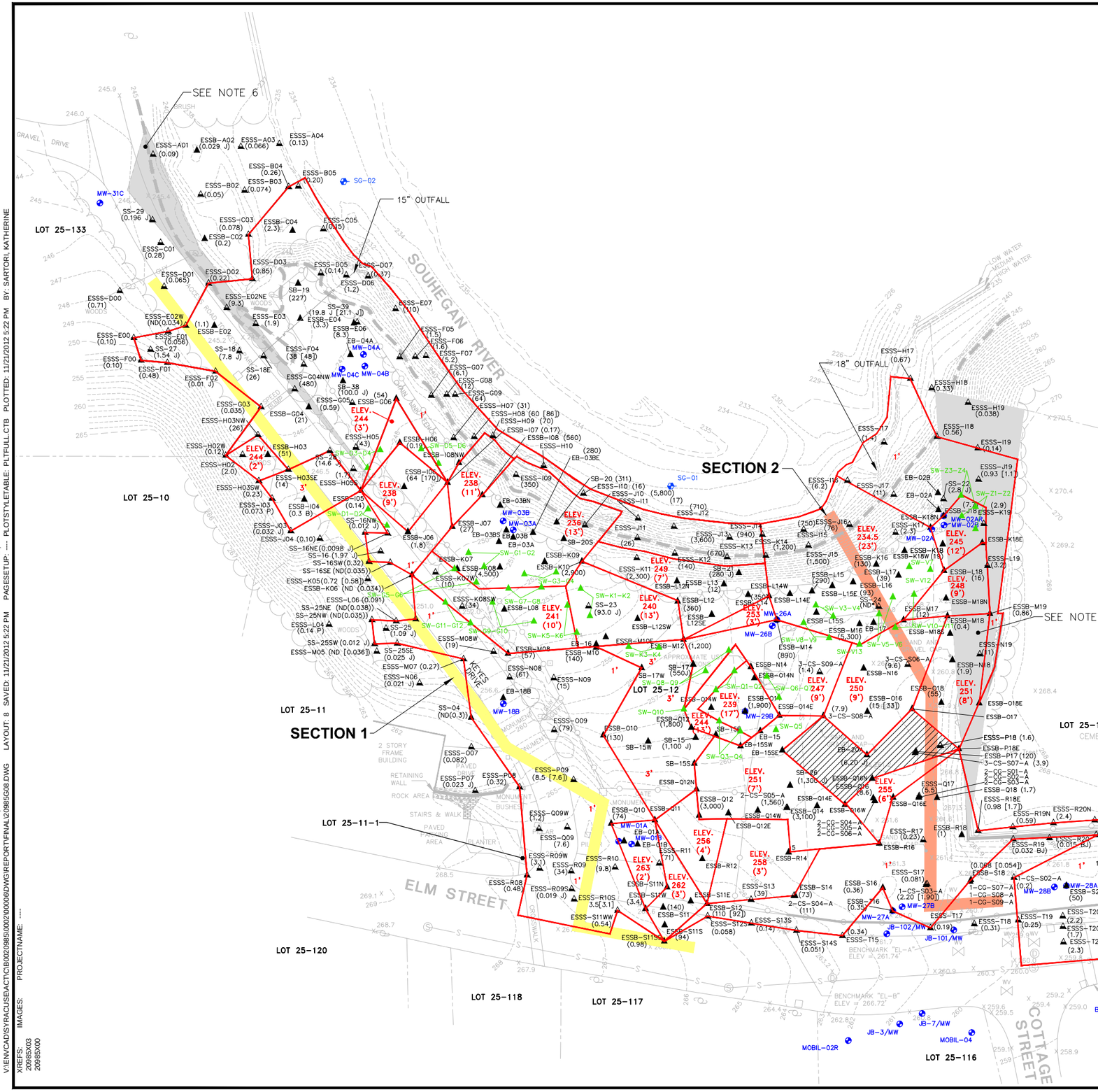

LEGEND FOR PRE-DESIGN INVESTIGATION AREA

- PROPERTY LINE
- UTILITY POLE
- CATCH BASIN
- SANITARY MANHOLE
- STORM MANHOLE
- WATER VALVE
- WATER METER
- TELEPHONE JACK
- 260 INDEX SURFACE ELEVATION CONTOUR
- 259 INTERMEDIATE SURFACE ELEVATION CONTOUR
- CHAIN LINK FENCE
- FIRE HYDRANT
- ESSB-J18 EXISTING SOIL BORING LOCATION
- ESSS-L19 EXISTING SURFACE (0-1') SOIL LOCATION
- (3.2) TOTAL SURFACE PCB CONCENTRATION (PPM, DRY WT.) DUPLICATE RESULTS SHOWN IN BRACKETS. ND = NON-DETECT.
- SW-Z1-Z2 PRE-CONSTRUCTION VERIFICATION SIDE WALL SAMPLE LOCATION
- SG-01 STAFF GAUGE
- MW-02A MONITORING WELL
- APPROXIMATE ELEVATION OF 100-YEAR FLOOD PLAIN
- EXCAVATION LIMITS
- ELEV. 245 (12') BOTTOM OF EXCAVATION ELEVATION (DEPTH SHOWN IN PARENTHESES REPRESENTS APPROXIMATE DEPTH OF SAMPLE(S) REQUIRING REMOVAL AND IS PROVIDED FOR INFORMATIONAL PURPOSES ONLY).
- 3' DEPTH OF EXCAVATION
- EXCAVATION IN THIS AREA TO BE SLOPED BETWEEN HIGHER ELEVATIONS IN EXCAVATION CELLS TO SOUTH/WEST AND LOWER ELEVATIONS IN EXCAVATION CELLS TO THE NORTH/EAST
- EXISTING UTILITY CORRIDOR
- PROPOSED REPLACEMENT STORM SEWER CORRIDOR

LEGEND FOR HISTORIC SOIL REMEDIATION AREA

- SS-1 ESE GRAB SAMPLE LOCATION
- PRIOR 1-FOOT REMOVAL

NOTES:

1. ELEVATIONS BASED ON NORTH AMERICAN VERTICAL DATUM OF 1988.
2. HORIZONTAL DATUM BASED ON NEW HAMPSHIRE STATE PLANE COORDINATE SYSTEM OF 1983.
3. CONTOUR INTERVAL = 1 FEET.
4. MAP COMPILED FROM ACTUAL FIELD SURVEY PERFORMED BY BBL, INC. FROM JULY 16, 2003 THROUGH AUGUST 14, 2003, BY MERIDAN LAND SERVICES, INC. JANUARY 22, 2004, AND BY ARCADIS ON MAY 24, 2007.
5. TITLE TO SHADED AREA IS UNCERTAIN AT THIS TIME. NO BOUNDARY LINE AGREEMENT (REFERRED TO IN THE CHAIN OF TITLE) HAS BEEN FOUND.
6. SHADED AREA AT THE NORTHWEST CORNER OF THE LOT DEPICTS AREA WHICH IS PART OF THE ROAD TO THE KEYES FIELD PARCEL. NO CONVEYANCE TO THE TOWN FOR THIS AREA HAS BEEN FOUND.
7. A SAND AND GRAVEL CAP WAS PREVIOUSLY INSTALLED OVER THE MAJORITY OF THE ELM STREET AREA BY USEPA. DURING THE PDI, THE CAP WAS OBSERVED TO BE APPROXIMATELY ONE FOOT THICK AT MOST LOCATIONS ACROSS THE PROPERTY. AT OTHER LOCATIONS, APPROXIMATE CAP THICKNESSES WERE MEASURED AS FOLLOWS: 1.5 FEET AT EB-15SE, G06, M12, N18, O16, Q10, Q12E, Q16N, Q18, AND S14; TWO FEET AT O14, O18, AND Q12; FOUR FEET AT M16; FIVE FEET AT S18; AND UP TO SIX FEET ALONG THE CEMETERY WALL AS MEASURED AT P18E. THE SAND AND GRAVEL CAP WILL BE REMOVED DURING THE SITE PREPARATION PHASE.
8. EXCAVATION CELLS WITH NO ELEVATION REFERENCE SHALL BE EXCAVATED TO THE DESIGNATED DEPTH AS MEASURED FROM GROUND SURFACE OR THE GEOTEXTILE LAYER (IF WITHIN THE SAND CAP).
9. ELM STREET SITE PROPERTY LINE SHOWN WAS ESTABLISHED FROM DEEDS OF RECORD, SURVEY, AND EXISTING MONUMENTATION. OTHER PROPERTY LINES SHOWN WERE OBTAINED FROM TOWN OF MILFORD TAX MAP 25.

Utility Corridor Information (Obtained from Town)
Section 1:
Water
Depth: 7'6"/ Width: 6'
Section 2:
Replacement Storm sewer
Electrical (portion)
Depth: 10-12'/ Width: 6'

0 30' 60'
GRAPHIC SCALE

DRAFT
FOR EPA REVIEW

GENERAL ELECTRIC COMPANY
FLETCHER'S PAINT WORKS AND STORAGE FACILITY
SUPERFUND SITE - MILFORD, NEW HAMPSHIRE
FINAL (100%) DESIGN REPORT

ELM STREET AREA - UTILITY CORRIDOR LOCATIONS

ARCADIS

FIGURE
8

CITY: SYRACUSE DIV/GROUP: ENVCAD DB: A. SCHILLING L: FORAKER, K.SARTORI PIC: P. FARR PM: C. AVERILL TM: C. AVERILL LYR: ON=*; OFF=*REF*
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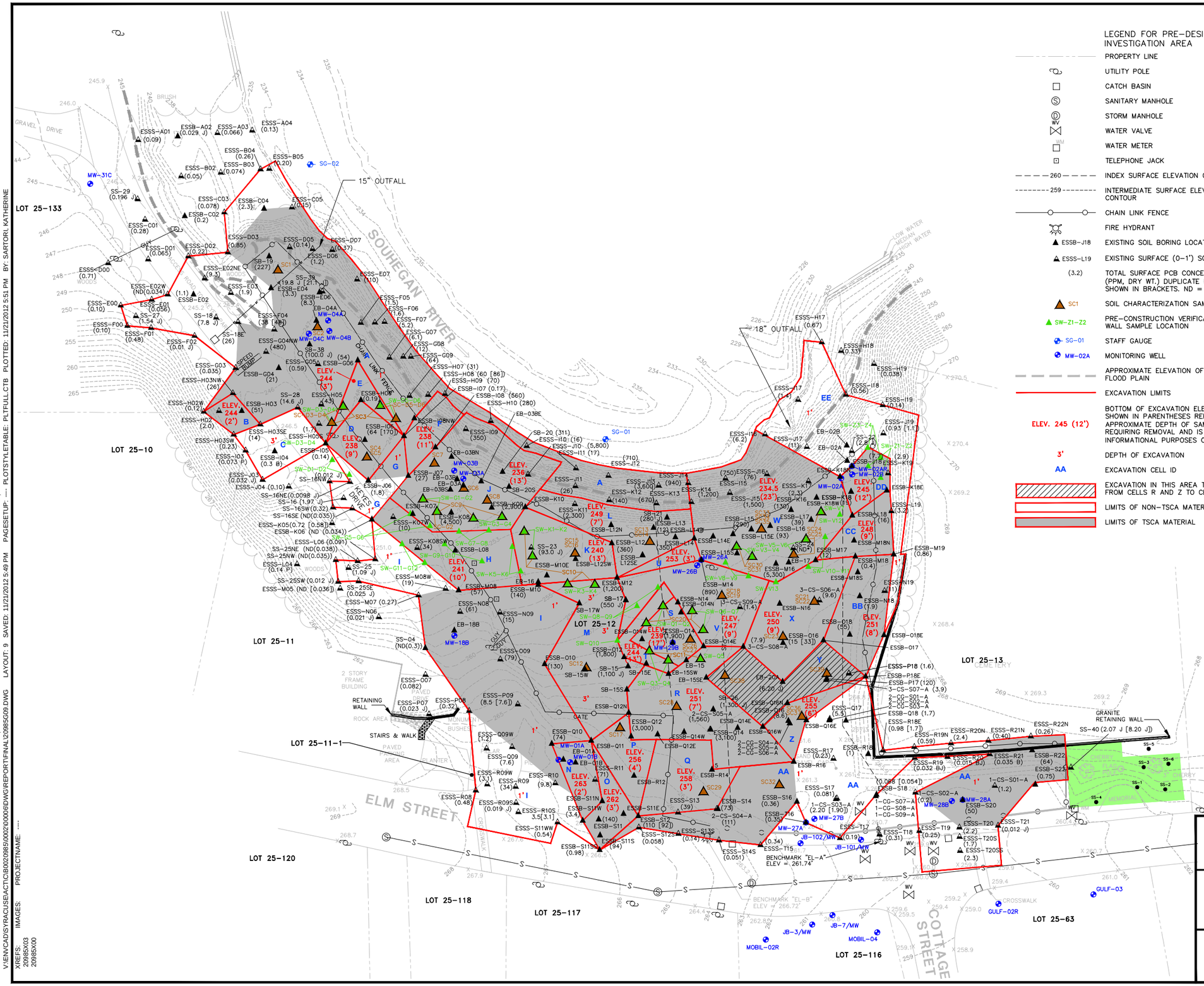

LEGEND FOR PRE-DESIGN INVESTIGATION AREA

- PROPERTY LINE
- UTILITY POLE
- CATCH BASIN
- SANITARY MANHOLE
- STORM MANHOLE
- WATER VALVE
- WATER METER
- TELEPHONE JACK
- 260 — INDEX SURFACE ELEVATION CONTOUR
- 259 — INTERMEDIATE SURFACE ELEVATION CONTOUR
- CHAIN LINK FENCE
- FIRE HYDRANT
- ESSB-J18 — EXISTING SOIL BORING LOCATION
- ESSS-L19 — EXISTING SURFACE (0-1') SOIL LOCATION
- (3.2) — TOTAL SURFACE PCB CONCENTRATION (PPM, DRY WT.) DUPLICATE RESULTS SHOWN IN BRACKETS. ND = NON-DETECT
- SC1 — SOIL CHARACTERIZATION SAMPLE LOCATION
- SW-Z1-Z2 — PRE-CONSTRUCTION VERIFICATION SIDE WALL SAMPLE LOCATION
- SG-01 — STAFF GAUGE
- MW-02A — MONITORING WELL
- APPROXIMATE ELEVATION OF 100-YEAR FLOOD PLAIN
- EXCAVATION LIMITS
- ELEV. 245 (12') — BOTTOM OF EXCAVATION ELEVATION (DEPTH SHOWN IN PARENTHESES REPRESENTS APPROXIMATE DEPTH OF SAMPLE(S) REQUIRING REMOVAL AND IS PROVIDED FOR INFORMATIONAL PURPOSES ONLY).
- 3' — DEPTH OF EXCAVATION
- AA — EXCAVATION CELL ID
- EXCAVATION IN THIS AREA TO BE SLOPED FROM CELLS R AND Z TO CELLS X AND BB
- LIMITS OF NON-TSCA MATERIAL
- LIMITS OF TSCA MATERIAL

LEGEND FOR HISTORIC SOIL REMEDIATION AREA

- SS-1 — ESE GRAB SAMPLE LOCATION
- PRIOR 1-FOOT REMOVAL

NOTES:

1. ELEVATIONS BASED ON NORTH AMERICAN VERTICAL DATUM OF 1988.
2. HORIZONTAL DATUM BASED ON NEW HAMPSHIRE STATE PLANE COORDINATE SYSTEM OF 1983.
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6. EXCAVATION CELLS WITH NO ELEVATION REFERENCE SHALL BE EXCAVATED TO THE DESIGNATED DEPTH AS MEASURED FROM GROUND SURFACE OR THE GEOTEXTILE LAYER (IF WITHIN THE SAND CAP).
7. ELM STREET SITE PROPERTY LINE SHOWN WAS ESTABLISHED FROM DEEDS OF RECORD, SURVEY, AND EXISTING MONUMENTATION. OTHER PROPERTY LINES SHOWN WERE OBTAINED FROM TOWN OF MILFORD TAX MAP 25.
8. REFER TO FIGURE 14 FOR WELLS TO BE DECOMMISSIONED/PROTECTED DURING IMPLEMENTATION OF REMEDIAL ACTION AND NEW WELLS TO BE INSTALLED FOLLOWING PERFORMANCE OF THE REMEDIAL ACTION.

DRAFT
FOR EPA REVIEW

GENERAL ELECTRIC COMPANY
FLETCHER'S PAINT WORKS AND STORAGE FACILITY
SUPERFUND SITE - MILFORD, NEW HAMPSHIRE
FINAL (100%) DESIGN REPORT

ELM STREET AREA - SOIL REMOVAL LIMITS TO ACHIEVE NON-CORRIDOR SCLs

ARCADIS

FIGURE
9

CITY: SYRACUSE DIV/GROUP: ENVCAD DB: A. SCHILLING L: FORAKER, K.SARTORI PIC: P. FARR PM: C. AVERILL TM: C. AVERILL LYR: ON=*; OFF=*REF*
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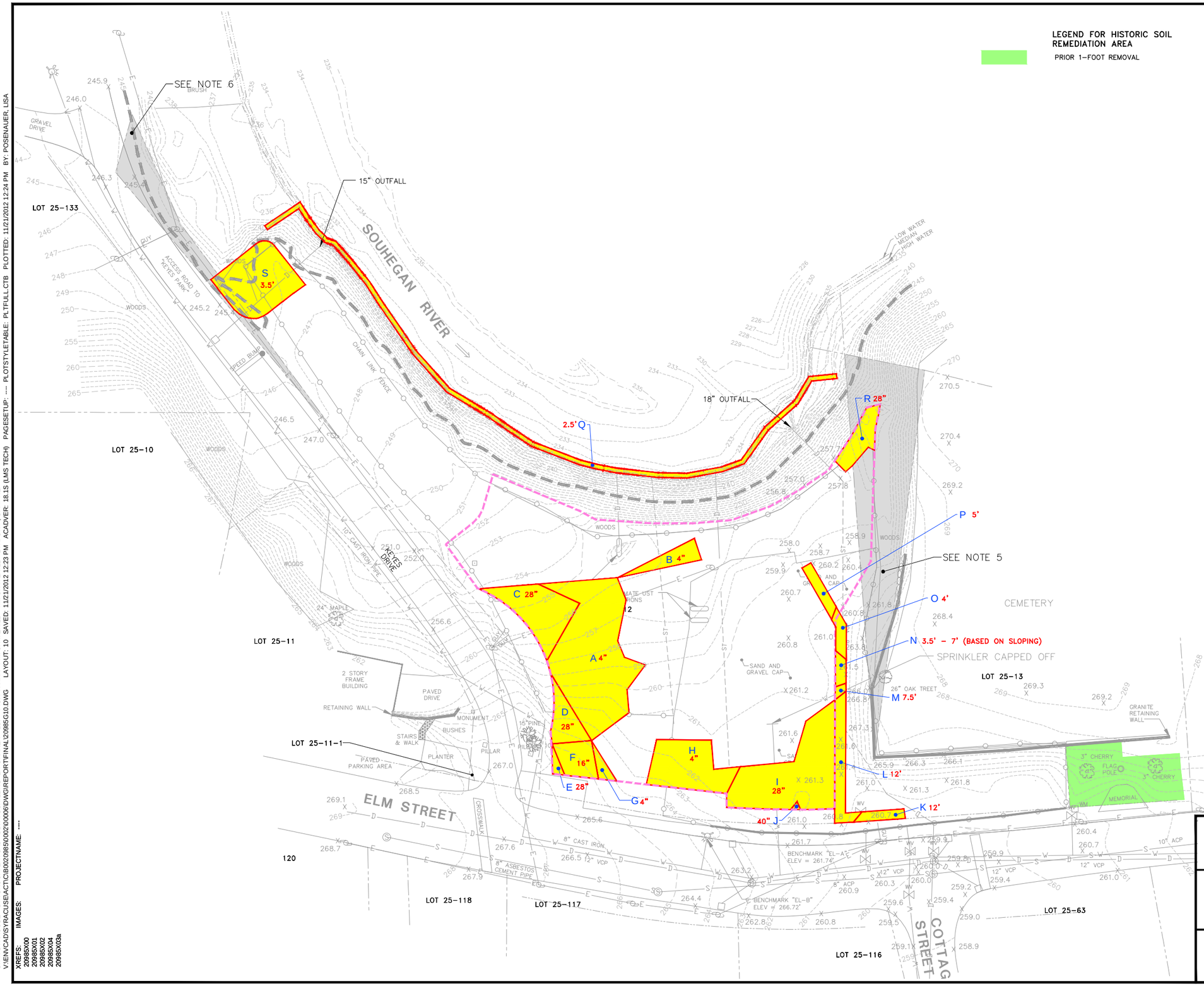

LEGEND FOR HISTORIC SOIL REMEDIATION AREA

PRIOR 1-FOOT REMOVAL

LEGEND FOR PRE-DESIGN INVESTIGATION AREA

- PROPERTY LINE
- UTILITY POLE
- CATCH BASIN
- SANITARY MANHOLE
- STORM MANHOLE
- WV — WATER VALVE
- WM — WATER METER
- TELEPHONE JACK
- 260 — INDEX SURFACE ELEVATION CONTOUR
- 261 — INTERMEDIATE SURFACE ELEVATION CONTOUR
- CHAIN LINK FENCE
- FIRE HYDRANT
- APPROXIMATE ELEVATION OF 100-YEAR FLOOD PLAIN
- COVER BOUNDARY
- EXCAVATION LIMITS
- A — EXCAVATION ID
- 5' — DEPTH OF EXCAVATION
- AREA OF ADDITIONAL EXCAVATION. DEPTH OF EXCAVATION NOTED ON DRAWING IS ADDITIONAL EXCAVATION BEYOND THAT REQUIRED TO ACHIEVE SCLs.

NOTES:

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8. ELM STREET SITE PROPERTY LINE SHOWN WAS ESTABLISHED FROM DEEDS OF RECORD, SURVEY, AND EXISTING MONUMENTATION. OTHER PROPERTY LINES SHOWN WERE OBTAINED FROM TOWN OF MILFORD TAX MAP 25.

0 30' 60'
GRAPHIC SCALE

DRAFT
FOR EPA REVIEW

GENERAL ELECTRIC COMPANY
FLETCHER'S PAINT WORKS AND STORAGE FACILITY
SUPERFUND SITE - MILFORD, NEW HAMPSHIRE
FINAL (100%) DESIGN REPORT

ELM STREET AREA - ADDITIONAL SOIL REMOVAL REQUIRED FOR REPLACEMENT STORM SEWER, COVER SYSTEM, STORM WATER RETNETION AREA, AND GABION WALL

ARCADIS

FIGURE
10

CITY: SYRACUSE DIV/GROUP: ENVCAD DB: A. SCHILLING L: FORAKER LD: PIC: P. FARR PM: C. AVERILL TM: C. AVERILL LYR: ON=*; OFF=*REF*
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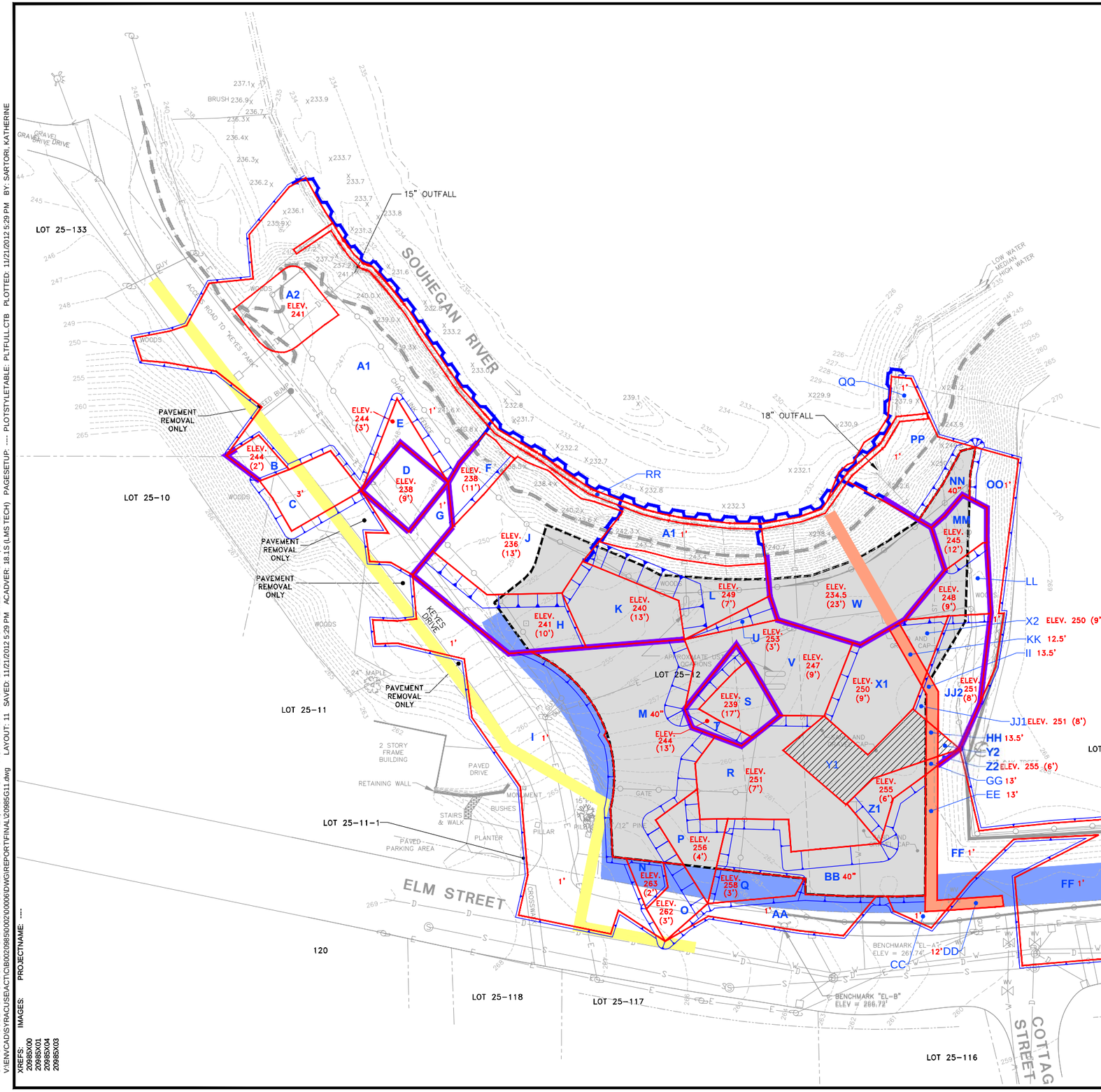

LEGEND FOR PRE-DESIGN INVESTIGATION AREA

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- WATER METER
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- 261 — INTERMEDIATE SURFACE ELEVATION CONTOUR
- CHAIN LINK FENCE
- FIRE HYDRANT
- APPROXIMATE ELEVATION OF 100-YEAR FLOOD PLAIN
- EXCAVATION LIMITS
- A — EXCAVATION CELL ID
- ELEV. 245 (12') — BOTTOM OF EXCAVATION ELEVATION (DEPTH SHOWN IN PARENTHESES REPRESENTS APPROXIMATE DEPTH OF SAMPLE(S) REQUIRING REMOVAL AND IS PROVIDED FOR INFORMATIONAL PURPOSES ONLY).
- 40" — DEPTH OF EXCAVATION
- EXCAVATION IN THIS AREA TO BE SLOPED BETWEEN HIGHER ELEVATIONS IN EXCAVATION CELLS TO SOUTH/WEST AND LOWER ELEVATIONS IN EXCAVATION CELLS TO THE NORTH/EAST
- APPROXIMATE AREA OF COVER SYSTEM
- EXISTING UTILITY CORRIDOR
- PROPOSED REPLACEMENT STORM SEWER
- PROPOSED TREE/SHRUB PLANTING CORRIDOR
- EXCAVATION SLOPING
- STEEL SHEET PILE
- SOLDIER PILES

LEGEND FOR HISTORIC SOIL REMEDIATION AREA

- PRIOR 1-FOOT REMOVAL

NOTES:

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7. ELM STREET SITE PROPERTY LINE SHOWN WAS ESTABLISHED FROM DEEDS OF RECORD, SURVEY, AND EXISTING MONUMENTATION. OTHER PROPERTY LINES SHOWN WERE OBTAINED FROM TOWN OF MILFORD TAX MAP 25.

0 30' 60'
GRAPHIC SCALE

DRAFT
FOR EPA REVIEW

GENERAL ELECTRIC COMPANY
FLETCHER'S PAINT WORKS AND STORAGE FACILITY
SUPERFUND SITE - MILFORD, NEW HAMPSHIRE
FINAL (100%) DESIGN REPORT

ELM STREET AREA - COMBINED LIMITS OF EXCAVATION

ARCADIS

FIGURE
11

CITY: SYRACUSE DIV/GROUP: ENVCAD DB: A. SCHILLING L. FORAKER, K.SARTORI PIC: P. FARR PM: C. AVERILL TM: C. AVERILL LYR: ON=*; OFF=*REF*
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XREFS: 20985X00 20985X01 20985X04 20985X03 IMAGES: PROJECTNAME: ----

NOTES:

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2. HORIZONTAL DATUM BASED ON NEW HAMPSHIRE STATE PLANE COORDINATE SYSTEM OF 1983.
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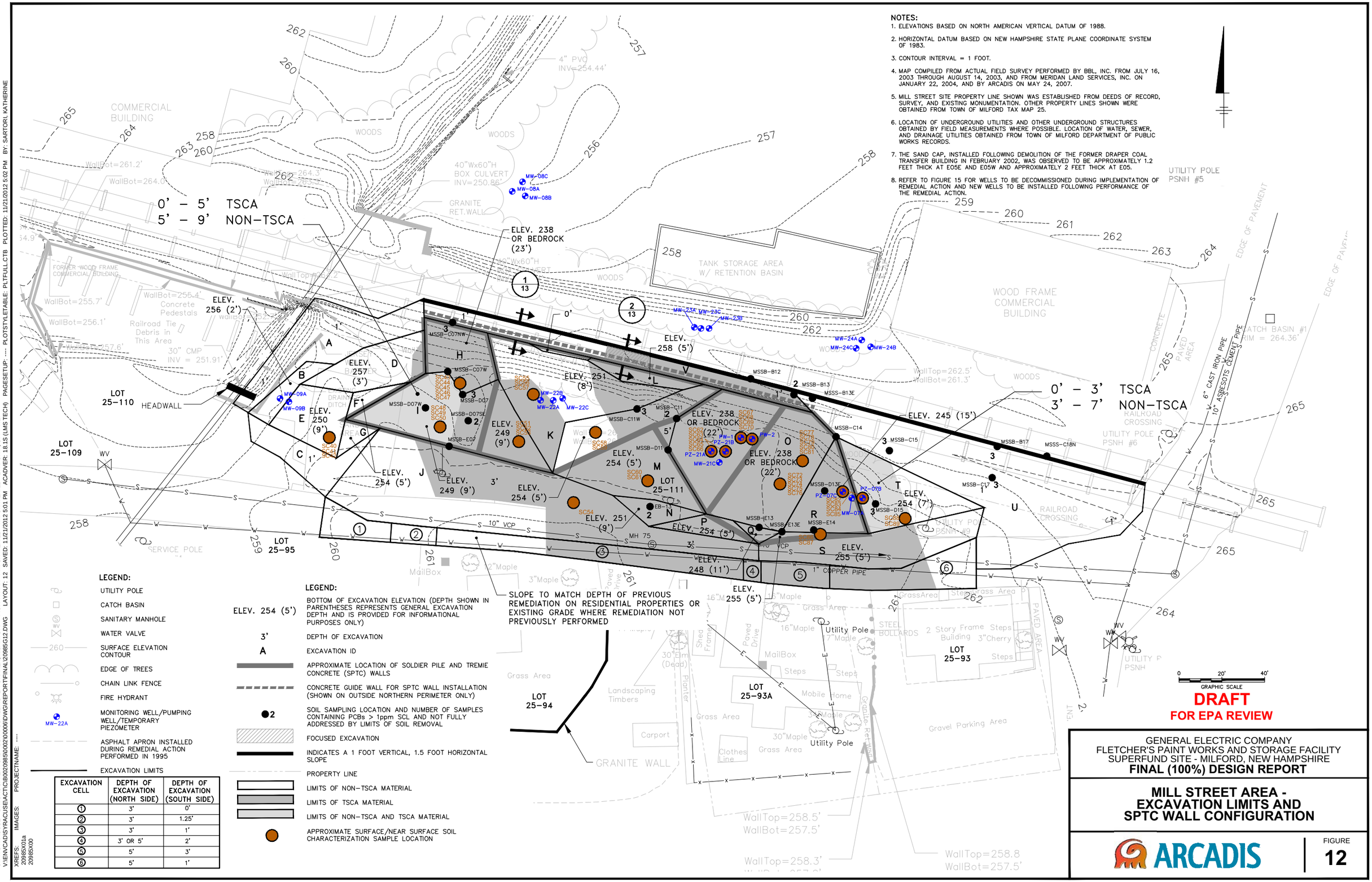
5. MILL STREET SITE PROPERTY LINE SHOWN WAS ESTABLISHED FROM DEEDS OF RECORD, SURVEY, AND EXISTING MONUMENTATION. OTHER PROPERTY LINES SHOWN WERE OBTAINED FROM TOWN OF MILFORD TAX MAP 25.
6. LOCATION OF UNDERGROUND UTILITIES AND OTHER UNDERGROUND STRUCTURES OBTAINED BY FIELD MEASUREMENTS WHERE POSSIBLE. LOCATION OF WATER, SEWER, AND DRAINAGE UTILITIES OBTAINED FROM TOWN OF MILFORD DEPARTMENT OF PUBLIC WORKS RECORDS.
7. THE SAND CAP, INSTALLED FOLLOWING DEMOLITION OF THE FORMER DRAPER COAL TRANSFER BUILDING IN FEBRUARY 2002, WAS OBSERVED TO BE APPROXIMATELY 1.2 FEET THICK AT E05E AND E05W AND APPROXIMATELY 2 FEET THICK AT E05.
8. REFER TO FIGURE 15 FOR WELLS TO BE DECOMMISSIONED DURING IMPLEMENTATION OF REMEDIAL ACTION AND NEW WELLS TO BE INSTALLED FOLLOWING PERFORMANCE OF THE REMEDIAL ACTION.



LEGEND:

- UTILITY POLE
- CATCH BASIN
- SANITARY MANHOLE
- WATER VALVE
- SURFACE ELEVATION CONTOUR
- EDGE OF TREES
- CHAIN LINK FENCE
- FIRE HYDRANT
- MW-22A — MONITORING WELL/PUMPING WELL/TEMPORARY PIEZOMETER
- ASPHALT APRON INSTALLED DURING REMEDIAL ACTION PERFORMED IN 1995
- EXCAVATION LIMITS

EXCAVATION CELL	DEPTH OF EXCAVATION (NORTH SIDE)	DEPTH OF EXCAVATION (SOUTH SIDE)
1	3'	0'
2	3'	1.25'
3	3'	1'
4	3' OR 5'	2'
5	5'	3'
6	5'	1'

LEGEND:

- ELEV. 254 (5') — BOTTOM OF EXCAVATION ELEVATION (DEPTH SHOWN IN PARENTHESES REPRESENTS GENERAL EXCAVATION DEPTH AND IS PROVIDED FOR INFORMATIONAL PURPOSES ONLY)
- 3' — DEPTH OF EXCAVATION
- A — EXCAVATION ID
- APPROXIMATE LOCATION OF SOLDIER PILE AND TREMIE CONCRETE (SPTC) WALLS
- CONCRETE GUIDE WALL FOR SPTC WALL INSTALLATION (SHOWN ON OUTSIDE NORTHERN PERIMETER ONLY)
- 2 — SOIL SAMPLING LOCATION AND NUMBER OF SAMPLES CONTAINING PCBs > 1ppm SCL AND NOT FULLY ADDRESSED BY LIMITS OF SOIL REMOVAL
- FOCUSED EXCAVATION
- INDICATES A 1 FOOT VERTICAL, 1.5 FOOT HORIZONTAL SLOPE
- PROPERTY LINE
- LIMITS OF NON-TSCA MATERIAL
- LIMITS OF TSCA MATERIAL
- LIMITS OF NON-TSCA AND TSCA MATERIAL
- APPROXIMATE SURFACE/NEAR SURFACE SOIL CHARACTERIZATION SAMPLE LOCATION

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MILL STREET AREA - EXCAVATION LIMITS AND SPTC WALL CONFIGURATION

ARCADIS

FIGURE **12**

CITY: SYRACUSE DIV/GROUP: ENVCAD DB: A. SCHILLING L. FORAKER, K.SARTORI PIC: P. FARR PM: C. AVERILL TM: C. AVERILL LYR: ON=*; OFF=*REF*
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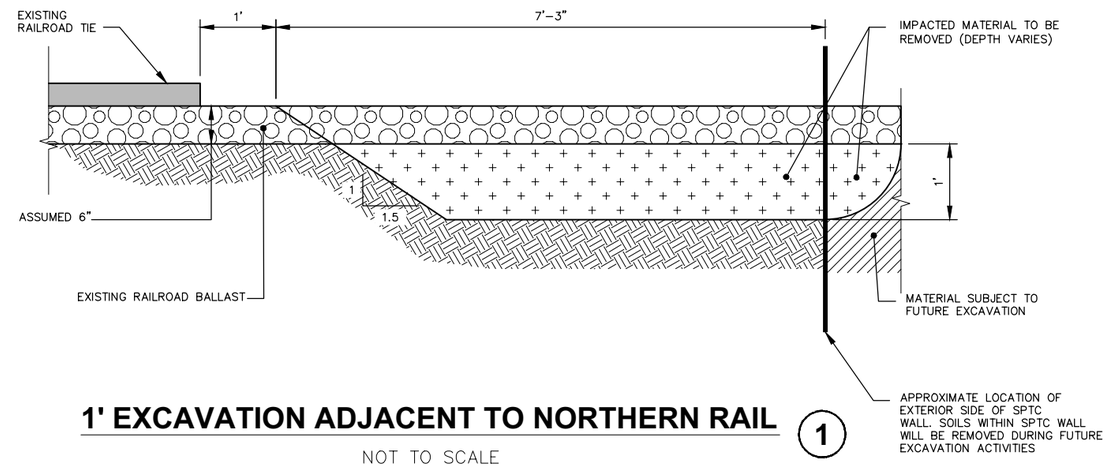
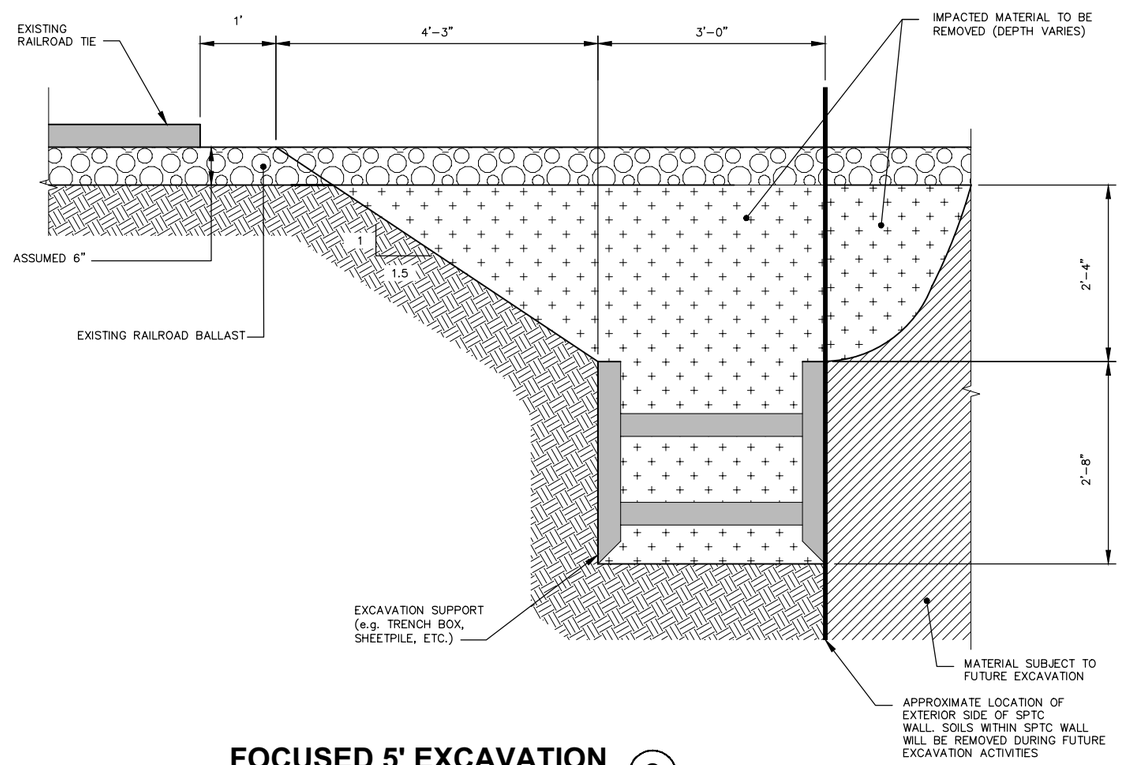


1' EXCAVATION ADJACENT TO NORTHERN RAIL (1)

NOT TO SCALE



FOCUSED 5' EXCAVATION (2)

NOT TO SCALE

GENERAL NOTES:

1. FINAL DIMENSIONS AND SLOPES ARE SUBJECT TO REVIEW AND APPROVAL OF GUILFORD RAILROAD.
2. FIGURE DOES NOT REPRESENT ACTUAL SURFACE TOPOGRAPHY.

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MILL STREET AREA - FOCUSED EXCAVATION DETAILS

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FIGURE
13

CITY: SYRACUSE DIV/GROUP: ENVCAD DB: A. SCHILLING L. FORAKER, K.SARTORI PIC: P. FARR PM: C. AVERILL TM: C. AVERILL LYR: ON=*; OFF=*REF*
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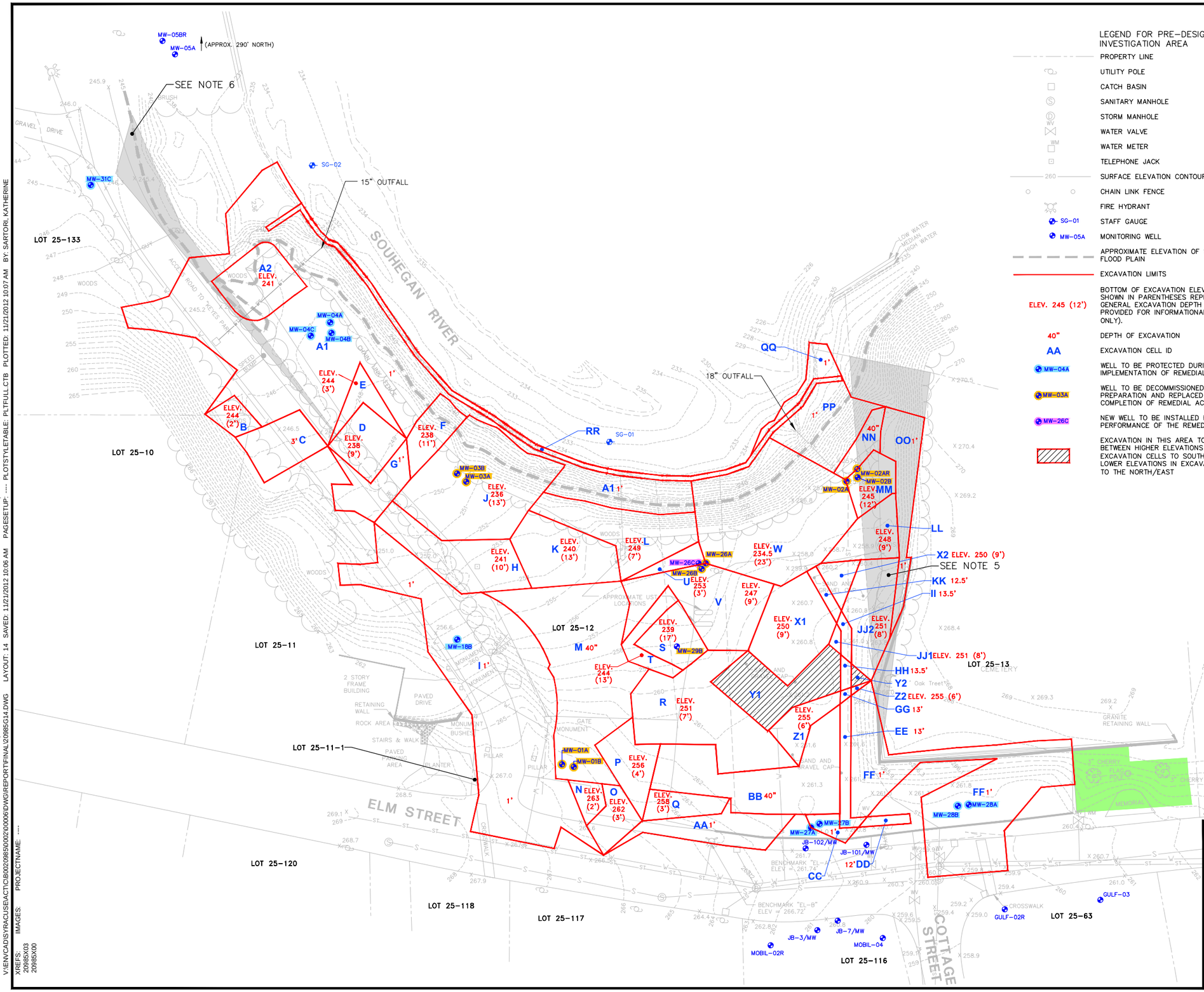

LEGEND FOR PRE-DESIGN INVESTIGATION AREA

- PROPERTY LINE
- UTILITY POLE
- CATCH BASIN
- SANITARY MANHOLE
- STORM MANHOLE
- WATER VALVE
- WATER METER
- TELEPHONE JACK
- 260 — SURFACE ELEVATION CONTOUR
- CHAIN LINK FENCE
- FIRE HYDRANT
- SG-01 — STAFF GAUGE
- MW-05A — MONITORING WELL
- APPROXIMATE ELEVATION OF 100-YEAR FLOOD PLAIN
- EXCAVATION LIMITS
- ELEV. 245 (12') — BOTTOM OF EXCAVATION ELEVATION (DEPTH SHOWN IN PARENTHESES REPRESENTS GENERAL EXCAVATION DEPTH AND IS PROVIDED FOR INFORMATIONAL PURPOSES ONLY).
- 40" — DEPTH OF EXCAVATION
- AA — EXCAVATION CELL ID
- MW-04A — WELL TO BE PROTECTED DURING IMPLEMENTATION OF REMEDIAL ACTION
- MW-03A — WELL TO BE DECOMMISSIONED DURING SITE PREPARATION AND REPLACED UPON COMPLETION OF REMEDIAL ACTION
- MW-26C — NEW WELL TO BE INSTALLED FOLLOWING PERFORMANCE OF THE REMEDIAL ACTION
- EXCAVATION IN THIS AREA TO BE SLOPED BETWEEN HIGHER ELEVATIONS IN EXCAVATION CELLS TO SOUTH/WEST AND LOWER ELEVATIONS IN EXCAVATION CELLS TO THE NORTH/EAST

LEGEND FOR HISTORIC SOIL REMEDIATION AREA

- 1-FOOT REMOVAL

NOTES:

1. ELEVATIONS BASED ON NORTH AMERICAN VERTICAL DATUM OF 1988.
2. HORIZONTAL DATUM BASED ON NEW HAMPSHIRE STATE PLANE COORDINATE SYSTEM OF 1983.
3. CONTOUR INTERVAL = 1 FEET.
4. MAP COMPILED FROM ACTUAL FIELD SURVEY PERFORMED BY BBL, INC. FROM JULY 16, 2003 THROUGH AUGUST 14, 2003, BY MERIDAN LAND SERVICES, INC. JANUARY 22, 2004, AND BY ARCADIS ON MAY 24, 2007.
5. TITLE TO SHADED AREA IS UNCERTAIN AT THIS TIME. NO BOUNDARY LINE AGREEMENT (REFERRED TO IN THE CHAIN OF TITLE) HAS BEEN FOUND.
6. SHADED AREA AT THE NORTHWEST CORNER OF THE LOT DEPICTS AREA WHICH IS PART OF THE ROAD TO THE KEYES FIELD PARCEL. NO CONVEYANCE TO THE TOWN FOR THIS AREA HAS BEEN FOUND.
7. A SAND AND GRAVEL CAP WAS PREVIOUSLY INSTALLED OVER THE MAJORITY OF THE ELM STREET AREA BY USEPA. DURING THE PDI, THE CAP WAS OBSERVED TO BE APPROXIMATELY ONE FOOT THICK AT MOST LOCATIONS ACROSS THE PROPERTY. AT OTHER LOCATIONS, APPROXIMATE CAP THICKNESSES WERE MEASURED AS FOLLOWS: 1.5 FEET AT EB-15SE, G06, M12, N18, O16, Q10, Q12E, Q16N, Q18, AND S14; TWO FEET AT O14, O18, AND Q12; FOUR FEET AT M16; FIVE FEET AT S18; AND UP TO SIX FEET ALONG THE CEMETERY WALL AS MEASURED AT P18E. THE SAND AND GRAVEL CAP WILL BE REMOVED DURING THE SITE PREPARATION PHASE.
8. ELM STREET SITE PROPERTY LINE SHOWN WAS ESTABLISHED FROM DEEDS OF RECORD, SURVEY, AND EXISTING MONUMENTATION. OTHER PROPERTY LINES SHOWN WERE OBTAINED FROM TOWN OF MILFORD TAX MAP 25.

0 30' 60'
GRAPHIC SCALE

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FLETCHER'S PAINT WORKS AND STORAGE FACILITY
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ELM STREET AREA - MONITORING WELLS SUBJECT TO DECOMMISSIONING/PROTECTION/ INSTALLATION/REPLACEMENT

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FIGURE
14

CITY: SYRACUSE DIV/GROUP: ENVCAD DB: A. SCHILLING L. FORAKER ; K.SARTORI PIC: P. FARR PM: C. AVERILL TM: C. AVERILL LYR: ON=*; OFF=*REF*
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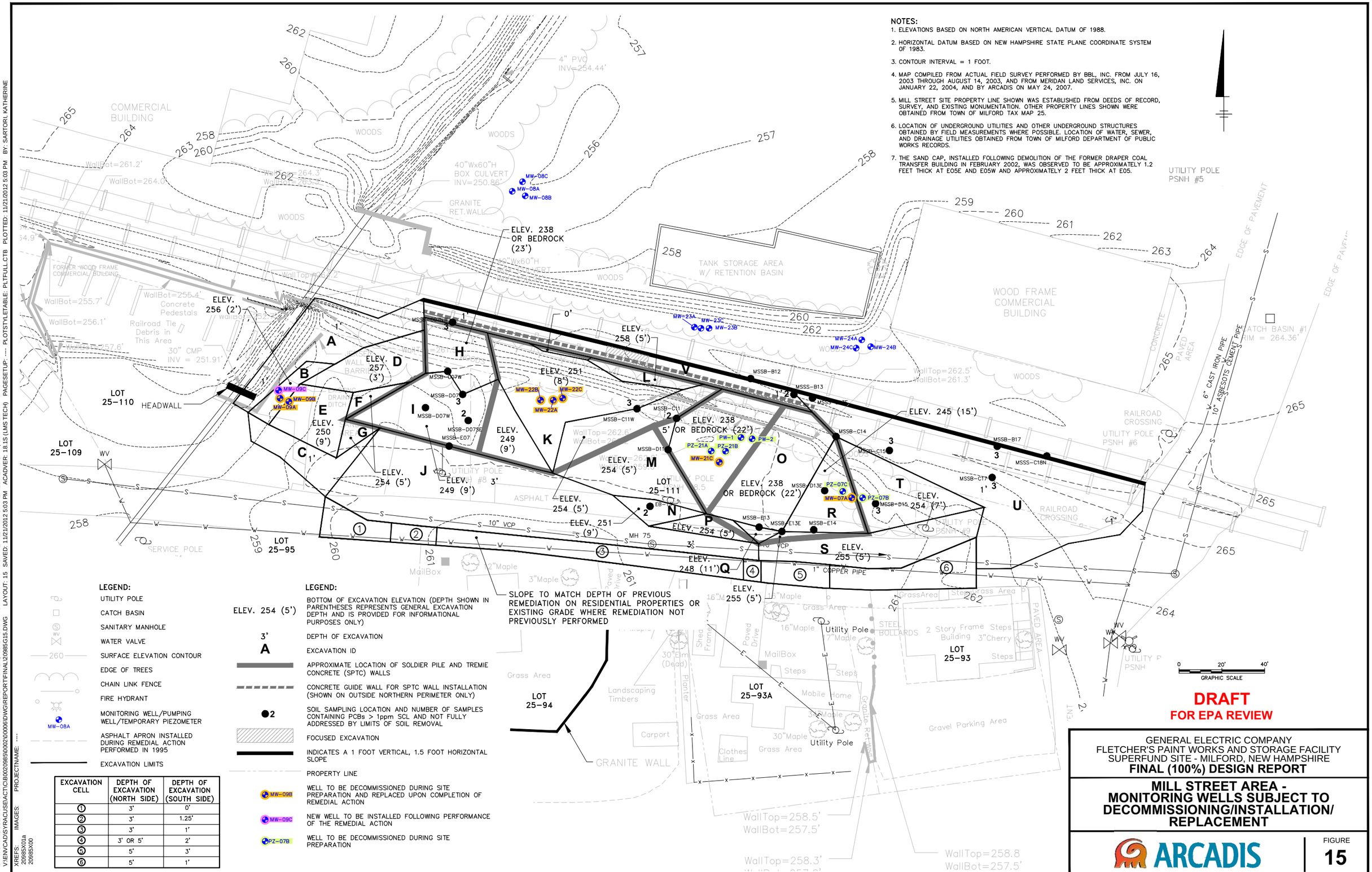

NOTES:

1. ELEVATIONS BASED ON NORTH AMERICAN VERTICAL DATUM OF 1988.
2. HORIZONTAL DATUM BASED ON NEW HAMPSHIRE STATE PLANE COORDINATE SYSTEM OF 1983.
3. CONTOUR INTERVAL = 1 FOOT.
4. MAP COMPILED FROM ACTUAL FIELD SURVEY PERFORMED BY BBL, INC. FROM JULY 16, 2003 THROUGH AUGUST 14, 2003, AND FROM MERIDAN LAND SERVICES, INC. ON JANUARY 22, 2004, AND BY ARCADIS ON MAY 24, 2007.
5. MILL STREET SITE PROPERTY LINE SHOWN WAS ESTABLISHED FROM DEEDS OF RECORD, SURVEY, AND EXISTING MONUMENTATION. OTHER PROPERTY LINES SHOWN WERE OBTAINED FROM TOWN OF MILFORD TAX MAP 25.
6. LOCATION OF UNDERGROUND UTILITIES AND OTHER UNDERGROUND STRUCTURES OBTAINED BY FIELD MEASUREMENTS WHERE POSSIBLE. LOCATION OF WATER, SEWER, AND DRAINAGE UTILITIES OBTAINED FROM TOWN OF MILFORD DEPARTMENT OF PUBLIC WORKS RECORDS.
7. THE SAND CAP, INSTALLED FOLLOWING DEMOLITION OF THE FORMER DRAPER COAL TRANSFER BUILDING IN FEBRUARY 2002, WAS OBSERVED TO BE APPROXIMATELY 1.2 FEET THICK AT EO5E AND EO5W AND APPROXIMATELY 2 FEET THICK AT EO5.

LEGEND:

- UTILITY POLE
- CATCH BASIN
- SANITARY MANHOLE
- WATER VALVE
- SURFACE ELEVATION CONTOUR
- EDGE OF TREES
- CHAIN LINK FENCE
- FIRE HYDRANT
- MW-08A — MONITORING WELL/PUMPING WELL/TEMPORARY PIEZOMETER
- ASPHALT APRON INSTALLED DURING REMEDIAL ACTION PERFORMED IN 1995
- EXCAVATION LIMITS

LEGEND:

- ELEV. 254 (5') — BOTTOM OF EXCAVATION ELEVATION (DEPTH SHOWN IN PARENTHESES REPRESENTS GENERAL EXCAVATION DEPTH AND IS PROVIDED FOR INFORMATIONAL PURPOSES ONLY)
- 3' — DEPTH OF EXCAVATION
- A — EXCAVATION ID
- APPROXIMATE LOCATION OF SOLDIER PILE AND TREMIE CONCRETE (SPTC) WALLS
- CONCRETE GUIDE WALL FOR SPTC WALL INSTALLATION (SHOWN ON OUTSIDE NORTHERN PERIMETER ONLY)
- 2 — SOIL SAMPLING LOCATION AND NUMBER OF SAMPLES CONTAINING PCBs > 1ppm SCL AND NOT FULLY ADDRESSED BY LIMITS OF SOIL REMOVAL
- FOCUSED EXCAVATION
- INDICATES A 1 FOOT VERTICAL, 1.5 FOOT HORIZONTAL SLOPE
- PROPERTY LINE
- MW-09B — WELL TO BE DECOMMISSIONED DURING SITE PREPARATION AND REPLACED UPON COMPLETION OF REMEDIAL ACTION
- MW-09C — NEW WELL TO BE INSTALLED FOLLOWING PERFORMANCE OF THE REMEDIAL ACTION
- PZ-07B — WELL TO BE DECOMMISSIONED DURING SITE PREPARATION

EXCAVATION CELL	DEPTH OF EXCAVATION (NORTH SIDE)	DEPTH OF EXCAVATION (SOUTH SIDE)
1	3'	0'
2	3'	1.25'
3	3'	1'
4	3' OR 5'	2'
5	5'	3'
6	5'	1'

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MILL STREET AREA - MONITORING WELLS SUBJECT TO DECOMMISSIONING/INSTALLATION/ REPLACEMENT

ARCADIS

FIGURE
15

CITY: SYRACUSE DIV/GROUP: ENVCAD DB: A. SCHILLING L: FORAKER, K.SARTORI PIC: P. FARR PM: C. AVERILL TM: C. AVERILL LYR: ON=*; OFF=*REF*
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