

Ref: 8P-AR

# <u>CERTIFIED MAIL</u> <u>RETURN RECEIPT REQUESTED</u>

Ms. Debbye Balcaen Lathrop Laramie County Clerk P.O. Box 608 Cheyenne, WY 82003

> Re: Black Hills Corp./Cheyenne Light Fuel & Power - Cheyenne Prairie Generating Station Draft Greenhouse Gas Prevention of Significant Deterioration Draft Permit # PSD-WY-000001-2011.001 supplemental information for the record

Dear Ms. Lathrop:

Please amend the public notice file for the above named facility, transmitted to your office under cover letter dated 5/17/2012, with the enclosed documents (including supplemental correspondence and Endangered Species Act information). As with the documents you already have, please make these documents available (in the same file folder as the others) for the remainder of the public comments period (through June 21, 2012). Thank you so much for your help and please don't hesitate to call with any questions or concerns you may have at (303) 312-6648. I apologize for any inconvenience this may have created for you, thank you.

Sincerely,

Christopher Razzazian, Engineer Air Program



Ref: 8P-AR

# <u>CERTIFIED MAIL</u> <u>RETURN RECEIPT REQUESTED</u>

Mr. William Allison Air Division Director Air Pollution Control Division (APCD-SS-B1) Colorado Department of Public Health & Environment 4300 Cherry Creek Drive South Denver, CO 80246-1530

> Re: Greenhouse Gas Prevention of Significant Deterioration Draft Permit # PSD-WY-000001-2011.001

Dear Mr. Allison:

The U.S. Environmental Protection Agency (EPA), Region 8, has completed its initial review of Black Hills Corporation/Cheyenne Light Fuel & Power's permit application dated September 23, 2011, for a Greenhouse Gas (GHG) Prevention of Significant Deterioration (PSD) permit to allow construction and operation of a new 220 MW natural gas fired combustion turbine electric generating utility to be known as the Cheyenne Prairie Generating Station.

Enclosed is the draft PSD permit and corresponding Statement of Basis, along with a copy of the public notice. A copy of these materials (in addition to the PSD application submitted to the EPA) are also being sent to the Laramie County Clerk's office. These documents are also available on EPA's website at: <u>http://www.epa.gov/region8/pubnotice.html</u>, under the heading "Region 8 Air Permitting comment opportunities" within the "PSD Permits" heading.

The Wyoming Department of Environmental Quality (WDEQ) will issue a draft PSD permit for PSD pollutants other than GHGs for this facility. The WDEQ will conduct a public comment period concurrent with the EPA's for its draft PSD permit.

The conditions contained in the permit will become effective and enforceable if the permit is issued as a final permit. If you wish to comment on the proposed action please submit your written comments to:

Christopher Razzazian - Permit Contact U.S. EPA, Region 8 Air Program (8P-AR) 1595 Wynkoop Street Denver, Colorado 80202-1129

If you have any questions concerning the enclosed materials, you may contact Mr. Razzazian at (303) 312-6648.

Sincerely,

Carl Daly, Director Air Program



Ref: 8P-AR

### <u>CERTIFIED MAIL</u> <u>RETURN RECEIPT REQUESTED</u>

Ms. Virginia Riley Executive Secretary to the Mayor of Cheyenne City of Cheyenne 2101 O'Neil Ave. Cheyenne, WY 82001

> Re: Greenhouse Gas Prevention of Significant Deterioration Draft Permit # PSD-WY-000001-2011.001

Dear Ms. Riley:

The U.S. Environmental Protection Agency (EPA), Region 8, has completed its initial review of Black Hills Corporation/Cheyenne Light Fuel & Power's permit application dated September 23, 2011, for a Greenhouse Gas (GHG) Prevention of Significant Deterioration (PSD) permit to allow construction and operation of a new 220 MW natural gas fired combustion turbine electric generating utility to be known as the Cheyenne Prairie Generating Station.

Enclosed is the draft PSD permit and corresponding Statement of Basis, along with a copy of the public notice. A copy of these materials (in addition to the PSD application submitted to the EPA) are also being sent to the Laramie County Clerk's office. These documents are also available on the EPA's website at: <u>http://www.epa.gov/region8/pubnotice.html</u>, under the heading "Region 8 Air Permitting comment opportunities" within the "PSD Permits" heading.

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Sincerely,

Carl Daly, Director Air Program



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Ms. Debbye Balcaen Lathrop Laramie County Clerk P.O. Box 608 Cheyenne, WY 82003

> Re: Greenhouse Gas Prevention of Significant Deterioration Draft Permit # PSD-WY-000001-2011.001

Dear Ms. Lathrop:

The U.S. Environmental Protection Agency (EPA), Region 8, has completed its initial review of Black Hills Corporation/Cheyenne Light Fuel & Power's permit application dated September 23, 2011, for a Greenhouse Gas (GHG) Prevention of Significant Deterioration (PSD) permit to allow construction and operation of a new 220 MW natural gas fired combustion turbine electric generating utility to be known as the Cheyenne Prairie Generating Station.

Enclosed is the draft PSD permit and corresponding Statement of Basis, along with a copy of the public notice, permit application and related correspondence (including two letters dated November 22, 2011, and May 3, 2012). Please make this information available to the public until the close of business on June 21, 2012. These documents are also available on EPA's website at: <a href="http://www.epa.gov/region8/pubnotice.html">http://www.epa.gov/region8/pubnotice.html</a>, under the heading "Region 8 Air Permitting comment opportunities" within the "PSD Permits" heading.

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Sincerely,

Carl Daly, Director Air Program



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### <u>CERTIFIED MAIL</u> <u>RETURN RECEIPT REQUESTED</u>

Mr. Gus Lopez Health Department Director Cheyenne-Laramie County Health Department 100 Central Ave. Cheyenne, WY 82007

> Re: Greenhouse Gas Prevention of Significant Deterioration Draft Permit # PSD-WY-000001-2011.001

Dear Mr. Lopez:

The U.S. Environmental Protection Agency (EPA), Region 8, has completed its initial review of Black Hills Corporation/Cheyenne Light Fuel & Power's permit application dated September 23, 2011, for a Greenhouse Gas (GHG) Prevention of Significant Deterioration (PSD) permit to allow construction and operation of a new 220 MW natural gas fired combustion turbine electric generating utility to be known as the Cheyenne Prairie Generating Station.

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If you have any questions concerning the enclosed materials, you may contact Mr. Razzazian at (303) 312-6648.

Sincerely,

Carl Daly, Director Air Program



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### <u>CERTIFIED MAIL</u> <u>RETURN RECEIPT REQUESTED</u>

Honorable Richard L. Kaysen Mayor of Cheyenne 2101 O'Neil Ave. Room 310 Cheyenne, WY 82001

> Re: Greenhouse Gas Prevention of Significant Deterioration Draft Permit # PSD-WY-000001-2011.001

Dear Honorable Kaysen:

The U.S. Environmental Protection Agency (EPA), Region 8, has completed its initial review of Black Hills Corporation/Cheyenne Light Fuel & Power's permit application dated September 23, 2011, for a Greenhouse Gas (GHG) Prevention of Significant Deterioration (PSD) permit to allow construction and operation of a new 220 MW natural gas fired combustion turbine electric generating utility to be known as the Cheyenne Prairie Generating Station.

Enclosed is the draft PSD permit and corresponding Statement of Basis, along with a copy of the public notice. A copy of these materials (in addition to the PSD application submitted to the EPA) are also being sent to the Laramie County Clerk's office. These documents are also available on EPA's website at: <u>http://www.epa.gov/region8/pubnotice.html</u>, under the heading "Region 8 Air Permitting comment opportunities" within the "PSD Permits" heading.

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Sincerely,

Carl Daly, Director Air Program



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#### <u>CERTIFIED MAIL</u> <u>RETURN RECEIPT REQUESTED</u>

Mr. Clark Smith Permit Section Supervisor Nebraska Department of Environmental Quality 1200 N. Street, Suite 400 Lincoln, NE 68508-8922

Re: Greenhouse Gas Prevention of Significant Deterioration Draft Permit # PSD-WY-000001-2011.001

Dear Mr. Smith:

The U.S. Environmental Protection Agency (EPA), Region 8, has completed its initial review of Black Hills Corporation/Cheyenne Light Fuel & Power's permit application dated September 23, 2011, for a Greenhouse Gas (GHG) Prevention of Significant Deterioration (PSD) permit to allow construction and operation of a new 220 MW natural gas fired combustion turbine electric generating utility to be known as the Cheyenne Prairie Generating Station.

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A copy of the administrative record for the draft permit, which consists of the draft permit, the draft Statement of Basis, the permit application and addendums, all data submitted by the permit applicant, and all permit-related correspondence, is available for public inspection through June 21, 2012, at the Region 8 office Monday through Friday, from 8:00 a.m. to 4:00 p.m. (excluding federal holidays).

The public notice will be published in the <u>Wyoming Tribune Eagle</u> on Monday, May 21, 2012. The public comment period will end on June 21, 2012, at 8:30 p.m. All written or emailed comments submitted by the close of the public comment period will be considered by the EPA in making its final permit decision. Please refer to the enclosed copy of the public notice for details on the public comment period.

The Wyoming Department of Environmental Quality (WDEQ) will issue a draft PSD permit for PSD pollutants other than GHGs for this facility. The WDEQ will conduct a public comment period concurrent with the EPA's for its draft PSD permit.

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Sincerely,

Carl Daly, Director Air Program



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### <u>CERTIFIED MAIL</u> <u>RETURN RECEIPT REQUESTED</u>

Ms. Susan Johnson, Chief Policy, Planning and Permit Review Air Resources Division National Park Service 12795 W. Alameda Pkwy. Lakewood, CO 80228

> Re: Greenhouse Gas Prevention of Significant Deterioration Draft Permit # PSD-WY-000001-2011.001

Dear Ms. Johnson:

The U.S. Environmental Protection Agency (EPA), Region 8, has completed its initial review of Black Hills Corporation/Cheyenne Light Fuel & Power's permit application dated September 23, 2011, for a Greenhouse Gas (GHG) Prevention of Significant Deterioration (PSD) permit to allow construction and operation of a new 220 MW natural gas fired combustion turbine electric generating utility to be known as the Cheyenne Prairie Generating Station.

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Christopher Razzazian - Permit Contact U.S. EPA, Region 8 Air Program (8P-AR) 1595 Wynkoop Street Denver, Colorado 80202-1129

If you have any questions concerning the enclosed materials, you may contact Mr. Razzazian at (303) 312-6648.

Sincerely,

Carl Daly, Director Air Program



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#### <u>CERTIFIED MAIL</u> <u>RETURN RECEIPT REQUESTED</u>

Richard L. Currit Senior Archaeologist Wyoming State Historic Preservation Office 2301 Central Ave., Barrett Bldg. 3rd Floor Cheyenne, WY 82002

> Re: Greenhouse Gas Prevention of Significant Deterioration Draft Permit # PSD-WY-000001-2011.001

Dear Mr. Currit:

The U.S. Environmental Protection Agency (EPA), Region 8, has completed its initial review of Black Hills Corporation/Cheyenne Light Fuel & Power's permit application dated September 23, 2011, for a Greenhouse Gas (GHG) Prevention of Significant Deterioration (PSD) permit to allow construction and operation of a new 220 MW natural gas fired combustion turbine electric generating utility to be known as the Cheyenne Prairie Generating Station.

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Christopher Razzazian - Permit Contact U.S. EPA, Region 8 Air Program (8P-AR) 1595 Wynkoop Street Denver, Colorado 80202-1129

Additionally, we will be requesting your written concurrence, by separate letter, on our analysis and conclusions with regard to the National Historic Preservation Act. We wish to thank you for working with us through this process. If you have any questions concerning the enclosed materials, you may contact Mr. Razzazian at (303) 312-6648.

Sincerely,

Carl Daly, Director Air Program



Ref: 8P-AR

### <u>CERTIFIED MAIL</u> <u>RETURN RECEIPT REQUESTED</u>

Sandra V. Silva Chief, Branch of Air Quality U.S. Fish & Wildlife Service 7333 W. Jefferson Ave., Suite 375 Lakewood, CO 80235

> Re: Greenhouse Gas Prevention of Significant Deterioration Draft Permit # PSD-WY-000001-2011.001

Dear Ms. Silva:

The U.S. Environmental Protection Agency (EPA), Region 8, has completed its initial review of Black Hills Corporation/Cheyenne Light Fuel & Power's permit application dated September 23, 2011, for a Greenhouse Gas (GHG) Prevention of Significant Deterioration (PSD) permit to allow construction and operation of a new 220 MW natural gas fired combustion turbine electric generating utility to be known as the Cheyenne Prairie Generating Station.

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Christopher Razzazian - Permit Contact U.S. EPA, Region 8 Air Program (8P-AR) 1595 Wynkoop Street Denver, Colorado 80202-1129

We wish to thank Julie Proell of your Cheyenne field office staff for working with us through this process. If you have any questions concerning the enclosed materials, you may contact Mr. Razzazian at (303) 312-6648.

Sincerely,

Carl Daly, Director Air Program



Ref: 8P-AR

#### <u>CERTIFIED MAIL</u> <u>RETURN RECEIPT REQUESTED</u>

Jeff Sorkin Air Program Manager USDA Forest Service Rocky Mountain Region 740 Simms Street Golden, CO 80401

> Re: Greenhouse Gas Prevention of Significant Deterioration Draft Permit # PSD-WY-000001-2011.001

Dear Mr. Sorkin:

The U.S. Environmental Protection Agency (EPA), Region 8, has completed its initial review of Black Hills Corporation/Cheyenne Light Fuel & Power's permit application dated September 23, 2011, for a Greenhouse Gas (GHG) Prevention of Significant Deterioration (PSD) permit to allow construction and operation of a new 220 MW natural gas fired combustion turbine electric generating utility to be known as the Cheyenne Prairie Generating Station.

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Sincerely,

Carl Daly, Director Air Program



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### <u>CERTIFIED MAIL</u> <u>RETURN RECEIPT REQUESTED</u>

Mr. Steven A. Dietrich Air Quality Administrator Air Quality Division Wyoming Department of Environmental Quality Herscher Building 122 West 25th Street Cheyenne, WY 82002

> Re: Greenhouse Gas Prevention of Significant Deterioration Draft Permit # PSD-WY-000001-2011.001

Dear Mr. Dietrich:

The U.S. Environmental Protection Agency (EPA), Region 8, has completed its initial review of Black Hills Corporation/Cheyenne Light Fuel & Power's permit application dated September 23, 2011, for a Greenhouse Gas (GHG) Prevention of Significant Deterioration (PSD) permit to allow construction and operation of a new 220 MW natural gas fired combustion turbine electric generating utility to be known as the Cheyenne Prairie Generating Station.

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If you have any questions concerning the enclosed materials, you may contact Mr. Razzazian at (303) 312-6648.

Sincerely,

Carl Daly, Director Air Program

Page	:	1 of 5 05/11/2012 12:53:03	Ad Number	:	57781637
			Ad Key	:	
Order Number	:	53765747	Salesperson	:	LGL - Nicki Romero
PO Number	:		Publication	:	Wyoming Tribune-Eagle
Customer	:	USEPAREG U.S. EPA REGION 8	Section	:	CLASSIFIED
Contact	:		Sub Section	:	CLASSIFIED
Address1	:	999 18TH ST	Category	:	800 Legal Notices
Address2	:	T&MS FIN MGMT PROGRAM	Dates Run	:	05/21/2012-05/21/2012
City St Zip	:	DENVER CO 80202	Days	:	1
Phone	:	(303) 312-7089	Size	:	1 x 23.38, 241 lines
Fax	:	(303) 294-1199	Words	:	971
Credit Card	:		Ad Rate	:	Open2009
Printed By	:	1F	Ad Price	:	312.36
Entered By	:	1F	Amount Paid	:	0.00
			Amount Due	:	312.36
Keywords	:	PUBLIC NOTICE OF A DRAFT PERMI	T WHICH REGULATES T	Η	
Notes	:				
Zones	:				

#### PUBLIC NOTICE OF A DRAFT PERMIT WHICH **REGULATES THE EMISSIONS** OF AIR POLLUTANTS The Region 8 office of the United States Environmental Protection Agency (EPA) is hereby providing opportunity through June 21, 2012, 8:30pm, for public comment on a draft permit which would grant conditional approval, under Title I, Parts A and C, of the Federal Clean Air Act, as amended, and under Federal Prevention of Significant Deterioration of Air Quality (PSD) permitting rules at 40 CFR 52.21, to the following permit applicant, to construct a new facility: Cheyenne Light, Fuel & Power (Black Hills Corporation) **Cheyenne Prairie Generating** Station Section 1, Township 13 North, Range 66 West Latitude: 41º 07' 27.83" North Longitude: 104º 43' 13.34" West Cheyenne, Laramie County, Wyoming **Corporate Address: Black Hills Corporation** P.O. Box 1400 625 Ninth Street Rapid City, South Dakota 57709 The proposed facility will be a nominal 220 MW gross electric generating utility, to be located approximately 7 miles east of Interstate-25 in Cheyenne, Wyoming. Pursuant to a national Federal Implementation Plan (FIP), EPA is the PSD permitting authority for greenhouse gases (GHGs) in Wyoming. Pursuant to the Wyoming State Implementation Plan (SIP), the Wyoming Department of Environmental Quality

(WDEQ) is the permitting authority implementing PSD requirements for all other regulated New Source Review :

			Ad Number Ad Key	:	57781637
Order Number	:	53765747	Salesperson	:	LGL - Nicki Romero
PO Number	:		Publication	:	Wyoming Tribune-Eagle
Customer	:	USEPAREG U.S. EPA REGION 8	Section	:	CLASSIFIED
Contact	:		Sub Section	:	CLASSIFIED
Address1	:	999 18TH ST	Category	:	800 Legal Notices
Address2	:	T&MS FIN MGMT PROGRAM	Dates Run	:	05/21/2012-05/21/2012
City St Zip	:	DENVER CO 80202	Days	:	1
Phone	:	(303) 312-7089	Size	:	1 x 23.38, 241 lines
Fax	:	(303) 294-1199	Words	:	971
Credit Card	:		Ad Rate	:	Open2009
Printed By	:	1F	Ad Price	:	312.36
Entered By	:	1F	Amount Paid	:	0.00
			Amount Due	:	312.36
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Notes	:				

Zones

(NSR) pollutants. Therefore, EPA will issue a PSD permit which covers only GHGs and WDEQ will issue a separate PSD permit covering all other NSR pollutants. The proposed generating station would consist of five 40 MW natural gas fired combustion turbines. Three turbines will be operated in simple cycle mode, while the remaining two will operate in combined cycle mode (powering a single steam turbine). Additional equipment will include six natural gas fired inlet air heaters, two natural gas fired fuel heaters, one diesel emergency generator, one diesel fire pump, one wet cooling tower, and three electric chillers (each with a cooling tower). Energy efficiency is proposed to minimize the emissions of GHGs. Potential GHG emissions from the proposed generating station, on a mass basis, are estimated at 962,929 tons per year of carbon dioxide, 34.25 tons per year of methane, 1.86 tons per year of nitrous oxide and 5.4 pounds per year of sulfur hexafluoride. The combined GHG emissions, taking into account global warming potentials for each pollutant, is estimated to be 964,289 tons per year of carbon dioxide equivalent. No emissions of the remaining two GHG pollutants, hydrofluorocarbons (HFCs), and perfluorocarbons (PFCs), are anticipated from this source. A copy of the administrative record for the draft permit,

which consists of the draft permit, the draft Statement of Basis, the permit application and addendums, all data submitted by the permit applicant, and all permit-related correspondence, is available for public inspection between 8:30 am and 4:00 pm Mountain Standard Time, through June

Page	:	3 of 5 05	/11/2012 12:53:03	Ad Number	:	57781637
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Contact	:			Sub Section	:	CLASSIFIED
Address1	:	999 18TH ST		Category	:	800 Legal Notices
Address2	:	T&MS FIN M	GMT PROGRAM	Dates Run	:	05/21/2012-05/21/2012
City St Zip	:	DENVER CO	80202	Days	:	1
Phone	:	(303) 312-708	89	Size	:	1 x 23.38, 241 lines
Fax	:	(303) 294-119	99	Words	:	971
Credit Card	:			Ad Rate	:	Open2009
Printed By	:	1F		Ad Price	:	312.36
Entered By	:	1F		Amount Paid	:	0.00
				Amount Due	:	312.36
Keywords	:	PUBLIC NOT	ICE OF A DRAFT PERMIT W	HICH REGULATES	TH	
Notes	:					
Zones	:					

21, 2012, at:		
US EPA Region 8		
Air Program Office (8P-AR)		
1595 Wynkoop Street		
Denver, Colorado 80202-1129		
Permit Contact:		
Christopher Razzazian		
email:		
razzazian.christopher@epa.gov		
phone: 303-312-6648		
toll-free: 800-227-8917		
fax: 303-312-6064		
All documents will be availa-		
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Region 8 office on Monday		
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Chevenne Wyoming A conv		
of the draft permit and draft		
Statement of Basis is also		
available on FPA website at		
http://www.ena.gov/region8		
/nubnotice html under the		
heading "Region 8 Air Per-		
mitting comment opportuni-		
ties" within the "PSD Per-		
mits" heading		
In accordance with 40 CEP		
52 21(a) Public participa-		
tion any interested person		
may submit written or		
amailed comments on the		
draft permit during the pub-		
lic comment period and may		
request a public bearing A		
public hearing will be held		
for this action on lune 21		
2012 from 7:30 nm to 8:30 nm		
in the Cottonwood Room of		
the Laramie County Library		
located at 2200 Pioneer Ave-		
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PO Number	:		Publication	:	Wyoming Tribune-Eagle
Customer	:	USEPAREG U.S. EPA REGION 8	Section	:	CLASSIFIED
Contact	:		Sub Section	:	CLASSIFIED
Address1	:	999 18TH ST	Category	:	800 Legal Notices
Address2	:	T&MS FIN MGMT PROGRAM	Dates Run	:	05/21/2012-05/21/2012
City St Zip	:	DENVER CO 80202	Days	:	1
Phone	:	(303) 312-7089	Size	:	1 x 23.38, 241 lines
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desiring to be heard on this matter are hereby notified to appear at the designated time and place. Oral statements will be accepted at the time of the hearing, but for accuracy of the record, written statements are encouraged and will be accepted at the time of the hearing or prior thereto. Since the EPA is not the permitting authority for the remainder of the NSR pollutants there will be a hearing held prior to the EPA GHG permit from 6:00 pm to 7:00 pm at the aforementioned date and location regarding the WDEQ draft PSD permit. All comments regarding pollutants other than GHGs from the proposed facility must be submitted to the WDEQ, which is running a concurrent public notice for this facility.

All written and emailed comments received before the close of the public hearing will be considered as well as all verbal comments received during the public hearing. All comments, written and emailed, should be addressed to the Permit Contact at the US EPA Region 8 address or email address listed above.

In accordance with 40 CFR 124.15, Issuance and effective date of permit, the permit shall become effective immediately upon issuance as a final permit, if no comments request a change in the draft permit. If changes are requested, the permit shall become effective thirty days after issuance of a final permit decision, unless review is requested on the permit under 40 CFR 124.19. Notice of the final permit decision shall be provided to the permit applicant and to each person who submitted written comments or requested notice of the final permit decision.

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Credit Card	:			Ad Rate	:	Open2009
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May 21, 2012

#### PUBLIC NOTICE OF A DRAFT PERMIT WHICH REGULATES THE EMISSIONS OF AIR POLLUTANTS

The Region 8 office of the United States Environmental Protection Agency (EPA) is hereby providing opportunity through June 21, 2012, 8:30pm, for public comment on a draft permit which would grant conditional approval, under Title I, Parts A and C, of the Federal Clean Air Act, as amended, and under Federal Prevention of Significant Deterioration of Air Quality (PSD) permitting rules at 40 CFR 52.21, to the following permit applicant, to construct a new facility:

Cheyenne Light, Fuel & Power (Black Hills Corporation) Cheyenne Prairie Generating Station Section 1, Township 13 North, Range 66 West Latitude: 41° 07' 27.83" North Longitude: 104° 43' 13.34" West Cheyenne, Laramie County, Wyoming

> Corporate Address: Black Hills Corporation P.O. Box 1400 625 Ninth Street Rapid City, South Dakota 57709

The proposed facility will be a nominal 220 MW gross electric generating utility, to be located approximately 7 miles east of Interstate-25 in Cheyenne, Wyoming. Pursuant to a national Federal Implementation Plan (FIP), EPA is the PSD permitting authority for greenhouse gases (GHGs) in Wyoming. Pursuant to the Wyoming State Implementation Plan (SIP), the Wyoming Department of Environmental Quality (WDEQ) is the permitting authority implementing PSD requirements for all other regulated New Source Review (NSR) pollutants. Therefore, EPA will issue a PSD permit which covers only GHGs and WDEQ will issue a separate PSD permit covering all other NSR pollutants.

The proposed generating station would consist of five 40 MW natural gas fired combustion turbines. Three turbines will be operated in simple cycle mode, while the remaining two will operate in combined cycle mode (powering a single steam turbine). Additional equipment will include six natural gas fired inlet air heaters, two natural gas fired fuel heaters, one diesel emergency generator, one diesel fire pump, one wet cooling tower, and three electric chillers (each with a cooling tower). Energy efficiency is proposed to minimize the emissions of GHGs. Potential GHG emissions from the proposed generating station, on a mass basis, are estimated at 962,929 tons per year of carbon dioxide, 34.25 tons per year of methane, 1.86 tons per year of nitrous oxide and 5.4 pounds per year of sulfur hexafluoride. The combined GHG emissions, taking into account global warming potentials for each pollutant, is estimated to be 964,289 tons per year of carbon dioxide equivalent. No emissions of the remaining two GHG pollutants, hydrofluorocarbons (HFCs), and perfluorocarbons (PFCs), are anticipated from this source.

A copy of the administrative record for the draft permit, which consists of the draft permit, the draft Statement of Basis, the permit application and addendums, all data submitted by the permit applicant, and all permit-related correspondence, is available for public inspection through June 21, 2012, at:

US EPA Region 8 Air Program Office (8P-AR) 1595 Wynkoop Street Denver, Colorado 80202-1129 Permit Contact: Christopher Razzazian email: razzazian.christopher@epa.gov phone: 303-312-6648 toll-free: 800-227-8917 fax: 303-312-6064

All documents will be available for review at the U.S. EPA Region 8 office on Monday through Friday, from 8:00 a.m. to 4:00 p.m. (excluding federal holidays). A copy of the draft permit, draft Statement of Basis, and permit application is also available for public inspection at the Laramie County Clerk's Office in Cheyenne, Wyoming. These documents are also available on EPA's website at: <u>http://www.epa.gov/region8/pubnotice.html</u>, under the heading "Region 8 Air Permitting comment opportunities" within the "PSD Permits" heading.

In accordance with 40 CFR 52.21(q), Public participation, any interested person may submit written or emailed comments on the draft permit during the public comment period and may request a public hearing. A public hearing will be held for this action on June 21, 2012 from 7:00 pm to 8:30 pm in the Cottonwood Room of the Laramie County Library located at 2200 Pioneer Avenue, Cheyenne, WY 82001. The purpose of the hearing is to gather comments concerning the issuance of the EPA GHG PSD permit. The scope of the hearing will be limited to such issues in order for the EPA to determine whether or not the applicable PSD Regulations have been appropriately applied to the construction and operation of the proposed generating station. All persons desiring to be heard on this matter are hereby notified to appear at the designated time and place. Oral statements will be accepted at the time of the hearing, but for accuracy of the record, written statements are encouraged and will be accepted at the time of the hearing or prior thereto. Since the EPA is not the permitting authority for the remainder of the NSR pollutants there will be a hearing held prior to the EPA GHG permit from 5:30 pm to 7:00 pm at the aforementioned date and location regarding the WDEQ draft PSD permit. All comments regarding pollutants other than GHGs from the proposed facility must be submitted to the WDEQ, which is running a concurrent public notice for this facility.

All written and emailed comments received before the close of the public hearing will be considered as well as all verbal comments received during the public hearing. All comments, written and emailed, should be addressed to the Permit Contact at the US EPA Region 8 address or email address listed above.

In accordance with 40 CFR 124.15, *Issuance and effective date of permit*, the permit shall become effective immediately upon issuance as a final permit, if no comments request a change

in the draft permit. If changes are requested, the permit shall become effective thirty days after issuance of a final permit decision, unless review is requested on the permit under 40 CFR 124.19. Notice of the final permit decision shall be provided to the permit applicant and to each person who submitted written comments or requested notice of the final permit decision.



# United States Department of the Interior

FISH AND WILDLIFE SERVICE



Ecological Services 5353 Yellowstone Road, Suite 308A Cheyenne, Wyoming 82009

In Reply Refer To: ES-61411/WY11SL0365

Christopher Razzazian, Mechanical/Environmental Engineer U.S. EPA Region 8 Air Program 80C-EISC 1595 Wynkoop Street Denver, CO 80202-1129 RECEIVE N SEP 19 2011

SEP 1 3 2011

Dear Mr. Razzazian:

Thank you for your email dated August 11, 2011, regarding the proposed Cheyenne Generating Station (CGS) to be located in T13N, R66W, Section 1, in Cheyenne, Laramie County, Wyoming. We understand that a permit from the U.S. Environmental Protection Agency has been requested by the project proponent, Cheyenne Light, Fuel, and Power, a subsidiary of Black Hills Power, for the proposed project activity. The purpose of the proposed CGS is to produce electricity for the City of Cheyenne and Black Hills Power areas in Wyoming and South Dakota. The proposed project includes the installation of five 40-mega-watt natural gas combustion turbine generators (CTGs) along with associated towers, heaters, emergency generator, and infrastructure including electrical transmission lines, natural gas pipelines, and wastewater pipelines. Current land use in the area is undeveloped grassland bounded by a wastewater treatment plant, Interstate 80, and ranchland.

You have requested information regarding species listed under the Endangered Species Act of 1973, as amended (Act), 16 U.S.C. 1531 *et seq.* In response to your request, the U.S. Fish and Wildlife Service (Service) is providing you with recommendations for protective measures for threatened and endangered species in accordance with the Act. We are also providing recommendations concerning migratory birds in accordance with the Migratory Bird Treaty Act (MBTA), 16 U.S.C. 703, and the Bald and Golden Eagle Protection Act (BGEPA), 16 U.S.C. 668. Wetlands are afforded protection under Executive Orders 11990 (wetland protection) and 11988 (floodplain management), as well as section 404 of the Clean Water Act. Other fish and wildlife resources are considered under the Fish and Wildlife Coordination Act, as amended, 16 U.S.C. 661 *et seq.*, and the Fish and Wildlife Act of 1956, as amended, 16 U.S.C. 742a-742j.

In accordance with Section 7(c) of the Act, we have determined that the following species or their designated habitat may be present in the proposed CGS project area. We would appreciate

receiving information as to the current status of each of these species within the proposed project area.

<b>Species/Critical Habitat</b>	Scientific Name	<u>Status</u>	<u>Habitat</u>
Preble's Meadow	Zapus hudsonius	Threatened	Heavily vegetated
Jumping Mouse	preblei		streamside areas and in
			adjacent grassland cover
Colorado Butterfly Plant	Gaura neomexicana	Threatened	Wet meadows and riparian
	coloradensis		areas
Colorado Butterfly Plant Critical Habitat	Designated for Colora and riparian areas with Wyoming (see 50 CFF	ado butterfly pla nin Laramie and R 17.96(a))	ant in specific wet meadows l Platte Counties of
Ute Ladies'-tresses	Spiranthes diluvialis	Threatened	Seasonally moist soils and wet meadows of drainages below 7,000 ft. elevation

Proposed Critical Habitat that may be in the proposed Project Arc	Listed, Proposed, Candidate Species and their Designated and	
rioposed eritiedi ridsitat that may se in the proposed riojeet in	posed Critical Habitat that may be in the proposed Project A	ea

**Preble's meadow jumping mouse:** In 2008, the Service removed ESA protection for the Preble's meadow jumping mouse (*Zapus hudsonius preblei*) (Preble's) in Wyoming but continued them in Colorado, based on an interpretation of the law that allowed the agency to apply ESA protections to those portions of a species' range where the Service believed it was most threatened, rather than in all the places where it is found. On August 6, 2011, the Service relisted the Preble's in order to comply with a requested court order. Preble's populations throughout the species' range in Colorado and Wyoming will be federally protected, with a special rule in place to allow rodent control, agricultural operations, landscape maintenance, noxious weed control, ditch maintenance, and other specified activities to occur provided they are conducted in accordance with the requirements of the special rule.

Preble's is a small rodent in the Zapodidae family and is 1 of 12 recognized subspecies of the species *Z. hudsonius*, the meadow jumping mouse. Preble's are 7 to 10-inches in length including a 4 to 6-inch bicolor tail, large hind feet adapted for jumping, and a distinct dark stripe down the middle of its back that is bordered on either side by gray to orange-brown fur. The diet of the Preble's consists of seeds, fruits, fungi, and insects. Preble's are primarily nocturnal or crepuscular, but have been observed during daylight. Hibernation occurs from October to May in small underground burrows the mouse excavates several centimeters underground.

Preble's exhibits a preference for lush vegetation along watercourses or herbaceous understories in wooded areas with close proximity to water. They occur in low undergrowth consisting of grasses, forbs, or a mix of both; in wet meadows and riparian corridors; or where tall shrubs and low trees provide adequate cover. Additionally, Preble's have been documented to use uplands at least as far out as 330 feet beyond the 100-year floodplain. In Wyoming, Preble's has been documented in Albany, Laramie, Platte and Converse Counties, and may occur in Goshen County. If a proposed project will result in a disturbance to suitable habitat within any of these five counties, surveys should be conducted prior to any action. Due to the difficulty in identifying the Preble's, surveys should be conducted by knowledgeable biologists trained in conducting these surveys.

Colorado Butterfly Plant: The Colorado butterfly plant (Gaura neomexicana coloradensis) is a perennial herb endemic to moist soils in wet meadows of flood plain areas. This plant occurs in southeastern Wyoming, north-central Colorado, and extreme western Nebraska between elevations of 5,000 and 6,400 feet. These plants are often found in low depressions or along bends in wide meandering stream channels a short distance upslope of the actual channel. Threats to the plant include non-selective herbicide spraying, having and mowing schedules that inhibit the setting of seed, land conversion for cultivation, and competition from noxious weeds. Low numbers and limited distribution contribute to the plant's vulnerability. Surveys should be conducted during flowering season, which normally occurs in July and August. Temporal variability in the flowering period exists from site to site and from year to year depending on annual climatic conditions. Surveys should be conducted by knowledgeable botanists trained in conducting rare plant surveys. The Service does not maintain a list of "qualified" surveyors but can refer those wishing to become familiar with the Colorado butterfly plant to experts who can provide training/services. Critical habitat is designated for Colorado butterfly plant in specific wet meadows and riparian areas within Laramie and Platte Counties of Wyoming (see 50 CFR 17.96(a)).

Ute Ladies'-tresses: Ute ladies'-tresses (Spiranthes diluvialis) is a perennial, terrestrial orchid, 8 to 20 inches tall, with white or ivory flowers clustered into a spike arrangement at the top of the stem. Ute ladies'-tresses typically blooms from late July through August; however, depending on location and climatic conditions, it may bloom in early July or still be in flower as late as early October. Ute ladies'-tresses is endemic to moist soils near wetland meadows, springs, lakes, and perennial streams where it colonizes early successional point bars or sandy edges. The elevation range of known occurrences is 4,200 to 7,000 feet (although no known populations in Wyoming occur above 5,500 feet) in alluvial substrates along riparian edges, gravel bars, old oxbows, and moist to wet meadows. Soils where Ute ladies'-tresses have been found typically range from fine silt/sand, to gravels and cobbles, as well as to highly organic and peaty soil types. Ute ladies'-tresses is not found in heavy or tight clay soils or in extremely saline or alkaline soils. Ute ladies'-tresses seems intolerant of shade and small scattered groups are found primarily in areas where vegetation is relatively open. Surveys should be conducted by knowledgeable botanists trained in conducting rare plant surveys. Ute ladies'-tresses is difficult to survey for primarily due to its unpredictability of emergence of flowering parts and subsequent rapid desiccation of specimens. The Service does not maintain a list of "qualified" surveyors but can refer those wishing to become familiar with the orchid to experts who can provide training or services.

#### **Species or Resource of Concern**

**Black-tailed Prairie Dog:** The range of the black-tailed prairie dog (*Cynomys ludovicianus*) once spanned the short and mixed grass prairies of North America east of the Rockies from southern Canada to northern Mexico. This species still occurs over much of its historic range, although in more widely scattered large colonies. Black-tailed prairie dogs occur within the eastern third of Wyoming. A population thought to have been intentionally introduced outside of

this range also occurs in the Bighorn Basin. We encourage the conservation of prairie dog colonies for their value to the prairie ecosystem and the many species that rely on them. Threats that may be significant to conserving black-tailed prairie dog populations include disease (sylvatic plague) and some control programs (poisoning). Prairie dogs serve as the primary prey species for the black-footed ferret and several raptors, including the golden eagle (*Aguila chrysaetos*) and ferruginous hawk (*Buteo regalis*). Prairie dog colonies and burrows also provide shelter or nest sites for species like the mountain plover (*Charadrius montanus*) and burrowing owl (*Athene cunicularia*). Because black-tailed prairie dog colonies in Wyoming do not currently support any ferret populations, black-footed ferret surveys are not necessary within Wyoming. However, we do encourage evaluating black-tailed prairie dog colonies for the potential reintroduction of black-footed ferrets.

**Wetlands/Riparian Areas:** Wetlands or riparian areas may be impacted by the proposed project, including Crow Creek and its associated wetlands. Wetlands perform significant ecological functions which include: (1) providing habitat for numerous aquatic and terrestrial wildlife species, (2) aiding in the dispersal of floods, (3) improving water quality through retention and assimilation of pollutants from storm water runoff, and (4) recharging the aquifer. Wetlands also possess aesthetic and recreational values. If wetlands may be destroyed or degraded by the proposed action, those wetlands in the project area should be inventoried and fully described in terms of their functions and values. Acreage of wetlands, by type, should be disclosed and specific actions should be outlined to avoid, minimize, and compensate for all unavoidable wetland impacts.

Riparian or streamside areas are a valuable natural resource and impacts, including discharge of wastewater, to these areas should be avoided whenever possible. Riparian areas are the single most productive wildlife habitat type in North America. They support a greater variety of wildlife than any other habitat. Riparian vegetation plays an important role in protecting streams, reducing erosion and sedimentation as well as improving water quality, maintaining the water table, controlling flooding, and providing shade and cover. In view of their importance and relative scarcity, impacts to riparian areas should be avoided. Any potential, unavoidable encroachment into these areas should be further avoided and minimized. Unavoidable impacts to streams should be assessed in terms of their functions and values, linear feet and vegetation type lost, potential effects on wildlife, and potential effects on bank stability and water quality. Measures to compensate for unavoidable losses of riparian areas should be developed and implemented as part of the project.

Plans for mitigating unavoidable impacts to wetland and riparian areas should include mitigation goals and objectives, methodologies, time frames for implementation, success criteria, and monitoring to determine if the mitigation is successful. The mitigation plan should also include a contingency plan to be implemented should the mitigation not be successful. In addition, wetland restoration, creation, enhancement, and/or preservation does not compensate for loss of stream habitat; streams and wetlands have different functions and provide different habitat values for fish and wildlife resources.

Best Management Practices (BMPs) should be implemented within the project area wherever possible. BMPs include, but are not limited to, the following: installation of sediment and

erosion control devices (*e.g.*, silt fences, hay bales, temporary sediment control basins, erosion control matting); adequate and continued maintenance of sediment and erosion control devices to insure their effectiveness; minimization of the construction disturbance area to further avoid streams, wetlands, and riparian areas; location of equipment staging, fueling, and maintenance areas outside of wetlands, streams, riparian areas, and floodplains; and re-seeding and re-planting of riparian vegetation native to Wyoming in order to stabilize shorelines and streambanks.

#### **Migratory Birds**

**MBTA and BGEPA Prohibitions:** The MBTA, enacted in 1918, prohibits the taking of any migratory birds, their parts, nests, or eggs except as permitted by regulations, and does not require intent to be proven. Section 703 of the MBTA states, "Unless and except as permitted by regulations ... it shall be unlawful at any time, by any means or in any manner, to ... take, capture, kill, attempt to take, capture, or kill, or possess ... any migratory bird, any part, nest, or eggs of any such bird...." The BGEPA prohibits knowingly taking, or taking with wanton disregard for the consequences of an activity, any bald or golden eagles or their body parts, nests, or eggs, which includes collection, molestation, disturbance, or killing.

The term "disturb" under the BGEPA has recently been defined as "to agitate or bother a bald or golden eagle to a degree that causes, or is likely to cause, based on the best scientific information available, (1) injury to an eagle, (2) a decrease in its productivity, by substantially interfering with normal breeding, feeding, or sheltering behavior, or (3) nest abandonment, by substantially interfering with normal breeding, feeding, or sheltering behavior (72 FR 31332)." In addition to immediate impacts, this definition also covers impacts that result from human-induced alterations initiated around a previously used nest site during a time when eagles are not present, if upon the eagle's return, such alterations agitate or bother an eagle to a degree that injures an eagle or substantially interferes with normal breeding, feeding, or sheltering habits and causes, or is likely to cause, a loss of productivity or nest abandonment. Removal or destruction of such nests or causing abandonment of a nest could constitute violation of one or both of the above statutes.

No permits will be issued for an active nest of any migratory bird species, unless removal of an active nest is necessary for reasons of human health and safety. Therefore, if nesting migratory birds are present on or near the project area, timing is a significant consideration and needs to be addressed in project planning. If nest manipulation is proposed for this project, you should contact the Service's Migratory Bird Office in Denver at 303-236-8171 to see if a permit can be issued for this project. If a permit cannot be issued, the project may need to be modified to ensure take of a migratory bird or eagle, young, eggs, or nest will not occur.

Additionally, the Service recommends that the proposed CGS be included within the scope of analysis of the April 5, 2011 Avian Protection Plan (APP) by Black Hills Power to minimize and avoid potential impacts to bird and bat species. Specifically, we recommend that the proposed project comply with Section 5.7: Construction and Modification to Avian-Safe Standards as well as additional practices to prevent birds from utilizing heaters and cooling towers associated with the project.
For our internal tracking purposes, the Service would appreciate notification of any decision made on this project (such as issuance of a permit or signing of a Record of Decision or Decision Memo). Notification can be sent in writing to the letterhead address or by electronic mail to FW6\_Federal\_Activities\_Cheyenne@fws.gov.

We appreciate your efforts to ensure the conservation of Wyoming's fish and wildlife resources. If you have questions regarding this letter or your responsibilities under the Act and/or other authorities or resources described above, please contact Julie Proell of my office at the letterhead address or phone (307) 772-2374, extension 232.

Sincerely,

R. Mark Sattelberg Field Supervisor Wyoming Field Office

cc: WGFD, Non-game Coordinator, Lander, WY (B. Oakleaf) WGFD, Statewide Habitat Protection Coordinator, Cheyenne, WY (M. Flanderka) **Black Hills Corporation (Black Hills)** 

Cheyenne Prairie Generating Station (CPGS), Cheyenne Wyoming

**Endangered Species Impacts Assessment** 

# In Support of USEPA Review of the Cheyenne Prairie Generating Station Greenhouse Gas (GHG) Air Permit Application

May 3, 2012

The following will summarize Black Hills' response to the species of interest and other resource concerns identified by the U.S. Fish and Wildlife Service (USFWS), Cheyenne office in an undated letter from mid-September 2011.

#### **Exhibit A - Study:**

• February 14, 2012 – Evaluation Endangered Species Habitat (Thompson and Johnson, WEST, Inc.)

#### **Exhibit B - Surveys:**

- April 16, 2012 Survey for raptor nests and prairie dog colonies (David Phillips, CH2M HILL, Inc). USFWS will be notified of the results of the survey.
- Planned Survey for June-July 2012 for the Colorado butterfly plant and the Ute ladies'-tresses orchid between the project site and the Crow Creek riparian area to determine presence of these species. Colorado butterfly plant surveys will be completed on the natural gas pipeline corridor at the location where it crosses Porter's Draw.
- Planned survey in the spring of 2013 to assess raptor nesting along Crow Creek to determine course of action.

#### Exhibit C - Black Hills Corporation – Wyoming Avian Protection Plan

**Prebble's Meadow Jumping Mouse (PMJM)**: Black Hills intends to directionally bore underneath Crow Creek and the adjacent riparian habitat and portions of the adjacent upland area thus avoiding the PMJM habitat. The setback distance for the drill angle from the edge of the riparian area is intended to satisfy the USFWS's setback requirements. It is Black Hills' assessment that any impact to the potential PMJM habitat and the PMJM, if present, will be avoided.

**Colorado Butterfly Plant (CBP)**: Black Hills intends to directionally bore underneath Crow Creek thus avoiding any potential CBP habitat. It is Black Hills' assessment that any impact to the potential CBP habitat and the CBP, if present, will be avoided in this area. Black Hills will conduct a one-time survey of the facility site to the riparian area and the location where the gas line will cross Porter's Draw to verify the presence or absence of the CBP. If the plant is found, avoidance measures will be taken, otherwise, no impact to the species is expected. USFWS will be notified of the results of the Survey.

**Ute Ladies'-tresses (ULT)**: Black Hills intends to directionally bore underneath Crow Creek thus avoiding the ULT habitat. It is Black Hills assessment that any impact to the ULT habitat and the ULT, if present, will be avoided. Black Hills will conduct a one-time survey of the facility site to the riparian area to verify the presence or absence of the ULT. If the species are found, avoidance measures will be taken. USFWS will be notified of the results of the Survey.

**Black-tailed Prairie Dog:** In a survey completed on April 16, 2012 by CH2M HILL, there were no prairie dogs, colonies, or individual burrows present at or within 500 feet of the project site or the pipeline corridor path. USFWS will be notified of the results of the Survey.

**Wetlands/Riparian Areas on Crow Creek:** Black Hills intends to directionally bore underneath Crow Creek and the adjacent riparian area thus avoiding the wetlands and riparian areas bordering Crow Creek. Black Hills will secure a Storm Water Construction Permit from Wyoming Department of Environmental Quality (WDEQ) and develop a Storm Water Pollution Prevention Plan (SWPPP) implementing Best Management Practices (BMPs) to control storm water run-off during construction. The facility will also have an active Industrial Storm Water Control Permit when operation commences with a SWPPP that requires BMPs.

**Migratory Birds Treaty Act and Bald and Golden Eagle Protection Act**: There are currently five known raptor nests in the project area (see map in April 16, 2012 survey report for location).

- 1. Active Spring of 2012 with red-tailed hawk. Southwest of project area on Crow Creek.
- 2. Active Spring of 2012 with great horned owl. South Southwest of project area on Crow Creek.
- 3. Inactive Spring of 2012. Immediately south of project site unknown raptor.
- 4. Nest confirmed gone Spring 2012 (nest branch broke) unknown raptor.
- 5. Inactive Spring of 2012. Southwest of project area next to nest #1 unknown raptor.
- 6. Inactive Spring of 2012. Northwest of project area across I-80 unknown raptor.

	Distance to Project fence-line (ft)	Distance to Plant (miles)	Elevation (ft asl)	Elevation Relative to Plant (plant average 5,950 ft asl)
Nest 1	2,060	0.39	5,927	-23
Nest 2	2,570	0.49	5,918	-32
Nest 3	1,905	0.36	5,915	-35
Nest 4	na	na	na	Na
Nest 5	2,060	0.39	5,927	-23
Nest 6	4,420	0.84	5,985	+35

#### **Project Construction Schedule**

Start Site Construction – April 1, 2013 (14-month duration) Gas-line Construction – winter 2013 (4-month duration) Commercial Operation (end of construction) – June 1, 2014

Black Hills will take the following measures to minimize impacts to raptors during nesting season in the immediate area (Crow Creek riparian area):

- 1. Avoid disturbance of any active raptor nests during nesting season by staying outside of the recommended disturbance buffer as identified by USFWS guidelines for the given species nesting
- 2. If work must occur within the avoidance buffer of the nest, confirm through survey that bird(s) have fledged the nest , or
- 3. If work must occur within the avoidance buffer of the nest, confirm through survey that the nest is inactive.

Black Hills will take the following measures to minimize impacts to migratory birds during nesting season in the immediate area in the pipeline corridor extending from the project site to the interconnection with the main gas line near the Wyoming/Colorado border, if there is a need to use the measure.

- 1. Employ ground preparation practices to discourage ground nesting at the project site and natural gas line corridor. This could involve mowing or tilling prior to nesting season or documenting the absence of nesting birds where disturbance will occur.
- 2. Avoiding the nesting seasons, or
- 3. Abiding by USFWS construction setback distance recommendations during the pipeline construction.

**Avian Protection Plan (Exhibit C):** In cooperation with the USFWS, Black Hills has developed an Avian Protection Plan for all Wyoming operations. The plan requires avian protection measures for new electrical line construction. Those measures will be employed for the applicable components of the project (e.g., substation, transmission line).

#### **Other Environmental related issues:**

**Industrial Surface Water Discharge to Dry Creek or Crow Creek**: There will be no industrial wastewater discharge to Dry Creek or Crow Creek. Black Hills will discharge wastewater directly to the Dry Creek Wastewater Facility adjacent to the plant through a sewer line.

**Storm Water Discharge:** Black Hills will secure Construction Storm Water Permit for construction activities and an Industrial Storm Water Permit for commercial activity after construction is completed. The permits will have associated Storm Water Pollution Prevention Plans that will require the implementation of Best Management Practices.

**Septic System:** There will be no septic system. Black Hills will discharge sanitary waste directly to the Dry Creek Wastewater Facility adjacent to the plant.

# **Raptor Nest and Prairie Dog Colony Survey -Cheyenne Prairie Generating Station Project**

TO: Black Hills Corporation

FROM: David Phillips, Senior Biologist, CH2M HILL Engineers, Inc.

DATE: April 19, 2012

CH2M HILL Engineers, Inc. (CH2M HILL) completed a survey to identify black-tailed prairie dog colonies (*Cynomys ludovicianus*) and raptor nests that could be potentially affected by construction of the Cheyenne Prairie Generating Station (CPGS) ("facility") and associated natural gas pipeline ("pipeline"), collectively referred to as the Project, proposed by Black Hills Corporation. Raptor nest surveys were completed within 1 mile, and prairie dog surveys were completed within 500 feet, of planned construction activity for the Project.

## **Project Description**

The facility site is located in Laramie County, Wyoming, approximately 5 miles east of downtown Cheyenne, and within the city limits. The facility would occupy approximately 30 acres within a 250-acre parcel located adjacent to and south of Interstate 80 (I-80). The parcel is located just west of the Dry Creek Wastewater Treatment Plant. Elevation at the facility is approximately 5,950 feet above mean sea level (amsl); the pipeline ranges from 5,950 to 6,200 feet amsl. Approximately 1.75 miles of 115-kilovolt (kV) transmission line will be installed to connect the facility to the grid at a point east of the facility. The Project would be supplied by an approximately 9-mile natural gas pipeline originating at a metering station in southern Laramie County and terminating at the Project site. The majority of the pipeline is outside the Cheyenne City limits and located on private and state lands within Laramie County. Figure 1 displays the Project location.

#### **Methods**

#### **Raptor Nest Survey**

A survey to determine presence or absence of raptor nests were completed on April 16, 2012, by visually inspecting all potential raptor nesting habitat within 1 mile of the Project. Potential nesting habitat included trees (and tree cavities if present or detectable), large shrubs, rock outcrops, cliffs, ridges, knolls, and artificial nest structures such as transmission towers, windmills, and other human structures. Additionally, raptors detected during the survey were observed to determine if behavior indicated any association with potential nest sites (e.g., courtship or defensive behavior, stick delivery). For all nests detected, location, status, condition, substrate, height, and photographs were recorded. Locations were recorded in the field using a Garmin eTrex Legend HCx Global Positioning System (GPS) unit. Nests were considered active if adult raptors were observed. The raptor nest survey area included 15,447 acres (24.1 square miles).

#### **Prairie Dog Survey**

Surveys to determine the presence or absence of black-tailed prairie dog colonies were completed by visually inspecting the ground within 500 feet of the Project. If prairie dog colonies or individual burrows were identified, the location and status was recorded. Colonies were reported as active if prairie dogs or recent sign (droppings, digging) were evident. The prairie dog survey area included 1,634 acres (2.6 square miles).

The surveys were completed by Dave Phillips, Senior Biologist, CH2M HILL. Mr. Phillips is a Certified Wildlife Biologist by The Wildlife Society with extensive experience surveying for wildlife species in this region, including

but not limited to raptors and prairie dogs. He has implemented large scale survey and habitat mapping efforts for special-status wildlife in Wyoming, Colorado, Montana, Idaho, Utah, and California since 2005.

# Results

#### **Raptor Nest Survey**

The raptor nest survey was completed between 0830-1700 hrs on April 16, 2012. All potential nesting habitat within 1 mile of the proposed project was directly accessible with the exception of a portion of the pipeline corridor for which access permission could not be obtained (Figure 2). Due to the topography of this inaccessible area and the presence of a public road bisecting the northern portion of this private parcel, the area was able to be evaluated completely for the presence or absence of nesting raptors using binoculars.

Five raptor nests (2 active and 3 inactive) were detected during the survey and are shown on Figure 2 and Table 1. One additional nest documented in fall 2011 (Nest 4 in Table 1 and Figure 2) was no longer present as its supporting branch had broken off since last evaluated. All nests recorded during the survey are presented in Figure 2.

#### TABLE 1

#### Raptor Nest Survey Results, April 16, 2012

#### Cheyenne Prairie Generating Station and Pipeline Project

Nest ID	Species	Status	Condition	Substrate	Approx. Nest Height (m)	Photo IDs	Comments
1	Red-tailed hawk	Active	Good	Live cottonwood	13	1,2	Adult incubating
2	Great horned owl	Active	Good	Live cottonwood	9	3,4	Adult and 2 nestlings observed
3	Unknown raptor	Inactive	Good	Live cottonwood	13	5	
4	-	-	Gone	Live cottonwood	-	-	Nest recorded in fall 2011. Nest branch broken and nest material observed on ground during this survey
5	Unknown raptor	Inactive	Good	Live cottonwood	4	6,7	-
6	Unknown raptor	Inactive	Good	Live cottonwood	8	8,9	-

Nest 1 was determined active. An adult red-tailed hawk (*Buteo jamaicensis*) was observed in incubating position (Photograph 1) and a second adult red-tailed hawk was observed perched in a live cottonwood tree approximately 0.25 mile east of the nest. No vantage was available to view into the nest to verify presence or count eggs in the nest; however, the adult was observed in incubating position for approximately 30 minutes between 0945 and 1015 hrs, and this or the other member of the nesting pair was observed on the nest in incubating position during a return visit to the nest at 1700 hrs.

Nest 2 was determined active. An adult great horned owl (*Bubo virginanus*) and two nestlings were observed in Nest 2 at 1045 hrs (Photograph 3). The nestlings were approximately 50 percent feathered.

#### **Prairie Dog Survey**

The prairie dog survey was completed between 0830-1700 hrs on April 16, 2012. All areas proposed for disturbance within 500 feet of the proposed project were directly accessible with the exception of a portion of the pipeline corridor for which access permission could not be obtained (see Figure 2). Due to the topography of this inaccessible area and the presence of a public road bisecting the northern portion of this private parcel, the area was able to be completely evaluated for the presence or absence of prairie dogs using binoculars.

With the exception of the Crow Creek Riparian area and associated irrigated hay fields, the project area is comprised almost entirely of open shortgrass prairie habitat. Representative habitat along the pipeline corridor is presented in Photograph 10. No prairie dogs, colonies, or individual burrows are present in or near the project area.

#### Other wildlife

During the course of the survey, the following wildlife species were observed within the survey area: American robin (*Turdus migratorius*), Canada goose (*Branta canadensis*), common raven (*Corvus corax*), European starling (*Sturnus vulgaris*), ferruginous hawk (*Buteo regalis*), great horned owl, horned lark (*Eremophila alpestris*), loggerhead shrike (*Lanius ludovicianus*), mallard (*Anas platyrhynchos*), western meadowlark (*Sturnella neglecta*), mule deer (*Odocoileus hemionus*), pronghorn (*Antilocapra americana*), red-tailed hawk, Swainson's hawk (*Buteo swainsonii*), white-tailed deer (*Odocoileus virginianus*).

# **Discussion and Recommendations**

Due to the presence of an active red-tailed hawk nest (2,041 feet [0.39 miles] from the plant) and great horned owl nest (1,611 feet [0.31 miles] from the pipeline) of the Project, consideration should be given to timing and location of construction activities to avoid impacts to these or other potentially nesting raptors in the Crow Creek riparian area. It is evident based on the presence of active and inactive raptor nests that the Crow Creek cottonwood riparian area is important to nesting raptors. Therefore, nest surveys during the year of construction are recommended if construction is to occur during the nesting season, to allow implementation of impact avoidance measures.

Based on nesting chronology of the species nesting this year, the red-tailed hawk nest can be expected to fledge young on or before July 1, 2012, and the great horned owl nest can be expected to fledge young prior to May 15, 2012. In future years, raptor nest location, status, species, and timing may differ from that observed during this survey; however, data from this survey indicate that construction planning should allow avoidance of the great horned owl nest from late February until late May and of the red-tailed hawk nest from early March through mid July. More conservative planning could simply avoid impacts within 0.25 miles of all mature cottonwoods located within the Crow Creek riparian area, recognizing that additional nests may be constructed in future years by red-tailed hawks or other raptors, or by late-nesting species not recorded in this survey, such as Swainson's hawk.

Based on the negative survey results for raptor nests along the pipeline corridor to the south of Crow Creek, it is unlikely that raptors will use this area for nesting in future years. However, potential nesting habitat does exist for ferruginous hawks in the form of rugged topography along drainages, and for this and other raptor species in the form of transmission line structures and windmills; therefore surveys during the year of construction are recommended if construction is to occur during the nesting season.

No prairie dogs were present at the combustion turbine facility site or along the pipeline route during this survey. Current land use consists almost entirely of cattle grazing, with some hay farming near Crow Creek, which makes it unlikely that landowners would allow prairie dogs to become established within the project area; therefore, consideration of measures to avoid or minimize impact prairie dogs can reasonably be considered not necessary for this project.



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Attachment 1

Survey Photographs



Photograph 1 – Nest 1. Active red-tailed hawk nest with adult in incubating position.



Photograph 2 – Nest 1. Landscape perspective.



Photograph 3 - Nest 2. Active great horned owl nest with adult and two nestlings present on nest.



Photograph 4 – Nest 2. Landscape perspective.



Photograph 5 - Nest 3. Inactive stick nest.



Photograph 6 - Nest 5. Inactive stick nest.



Photograph 7 - Nest 5. Landscape perspective.



Photograph 8 - Nest 6. Inactive stick nest



Photograph 9 - Nest 6. Landscape perspective.



Photograph 10 – representative habitat along the pipeline corridor



# BLACK HILLS POWER & LIGHT CO. BLACK HILLS GENERATION

A Black Hills Corporation Enterprise

Tim Rogers Environmental Manager 605•721•2286

March 2, 2012

Chris Razzazian USEPA Region 8 1595 Wynkoop Street Mail Code 8P-AR Denver, CO 80202-1129

# RE: Black Hills Corporations (BHC) Cheyenne Prairie Generating Station (CPGS) – Endangered Species and Migratory Birds

Chris,

This letter is being submitted to the Environmental Protection Agency (EPA) for consideration during the GHG Prevention of Significant Deterioration permit evaluation of the Cheyenne Prairie Generating Station in Cheyenne, Laramie County, Wyoming and the anticipated EPA consultation with the U.S. Fish and Wildlife Service (USFWS) under Section 7 of the Endangered Species Act (ESA).

**Project Description:** 

BHC plans to construct a new nominal 220-megawatt (MW) gross simple and combined-cycle combustion turbine power plant. There will be five 40-MW LM 6000 combustion turbine generators (CTGs). Two of the turbines will be operated in combined-cycle mode and three will be operated in simple-cycle mode. Operating in combined-cycle will provide approximately 20-MW.

The CTGs will be developed on a 40-acre <u>Project Site</u> on private land plotted in the middle of a 250-acre parcel owned by BHC in Township 13N, Range 66W, Section 1. The parcel is bordered on the north by Interstate 80 (I-80), Crow Creek to the south, the Dry Creek Wastewater Plant to the east, and the HR Residential complex to the west. The access road will run north approximately ¼ mile from the Project Site to an existing road that runs parallel to I-80. The transmission line interconnect will run north from the Project Site to I-80 and then run east parallel and next to an existing transmission line for approximately 1.5 miles to the interconnect location.

The CTGs will be fired by pipeline quality natural gas. The natural gas pipeline will extend from the Project Site approximately 10 miles south to the Wyoming/Colorado Border. BHC ownership of the pipeline will end on the Wyoming side of the border. A Natural Gas Transmission company will be selected and they will provide a gas-line interconnect from their transmission line in Colorado to our pipeline in Wyoming. This transmission interconnect will extend south from our pipeline in Wyoming to approximately 5 miles south to their main transmission line.

In this letter, BHC provides a summary of our consultants findings (enclosed West Inc. report), lists our understanding of the USFWS recommendations (based upon phone conversations, meetings, and guidance documents), and BHC's approach to avoid impacts to these resources to enable the USFWS to make a finding of no adverse effect to the federally listed species and resources for the Project. BHC hopes that our proactive efforts assist EPA in its consultation with USFWS.

Rapid City, SD 57709-1400

USFWS Candidate Species or Critical Habitat: Preble's Meadow Jumping Mouse (PMJM - Zapus hudsonius preblei), Colorado Butterfly Plant (CBP - Gaura neomexicana ssp. coloradensis) and Ute Ladies'-tresses (ULT - Spiranthes diluvalis).

Project Site: The WEST Report finds the habitat is not suitable for PMJM or the two listed plants indicating that a no effect determination is appropriate since the habitat is not suitable for these species at the Project Site.

Natural Gas Pipeline Corridor:

Crow Creek: WEST determined that potential habitat may exist in the Crow Creek riparian area for PMJM, CBP, and ULT. BHC intends to bore under the potential Crow Creek riparian habitat, thus resulting in no impact to these species or their potential habitat. The bore hole, entry and exit, will be 300 ft outside the 100-year flood plain and will be less than 1/10 acre. The bore holes are 30 ft x 30 ft excavation, therefore BHC anticipates no impact to critical habitat or for the species if they were to be present. USFWS recommends that a one-time survey for the CBP and ULT be completed in Crow Creek during summer 2012 to confirm or deny the presence of the species where the pipeline will cross. BHC will conduct the study and provide the results to the USFWS.

Porter Draw: The USFWS indicated they do not expect PMJM or ULT to occur in Porter Draw, an ephemeral drainage approximately 4 miles south of Crow Creek. However, habitat may be suitable for CBP. Therefore, USFWS recommends that a one-time survey for the CBP be completed in Porter Draw during summer 2012 to confirm or deny the presence of the species where the pipeline will cross. BHC will complete the survey and submit to USFWS. If the CBP are present in the vicinity of where the pipeline will cross, BHC will avoid or drill under the plants to avoid impact to the species.

Transmission Line in Colorado: BHC ownership of the natural gas transmission line will end at the Wyoming border and BHC will not own the pipeline that extends into Colorado. This will be owned by a natural gas transmission company that has not been selected at this point. It has been conveyed to BHC that the selected transmission company will conduct a Biological Assessment on the pipeline they will construct.

**Species or Resources of Concern:** The USFWS letter noted the ecological importance of black-tailed prairie dog colonies, and the benefits of their preservation.

Project Site: WEST Surveys have not found any prairie dog colonies within the Project Site area, and therefore impacts to that species are not expected.

Natural Gas Line: BHC will conduct a survey on the gas line path owned by BHC in the summer of 2012 for prairie dog colonies. This information will be provided to the USFWS. If colonies are discovered, BHC commits to avoiding impacts to the colonies as discussed with USFWS.

The USFWS also noted the ecological importance of wetlands and riparian areas, and recommended measures to proactively protect these potential habitats from Project impacts.

Project Site: There are no wetlands or riparian areas in the Project Site area. BHC is securing a storm water construction permit for the Project Site from WDEQ that will provide protections of sediment run-off to these resources. Therefore, there will be no impact to these resources.

Natural Gas Line: The only riparian areas of concern are associated with Crow Creek where the pipeline will cross the creek. BHC intends to directional bore beneath Crow Creek, leaving the riparian corridor intact; therefore avoiding adverse impacts. Additionally, BHC will secure a storm water construction permit for the gas line construction that will provide protections of sediment run-off to these resources.

Rapid City, SD 57709-1400

**Migratory Birds: Migratory Bird Treaty Act (MBTA) and the Bald and Golden Eagle Protection Act (BGEPA) Recommendations:** The USFWS letter notes the Project should proactively consider recommendations concerning migratory birds in accordance with the MBTA and the BGEPA in Project planning. With respect to those resources near the Project area, the report identifies two potential raptor nests and one known historical raptor nest in the trees along Crow Creek, all located some distance away from construction activity at the Project Site. The one known historical nest supported Swainson's hawk (*Buteo swainsoni*) and great-horned owl (*Bubo virginianus*). The USFWS recommended that construction activity be located greater than 0.125 mi from active great horned owl nests and 0.25 mi for Swainsons' hawk and red-tailed hawk (*Buteo jamaicensis*) nests.

Project Site: The closest existing raptor nest to the Project Site is 0.36 miles. The USFWS confirmed that these raptor nests were outside the distance where disturbance during plant construction would be of concern, assuming the nests were occupied by the great horned owl and Swainson's hawk or by other species (e.g., red-tailed hawk, ferrugious hawk, or eagles). These raptor nests and the area surrounding the project site will be further evaluated in spring 2012 and 2013, prior to and during construction. BHC will provide this information to the USFWS. Based upon the available information, at the present time, the Project Site does not pose impacts to Raptor nests. If the circumstances change based upon the surveys conducted in 2012 or 2013, BHC will employ measures to avoid the nesting season or the spatial distance requirements established for the avian species of concern as discussed with USFWS.

Natural Gas Line: The USFWS recommended that BHC avoid disturbance of any active raptor nests during nesting season either by avoiding construction during the nesting season or conducting construction at the spatial recommendations identified for the specific avian species of concern. BHC intends to avoid the nests by the distances recommended by the USFWS or will plan construction of the pipeline, in proximity to these nests to occur, outside the nesting season resulting in no impact to the species. BHC will use the survey discussed above to evaluate the potential avian species located near the planned pipeline crossing of Crow Creek to determine if further discussions are needed with USFWS due to nest occupancy or a change in avian species type.

Ground Nesting Birds: The USFWS also recommended that measures be taken to avoid or minimize risk of impact to MBTA protected ground and grassland/shrub nesting birds nesting along the gas line. If ground nest are discovered along the natural gas pipeline corridor, BHC will employ measures of avoidance (nesting season or spatial distances) or other acceptable practices that result in a no impact to the nesting birds.

With respect to migratory birds in general, the USFWS letter indicates the BHC Avian Protection Plan (WY-APP enclosed) should guide Project Site design. BHC is in agreement with the USFWS, and per the APP, the Project will employ techniques recommended by the Avian Power Line Interaction Committee (APLIC). This will include compliance with Section 5.7 of the APP, Construction and Modification to Avian-Safe Standards in design aspects of the transmission line and substation to minimize impacts to birds.

BHC believes the results of this study and coordination with the USFWS, coupled with responsible construction practices, clearly demonstrate there will be no significant adverse impacts to ESA-listed species, species and resources of concern, or migratory birds, including raptors and eagles. During the construction phase of the project involving federally protected species, BHC will consult with the USFWS as appropriate and necessary to ensure protection.

If you have any questions on these materials, please contact me at (605) 721-2286 or <u>Tim.Rogers@blackhillscorp.com</u>.

Sincerely,

Tim Rogers Environmental Manager

Rapid City, SD 57709-1400

cc: Fred Carl, Black Hills Corporation

Enclosures:

Attachment 1: Figure 1 – Crow Creek Raptor Nests

Attachment 2: BHC Avian Protection Plan for Wyoming

Attachment 3: Evaluation of Habitat for Ute Ladies'-tresses, Colorado butterfly plant, and Preble's meadow jumping mouse at the proposed Cheyenne Prairie Generating Station and Pipeline. February 14, 2012.

# Evaluation of Habitat for Ute Ladies'-tresses, Colorado butterfly plant, and Preble's meadow jumping mouse at the proposed Cheyenne Prairie Generating Station and Pipeline

Laramie County, WY

Prepared for:

CH2M HILL Engineers, Inc. 9191 S Jamaica Street Englewood, CO 80112-5946

Prepared by:

Joel Thompson and Gregory Johnson Western EcoSystems Technology (WEST), Inc. 2003 Central Avenue Cheyenne, Wyoming 82001

February 14, 2012



# INTRODUCTION

CH2M HILL Engineers, Inc. (CH2M HILL) contracted with Western EcoSystems Technology, Inc. (WEST) to assess the habitat suitability for three federally listed threatened species, Preble's meadow jumping mouse [PMJM; *Zapus hundsonius preblei*]), Ute ladies'-tresses orchid (*Spiranthes diluvialis*), and Colorado butterfly plant (*Gaura neomexicana* ssp. *coloradensis*) at the site of a proposed natural gas plant and pipeline to be constructed in Laramie County, just east of Cheyenne, Wyoming. This report is based on a site visit to the proposed gas plant development site and pipeline corridor by qualified WEST personnel (J. Thompson who holds a USFWS permit for Preble's meadow jumping mouse and G. Johnson who is highly experienced with both listed plant species), in which the area proposed for development was evaluated for potential habitat for each listed species. The purpose of the survey was to assess the potential for these species to occur and determine if additional presence/absence surveys or mitigation strategies developed through federal Endangered Species Act (ESA)(16 USC § 1531 et seq.) consultation may be warranted.

The proposed development site (Figure 1) was visited by WEST personnel on December 16, 2011 to assess the habitat suitability for the three threatened species. Areas surveyed included the parcel that will contain the plant, as well as the three primary drainages that intersect the proposed pipeline corridor. The primary area of concern for potential occurrence of any of the three listed species is along Crow Creek within the pipeline corridor. The gas plant project site, located to the northeast of the pipeline corridor was determined to not contain any suitable habitat for the three species; all of which are dependent upon moist riparian habitats which are nonexistent within the gas plant project site. Therefore, the gas plant project site is not discussed further in this report.

Additionally, the gas plant access road and transmission interconnection site (Figure 1) were visited on January 31 and February 2 to assess habitat suitability for the three listed species. The access road follows a previously developed access road (gravel-based) which parallels Interstate 80. There are two ditch crossings along its route to the project site, both of which utilize a series of high-strength concrete culverts. At the westernmost crossing, the culverts run under Interstate 80. At the eastern ditch crossing, the culverts do not extend under Interstate 80, but are rip-rapped on both sides of the access road (see photos Appendix A). Based on the field evaluation of the two ditch crossings, it was determined that habitats were not suitable for the three listed species. With the exception of small areas of heavy, sandy sedimentation at the downstream edge of each series of culverts caused by occasional high runoff flows (see photos Appendix A), both ditches have incised channels bordered by dense vegetation (primarily upland vegetation, not wetland species) all the way the channel edge. The areas immediately downstream of the culverts are more open; however the sandy sediment comprising the substrate in these areas is not conducive to establishment of riparian vegetation, including Utes

Western EcoSystems Technology, Inc.

ladies'-tresses orchid or Colorado butterfly plant. Neither ditch has riparian habitats considered suitable for Preble's meadow jumping mouse. Due to the lack of suitable habitats along the access road, there should be no effect on listed species due to the use or upgrading of the road and it is not addressed further in this report.

The transmission interconnection site is located approximately 1.5 miles east of the project area, south of Interstate 80 and east of Campstool Rd (Figure 1). The interconnection site is located on a gently sloping prairie hillside, with no suitable habitat for listed species occurring in close proximity. Development at the interconnection site will have no effect on listed species and is not discussed further in this report.



Figure 1. Proposed Cheyenne Prairie Generation Station and pipeline project area.

#### Ute Ladies'-tresses

Ute ladies'-tresses orchid is a perennial forb in the orchid family. It was first described as a species in 1984. It generally blooms from late July through August; however, depending on location and climatic conditions, may bloom in early July or still be in flower as late as early October (USFWS 1995). Its seeds are very small and require specific symbiotic association with mycorrhizal fungi for germination (Arditti 1992). Like other orchids, some plants may germinate and remain underground in a saprophytic state for many years before emerging. After emerging, individual plants may be dormant for many years and bloom only rarely. Reproduction appears to be strictly sexual, with bumblebees as the primary pollinators (Dressler 1981, Sipes et al. 1993).

Utes Ladies'-tresses is found in 60 locations representing at least 30 distinct biological populations (Fertig 2000a). Locations are in Wyoming, Nebraska, Colorado, Utah, Idaho, Montana, and Washington. In Wyoming, there are nine known populations of Ute ladies'-tresses spread across Laramie, Goshen, Niobrara, and Converse Counties (Fertig et al. 2005). In Laramie County, Ute ladies'-tresses is only known from the Horse Creek drainage. No populations have been found within the Crow Creek drainage, although numerous surveys along Crow Creek have been conducted (Heidel 2007).

This species inhabits moist soils in mesic or wet meadows, gravel bars, wet streambanks, and old oxbows at elevations of 4,300 to 7,000 feet (Stone 1993). Jennings (1990) and Coyner (1989) observed that the orchid seems to require "permanent sub-irrigation," indicating a close affinity with floodplain areas where the water table is near the surface throughout the growing season and into the late summer or early autumn. This orchid colonizes early successional riparian habitats subject to seasonal flooding from snowmelt and intermittent heavy thunderstorms. It is not tolerant of long-term standing water and emergent vegetation development. It is generally found with grasses, sedges, rushes, shrubs and riparian trees such as willows. It rarely occurs in deeply shaded sites and prefers partially shaded open glades or pastures and meadows in full sunlight (USFWS 1992). In Wyoming this species occurs primarily on low, flat floodplain terraces or abandoned oxbows within 0.5 to 50 m of small perennial streams or rivers at elevations of 4,750 to 5,400 feet. The terrace sites are typically subirrigated, often seasonally flooded, and remain moist well into the summer. Associated vegetative cover is usually 75-90%, and is typically short (i.e., <18 inches; Fertig and Heidel 2007).

A draft recovery plan for this species was prepared in 1995. This draft does not include population and habitat recovery goals and delisting criteria. The recovery plan direction focuses on restoring natural stream dynamics (hydrologic patterns). Critical habitat has not been designated for this species.

#### **Colorado Butterfly Plant**

Colorado butterfly plant is a short-lived biennial (sometimes perennial) herb that grows 19.7-31.5 inches tall. Leaves are lanced shaped with smooth edges and are 2 to 5.9 inches long. The Colorado butterfly plant has small (5-14 mm) white flowers that turn pink or reddish with age. This species flowers from June through October and produces fruit from July to October. This plant will continue to flower until the first frost of the year. Non-flowering plants consist of a prostrate rosette of oblong, mostly glabrous entire or toothed leaves 4-18 cm long (Fertig 2000b).

Colorado butterfly plant is found in moist meadows typified by sub-irrigated, alluvial soils of streams surrounded by mixed grass prairie. It is found at elevations of 5,000 to 6,400 feet. Colonies are often found in low depressions or along bends in wide, meandering stream channels (Fertig 2000b). The Colorado butterfly plant prefers open habitat without dense or overgrown vegetation (USFWS 2010). Establishment and survival of seedlings is enhanced where tall and dense vegetation has been removed by some form of disturbance (Fertig 2000b).

Since 1977, over 20 populations have been discovered in Colorado, Wyoming and Nebraska. Currently, this plant is restricted to Laramie and Platte Counties, Wyoming, Kimball County, Nebraska, and Weld County, Colorado (Jennings et al. 1997). Current populations occur along Bear, Crow, Horse, Lodgepole and Spring Creeks (Fertig 2000b). The populations along Crow Creek and its tributaries occur west of Cheyenne. No populations have been found along these drainages east of Cheyenne. The nearest known populations are located on F.E. Warren Air Force Base approximately five miles west of the project.

Loss of habitat and the small population are the main issues of concern regarding this species. Critical habitat for this species has been designated in Laramie and Platte Counties along Tepee Ring Creek, Bear Creek, Little Bear Creek, Horse Creek, Lodgepole Creek, and Lone Tree Creek (Figure 2), but no critical habitat has been designated in the project area (USFWS 2010). The nearest critical habitat is located along Diamond Creek approximately eight miles west of the project (USFWS 2010; Figure 2).



Figure 2. Designated critical habitat for Colorado Butterfly plant in Laramie County, Wyoming (from USFWS 2010).

## Preble's Meadow Jumping Mouse

Meadow jumping mice (*Zapus hudsonius*) are small rodents with large hind feet, long back legs, and long tails which typically occur in moist habitats consisting of a low undergrowth of grasses and/or forbs, in open wet meadows and riparian corridors, or where shrubs and trees provide adequate cover (USFWS 2007). Preble's meadow jumping mouse (Preble's) is a subspecies which occurs primarily in riparian corridors along the Front Range of northern Colorado and southeastern Wyoming. Preble's typically enter hibernation in the early fall (September-October) and emerge during the spring (May). Due to the timing of hibernation, trapping protocols designed to document the presence/absence of Preble's focus on the period of greatest activity, which occurs from June through the end of August.

Preble's were listed as threatened under the Endangered Species Act in May 1998 (USFWS 1998). Citing a presumed lower prevalence and severity of threats in Wyoming relative to its range in Colorado, the USFWS delisted Preble's in the Wyoming portion of its range in 2008 (USFWS 2008). In August 2011, the USFWS again revised the status of Preble's, reinstating its status as Threatened in the Wyoming portion of its range (USFWS 2011). Currently, Preble's is listed at Threatened throughout its entire range in Wyoming and Colorado. Designated Critical Habitat for the species only occurs in Colorado. Those areas previously designated as Critical Habitat in Wyoming prior to its delisting were not reinstated with the 2011 revision reinstating its Threatened status in Wyoming.

Typical Preble's habitat has been described as well-developed plains riparian vegetation with relatively undisturbed grassland with a water source in close proximity (USFWS 2007). It has also been noted that Preble's apparently lacks a preference for any single plant species and instead favored sites which are structurally diverse (Shenk and Eusen 1999 in USFWS 2007). Although Preble's are rarely trapped in uplands adjacent to riparian areas, detailed studies of Preble's movements using radio telemetry have documented them feeding and resting in adjacent uplands (USFWS 2007). These studies reveal that the Preble's regularly uses uplands at least as far out as 100 meters beyond the 100-year floodplain (USFWS 2007). Preble's can also move considerable distances along streams, with travel as great as 1.6 km (1.0 miles) documented in one evening (Ryon 1999 in USFWS 2007).

# **METHODS**

All drainages containing potentially suitable habitat that could be crossed by the pipeline were examined. These included Crow Creek, Porter Draw and a northern branch of Simpson Creek (Figure 1). The riparian area and associated wetlands along Crow Creek potentially affected by construction of the pipeline were visually inspected on foot on December 16, 2011 to determine habitat suitability for all three species. Transects were walked within and adjacent to all wetland areas. Plant species observed and general habitat notes were recorded during the site visit. Photos were taken of representative sections of all drainages surveyed (Appendix A). Porter Draw and the Simpson Creek tributaries were assessed on foot at readily accessible points

(Figure 1) within the pipeline corridor and visually from a distance (i.e., with binoculars) from public roads.

# RESULTS

With the exception of Crow Creek, which is a perennial stream, all drainages in the project area are ephemeral. Based on the field visit all drainages were determined to present hydrology that would not support either Ute's ladies'-tresses or Colorado butterfly plant (see photographs in Appendix A). Additionally, due to the lack of well-developed riparian habitat in the drainages other than Crow Creek, it was determined that Porter Draw and the Simpson Creek tributary were unsuitable for supporting populations of Preble's meadow jumping mice.

# Plants

The riparian area along Crow Creek in the project area is dominated almost entirely by reed canarygrass (*Phalaris arundinacea*). This grass forms dense, tall mats along Crow Creek which would greatly restrict habitat for the two listed plant species, as they do not tolerate dense, tall vegetation and extreme shading. Wetter depressions along Crow Creek not dominated by reed canarygrass were dominated by broadleaf cattail (*Typha latifolia*) and softstem bulrush (*Scirpus validus*), both of which also form dense, tall mats of vegetation that would preclude establishment of Ute's ladies'-tresses or Colorado butterfly plant. Other species occurring in the understory along Crow Creek included licorice (*Glycyrrhiza lepidota*), Canada thistle (*Cirsium arvense*), kochia (*Kochia scoparia*), curly dock (*Rumex crispus*), smooth brome (*Bromus inermis*), and wheatgrass (*Agropyron* spp.). Overstory plants along the riparian area included sandbar willow (*Salix exigua*), peachleaf willow (*Salix amygdaloides*), and plains cottonwood (*Populus deltoides*).

From a hydrologic perspective, the Crow Creek channel is heavily incised with relatively steep banks along most of its length, resulting in a very narrow riparian area and groundwater tables that are far below the adjacent bank during most of the growing season. Based on presence of flood debris in uplands, Crow Creek may occasionally flood in the spring during extremely high runoff years, but the incised channel likely prevents flooding during most years, especially late in the growing season after spring runoff. This hydrologic regime along with steep banks do not allow for formation of areas in the riparian corridor where groundwater tables are near the surface. Therefore, conditions are not suitable for establishment of either Ute ladies'-tresses or Colorado butterfly plant along this reach of Crow Creek. The ephemeral drainages in the project area between Crow Creek and the Colorado State Line were dry at the time of the site visit and did not have any wetland vegetation or other characteristics typically associated with presence of either Ute ladies'-tresses or Colorado butterfly plant (Appendix A).

According to maps showing probability of occurrence for both Ute ladies'-tresses and Colorado butterfly plant created by the Wyoming Natural Diversity Database, there is no probability of occurrence of Ute ladies'-tresses in the project area (Figure 3), which is consistent with our field observations. However, the map predicting potential probability of occurrence of Colorado

butterfly plant indicates high probability of occurrence of Colorado butterfly plant within the project area along Crow Creek and Porter Draw (Figure 4), which is not supported by our onsite evaluation of habitat and hydrologic features. It should be noted that this map indicates high probability of occurrence for Colorado butterfly plant in a substantial area within Laramie County, even though very few populations are actually known to occur in Laramie County.



Figure 3. Predicted probability of occurrence of Ute ladies'-tresses in Laramie County, Wyoming



Figure 4. Predicted probability of occurrence of Colorado butterfly plant in Laramie County, Wyoming.

#### Preble's Meadow Jumping Mouse

The riparian corridor along Crow Creek is dominated by dense stands of reed canarygrass, with scattered clusters of woody shrubs and trees (e.g., willow and cottonwood) intermixed along its length. Other riparian species (e.g., cattail, bulrush) occur in some of the wider, lower lying wetland areas along the creek. Unlike the two plant species discussed previously, which would not likely occur in the dense vegetation along Crow Creek, Preble's tend to occupy this type of habitat, and based on the availability, could potentially occur anywhere along the length of Crow Creek that lies within the pipeline corridor. Much of the grasslands adjacent to Crow Creek appear to be cut for hay (Figure 5) and in some areas that lack woody cover, hay swathing comes quite close to the creek channel which may affect habitat quality for Preble's later in the season. There are sections along Crow Creek where there is a lack of willow and other woody species, and the channel and associated riparian habitats are quite narrow. These stretches, (identified in Figure 5 with photos included in Appendix A) may provide areas where the pipeline could cross the creek while minimizing potential direct impacts to Preble's and higher-quality Preble's habitat.

It is unknown if trapping for Preble's has occurred along this section of Crow Creek in the past. Based on data available from the Wyoming Natural Diversity Database (WYNDD), Preble's have been documented along Crow Creek approximately eight miles upstream on F.E. Warren Air Force Base (WYNDD 2009); however, several other trapping efforts in the Cheyenne area (not necessarily along Crow Creek) apparently failed to document the presence of Preble's (USFWS 2007).

Based on the presence of potentially suitable habitat for Preble's along Crow Creek, it is recommended that consultation under the ESA be initiated early in the process of permitting to determine the options available for dealing with potential Preble's issues. Four possible scenarios may provide compliance with the ESA:

- 1) Avoidance of impacts to Preble's habitat along Crow Creek. Habitat at the specific crossing location would need evaluation to determine the distance from the channel that would be considered potentially used by Preble's.
- 2) Directionally bore the pipeline beneath Crow Creek in consultation with the USFWS.
- 3) Complete a protocol-level trapping survey during the June 1- August 31 time period to assess the presence/absence of Preble's within the proposed crossing area. If absence is confirmed, no further compliance measures would be necessary. If presence is confirmed, develop adequate avoidance measures, or implement appropriate impact minimization and mitigation measures to allow take of the species.
- 4) Presence of Preble's could be assumed and suitable mitigation measures could be developed through consultation to allow construction to proceed.

# Other Wildlife

Three potential raptor nest sites (Figure 5, Nests 1, 3, and 4) and one known historical raptor nest (Figure 5, Nest 2) were also observed while on site conducting the habitat assessment. All were located along the riparian corridor of Crow Creek. One (Nest 2) is known to historically support both great-horned owls (*Bubo virginianus*) and Swainson's hawks (*Buteo swainsoni*), while the historical status of the others are unknown. To avoid/minimize impacts to nesting raptors BH will work with the USFWS and WYGFD to determine the appropriate timing and distance buffers should these nests be active during the construction period of the natural gas pipeline.



Figure 5. Raptor nests and potential creek crossings with lower quality Preble's jumping mouse habitat.

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Appendix A. Photographs of drainages in project area


Crow Creek riparian area dominated by reed canarygrass and scattered patches of willow.



Crow Creek riparian corridor dominated by reed canarygrass. Lengthy stretch of narrow riparian corridor lacking woody cover exists in this area (Point A on figure 5).



Crow Creek riparian corridor dominated by reed canarygrass. Area east of foot-bridge lacks developed woody cover (Point B on figure 5).



Crow Creek riparian corridor at Point D in southwest portion of project area, east side of pipeline corridor.



Representative photo of incised stream channel along Crow Creek.



Photograph of Crow Creek riparian corridor with incised stream channel



Porter Draw. Ephemeral channel in central portion of pipeline corridor. Location identified on Figure 1.



Tributary to Simpson Creek. Ephemeral channel near Colorado state line in southern portion of pipeline corridor. Location identified on Figure 1.



Raptor nest (Nest 2 on figure 5). Historically used by great-horned owl and/or Swainson's hawk.



Potential raptor nest (Nest 1 on Figure 5). Historical status unknown.



Potential raptor nest (Nest 3 on Figure 5). Historical status unknown.



Potential raptor nest (Nest 4 on Figure 5). Historical status unknown.



Western ditch crossing on access road.



Eastern ditch crossing on access road.

# **Avian Protection**



# **Avian Protection Plan**

# Black Hills Corporation Wyoming Operations



Improving life with energy



September 6, 2011

# BLACK HILLS CORPORATION COMPANY PROCEDURE

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SUPERSEDES	Environmental	Fla
History Log: Revisions made 07/07/11 to USFWS permit requirements, clarification of terms, revised definitions	REVIEWED BY	2011-09-02

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## **APPENDIX A: RESPONSE AND REPORTING FLOWCHARTS**

## **APPENDIX B: PROTECTION OF RAPTORS**

### **APPENCIX C: CONTACTS**

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#### 1. PURPOSE

The Company's Wyoming Avian Protection Plan (APP or "Plan") provides guidance to mitigate the impact of company operations on protected bird species. Various federal treaties, acts, federal and state regulations and laws protect migratory birds, eagles and endangered species. These laws apply a strict liability approach to the "taking" of protected species, their parts, nests and habitat. Implementation of this Plan will reduce bird mortalities, incidents and negative interactions, and impacts to habitat. This Plan identifies actions needed to comply with legal requirements while continuing to provide the safe and reliable services provided by the company.

#### 2. SCOPE

The Plan applies to all Company operations in Wyoming including Electric Distribution and Transmission, Generation, Mining, and Oil and Gas Exploration, Production and Midstream activities which may impact protected bird species.

NOTE: A separate Plan covers BHP Electric Distribution and Transmission, Generation Operations in South Dakota, Montana, and Nebraska.

#### 3. **RESPONSIBILITY**

The personnel of the various Wyoming operations are responsible for implementing the Plan within their individual projects or systems.

Avian Protection Program Coordinator: The Avian Protection Program Coordinator (APPC) or designee is responsible for developing and documenting Program Standards, Procedures, and Practices, developing and implementing the Plan, communicating with regulatory agencies, and monitoring the implementation of the Plan.

**Power Generation, Mining, Exploration and Production (E&P)/Midstream**: Environmental personnel are responsible for managing aspects of the Plan including monitoring, incident investigation, reporting, and mitigation design and operational changes needed to appropriately reduce the risk of negative interactions with protected avian species.

**Electrical Transmission/Distribution**: Transmission/Distribution will delegate personnel who are responsible managing all aspects of the Plan including monitoring, incident investigation, reporting, and mitigation design and operational changes needed to appropriately reduce the risk of negative interactions with protected avian species.

**Environmental Services**: Environmental Services (ES) personnel assist operations to implement the plan including monitoring, incident investigation, reporting, and mitigation design and operational changes needed to appropriately reduce the risk of negative interactions with protected avian species.

**Electric Construction Standards Committees**: The Company's electrical design standards committees are responsible for the approval of electrical structure and electrical design modifications needed to meet Plan requirements.

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#### 4. **DEFINITIONS**

<u>Active Nest</u> – A nest that has eggs or young present at the time of observation. A nest is considered inactive when eggs or young are not present, such as in the fall or winter, or if the nest is not used during breeding season. The term <u>occupied nest</u> is used synonymously.

**<u>AITS</u>** – Avian Incident Tracking System is a Company electronic database.

APP – Avian Protection Plan

<u>APPC</u> – Avian Protection Program Coordinator which is a role assigned in the Environmental Services Department.

**<u>APP-WY</u>** - Company's Avian Protection Plan for its Wyoming operations.

**BGEPA** – the Bald and Golden Eagle Protection Act. The BGEPA prohibits knowingly taking, or taking with wanton disregard for the consequences of an activity, any bald or golden eagle or their body parts, nests, chicks or eggs, which includes collection, molestation, disturbance, or killing. The term "disturb" is defined as "to agitate or bother a bald or golden eagle to a degree that causes, or is likely to cause, based on the best scientific information available, (1) injury to an eagle, (2) a decrease in its productivity, by substantially interfering with normal breeding, feeding, or sheltering behavior, or (3) nest abandonment, by substantially interfering with normal breeding, feeding, or sheltering behavior

**<u>ESA</u>** – Endangered Species Act. The Endangered Species Act protects plants and animals that are listed by the federal government as "endangered" or "threatened.

**Inactive Nest** – A nest that does not have eggs or young at the time of observation. Term is used synonymously with <u>unoccupied nest</u>.

**Lek**: A lek is a gathering of males, of certain animal species, for the purposes of competitive mating display. Leks assemble before and during the breeding.

<u>MBTA</u> – Migratory Bird Treaty Act. The MBTA prohibits the taking of any migratory birds, their parts, nests, or eggs except as permitted by regulations and does not require intent to be proven.

<u>Migratory Bird</u> – The definition of the migratory birds that are protected by federal law were identified through various conventions. Migratory birds for purposes of the Migratory Bird Treaty Act include those defined in the Convention of Mar. 4, 1972, concluded with Government of Japan and the Convention of Nov. 19, 1976, concluded with Union of Soviet Socialist Republics. 1966 - Pub. L. 89-669 inserted "(39 Stat. 1702)" and defined migratory birds to include those defined in the Treaty of Feb. 7,1936 (50 Stat. 1311) with the United Mexican States.

The list of the Migratory Birds and bird species of concern identified can be found in Appendix D. The entire list of migratory birds can be forum at: <u>http://migratorybirds.fws.gov</u>

**<u>Negative Interaction</u>** – a situation that could or has resulted in take of a bird protected by the MBTA, BGEPA, and or ESA.

<u>Occupied Nest</u> – A nest with an incubating adult (sitting on eggs), or eggs or young present. Term is used synonymously with <u>active nest</u>. Nests may be occupied during the breeding season (approximately February through August).

**<u>Problem Nest</u>** – A nest that may cause electrocution and death to the birds, electrical outage, property damage, or otherwise interfere with power operations.

<u>**Raptors**</u> – Birds of prey with exceptionally keen eyesight, a sharp, hooked beak for tearing flesh, and strong grasping feet with large, sharp talons for killing and holding prey; includes eagles, hawks, falcons, owls, buteos, osprey, and vultures. Raptors frequently use power poles for perching or nesting.

<u>**Raptor Safe**</u> – A power line configuration designed to eliminate raptor electrocution by having sufficient spacing between phases and phase to ground which provides safe perching areas on the pole.

**Take/Taking:** As defined by 50 CFR 10.12, take means to pursue, hunt, shoot, wound, kill, trap, capture, or collect, or attempt to pursue hunt, shoot, wound, kill, trap, capture, or collect.

<u>**Tended nest**</u> – Prior to egg-laying, birds construct or add materials to nests that they will occupy during the nesting season.

**<u>Threatened & Endangered Species</u>** – ESA-listed species and those that are threatened with extinction and protected by federal law. Specifically, an "endangered species" is one that is "in danger of extinction" throughout all or a significant portion of its range. A "threatened" species is one that is "likely to becomeendnagered" within the forseable future".

<u>Unoccupied Nest</u> – A nest that does not have eggs or young at the time of observation. Term is used synonymously with <u>inactive nest</u>.

**<u>USFWS</u>** – United States Fish and Wildlife Service, which is the regulatory agency that oversees the protection of wildlife and is a service under the Department of Interior.

- Wyoming Ecological Services, Cheyenne, Wyoming: This office can assist you with avoiding, minimizing and mitigating impacts to migratory birds, and may provide assistance in obtaining migratory bird permits from the Migratory Bird Permit Office.
- Migratory Bird Permit Office, Denver, Colorado: This office provides information about migratory bird permits and issues permits when appropriate.
- Law Enforcement, Wyoming. Law enforcement will provide you with information as to how to avoid violations under the ESA, MBTA, and BGEPA. Mortalities and injuries should be reported to law enforcement. Eagle mortalities need to be reported within 24 hours.

**WGFD** – Wyoming Game and Fish Department, which is the wildlife regulatory agency in Wyoming.

#### PROCEDURE

#### 5.1 Communication of the Avian Protection Plan (APP)

#### 5.1.1 Communicating the Plan

The Plan will be communicated throughout affected company operations to assure that personnel are aware of the company's avian protection policy and procedures. The Plan will be communicated through formal training, periodic management reports, electrical standards committee meetings, and ongoing environmental and operational meetings.

#### 5.1.2 Training

Training will be provided to all affected employees who may discover or investigate avian incidents, engineers responsible for the design of raptor safe structures, and operational personnel who may be responsible for mitigating incidents through operation and maintenance activities. Training will be provided as part of the initial communication of the plan and thereafter as often as needed to assure compliance with the plan. The training will include:

- Identification of protected and non-protected species.
- Review of applicable regulations including the Migratory Bird Treaty Act (MBTA), the Bald and Golden Eagle Protection Act (BGEPA), the Endangered Species Act (ESA), and state regulations to ensure personnel are aware of the legal requirements and the potential liability associated with non-compliance.
- Bird biology and behavior related to interactions (collision or electrocution) with power structures including bird sizes, perching, and nesting, hunting and feeding habits, as well as habitat preferences and flight path tendencies.
- Bird biology and behavior related to interactions with facility buildings and other structures that may provide perching, nesting, hunting or feeding habitats.
- Discussion of the state and federal agencies that may need to be contacted and how soon following the incident they should be contacted.
- Proper procedures to follow when an avian incident is encountered.
- Internal and external reporting requirements for all incidents.
- Use of the US Fish and Wildlife Service (USFWS) Bird Fatality/Injury Reporting Program for incidents related to electrical systems.
- Use of the AITS Company electronic database system.

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- A discussion regarding "High Use Areas" where high year-round and seasonal bird concentrations may occur.
- Emphasis is to be placed on specific examples and corrective actions that are operations specific. For example: Electric operations should discuss separation and insulation concepts and applications, perch preventers, substitute perches, and nest platforms; expectations for corrective actions on lines and equipment where mortalities have occurred; and circumstances where no meaningful remedial steps can be reasonably taken such as weather, unavoidable biological interactions, or other contributory factors. Exploration and Production should discuss descriptions of when and how to apply exclusionary devices such as caps or nets, and describe how to maintain open water to keep it clean from contaminants.
- Use of additional training videos or other materials when available from the USFWS, the Avian Power Line Interaction Committee or the Edison Electric Institute, and other resources as identified.

#### 5.1.3 External Communication of the APP

The APP will be provided upon request to federal and state agencies. A copy of this plan will be maintained and available at all affected company facilities.

#### 5.2 Investigating Avian Incidents

Operations personnel will ensure that the causes of "negative interactions" are investigated; and the implementation of mitigation or preventative measures are completed where needed. Appendix A provides a general flowchart of steps to take when incidents occur. Appendix C provides a list of company personnel, and state and federal contacts.

#### 5.2.1 Identification of Dead or Injured Birds

Employees will immediately report to their supervisor and ES Coordinator all protected birds found dead or injured within the company's operation areas or right-of-ways.

#### 5.2.2 Bird Handling Restrictions and Public Safety Considerations

Field personnel will not attempt to handle, capture, collect, move, or transport any injured or dead protected bird.

**Safety Exception**: If required to ensure public safety, the safety of company personnel, and/or its operations, equipment or electrical systems, a bird may be moved away from a structure or piece of electrical equipment provided the proper personnel and agencies are notified as soon as possible after removal.

**USFWS Authorization:** Specific permission from an authorized agent of the USFWS is required to transport, collect, or capture a protected bird or eggs. Injured birds should only be handled by the USFWS, the State agency or a local rehabilitator (see Appendix C, Contact List) who has the appropriate authorization to handle protected birds.

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#### 5.2.3 Transportation of Injured Birds

To facilitate transportation of all injured birds to a rehabilitator, call the FWS Law Enforcement or Ecological Services Office to report the injury. Per communication with the FWS, BHC has been given permission to transport the bird to one of the listed rehabilitators as soon as possible. Contact the selected rehabilitator to ensure they will be able to receive and have capacity to care for the injured bird.

After the injured bird is transported to the rehabilitator, provide documentation to FWS Law Enforcement or Ecological Services Office, preferably by email. Documentation should include:

- 1. Who found the bird,
- 2. When and where the bird was found,
- 3. The date and time the Service was notified,
- 4. Suspected cause of injury and bird species involved,
- 5. Type and severity of injury,
- 6. Who transported the bird,
- 7. Name of the rehabilitator, and
- 8. When it arrived at the rehabilitation center.

#### 5.2.4 Photographic Documentation

Whenever feasible, the incident investigator will take picture sufficient to support the findings of the investigation. Take photos of the bird and it's location as initially found and the surrounding area. If electric systems are involved, the structure and any electrical equipment involved or suspected to be involved; the line including other structures to show that similar conditions exist or not. If feasible, take photos from above and below the equipment and top of structure.

#### 5.2.5 Field Report Form

When obtaining information related to a negative interaction or nesting situation, use the Field Report Form available on the ES MyBHC Avian protection webpage. Provide as much information as possible to facilitate communication with agencies regarding the incident.

# 5.3 Tracking, Monitoring, and Reporting Negative Interactions and Corrective Actions

The Company will track information about "negative interactions" between protected birds and Company facilities.

#### 5.3.1 USFWS Bird Fatality/Injury Reporting Program

Responsible personnel will report all negative interactions involving the fatality of any protected bird species associated with electrical systems to the USFWS through an online program available at <a href="https://birdreport.fws.gov">https://birdreport.fws.gov</a> and/or report directly to a field agent as requested. This reporting program also provides a clearinghouse of information for the electric utility industry to mitigate the impact of electrical systems in the loss of birds.

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This program is ONLY applicable to reporting negative avian interactions from electric operations. It is not to be used for reporting incidents at either coal mining or E&P facilities.

#### 5.3.2 Avian Incident Tracking System (AITS)

The AITS is an electronic database used for recording all avian interactions including fatalities, injuries, and nesting situations.

ES will administer the tracking system. Operations personnel or ES will enter all incidents, record investigation findings and document actions taken to mitigate future impacts.

#### 5.4 Evaluation of Avian High Use Areas

Evaluations of company territory, operations and facilities for high bird use areas may be performed to minimize impacts. Evaluations may include scientific studies and literature, breeding bird surveys, winter bird counts, observations and other relevant information. The evaluations may be used to identify areas where mitigation efforts can reduce negative interactions before they occur. The APPC or designee will be responsible for obtaining evaluations as warranted.

#### 5.5 Nest Management

Company personnel will ensure that active and inactive nests are properly managed and permits are obtained, from the USFWS and WGFD as required before action is taken. Any nest, active or inactive, that is moved by company personnel will be documented in AITS. Impacts to existing nest sites during construction of new projects or systems will be evaluated.

#### 5.5.1 Active Nests

Active nests of protected bird species are regulated under the Migratory Bird Treaty Act. Moving active nests requires approval from USFWS and WGFD and has to be completed under permits issued by the USFWS and WGFD. ES can assist with communications and obtaining permits, if needed.

#### 5.5.2 Tended Nests

Although only active/occupied nests of species other than eagles are protected under the MBTA, awareness of tended nests on or near company property provides time to address the need for nest management action before eggs or hatchlings are present. The presence of eggs or hatchlings reduce the options and increase the potential for negative interactions.

#### 5.5.3 Inactive Nests

<u>Except for eagle nests</u>, unoccupied nests that need to be removed, can be removed without a reporting requirement or permit from the USFWS but a permit is still required from the WGFD. Note that many bird species will continue to use the same location for nesting year after year. Annually, a review of locations known to be nesting sites should be inspected for nesting activity. If activity is identified, ES should be contacted immediately.

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Eagles may reuse nests for decades and they have been granted special status under the Bald and Golden Eagle Protection Act. All operations will consult with ES before moving an eagle nest. Permits will have to be obtained from the USFWS <u>and</u> WGFD before an active or inactive eagle nest can be moved. However, if there is a clear, imminent danger posed to workers, the provision of safe and reliable electrical service, or other operations, a nest may be moved, provided that the USFWS and WGFD are consulted prior to the move and permits obtained for the incident after the fact.

#### 5.6 Permit Requirements

The USFWS no longer issues permits for the removal of live or dead birds. Permits may be required to move nests, eggs or young. The permit process generally takes a substantial amount of time which may exacerbate the situation so every attempt should be made to obtain immediate verbal permission from an agency to rectify situations which are within their authorization.

Operations is responsible to report incidents immediately to ES. Operations and ES will then coordinate and provide the information to the USFWS and to the State agency, input into AITS, and obtain permits, if required.

#### Agency contacts are provided in Appendix C of this APP.

#### 5.6.1 US Fish and Wildlife (USFWS) Permits

Local USFWS personnel should be contacted when a mortality, injury or nesting incident occurs. For mortalities the USFWS can usually give verbal authorization to remove and properly dispose of a carcass but they may also want to investigate the situation. For injured birds the USFWS may also give verbal authorization to remove and transport a bird to a rehabilitator. For certain injured bird species such as raptors or T&E the agency may need to handle those birds themselves or request the WGFD or a permitted rehabilitator retrieve the birds.

When verbal approval is given or the incident is referred to the WGFD or authorized rehabilitator a permit should not be needed. For nest starts or unoccupied nests of all species except for eagles and T&E a permit is not required from the USFWS to remove those nests as long as eggs and young are not present. A USFWS permit is generally required to remove all bald or golden eagle nests (active or inactive) and all active nests of other species where eggs or young are present.

#### 5.6.2 Wyoming Game and Fish Department (WGFD) Permits

Local WGFD personnel should be contacted when a mortality, injury or nesting incident occurs. Verbal approval from the WGFD may be obtained in many instances and in such case where verbal approval is given a permit should not be required. For mortalities the WGFD can usually give verbal authorization to remove and properly dispose of a carcass.

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For injured birds, the WGFD may also give verbal authorization to remove and transport a bird to a rehabilitator. For certain injured bird species such as raptors or threatened or endangered (T&E) the agency may need to handle those birds themselves.

For new nest starts where eggs or young are not present and have never been produced, a permit may not be needed but that should be verified through contact with the WGFD prior to removal of the nest start. For existing nests where eggs or young are present or have been produced in the past a WGFD Chapter 33 Permit, as described in Section 7 of this APP, may be required. Again the WGFD should be first contacted and may be able to give verbal authorization for those activities without the need of a formal permit.

#### 5.7 Avian Protection Measures for Company Operations

#### 5.7.1 Electric Construction Design Standards

The Company's Electric Construction Design Standards Committee has developed Electrical Construction Standards. The Committee will utilize the following guidance in addressing avian protection measures.

- <u>Suggested Practices for Avian Protection on Power Lines: The State of the Art in 2006</u>, published by the Avian Power Line Interaction Committee (APLIC), the Edison Electric Institute and the California Energy Commission. 2006. Washington, D.C. and Sacramento, CA.
- <u>Mitigating Bird Collisions with Power Lines The State of the Art in 1994</u>, published by the Edison Electric Institute, and the Raptor Research Foundation. 1994. Washington, D.C.

#### 5.7.2 Avian Protection Measures for Electrical Structures

The Company will evaluate whether to apply avian protection measures utilizing available guidance documents as identified in Section 5.7.1, or by utilizing avian protection expertise.

**Siting New Electrical Lines: Siting New Electrical Lines:** Avian protection measures will be taken into consideration when siting new electrical lines.

**New Line Construction:** Avian-safe designs will be employed for all new construction. In areas with known populations of raptors or other birds of concern, new lines will be designed with adequate separations for birds.<sup>1</sup>

**Retrofit of Existing Lines**: Where studies or avian incidents have deemed necessary, lines will be rebuilt or retrofitted to avian-safe standards.

<sup>&</sup>lt;sup>1</sup> <u>Suggested Practices for Avian Protection on Power Lines: The State of the Art in 2006</u>, published by the Avian Power Line Interaction Committee (APLIC), the Edison Electric Institute and the California Energy Commission. 2006. Washington, D.C. and Sacramento, CA. Page 60.

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**Isolated incidents**: If a death or injury of a bird is due to electrocution, the structure will be retrofitted to avian safe standards as soon as feasible.

#### 5.7.3 Avian Protection Measures for Other Structures and Facilities

Every effort will be made to construct facilities and structures at generation facilities, drilling sites, compressor stations and other exploration and production facilities, and mining operations in such a manner as to minimize impact to protected avian species. Where feasible new facilities are typically designed and constructed to minimize access to protected species; and netting or mesh will be placed over containers, pits, tanks, lagoons and ponds to prevent access to oil, condensate, and other hydrocarbons, and hazardous or toxic substances.

**Isolated incidents**: If a death or injury of a bird is discovered, the structure, container, pit, tank, lagoon, pond or other feature will be evaluated and repaired or retrofitted to avian safe standards as soon as feasible.

#### 5.7.4 Avian Protection Measures for Construction Sites

Every effort will be made to keep construction sites clean and free of debris and contaminants, including oil, condensate, and other hydrocarbons, and hazardous or toxic substances.

#### 5.8 Periodic Inspections

The company performs a number of operational and maintenance inspections of facilities on a regularly scheduled basis (monthly, annually). These inspections are documented and include awareness of avian issues and provide for a random check of facilities. Employees finding evidence of negative interactions during these inspections are required to inform ES when such evidence is encountered. These inspections are performed for exploration and production, mining and electric operations and facilities.

#### 5.9 Assessments

#### 5.9.1 Annual Assessment

The APPC will compile an annual report of all incidents including fatalities, nonfatality and nesting incidents based upon information submitted to the AITS. The APPC will distribute the report to affected operations for review.

#### 5.9.2 Electric Systems (USFWS Reporting Database)

The USFWS Bird Fatality/Injury Reporting Program at <u>http://birdreport.fws.gov</u> provides report development processes for all incidents involving the fatality of a protected bird. A report of this information to USFWS is not planned since this information is publically available.

#### 5.9.3 Wyodak Mine

Annual wildlife monitoring, conducted since 1986, meets requirements of the Wyoming Department of Environmental Quality/Land Quality Division (WDEQ/LQD), WGFD, Office of Surface Mining (OSM) and the USFWS. Surveys are conducted periodically. Results are presented annually in the

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Annual Mining Report submitted to the WDEQ/LQD and OSM and are also available for public review. The study area includes the Wyodak Mine permit boundary and one-mile perimeter which includes the Neil Simpson generation facilities. A review of mining activities will be summarized in the annual report described above in section 5.8.1 by reviewing this report and information submitted to AITS.

In addition to the annual monitoring report filed with the WDEQ/LQD, Wyodak submits a "Monitoring and Mitigation Plan for Raptors and Species of High Federal Interest" to the USFWS every five years. The current plan is included in Addendum MP-C of the Mine Plan and was approved by the USFWS on March 10, 2006.

Surveys conducted at Wyodak Mine include:

#### • Winter – February & March

Raptor nesting surveys for the early nesting species including great horned owls and golden eagles.

#### • Spring – March, April & May

- Surveys of raptors to monitor nests previously located and search for new nests.
- Surveys of game birds to record lek locations and number of birds using leks.
- Surveys for threatened or endangered ((T&E) and Migratory Birds of High Federal Interest (MBHFI) species.

#### • Summer – June, July & August

- Survey of raptor production for nests previously located and search for nest sites of late nesting raptors.
- Record opportunistic observations of all wildlife species and surveys for T&E species and MBHFI species.
- Lagomorph density surveys of the permit area.

#### 5.9.4 Exploration, Production and Midstream Operations

E&P personnel will record avian interaction observations when observed or monthly as part of the Spill Prevention Control and Countermeasure (SPCC) monthly inspection process. Annually in the first quarter, ES will compile information for the previous year, into a report that summarizes available information, distribute it in management reports, and share trends with the affected operations and company management. This information and information submitted to the AITS will be summarized in the annual report described in section 5.8.1.

#### 5. RECORDS

• Avian Incident Tracking System (AITS): The Company's internal database for tracking negative interactions

• USFWS Bird Fatality/Injury Reporting Program at http://birdreport.fws.gov.

#### 6. REFERENCES

- 7.1 Regulatory References
  - 7.1.1 Bald and Golden Eagle Protection Act, 16 U.S.C. §§ 668 to 668d
  - 7.1.2 Migratory Bird Treaty Act, 16 U.S.C. §§ 703 to 712
  - 7.1.3 Endangered Species Act, 16 U.S.C. §§ 1531 to 1544
  - 7.1.4 Wyoming Game and Fish Department Chapter 33 Regulations

#### 7.2 Technical References

#### 7.2.1 Construction Standards

- <u>Suggested Practices for Avian Protection on Power Lines: The State of the Art in 2006</u>, published by the Avian Power Line Interaction Committee (APLIC), the Edison Electric Institute and the California Energy Commission. 2006. Washington, D.C. and Sacramento, CA.
- <u>Mitigating Bird Collisions with Power Lines The State of the Art in 1994</u>, published by the Edison Electric Institute, and the Raptor Research Foundation. 1994. Washington, D.C.
- <u>Avian Protection Plan Guidelines</u>, published by the Edison Electric Institute's Avian Power Line Interaction Committee and the US Fish and Wildlife Service. 2005.

#### 7.2.2 Other References

- <u>A Pocket Guide To Kansas Raptors</u>. This guide, which is published by the Friends of the Great Plains Nature Center, provides a reference to raptors found in the Midwest and West.
- <u>Peterson Field Guide to Birds of Western North America</u>. 2010. Fourth Edition. Houghton Mifflin Company. Boston, MA. Available from Amazon Books.
- <u>Migratory Bird List:</u> <u>http://migratorybirds.fws.gov/</u>

See Appendix D for the complete list of protected migratory bird species as of May 2010 in Wyoming.

Guidance on active nesting buffers: See Appendix B

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# APPENDIX A: RESPONSE AND REPORTING FLOWCHARTS

Response to Finding a dead or Injured Bird



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#### Detail for Responding to the Discovery of a Dead or Injured Bird

FWS = Fish and Wildlife Service



Response to Finding a Nest

#### APPENDIX B: PROTECTIONS FOR RAPTORS/SEASONAL BUFFER ZONES

#### Raptors in Wyoming

(http://www.fws.gov/wyominges/Pages/Species/Species\_SpeciesConcern/Raptors.html)

Raptors, or birds of prey, and the majority of other birds in the United States are protected by the <u>Migratory Bird Treaty Act</u>, 16 U.S.C. 703 (MBTA). A complete list of migratory bird species can be found in the Code of Federal Regulations at <u>50 CFR 10.13</u>. Eagles are also protected by the <u>Bald and Golden</u> <u>Eagle Protection Act</u>, 16 U.S.C. 668 (Eagle Act).

The MBTA protects migratory birds, eggs and nests from possession, sale, purchase, barter, transport, import, export, and take. The regulatory definition of take, defined in <u>50 CFR 10.12</u>, means to pursue, hunt, shoot, wound, kill, trap, capture, or collect, or attempt to hunt, shoot, wound, kill, trap, capture, or collect a migratory bird. Activities that result in the unpermitted take (e.g., result in death, possession, collection, or wounding) of migratory birds or their eggs are illegal and fully prosecutable under the MBTA. Removal or destruction of active nests (i.e., nests that contain eggs or young), or causing abandonment of an active nest, could constitute a violation of the MBTA, the Eagle Act, or both statutes. <u>Removal of any active migratory bird nest or any structure that contains an active nest (e.g., tree) where such removal results in take is prohibited</u>. Therefore, if nesting migratory birds are present on or near a project area, project timing is an important consideration during project planning. As discussed below, the Eagle Act provides additional protections for bald and golden eagles and their nests. For additional information concerning nests and protections under the MBTA, please see the U.S. Fish and Wildlife Service's (Service) <u>Migratory Bird Permit Memorandum, MBMP-2</u>.

The Service's Wyoming Ecological Services Field Office works to raise public awareness about the possible occurrence of birds in proposed project areas and the risk of violating the MBTA, while also providing guidance to minimize the likelihood that take will occur. We encourage you to coordinate with our office before conducting actions that could lead to the take of a migratory bird, their young, eggs, or active nests (e.g., construction or other activity in the vicinity of a nest that could result in a take). If nest manipulation is proposed for a project in Wyoming, the project proponent should also contact the Service's Migratory Bird Office in Denver at 303-236-8171 to see if a permit can be issued. Permits generally are not issued for an active nest of any migratory bird species, unless removal of the nest is necessary for human health and safety. If a permit cannot be issued, the project may need to be modified to ensure take of migratory birds, their young or eggs will not occur.

For infrastructure (or facilities) that have potential to cause direct avian mortality (e.g., wind turbines, guyed towers, airports, wastewater disposal facilities, transmission lines), we recommend locating structures away from high avian-use areas such as those used for nesting, foraging, roosting or migrating, and the travel zones between high-use areas. If the wildlife survey data available for the proposed project area and vicinity do not provide the detail needed to identify normal bird habitat use and movements, we recommend collecting that information prior to determining locations for any infrastructure that may create an increased potential for avian mortalities. We also recommend contacting the Service's Wyoming Ecological Services office for project-specific recommendations.

#### Additional Protections for Eagles

The Eagle Act protections include provisions not included in the MBTA, such as the protection of unoccupied nests and a prohibition on disturbing eagles. Specifically, the Eagle Act prohibits knowingly taking, or taking with wanton disregard for the consequences of an activity, any bald or golden eagle or their body parts, nests, chicks or eggs, which includes collection, possession, molestation, disturbance, or killing. The term "disturb" is defined as "to agitate or bother a bald or golden eagle to a degree that causes, or is likely to cause, based on the best scientific information available, (1) injury to an eagle, (2) a decrease in its productivity, by substantially interfering with normal breeding, feeding, or sheltering behavior, or (3) nest abandonment, by substantially interfering with normal breeding, feeding, or sheltering behavior" (50 CFR 22.3 and see also 72 FR 31132).

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The Eagle Act includes limited exceptions to its prohibitions through a permitting process. The Service has issued regulations concerning the permit procedures for exceptions to the Eagle Act's prohibitions (74 FR 46836), including permits to take golden eagle nests which interfere with resource development or recovery operations (50 CFR 22.25). The regulations identify the conditions under which a permit may be issued (i.e., status of eagles, need for action), application requirements, and other issues (e.g., mitigation, monitoring) necessary in order for a permit to be issued.

For additional recommendations specific to Bald Eagles please see our <u>Bald Eagle information web page</u>.

#### Recommended Steps for Addressing Raptors in Project Planning

Using the following steps in early project planning, agencies and proponents can more easily minimize impacts to raptors, streamline planning and permitting processes, and incorporate measures into an adaptive management program:

- 1. Coordinate with appropriate Service offices, Wyoming Game and Fish Department, Tribal governments, and land-management agencies at the earliest stage of project planning.
- 2. Identify species and distribution of raptors occurring within the project area by searching existing data sources (e.g., Wyoming Game and Fish Department, Federal land-management agencies) and by conducting on-site surveys.
- 3. Plan and schedule short-term and long-term project disturbances and human-related activities to avoid raptor nesting and roosting areas, particularly during crucial breeding and wintering periods
- 4. Determine location and distribution of important raptor habitat, nests, roost sites, migration zones and, if feasible, available prey base in the project impact area.
- 5. Document the type, extent, timing, and duration of raptor activity in important use areas to establish a baseline of raptor activity.
- 6. Ascertain the type, extent, timing, and duration of development or human activities proposed to occur, and the extent to which this differs from baseline conditions.
- 7. Consider cumulative effects to raptors from proposed projects when added to past, present, and reasonably foreseeable actions. Ensure that project mitigation adequately addresses cumulative effects to raptors.
- 8. Minimize loss of raptor habitats and avoid long-term habitat degradation. Mitigate for unavoidable losses of high-valued raptor habitats, including (but not limited to) nesting, roosting, migration, and foraging areas.
- 9. Monitor and document the status of raptor populations and, if feasible, their prey base post project completion, and evaluate the success of mitigation efforts.
- 10. Document meaningful data and evaluations in a format that can be readily shared and incorporated into wildlife databases (contact the Service's Wyoming Ecological Services office for details).

Protection of nesting, wintering (including communal roost sites), and foraging activities is considered essential to conserving raptors. In order to promote the conservation of migratory bird populations and their habitats, Federal agencies should implement those strategies directed by <u>Executive Order 13186</u>, "<u>Responsibilities of</u> <u>Federal Agencies To Protect Migratory Birds</u>" (66 FR 3853).

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#### Recommended Seasonal and Spatial Buffers to Protect Nesting Raptors

Because many raptors are particularly sensitive to disturbance (that may result in take) during the breeding season, we recommend implementing spatial and seasonal buffer zones to protect individual nest sites/territories (Table 1). The buffers serve to minimize visual and auditory impacts associated with human activities near nest sites. Ideally, buffers would be large enough to protect existing nest trees and provide for alternative or replacement nest trees. The size and shape of effective buffers vary depending on the topography and other ecological characteristics surrounding the nest site. In open areas where there is little or no forested or topographical separation, distance alone must serve as the buffer. Adequate nesting buffers will help ensure activities do not take breeding birds, their young or eggs. For optimal conservation benefit, we recommend that no temporary or permanent surface occupancy occur within species-specific spatial buffer zones. For some activities with very substantial auditory impacts (e.g., seismic exploration and blasting) or visual impacts (e.g., tall drilling rig), a larger buffer than listed in Table 1 may be necessary, please contact the Service's Wyoming Ecological Services office for project specific recommendations on adequate buffers.

As discussed above, for infrastructure that may create an increased potential for raptor mortalities, the spatial buffers listed in Table 1 may not be sufficient to reduce the incidence of raptor mortalities (for example, if a wind turbine is placed outside a nest disturbance buffer, but inadvertently still within areas of normal daily or migratory bird movements); therefore, please contact the Service's Wyoming Ecological Services office for project specific recommendations on adequate buffers.

Buffer recommendations may be modified on a site-specific or project-specific basis based on field observations and local conditions. The sensitivity of raptors to disturbance may be dependent on local topography, density of vegetation, and intensity of activities. Additionally, individual birds may be habituated to varying levels of disturbance and human-induced impacts. Modification of protective buffer recommendations may be considered where biologically supported and developed in coordination with the Service's Wyoming Ecological Services Field Office.

Because raptor nests are often initially not identified to species (e.g., preliminary aerial surveys in winter), we first recommend a generic raptor nest seasonal buffer guideline of January 15th – August 15th. Similarly, for spatial nesting buffers, until the nesting species has been confirmed, we recommend applying a 1-mile spatial buffer around the nest. Once the raptor species is confirmed, we then make species-specific and site-specific recommendations on seasonal and spatial buffers (Table 1).

Activities should not occur within the spatial/seasonal buffer of any nest (occupied or unoccupied) when raptors are in the process of courtship and nest site selection. Long-term land-use activities and human-use activities should not occur within the species-specific spatial buffer of occupied nests. Short-term land use and human-use activities proposed to occur within the spatial buffer of an occupied nest should only proceed during the seasonal buffer after coordination with the Service, State, and Tribal wildlife resources management agencies, and/or land-management agency biologists. If, after coordination, it is determined that due to human or environmental safety or otherwise unavoidable factors, activities require temporary incursions within the spatial and seasonal buffers, those activities should be planned to minimize impacts and monitored to determine whether impacts to birds occurred. Mitigation for habitat loss or degradation should be identified and planned in coordination with applicable agencies.

Please contact the Service's Wyoming Ecological Services Field Office if you have any questions regarding the status of the bald eagle, permit requirements, or if you require technical assistance regarding the MBTA, Eagle Act, or the above recommendations. The recommended spatial and seasonal buffers are voluntary (unless made a condition of permit or license) and are not regulatory, and they do not supersede provisions of the MBTA, Eagle Act, <u>Migratory Bird Permit Memorandum (MBMP-2</u>), and Endangered Species Act. Assessing legal compliance with the MBTA or the Eagle Act and the implementing regulations is ultimately the authority and responsibility of the Service's law enforcement personnel. Our recommendations also do not supersede Federal, State, local, or Tribal regulations or permit conditions that may be more restrictive.
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Table 1. Service's Wyoming Ecological Services Field Office's Recommended Spatial and SeasonalBuffers for Breeding Raptors for construction projects, <u>excluding</u> wind energy. For information on windenergy projects please contact the <u>Wyoming Ecological Services Office</u> (307) 772-2374.

Common Name	Spatial buffer (miles)	Seasonal buffer
Golden Eagle	0.5	January 15 - July 31
Ferruginous Hawk	1	March 15 - July 31
Swainson's Hawk	0.25	April 1 - August 31
Bald Eagle	see <u>Bald Eagl</u>	e information web page
Prairie Falcon	0.5	March 1 - August 15
Peregrine Falcon	0.5	March 1 - August 15
Short-eared Owl	0.25	March15- August 1
Burrowing Owl	0.25	April 1 – September 15
Northern Goshawk	0.5	April 1 - August 15
Additional Wyoming Raptors		
Common Name	Spatial buffer (miles)	Seasonal buffer
Osprey	0.25	April 1 - August 31
Cooper's Hawk	0.25	March 15 – August 31
Sharp-shinned Hawk	0.25	March 15 – August 31
Red-tailed Hawk	0.25	February 1 – August 15
Rough-legged Hawk (winter resident only)		
Northern Harrier	0.25	April 1 - August 15
Merlin	0.5	April 1 - August 15
American Kestrel	0.125	April 1 – August 15
Common Barn Owl	0.125	February 1 – September 15
Northern Saw-whet Owl	0.25	March 1 - August 31
Boreal Owl	0.25	February 1 – July 31
Long-eared Owl	0.25	February 1 – August 15

### Raptors of Conservation Concern (see below for more information)

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Great Horned Owl	0.125	December 1 – September 31
Northern Pygmy-Owl	0.25	April 1 – August 1
Eastern Screech -owl	0.125	March 1 – August 15
Western Screech-owl	0.125	March 1 – August 15
Great Gray Owl	0.25	March 15 – August 31

#### Raptors of Conservation Concern

The Service's <u>Birds of Conservation Concern (2008)</u> report identifies "species, subspecies, and populations of all

migratory nongame birds that, without additional conservation actions, are likely to become candidates for listing" under the Endangered Species Act (16 U.S.C 1531 et seq.). This report is intended to stimulate coordinated and proactive conservation actions among Federal, State, and private partners. The <u>Wyoming</u> <u>Partners in Flight Wyoming Bird Conservation Plan</u> identifies priority bird species and habitats, and establishes objectives for bird populations and habitats in Wyoming. This plan also recommends conservation actions to accomplish the population and habitat objectives.

We encourage project planners to develop and implement protective measures for the Birds of Conservation Concern as well as other high-priority species identified in the Wyoming Bird Conservation Plan. For additional information on the Birds of Conservation Concern that occur in Wyoming, please see our <u>Birds of Conservation</u> <u>Concern</u> web page.

#### Additional Planning Resources

Avian Power Line Interaction Committee (APLIC). 2006. Suggested Practices for Avian Protection on Power Lines: The State of the Art in 2006. Edison Electric Institute, APLIC, and the California Energy Commission. Washington, D.C. and Sacramento, CA.

Edison Electric Institute and the Raptor Research Foundation. 1996. Suggested Practices for Raptor Protection on Power Lines - The State of the Art in 1996. Washington, D.C.

Edison Electric Institute's Avian Power Line Interaction Committee and U.S. Fish and Wildlife Service. 2005. Avian Protection Plan Guidelines.

Edison Electric Institute and the Raptor Research Foundation. 1994. Mitigating Bird Collisions with Power Lines - The State of the Art in 1994. Washington, D.C.

U.S. Fish and Wildlife Service. 2000. Siting, Construction, Operation and Decommissioning of Communications Towers and Tower Site Evaluation Form (Directors Memorandum September 14, 2000), Arlington, Virginia.

U.S. Fish and Wildlife Service. 2007. National Bald Eagle Management Guidelines. United States Department of Interior, Fish and Wildlife Service, Arlington, Virginia. 23 pp.

Wyoming Game and Fish Department Internet Link to Raptor Information

#### **References**

50 CFR 10.12 – Code of Federal Regulations. Title 50--Wildlife and Fisheries, Chapter I--United States Fish and Wildlife Service, Department of the Interior, Part 10--General Provisions.

50 CFR 10.13– Code of Federal Regulations. Title 50--Wildlife and Fisheries, Chapter I--United States Fish and Wildlife Service, Department of the Interior, Part 10--General Provisions.

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50 CFR 22.3 – Code of Federal Regulations. Title 50--Wildlife and Fisheries, Chapter I--United States Fish and Wildlife Service, Department of the Interior, Part 22—Eagle Permits.

50 CFR 22.25– Code of Federal Regulations. Title 50--Wildlife and Fisheries, Chapter I--United States Fish and Wildlife Service, Department of the Interior, Part 22—Eagle Permits.

<u>66 FR 3853 - Presidential Documents. Executive Order 13186 of January 10, 2001. Responsibilities of Federal Agencies to Protect Migratory Birds. Federal Register, January 17, 2001.</u>

72 FR 31132 - Protection of Eagles; Definition of "Disturb". Final Rule. Federal Register, June 5, 2007.

74 FR 46836 - Eagle Permits; Take Necessary To Protect Interests in Particular Localities. Final Rule. Federal Register, September 11, 2009.

U.S. Fish and Wildlife Service. 2003. Migratory Bird Permit Memorandum, MBMP-2, Nest Destruction (Directors Memorandum April 15, 2003), Washington, D.C.

U.S. Fish and Wildlife Service. 2008. Birds of Conservation Concern 2008. United States Department of Interior, Fish and Wildlife Service, Division of Migratory Bird Management, Arlington, Virginia. 85 pp.

Last updated: July 1, 2010

# APPENDIX C: CONTACTS (NAMES AND PHONE NUMBERS AS OF MAY 2010.)

#### **Black Hills Corporation**

Avian Protection Plan Coordinator (APPC) Joe Jenkins, Fountain CO, Office 719-393-6685, Cell 719-650-2922

#### Environmental Services Tim Rogers, Rapid City SD, Office 605-721-2286, Cell 605-484-0134

Wyodak Mine Steve Mueller, Gillette WY, Office 307-682-3410, Cell 307-670-0368

Black Hills Power - Generation Gary Theis, Gillette WY, Office 307-687-8705, Cell 307-670-2787

Black Hills Power – Electric Distribution and Transmission Wade Hatch, Office 605-721-1470, Cell 605-786-5503

**Cheyenne Light Fuel and Power** George Escobedo, Office 307-778-2150, Cell 307-631-0841 Sandy Fuller, Office 307-778-2177

Black Hills Exploration, Production, Midstream Eric Barndt, Office 303-566-3446, Cell 303-775-9622

#### US Fish and Wildlife Service

Special Agent Scott Darrah, Casper WY, Office 307-261-6365 Ecological Services, Cheyenne WY, Office 307-772-2374 Migratory Bird Permit Office, Denver CO, 303-236-8171

#### Wyoming Game and Fish Department

Gillette Game Warden, Troy Achterhof, Gillette WY, 307-682-4353 Gillette Game Warden, Ira Leonetti, Gillette WY, 307-687-7157 Moorcroft Game Warden, John Davis, Moorcroft WY, 307-756-3357 Newcastle Game Warden, Dustin Shorma, Newcastle WY, 307-746-2248 Sundance Game Warden, Chris Teeter, Sundance WY, 307-283-1276 Cheyenne Game Warden, Mark Nelson, Cheyenne WY, 307-638-8354 Permitting Officer, Carol Havlik Casper WY, 307-233-6413 Cheyenne Office, Matt Withroder, 307-777-4585 Cheyenne Office, Joetta Osborne, 307-777-4582 Sheridan Regional Office, Sheridan WY, 307-672-7418 Casper Regional Office, Casper WY, 307-473-3400

#### Raptor Rehabilitators

Dr. Robert Farr, Cheyenne Pet Clinic, Cheyenne, 307-635-4121 Diane Morse, Gillette, 307-682-2532

Procedure Name:	Appendix D	POLICY NO.
Avian Protection – Black Hills Wyoming Operations	Page 1	E-01-01-02

### APPENDIX D: PROTECTED SPECIES AND SCEPIES OF CONCERN, WYOMING

# Wyoming Partners in Flight: Wyoming Bird Conservation Plan, Version 2.0, 1 May 2003

- Table 1:
   Level I Species Conservation Action
- Table 2: Level II Species Monitoring
- Table 3: Level III Species Local Interest
- Table 4: Level IV Species Not Considered Priority
- Table 5:Fish and Wildlife Service's Wyoming Ecological Services Field Office's Recommended<br/>Spatial and Seasonal Buffers for Breeding Raptors
- Table 6: Birds Protected by the Migratory Bird Treaty Act

Procedure Name:	Appendix D	POLICY NO.
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Table 1.

Level I (Conservation Action). Species clearly needs conservation action (CA). Declining population trend and/or habitat loss may be significant. Includes species of which Wyoming has a high percentage of and responsibility for the breeding population (R), monitoring (M), and the need for additional knowledge (K) through research into basic natural history, distribution, etc.

#### **Species**

American Bittern Trumpeter Swan<sup>a</sup> Bald Eagle<sup>a</sup> Northern Goshawk Swainson's Hawk Ferruginous Hawk Peregrine Falcon Greater Sage-Grouse<sup>a</sup> Columbian Sharp-tailed o Mountain Plover Upland Sandpiper

Peregrine Falcon Greater Sage-Grouse<sup>a</sup> **Columbian Sharp-tailed Grouse** Mountain Plover Upland Sandpiper Long-billed Curlew Wilson's Phalarope Franklin's Gull Forster's Tern Black Tern Burrowing Owl Short-eared Owl Brewer's Sparrow Sage Sparrow Baird's Sparrow<sup>b</sup> McCown's Longspur

#### Primary Habitat Type(s) Wetlands Wetlands Montane Riparian, Plains/Basin Riparian High Elevation Conifer, Mid Elevation Conifer, Aspen Plains/Basin Riparian Shrub-steppe, Shortgrass Prairie Specialized (cliffs) Shrub-steppe Mountain-foothills Shrub Shortgrass Prairie, Shrub-steppe Shortgrass Prairie Shortgrass Prairie, Meadows Wetlands Wetlands Wetlands Wetlands Shortgrass Prairie Shortgrass Prairie, Meadows Shrub-steppe, Mountain-foothills Shrub Shrub-steppe, Mountain-foothills Shrub Shortgrass Prairie Shortgrass Prairie, Shrub-steppe

<sup>a</sup>Specific management plans already exist for the Trumpeter Swan, Greater Sage-Grouse, and Bald Eagle in Wyoming.

<sup>b</sup>Species is peripheral in Wyoming.

Procedure Name:	Appendix D	POLICY NO.
Avian Protection – Black Hills Wyoming Operations	Page 3	E-01-01-02

#### Table 2.

Level II (Monitoring). The action and focus for the species is monitoring (M). Declining population trends and habitat loss are not significant at this point. Includes species of which Wyoming has a high percentage of and responsibility for the breeding population (R), species whose stability (S) may be unknown (S?), species that are peripheral (P) for breeding in the habitat or state, or additional knowledge (K) may be needed.

#### **Species**

Common Loon American White Pelican Harlequin Duck Montane Merlin Low Elevation Snowy Plover<sup>a</sup> Black-billed Cuckoo Yellow-billed Cuckoo Western Screech-Owl Eastern Screech-Owl Great Gray Owl Boreal Owl White-throated Swift Black-chinned Hummingbird<sup>a</sup> Calliope Hummingbird

Rufous Hummingbird Lewis' Woodpecker Williamson's Sapsucker Red-naped Sapsucker Three-toed Woodpecker Black-backed Woodpecker Black-backed Woodpecker Olive-sided Flycatcher Willow Flycatcher Hammond's Flycatcher Gray Flycatcher Juniper Dusky Flycatcher

Cordilleran Flycatcher Ash-throated Flycatcher Cassin's Kingbird<sup>a</sup> Loggerhead Shrike Plumbeous Vireo Western Scrub-Jay Juniper Titmouse Bushtit Juniper Pygmy Nuthatch Brown Creeper Marsh Wren

#### Primary Habitat Type(s)

Wetlands, Aquatic Aquatic Riparian Conifer Wetlands Plains/Basin Riparian Plains/Basin Riparian Plains/Basin Riparian Plains/Basin Riparian Mid Elevation Conifer, High Elevation Conifer **High Elevation Conifer** Specialized (cliffs and canyons) Plains/Basin Riparian, Shrub-steppe Mid Elevation Conifer, Montane Riparian Montane Riparian, Plains/Basin Riparian, Mid **Elevation Conifer** Mid Elevation Conifer Low Elevation Conifer, Plains/Basin Riparian Mid Elevation Conifer Aspen Mid Elevation Conifer, High Elevation Conifer Mid Elevation Conifer. High Elevation Conifer High Elevation Conifer, Mid Elevation Conifer Montane Riparian, Plains/Basin Riparian High Elevation Conifer, Aspen, Montane Riparian Woodland, Mountain-foothills Shrub Low Elevation Conifer, Aspen, Mountain-foothills Shrub Montane Riparian, Mid Elevation Conifer Juniper Woodland Juniper Woodland, Plains/Basin Riparian Shrub-steppe Mid Elevation Conifer, Low Elevation Conifer Juniper Woodland Juniper Woodland Woodland Low Elevation Conifer Mid Elevation Conifer, High Elevation Conifer Wetlands

Table 2. Continued

#### **Species**

American Dipper Golden-crowned Kinglet Western Bluebird Townsend's Solitaire

Sage Thrasher Townsend's Warbler MacGillivray's Warbler Wilson's Warbler Vesper Sparrow Lark Sparrow Lark Bunting Grasshopper Sparrow Chestnut-collared Dickcissel Bobolink Scott's Oriole

#### Primary Habitat Type(s)

Montane Riparian High Elevation Conifer Juniper Woodland, Low Elevation Conifer Mid Elevation Conifer, High Elevation Conifer, Juniper Woodland Shrub-steppe High Elevation Conifer, Mid Elevation Conifer Montane Riparian, Plains/Basin Riparian Montane Riparian Shrub-steppe Shrub-steppe Shortgrass Prairie, Shrub-steppe Shortgrass Prairie, Shrub-steppe Longspur Shortgrass Prairie Shortgrass Prairie Shortgrass Prairie, Agricultural Lands, Meadows Juniper Woodland

<sup>a</sup>Species is peripheral in Wyoming.

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Table 3.

Level III (Local Interest). Species that Wyoming Partners in Flight may recommend for conservation action (CA) that are not otherwise high priority but are of local interest (LI). Can include monitoring (M).

Species Primary	<u>Habitat Type(s)</u>
Western Grebe	Wetlands, Aquatic
Clark's Grebe	Wetlands, Aquatic
Northern Harrier	Wetlands, Meadows
Golden Eagle	Specialized (cliffs)
Prairie Falcon	Specialized (cliffs)
White-tailed Ptarmigan <sup>a</sup>	Alpine Tundra/Grassland
Blue Grouse <sup>a</sup>	Mid Elevation Conifer, High Elevation Conifer
American Avocet	Wetlands
Willet	Wetlands
Common Poorwill	Mountain-foothills Shrub, Shrub-steppe
Red-headed Woodpecker	Plains/Basin Riparian, Low Elevation Conifer
Say's Phoebe	Shrub-steppe
Clark's Nutcracker	High Elevation Conifer, Mid Elevation Conifer
Northern Rough-winged Swallow	Plains/Basin Riparian
Rock Wren	Specialized (rock outcrops)
Canyon Wren	Specialized (canyons)
Bewick's Wren	Juniper Woodland
Veery Montane	Riparian
Virginia's Warbler	Juniper Woodland, Mountain-foothills Shrub
Black-throated Gray Warbler	Juniper Woodland, Mountain-foothills Shrub
Ovenbird	Plains/Basin Riparian
Lazuli Bunting	Montane Riparian, Plains/Basin Riparian, Mountain-
Foothills Shrub	
Bullock's Oriole	Montane Riparian, Plains/Basin Riparian
Black Rosy-Finch	Alpine Tundra/Grassland, Specialized (cliffs)
Brown-capped Rosy-Finch	Alpine Tundra/Grassland, Specialized (cliffs)

<sup>a</sup>Classified as a game species in Wyoming.

Procedure Name:	Appendix D	POLICY NO.
Avian Protection – Black Hills Wyoming Operations	Page 6	E-01-01-02

Table 4.

Level IV (Not Considered Priority). Additional species of concern, but not considered a priority species; species is known to be stable (S) or increasing, or is addressed elsewhere in other management plans; no action is needed; monitoring (M) is not precluded but is not the focus; or species is extirpated (E) and no action is needed.

#### **Species**

Wood Duck<sup>a</sup> Cinnamon Teal<sup>a</sup> Canvasback<sup>a</sup> Redhead<sup>a</sup> Ring-necked Duck<sup>a</sup> **Bufflehead**<sup>a</sup> Barrow's Goldeneye<sup>a</sup> Hooded Merganser<sup>a</sup> Northern Bobwhite<sup>b</sup> Sandhill Crane<sup>a</sup> California Gull Chimney Swift Warbling Vireo Pinyon Jay Juniper **Black-billed Magpie** Mountain Chickadee Mountain Bluebird Western Tanager Green-tailed Towhee Clay-colored Sparrow **Rose-breasted Grosbeak** Black-headed Grosbeak Cassin's Finch

#### Primary Habitat Type(s)

Plains/Basin Riparian Wetlands Wetlands Wetlands Wetlands Wetlands Wetlands Aquatic Plains/Basin Riparian Wetlands Aquatic Urban Plains/Basin Riparian, Mid Elevation Conifer, Aspen Woodland Generalist High Elevation Conifer, Mid Elevation Conifer Mountain-foothills Shrub, Shrub-steppe Mid Elevation Conifer, High Elevation Conifer Mountain-foothills Shrub, Shrub-steppe Mountain-foothills Shrub, Shrub-steppe Plains/Basin Riparian, Montane Riparian Mid Elevation Conifer, Aspen Mid Elevation Conifer, High Elevation Conifer

<sup>a</sup>Specific management plans already exist for waterfowl and the Rocky Mountain Greater Sandhill Crane.

<sup>b</sup>Classified as a game species in Wyoming

Table 5: Fish and Wildlife Service's Wyoming Ecological Services Field Office's Recommended Spatial and Seasonal Buffers for Breeding Raptors

#### Raptors of Conservation Concern (see below for more information)

Common Name	Spatial buffer (miles)	Seasonal buffer
Golden Eagle	0.5	January 15 - July 31
Ferruginous Hawk	1	March 15 - July 31
Swainson's Hawk	0.25	April 1 - August 31
Bald Eagle <sup>a</sup>	see instructions below <sup>a</sup>	
Prairie Falcon	0.5	March 1 - August 15
Peregrine Falcon	0.5	March 1 - August 15
Short-eared Owl	0.25	March15- August 1
Burrowing Owl	0.25	April 1 – September 15
Northern Goshawk	0.5	April 1 - August 15

#### **Additional Wyoming Raptors**

Common Name	Spatial buffer (miles)	Seasonal buffer
Osprey	0.25	April 1 - August 31
Cooper's Hawk	0.25	March 15 – August 31
Sharp-shinned Hawk	0.25	March 15 – August 31
Red-tailed Hawk	0.25	February 1 – August 15
Rough-legged Hawk		(winter resident only)
Northern Harrier	0.25	April 1 - August 15
Merlin	0.5	April 1 - August 15
American Kestrel	0.125	April 1 – August 15
Common Barn Owl	0.125	February 1 – September 15
Northern Saw-whet Owl	0.25	March 1 - August 31
Boreal Owl	0.25	February 1 – July 31
Long-eared Owl	0.25	February 1 – August 15
Great Horned Owl	0.125	December 1 – September 31
Northern Pygmy-Owl	0.25	April 1 – August 1
Eastern Screech -owl	0.125	March 1 – August 15
Western Screech-owl	0.125	March 1 – August 15
Great Gray Owl	0.25	March 15 – August 31

<sup>a</sup>Bald Eagles: When the proposed infrastructure and facilities do not pose an increased risk of direct mortality, we recommend using the following general guidelines for work within Wyoming in order to avoid disturbing eagles and adequately protecting their habitat:

1. Conduct surveys within 0.5 mile of proposed activity for eagle nests and/or roosts during the appropriate time of year. Contact the Service's Ecological Services Wyoming Field Office if your project will occur within 0.5 mile of a known nest or roost to determine the potential impact of your activity to nesting and/or roosting bald eagles.

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- 2. Avoid project-related disturbance and habitat alteration within 0.5-mile of bald eagle nests from the period of early courtship to post-fledging of chicks (January 1 through August 15).
- 3. Avoid disturbance within 0.5 mile of communal winter roosts from November 1 to April 1.
- 4. Avoid construction of above-ground structures within 0.5-mile of bald eagle nest sites and communal winter roost sites. Below ground structures (e.g., pipelines, buried power lines, fiber optic lines) may be sited closer as long as construction occurs outside of the active nesting or roosting season and will not result in the loss of alternate nest sites or roost trees.

A protective buffer for foraging areas (i.e., a linear length of river) will also be needed if the proposed activity may preclude use of foraging areas (e.g., extensive human activities on or near the water).

In Wyoming, the nesting season occurs from February 1 to August 15 and bald eagle nest buffers should receive full implementation during this time period. For some activities (construction, seismic exploration, blasting, and timber harvest), a larger buffer around the nest may be necessary.

Sensitivity to disturbance by roosting and nesting bald eagles may vary between individual eagles based on topography, density of vegetation, and intensity of activities. Modification of protective buffer recommendations may be considered where biologically supported and developed in coordination with the Service's Wyoming Ecological Services Field Office.

### APPENDIX E: SERVICE TERRITORY MAPS

#### Black Hills Exploration and Production

### • Black Hills Power / Wyodak Mine

- > Campbell County, Wyodak, WY Electric Distribution System and Wyodak Mine
- > Weston County, Upton, WY Electric Distribution System
- > Weston County, Osage, WY Electric Distribution System
- > Weston County, New Castle, WY Electric Distribution System

# • Cheyenne Light Fuel & Power Company

> Laramie County, Cheyenne, WY – Electric Distribution System

Procedure Name:	Appendix E	POLICY NO.
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Procedure Name:	Appendix E	POLICY NO.
Avian Protection – Black Hills Wyoming Operations	Page 3	E-01-01-02

# BLACK HILLS POWER, WYOMING OPERATIONS



# Campbell County, Wyodak, WY, Electric Distribution System, and Wyodak Mine





Procedure Name:	Appendix E	POLICY NO.
Avian Protection – Black Hills Wyoming Operations	Page 5	E-01-01-02

# Weston County, Upton, WY Distribution System



# Weston County, Osage, WY Distribution System



Procedure Name:	Appendix E	POLICY NO.
Avian Protection – Black Hills Wyoming Operations	Page 7	E-01-01-02

# Weston County, New Castle, WY Distribution System



# CHEYENNE LIGHT FUEL & POWER



Procedure Name:	Appendix E	POLICY NO.
Avian Protection – Black Hills Wyoming Operations	Page 9	E-01-01-02

# Cheyenne WY, Distribution System



Procedure Name:	Appendix F	POLICY NO.
Avian Protection – Black Hills Wyoming Operations	Page 1	E-01-01-02

# APPENDIX F: BIRD MANAGEMENT POLICY

# BLACK HILLS CORPORATION COMPANY POLICY

Policy Name:				DATE ISSUED	POLICY NO.
AVIAN PR	OTECTION P	OLICY		3.15.11	E-01-02-01
				DATE EFFECTIVE	PAGE NO.
				3.15.11	Page 1 of 2
	(PAGE NO.)	(POLICY NO.)	DATED	Department	APPROVED
SUPERSEDES				Environmental Services	Management
				Reviewed by	Reviewed Date
					3.15.11

#### 1. PURPOSE

The purpose of this Policy is to set forth Black Hills Corporation's policy on managing bird interactions with electric, exploration and production, and mining operations with a commitment to reducing detrimental effects of these interactions.

### 2. SCOPE

This Policy applies to Black Hills Corporation's electric, exploration and production, and mining operations that own or operate above ground power lines and appurtenances that may cause detrimental interactions.

## 3. **DEFINITIONS**

- 3.1 <u>Company:</u> Black Hills Corporation, its subsidiaries and affiliates.
- 3.2 <u>Avian Protection Plan (APP)</u>: The programs in effect for each subsidiary of the Company to reduce the operational and avian risks that result from avian interactions.

#### 4. POLICY

Bird interactions with Company operations may cause bird injuries and mortalities, which, in turn, may result in violations of bird protection laws, outages, grass and forest fires, or raise concerns by employees, resource agencies and the public.

This Policy is intended to ensure compliance with legal requirements while improving distribution system reliability.

To fulfill this commitment, the Company will:

• Implement and comply with each comprehensive Avian Protection Plan.

Policy Name:	PAGE	POLICY NO.
Avian Protection Policy	Page 2 of 2	

- Ensure its actions comply with applicable laws, regulations, permits, and APP procedures.
- Document bird mortalities, problem poles and lines, and problem nests.
- Provide information, resources, and training to improve its employees' knowledge and awareness of the APP.
- Construct all new facilities to avian-safe standards.
- Retrofit or modify power poles where a protected bird has died or been injured. Modifications will be in accordance with APP procedures.
- Participate with public and private organizations in programs and research to reduce detrimental effects of bird interactions with power lines.

## 5. **RESPONSIBILITIES**

Company management and employees are responsible for managing bird interactions with power lines and other facilities where such interactions may occur, and are committed to reducing the detrimental effects of these interactions.



Greenhouse Gas PSD draft air permit notice for Cheyenn Prairie Generating Station Christopher Razzazian to: richard.currit

Bcc: Sara Laumann, Deirdre Rothery, Michael Boydston

05/18/2012 11:55 AM

Christopher Razzazian/R8/USEPA/US From: To: richard.currit@wyo.gov

Bcc:

Sara Laumann/R8/USEPA/US@EPA, Deirdre Rothery/R8/USEPA/US@EPA, Michael Boydston/R8/USEPA/US@EPA

Mr. Currit,

Please see attached EPA's public notice, Statement of Basis, and Draft Permit for the proposed new facility.

We will be contacting you under separate letter to satisfy our requirements under the NHPA. These documents have been sent to your office. However, we are not sure whether they will be received prior to the opening of the public comment period on Monday morning. Therefore, we are transmitting the documents electronically at this time as well.

Please do not hesitate to call with any questions or concerns. Thank you

Christopher Razzazian US EPA Region 8 (303)312-6648 razzazian.christopher@epa.gov

Chevenne Light, Fuel & Power - CPGS - 5-16-2012 cover letter to SHPO.pdf POF 🛓

Cheyenne Light, Fuel & Power - CGS - public notice for draft PSD permit.pdf

POF



Greenhouse Gas PSD draft air permit notice for Cheyenn Prairie Generating Station Christopher Razzazian to: sandra\_v\_silva 05/18/2012 11:48 AM

Cc: mark sattelberg, Julie\_Proell Bcc: Sara Laumann, Deirdre Rothery, Kimi Matsumoto

From: Christopher Razzazian/R8/USEPA/US To: sandra\_v\_silva@fws.gov Cc: mark sattelberg@fws.gov, Julie Proell@fws.gov Bcc: Sara Laumann/R8/USEPA/US@EPA, Deirdre Rothery/R8/USEPA/US@EPA, Kimi Matsumoto/R8/USEPA/US@EPA

Ms. Silva,

Per our discussion please see the public notice, Statement of Basis and Draft Permit for the new proposed facility. We are unsure whether the hard copy will be received by your office by Monday morning so we have transmitted the documents electronically in this email. Also, thank you very much Julie, for your help on this project, we'll be in touch over the following months as we finalize this action .

Thank you.

Christopher Razzazian US EPA Region 8 (303)312-6648

Chevenne Light, Fuel & Power - CPGS - 5-16-2012 cover letter to US FWS.pdf

Chevenne Light, Fuel & Power - CGS - public notice for draft PSD permit.pdf

POF

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	FYI - Fw: Greenhouse Gas PSD draft air permit notice for Cheyenn Prairie Generating Station	
Connected	Christopher Razzazian to: dcmiller 05/18/2012 11:44 AM	
	Bcc: Sara Laumann, Deirdre Rothery	
From:	Christopher Razzazian/R8/USEPA/US	
To:	dcmiller@fs.fed.us	
Bcc:	Sara Laumann/R8/USEPA/US@EPA, Deirdre Rothery/R8/USEPA/US@EPA	

Ms. Miller - FYI, please see the documents attached below.

Thank you,

Christopher

----- Forwarded by Christopher Razzazian/R8/USEPA/US on 05/18/2012 11:44 AM -----

From:	Christopher Razzazian/R8/USEPA/US
To:	jasorkin@fs.fed.us
Date:	05/18/2012 11:43 AM
Subject:	Greenhouse Gas PSD draft air permit notice for Cheyenn Prairie Generating Station

Hi Jeff,

As discussed, here is our public notice, SOB, and Draft Permit for the proposed new source. The hardcopy is in the mail, but may not arrive by Monday morning. So, here they are electronically as well.

Cheyenne Light, Fuel & Power - CGS - DRAFT SOB.pdfCheyenne Light, Fuel & Power - CPGS - DRAFT Permit.pdf

Don't hesitate to call if you have any questions or concerns. Thank you.

Christopher Razzazian US EPA Region 8 (303)312-6648 razzazian.christopher@epa.gov

Cheyenne Light, Fuel & Power - CPGS - 5-16-2012 cover letter to USDA FS.pdf

Cheyenne Light, Fuel & Power - CGS - public notice for draft PSD permit.pdf

PDF

PDF



Greenhouse Gas PSD draft air permit notice for Cheyenn Prairie Generating Station Christopher Razzazian to: jasorkin 05/18/2012 11:43 AM Bcc: Sara Laumann, Deirdre Rothery

From:Christopher Razzazian/R8/USEPA/USTo:jasorkin@fs.fed.usBcc:Sara Laumann/R8/USEPA/US@EPA, Deirdre Rothery/R8/USEPA/US@EPA

Hi Jeff,

As discussed, here is our public notice, SOB, and Draft Permit for the proposed new source. The hardcopy is in the mail, but may not arrive by Monday morning. So, here they are electronically as well.

Don't hesitate to call if you have any questions or concerns. Thank you.

Christopher Razzazian US EPA Region 8 (303)312-6648 razzazian.christopher@epa.gov

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Cheyenne Light, Fuel & Power - CPGS - 5-16-2012 cover letter to USDA FS.pdf

Cheyenne Light, Fuel & Power - CGS - public notice for draft PSD permit.pdf



 Greenhouse Gas PSD draft air permit notice for Cheyenn Prairie Generating

 Station

 Christopher Razzazian
 to: Susan\_Johnson, don\_shepherd
 05/18/2012 11:39 AM

 Bcc:
 Sara Laumann, Deirdre Rothery
 05/18/2012 11:39 AM

From: Christopher Razzazian/R8/USEPA/US

To: Susan\_Johnson@nps.gov, don\_shepherd@nps.gov

Bcc: Sara Laumann/R8/USEPA/US@EPA, Deirdre Rothery/R8/USEPA/US@EPA

Susan and Don,

Please see attached our public notice, Statement of Basis, and Draft Permit for the proposed new facility. We have sent a hard copy to Susan, but are unsure whether it will arrive by Monday morning at the start of the public comment period. Therefore, we are transmitting the documents electronically in this email.

Don't hesitate to call with any questions you may have. Thank you.

Christopher Razzazian US EPA Region 8 (303) 312-6648

Cheyenne Light, Fuel & Power - CPGS - 5-16-2012 cover letter to NPS.pdf

Cheyenne Light, Fuel & Power - CGS - public notice for draft PSD permit.pdf

POF



Greenhouse Gas PSD draft air permit notice for Cheyenn Prairie Generating Station Christopher Razzazian to: glopez 05/18/2012 11:32 AM

From: Christopher Razzazian/R8/USEPA/US To: glopez@laramiecounty.com Bcc: Sara Laumann/R8/USEPA/US@EPA, Deirdre Rothery/R8/USEPA/US@EPA

Bcc: Sara Laumann, Deirdre Rothery

Dear Mr. Lopez,

Please see attached our letter to your office and the enclosed public notice, Statement of Basis, and Draft Permit for the proposed new facility. A hard copy of these documents has been sent to your office. However, it is not clear whether they will be received by Monday morning by the opening of the public comment period. Therefore, we are providing electronic copies of these documents to you in this email.

Please do not hesitate to call with any questions you may have. Thank you,

Christopher Razzazian **US EPA Region 8** (303)312-6648 razzazian.christopher@epa.gov

Cheyenne Light, Fuel & Power - CPGS - 5-16-2012 cover letter to county health.pdf

Cheyenne Light, Fuel & Power - CGS - public notice for draft PSD permit.pdf

POF



 Fw: Greenhouse Gas PSD draft air permit notice for Cheyenn Prairie

 Generating Station

 Christopher Razzazian

 to: Allison.william

 05/18/2012 11:27 AM

 Cc:

 r.hancock, roland.hea

 Bcc:

 Sara Laumann, Deirdre Rothery

From:	Christopher Razzazian/R8/USEPA/US
To:	Allison.william@state.co.us
Cc:	r.hancock@state.co.us, roland.hea@state.co.us
Bcc:	Sara Laumann/R8/USEPA/US@EPA, Deirdre Rothery/R8/USEPA/US@EPA

Hi - for some reason the last message to you bounced back to me. I hope this makes it to you, however perhaps Roland or Chip could help me out?

Thank you very much!

Christopher

----- Forwarded by Christopher Razzazian/R8/USEPA/US on 05/18/2012 11:26 AM -----

From:	Christopher Razzazian/R8/USEPA/US
To:	sdietr@wyo.gov, allison.william@state.co.us, clark.smith@nebraska.gov
Cc:	akeyfa@wyo.gov, cander@wyo.gov, roland.hea@state.co.us, r.hancock@state.co.us
Date:	05/18/2012 11:22 AM
Subject:	Greenhouse Gas PSD draft air permit notice for Cheyenn Prairie Generating Station

Hello Gentlemen.

Please see below our letters to your offices regarding the public notice of our draft permit for the proposed Cheyenne Prairie Generating Station. We hope that the hard copies arrive at your offices by the opening of the public comment period on Monday. However, in the event that they do not, please see attached the documents in electronic format.

Please do not hesitate to call with any questions you may have. Thank you.

Christopher Razzazian US EPA Region 8 (303)312-6648 razzazian.christopher@epa.gov



Cheyenne Light, Fuel & Power - CGS - public notice for draft PSD permit.pdf



#### Cheyenne Light, Fuel & Power - CGS - DRAFT SOB.pdfCheyenne Light, Fuel & Power - CPGS - DRAFT Permit.pdf

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Greenhouse Gas PSD draft air permit notice for Cheyenn Prairie Generating Station Christopher Razzazian to: mayor, vriley

Bcc: Sara Laumann, Deirdre Rothery

05/18/2012 11:15 AM

Christopher Razzazian/R8/USEPA/US From: To: mayor@cheyennecity.org, vriley@cheyennecity.org Sara Laumann/R8/USEPA/US@EPA, Deirdre Rothery/R8/USEPA/US@EPA Bcc:

Honorable Mr. Kaysen and Ms. Riley,

Please see attached our letters to you allow with their enclosures including a public notice for this draft pre-construction air permit and the Statement of Basis and Draft Permit.

In the event that the hard copies of these documents do not arrive by mail by Monday morning at the opening of the public comment period we are transmitting the documents electronically via this email.

Please do not hesitate to call with any questions you may have. Thank you very much.

Christopher Razzazian US EPA Region 8 (303)312-6648 razzazian.christopher@epa.gov

Cheyenne Light, Fuel & Power - CPGS - 5-16-2012 cover letter to mayor of cheyenne.pdf PDF

Cheyenne Light, Fuel & Power - CPGS - 5-16-2012 cover letter to city of Cheyenne.pdf

Cheyenne Light, Fuel & Power - CGS - public notice for draft PSD permit.pdf

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Greenhouse Gas PSD draft air permit notice for Cheyenn Prairie Generating Station Christopher Razzazian to: dlathrop

Bcc: Sara Laumann, Deirdre Rothery

05/18/2012 11:09 AM

From: Christopher Razzazian/R8/USEPA/US

To: dlathrop@laramiecountyclerk.com

Bcc: Sara Laumann/R8/USEPA/US@EPA, Deirdre Rothery/R8/USEPA/US@EPA

Good morning Ms. Lathrop.

Please see attached our letter to you regarding the opening of a public comment period for the proposed Chevenne Prairie Generating Station, and the enclosed documents including the public notice (to run on Monday in the Wyoming Tribune), SOB, and Draft Permit, two letters, and the GHG PSD permit application. We anticipate that the documents will arrive via fedex by, or near, Monday morning 5/21/2012. Please retain those copies and make them available as requested in our attached letter. Thank you very much for your time and service.

Please don't hesitate to call if there are any questions.

Christopher Razzazian **US EPA Region 8** (303)312-6648 razzazian.christopher@epa.gov

Cheyenne Light, Fuel & Power - CPGS - 5-16-2012 cover letter to county clerk.pdf

The Public Notice, Statement of Basis, and Draft Permit:



Cheyenne Light, Fuel & Power - CGS - public notice for draft PSD permit.pdf

Cheyenne Light, Fuel & Power - CGS - DRAFT SOB.pdfCheyenne Light, Fuel & Power - CPGS - DRAFT Permit.pdf

The two letters referenced:





2012-05-03\_Letter\_EPA GHG PSD Comments on CO2 BACT.pdf2011-11-22\_Letter\_Response to EPA Inquires.pdf

The GHG PSD Permit Application (original and revised):

2011-09-23 Application EPA GHG - Revised - Combined.pdf Black\_Hills\_Final\_Draft\_Combined\_080411.pdf

	Greenhouse Gas PSD draft air permit notice for Cheyenn Prairie Generating Station Mark Lux Tim Rogers			
	Christopher Razzazian to: Tim.Mordhorst, Fred.Carl, 05/18/2012 10:57 AM			
	Bcc: Sara Laumann, Deirdre Rothery			
From:	Christopher Razzazian/R8/USEPA/US			
То:	Mark.Lux@blackhillscorp.com, Tim.Rogers@blackhillscorp.com, Tim.Mordhorst@blackhillscorp.com, Fred.Carl@blackhillscorp.com, Jason.Hartman@blackhillscorp.com, George.Tatar@blackhillscorp.com			
Bcc:	Sara Laumann/R8/USEPA/US@EPA, Deirdre Rothery/R8/USEPA/US@EPA			
Gentlemen -				
Good morning. Please see attached our letter to Mr. Lux, and the enclosed documents including the public notice (to run on Monday in the Wyoming Tribune), SOB, and Draft Permit.				
Cheyenne Light, Fuel & Power - CPGS - 5-17-2012 cover letter to BHC.pdf				
PDF				
Cheyenne Light, Fuel & Power - CGS - public notice for draft PSD permit.pdf				
Cheyenne Light, Fuel & Power - CPGS - DRAFT Permit.pdfCheyenne Light, Fuel & Power - CGS - DRAFT SOB.pdf				
Don't hesitate to call with any questions or concerns. Hard copy is in the mail to Mr. Lux, however it is unclear whether it will arrive by Monday morning.				
Thank you so much for working with us.				

Christopher Razzazian US EPA Region 8 (303)312-6648 razzazian.christopher@epa.gov Constructions and PSR rectify in permit nation for Querent arthropy and Substation.

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RE: Black Hills Corporation information request Rogers, Tim to: Christopher Razzazian

05/11/2012 09:51 AM

 From:
 "Rogers, Tim" <Tim.Rogers@blackhillscorp.com>

 To:
 Christopher Razzazian/R8/USEPA/US@EPA

Alright – let me know if you need anything from our end. Looking forward to seeing a draft. Have a good weekend.

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

From: Christopher Razzazian [mailto:Razzazian.Christopher@epamail.epa.gov] Sent: Friday, May 11, 2012 9:37 AM To: Rogers, Tim Subject: Re: Black Hills Corporation information request

Thanks Tim,

I thought it was 625, but one of the old emails had 629 so just had to triple check. Almost there!

Chris

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History:	This message has been replied to
To:	Christopher Razzazian/R8/USEPA/US@EPA
From:	"Rogers, 1 im" <1 im.Rogers@blackhillscorp.com>

Chris,

I've been out of town for two days in Gillette - here is the information you requested.

George Tatar DIRECTOR of GENERATION OPERATIONS II 719-696-3217

Addresses:

Black Hills Corporation 625 9th Street Rapid City, SD 57701

Black Hills Corporation P.O. Box 1400 Rapid City, SD 57709

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

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Re: Black Hills Power, Cheyenne Prairie Generating Station Christopher Razzazian to: Richard Currit Bcc: Sara Laumann, Deirdre Rothery, Mike Owens

05/09/2012 02:59 PM

From: Christopher Razzazian/R8/USEPA/US

To: Richard Currit <richard.currit@wyo.gov>

Bcc: Sara Laumann/R8/USEPA/US@EPA, Deirdre Rothery/R8/USEPA/US@EPA, Mike Owens/R8/USEPA/US@EPA

Hello Mr. Currit,

Just left you a voicemail as well. Would like to chat with you prior to all this needing to be transmitted and finalized.

The permit is scheduled to be public noticed on 5/21/2012 for thirty days, however if our letter were to be sent after that date we realize you would still be afforded a 30 day comment period if needed.

Thus far I searched the online registry (produced a list with distances to the plant site) and found nothing that could be affected. The site specific survey identified a ditch and two artifacts. I would like to get your opinion on whether the ditch needs any special treatment. My understanding is that Black Hills Corp., would not be disturbing that area.

Thanks you very much for reaching out to me.

Sincerely,

Christopher Razzazian (303)312-6648 (303)941-1796

-----Richard Currit <richard.currit@wyo.gov> wrote: ----To: Christopher Razzazian/R8/USEPA/US@EPA From: Richard Currit <richard.currit@wyo.gov> Date: 05/09/2012 12:52PM Subject: Re: Black Hills Power, Cheyenne Prairie Generating Station

Hi Christopher,

It's been about a month since we last emailed. I've received the industrial siting application, but am unable to review or comment on it until we have completed the Section 106 consultation. When might I expect a letter from your office with EPA's comments on the report and determinations of eligibility and effect? Sincerely,

Richard L. Currit Senior Archaeologist Wyoming State Historic Preservation Office 2301 Central Ave., Barrett Bldg. 3rd Floor Cheyenne, WY 82002 307-777-5497

On Tue, Apr 10, 2012 at 3:29 PM, Christopher Razzazian <Razzazian.Christopher@epamail.epa.gov> wrote:

Great,

I've been trying to get in touch with your office for quite some time. I have completed a search of the registry and Black Hills has conducted a site evaluation. I will be contacting you soon to hammer this out.

Thank you,

# Christopher Razzazian

Richard Currit ---04/10/2012 01:00:40 PM---Mr. Razzazian, Our office has received information from Black Hills Power, Inc., regarding

From: Richard Currit <richard.currit@wyo.gov> To: Christopher Razzazian/R8/USEPA/US@EPA Date: 04/10/2012 01:00 PM Subject: Black Hills Power, Cheyenne Prairie Generating Station

Mr. Razzazian,

Our office has received information from Black Hills Power, Inc., regarding the Cheyenne Light, Fuel & Power Company, Cheyenne Prairie Generating Station. According to the information from Black Hills Power you are the EPA contact for this project. This note is just to inform you that I will be the SHPO reviewer for the EPA's compliance with Section 106 of the National Historic Preservation Act, and that you may address your consultation with our office under that act to me.

I look forward to further consultation with your office concerning this project. If you have any questions, do not hesitate to contact me.

Sincerely,

Richard L. Currit Senior Archaeologist Wyoming State Historic Preservation Office 2301 Central Ave., Barrett Bldg. 3rd Floor Cheyenne, WY 82002 307-777-5497

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Re: Black Hills Power, Cheyenne Prairie Generating Station Richard Currit to: Christopher Razzazian

05/09/2012 12:52 PM

From:	Richard Currit <richard.currit@wyo.gov></richard.currit@wyo.gov>	
To:	Christopher Razzazian/R8/USEPA/US@EPA	
History:	This message has been replied to.	

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Sincerely,

Richard L. Currit Senior Archaeologist Wyoming State Historic Preservation Office 2301 Central Ave., Barrett Bldg. 3rd Floor Cheyenne, WY 82002 307-777-5497

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FW: CPGS Rogers Time to:

Rogers, Tim to: Christopher Razzazian

05/07/2012 10:03 AM

From: "Rogers, Tim" <Tim.Rogers@blackhillscorp.com> To: Christopher Razzazian/R8/USEPA/US@EPA

FYI - no address at the present time. My Plant Engineer is putting all the weight on my shoulders.

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

From: Hartman, Jason Sent: Monday, May 07, 2012 9:58 AM To: Rogers, Tim; Tatar, George Subject: RE: CPGS

We will not have an address until we record the final plat, which won't happen until we close on the purchase of the land, which won't happen until we get the air permit...

From: Rogers, Tim Sent: Monday, May 07, 2012 9:51 AM To: Tatar, George; Hartman, Jason Subject: CPGS

Good Morning,

Do we have a plant address for the site? EPA is asking.

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

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# FW: Emailing: SNL (EPA's CO2 Emissions Rule) Rogers, Tim to: Christopher Razzazian

05/03/2012 03:51 PM

 From:
 "Rogers, Tim" <Tim.Rogers@blackhillscorp.com>

 To:
 Christopher Razzazian/R8/USEPA/US@EPA

 History:
 This message has been forwarded.

Chris - I have not read the entire report yet, but thought I would send your way.

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

From: Finley, Steven Sent: Thursday, May 03, 2012 7:07 AM To: Rogers, Tim; Mordhorst, Tim; Carl, Fred Subject: Emailing: SNL (EPA's CO2 Emissions Rule)

**SNL**Financial

# Wednesday, May 02, 2012 5:51 PM ET 💥 Exclusive

Study: Smaller-than-expected number of gas plants would meet EPA's CO2 emissions rule

## By Jonathan Crawford

The U.S. EPA's proposed carbon dioxide emissions standards for new power plants may affect more recently constructed natural gas-fired plants than estimated by the agency, according to a new study by the University of California Center for Energy and Environmental Economics.

While the EPA reported that 95% of combined-cycle gas turbine units that began operations between 2006 and 2010 would meet the 1,000 pounds of CO2 per megawatt-hour standard that the agency proposed, an analysis of actual emissions and self-reported generation shows that 84% of such power plants would meet the standard, the study's authors explained in their report, "How Stringent is the EPA's Proposed Carbon Pollution Standard for New Power Plants?"

The study examined three years of CO2 emissions of combined-cycle gas turbine units that began operations between 2006 and 2010 to understand how the standards could affect generating units that are modified and become subject to the standard under the Clean Air Act's New Source Review provisions.

"If you want to know how stringent the rules are based on how power plants are constructed in the next few years, the best way is to look at the ones most recently constructed," said Matthew Kotchen, co-author of the study and an associate professor of environmental economics and policy at Yale University.

The report revealed that 71% of combined-cycle gas turbine units slated for construction through 2017 would meet the emissions target because of a trend toward smaller capacity. The authors predicted that such units with a generating capacity of 226 MW or less would fail to meet the standard. Power plants that fail to meet the standard would potentially need to employ carbon capture and storage, which has not been demonstrated on a large scale and is deemed prohibitively expensive.

The EPA's impact analysis, however, does not appear to reflect such a level of noncompliance. The agency contends that its rule will impose few costs on the power sector as the standard generally reflects the emissions profile of an efficient combined-cycle gas turbine. Combined-cycle gas turbines, which are used for

baseload generation, are generally more efficient than other types of plants as they produce additional electricity through driving a steam turbine from exhaust heat.

Kotchen noted his study's analysis does not account for the possibility that operators will adjust their power plant operations to meet the standard. As natural gas becomes cheaper, it will be more economical to run gas-fired power plants at higher utilization rates, which in turn will make it easier to comply with the proposed standards, he said.

"That 71% level is the worst case scenario. As power plants adjust their operations, I would expect that number to get quite a bit higher," he said.

While the proposed rule exempts such facilities that are used for meeting peak demand, only 10% of simple-cycle gas turbine units that began operations between 2006 and 2010 would be able to comply without additional measures.

Consistent with projections by the EPA and industry, the report found that no coal units would comply with the annual target without use of carbon capture and storage. The report analyzed CO2 emissions data for 2008, 2009 and 2010. Data was collected from the EPA's Continuous Emissions Monitoring System program as well as data on power plants from the U.S. Energy Information Administration.

The University of California Center for Energy and Environmental Economics is a joint venture of the University of California Energy Institute and the University of California Santa Barbara Bren School of Environmental Science and Management.

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SNL Financial LC, One SNL Plaza, PO Box 2124, Charlottesville, Virginia 22902 USA, (434) 977-1600

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	Report on USFWS ES Concerns Rogers, Tim to: Christopher Razzazian "Carl, Fred", "Arfmann, Dennis", "Joe.Hammond@ch2m.com"	05/03/2012 09:46 AM
	, "Rogers, Tim"	
From:	"Rogers, Tim" <tim.rogers@blackhillscorp.com></tim.rogers@blackhillscorp.com>	
To:	Christopher Razzazian/R8/USEPA/US@EPA	
Cc:	"Carl, Fred" <fred.carl@blackhillscorp.com>, "Arfmann, Dennis" <dennis.arfmann@hoganlovells.com>, "Joe.Hammond@ch2m.com" <joe.hammond@ch2m.com>, "Matt.Kizlinski@CH2M.com" <matt.kizlinski< td=""><td>@CH2M.com&gt;,</td></matt.kizlinski<></joe.hammond@ch2m.com></dennis.arfmann@hoganlovells.com></fred.carl@blackhillscorp.com>	@CH2M.com>,
History:	This message has been replied to and forwarded.	

Chris.

Another action item from our April 24, 2012 meeting was for Black Hills to provide a summary of measures taken or planned to address USFWS endangered species concerns. This document is attached - it basically provides an update to our March 2, 2012 letter. I am also taking this opportunity to package all of the associated endangered species documents in one email to assist with your response to USFWS.

- May 3, 2012 Black Hills summary of measures to address USFWS and EPA concerns related to . endangered species.
- April 16, 2012 CH2MHILL Raptor and Prairie Dog Survey.
- March 2, 2012 BHC letter addressing USFWS endangered species concerns. .
- February 14, 2012 WEST, Inc. Evaluation of Endangered Species as it is related to the CPGS.
- Black Hills Wyoming Avian Protection Plan

If you have question, please call. Thanks.

**Tim Rogers Environmental Services** (605) 721-2286 - work (605) 484-0134 - cell

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further reading.2012-05-03\_Supp\_BHC measures to address USFWS Species List for EPA .pdf

2012-04-19\_Report\_Raptor Nest and Prairie Dog Survey.pdf2012-03-02\_Letter\_ESA BA Study to EPA.pdf

2012-02-14\_Final Report\_West ESA.pdfE-01-01-02-WY Avian Protection FINAL 2011-09-06 Revised.pdf



	Black Hills: Cheyenne Prairie Generating - Comments on CO permit Rogers, Tim to: Christopher Razzazian "Carl, Fred", "Arfmann, Dennis", "Joe.Hammond@ch2m.com" Cc:, "Gordon.Schott@CH2M.com", "Doug.Huxley@CH2M.com", "Mordhorst, Tim", "Finley, Steven", Deirdre Bothery, Christian	02 BACT limits in 05/03/2012 09:14 AM
From:	"Rogers. Tim" <tim.rogers@blackhillscorp.com></tim.rogers@blackhillscorp.com>	
To:	Christopher Razzazian/R8/USEPA/US@EPA	
Cc:	"Carl, Fred" <fred.carl@blackhillscorp.com>, "Arfmann, Dennis" <dennis.arfmann@hoganlovells.com>, "Joe.Hammond@ch2m.com" <joe.hammond@ch2m.com>, "Gordon.Schott@CH2M.com" <gordon.schot< td=""><td>ott@CH2M.com&gt;,</td></gordon.schot<></joe.hammond@ch2m.com></dennis.arfmann@hoganlovells.com></fred.carl@blackhillscorp.com>	ott@CH2M.com>,
History:	This message has been replied to.	

Chris,

One of the action items from our April 24, 2012 meeting was for Black Hills to provide further analysis on our justification for the CO2 BACT limits (simple and combined cycle) we proposed in the permit application. The analysis also includes discussion on our ability to comply with the EPA's proposed NSPS limit (1000 CO2 lb/MWh).

Hard copy is in the mail. Please call if you have any questions. Thanks.

Tim Rogers **Environmental Services** (605) 721-2286 - work (605) 484-0134 - cell

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further reading.2012-05-03\_Letter\_EPA GHG PSD Comments on CO2 BACT.pdf

PDF



The BACT write-up is taking longer than I wanted - it will be coming as will the other info we discussed Friday - thanks. Rogers, Tim to: Christopher Razzazian 04/30/2012 10:49 AM

"Rogers, Tim" <Tim.Rogers@blackhillscorp.com> From: Christopher Razzazian/R8/USEPA/US@EPA To: History: This message has been replied to.

Tim Rogers **Environmental Services** (605) 721-2286 - work (605) 484-0134 - cell

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Accepted: GHG PSD - Black Hills Cheyenne Prairie Generating Station Tue 04/24/2012 2:00 PM - 4:00 PM

Location: EPA Conf. Center 2nd floor ASPEN ROOM - Call in # 1-866-299-9141 Passcode:

Tim.Rogers@	blackhillscorp.com "Rogers, Tim" has accepted this meeting invitation	
Required:	April Nowak/R8/USEPA/US@EPA, Christian Fellner/RTP/USEPA/US@EPA, Dave Svendsgaard/RTP/USEPA/US@EPA, David Painter/RTP/USEPA/US@EPA, Deirdre Rothery/R8/USEPA/US@EPA, Mike Owens/R8/USEPA/US@EPA, Sara	
Optional:	Carl Daly/R8/USEPA/US@EPA	

Portions of this document redacted. Personal privacy.



RE: Agenda for Meeting April 24, 2012 Rogers, Tim to: Christopher Razzazian 04/23/2012 11:01 AM Hide Details

From: "Rogers, Tim" <Tim.Rogers@blackhillscorp.com>

To: Christopher Razzazian/R8/USEPA/US@EPA

History: This message has been forwarded.

1 Attachment

EPA Pre-PN Meeting April 24, 2012\_final.doc

Chris,

Must have been the Friday rush to get out of the Office. Here you go.

303 - 844 - 0154 - is this the call-in number. If it would work better, I could use my call in card and set up a conference call. I could then distribute that number to the group.

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

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# Agenda

# EPA – State – BHC Meeting April 24, 2012 (2:00 pm to 4:00 pm) Bighorn Room, EPA Region VIII – Denver, CO

# **Planned attendees:**

BHC: Tim Rogers, Joe Hammond – CH2MHILL, Dennis Arfmann – Legal
EPA: Chris Razzazian, Deirdre Rothery, Mike Owens, Carl Daly, Sara Laumann, J.D.
State: Andrew Keyfauver, Cole Anderson (tentative), Nancy Vehr, AAG

2:00 pm	Introductions
2:10 pm	Topics for Discussion

# **EPA Update on GHG PSD Permit Review Status**

# **GHG BACT Limits**

- Two efficiency limits (CO2 lbs/MW-hr and Btu/kW-hr)
- Level of CO2 lbs/MW-hr in permit BHC proposed 1100 and EPA proposed 1000.

## **Endangered Species Review**

• EPA indicated no need for USFWS Consultation

## Historical, Cultural, and Archaeological Assessment.

• EPA to send letter to SHPO providing their assessment and asking for the State's comments.

## Environmental Justice – Disadvantaged Areas

- EPA recommended more public notice
- Wyoming vs National Database
- Discussion on Public Notice

3:00 pm

# **Conference Call State into meeting:**

EPA update on GHG PSD Permit Review and Date they will be prepared to PN

State update on PSD Permit Review and Date they will be prepared to PN

## Discussion on Coordinated Effort to PN Proposed AQ Permits

- Anticipated PN Date
- Newspapers
- Pre-emptive Hearing Date

### 100128

# April 24, 2012 (19) parts (19) April 24, 2012 (19) parts (19) parts Rennes Roman (FPA Weignes 10)

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Black Hills Power, Cheyenne Prairie Generating Station Richard Currit to: Christopher Razzazian

04/10/2012 01:00 PM

From:	Richard Currit <richard.currit@wyo.gov></richard.currit@wyo.gov>	
To:	Christopher Razzazian/R8/USEPA/US@EPA	
History:	This message has been replied to.	*****

Mr. Razzazian,

Our office has received information from Black Hills Power, Inc., regarding the Cheyenne Light, Fuel & Power Company, Cheyenne Prairie Generating Station. According to the information from Black Hills Power you are the EPA contact for this project. This note is just to inform you that I will be the SHPO reviewer for the EPA's compliance with Section 106 of the National Historic Preservation Act, and that you may address your consultation with our office under that act to me.

I look forward to further consultation with your office concerning this project. If you have any questions, do not hesitate to contact me.

Sincerely,

Richard L. Currit Senior Archaeologist Wyoming State Historic Preservation Office 2301 Central Ave., Barrett Bldg. 3rd Floor Cheyenne, WY 82002 307-777-5497

E-Mail to and from me, in connection with the transaction of public business, is subject to the Wyoming Public Records Act and may be disclosed to third parties. e e real 1997 - De la Staats vielen en gebruit staar gemeenten en stagengestiengestiengestienen. 1997 - De la Staarsen staar staar en gesensteren begin en e

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# RE: Black Hills Corporation: Cheyenne Prairie Generating Station - Cultural Resource Survey - January 2012 Rogers, Tim to: Christopher Razzazian 03/28/2012 08:54 AM

 From:
 "Rogers, Tim" <Tim.Rogers@blackhillscorp.com>

 To:
 Christopher Razzazian/R8/USEPA/US@EPA

 History:
 This message has been replied to.

Chris,

My error - 220 MW.

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

From: Christopher Razzazian [mailto:Razzazian.Christopher@epamail.epa.gov] Sent: Wednesday, March 28, 2012 8:53 AM To: Rogers, Tim Subject: Re: Black Hills Corporation: Cheyenne Prairie Generating Station - Cultural Resource Survey -January 2012

Tim,

Thanks for including me in that email and I will follow up with their office. Much appreciated.

I noticed you said 240 MW. That's a change from the 220 we had before. Can you confirm?

Thanks so much and hope you're having a good day.

Chris

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Black Hills Corporation: Cheyenne Prairie Generating Station - Cultural Resource Survey - January 2012 Rogers, Tim to: mary.hopkins@wyo.gov 03/27/2012 05:13 PM Cc: "Rogers, Tim", Christopher Razzazian

 From:
 "Rogers, Tim" <Tim.Rogers@blackhillscorp.com>

 To:
 "mary.hopkins@wyo.gov" <mary.hopkins@wyo.gov>

 Cc:
 "Rogers, Tim" <Tim.Rogers@blackhillscorp.com>, Christopher

 Razzazian/R8/USEPA/US@EPA
 History:

## Hi Mary,

Thanks for the insight on the Cultural Resource review process in our phone conversation today. As I discussed on the phone, Black Hills is in the process of permitting the Cheyenne Prairie Generating Station. This will be Natural Gas Combustion Turbine project designed to generate 240 MW of electricity and will be located in the Southeast portion of Cheyenne on the south-side of I-18 close immediately west of the Dry Creek Waste Water Treatment Plant.

As explained, we need to obtain an air quality permit from WDEQ and EPA (Region VIII in Denver). We are required to obtain an Air Quality Greenhouse Gas permit from EPA because the State of Wyoming elected not to regulate Greenhouse Gas emissions. Since we are obtaining a permit from a Federal Agency, we need to conduct a Cultural Resource Review on the site. You have not received requests like this from EPA in the past since the decision not to address Greenhouse Gas emissions was decided last year. It is my understanding that the legislature is reversing this decision this year.

Attached is the Cultural Resource Survey. If you have any questions concerning the report, please feel free to contact me. I will send a hard copy in the mail as well.

EPA will need to conduct the consultation, as you indicated in our phone conversation. The EPA contact is Chris Razzazian and Chris has received a copy of the survey. I have included him on the Email to facilitate the communications. Here is his full contact information. My information is below his. Also – you will be reviewing the same report through the Industrial Siting Permit process with WDEQ. Thanks again – hope to hear from you soon.

Chris Razzazian USEPA Region 8 1595 Wynkoop Street Mail Code 8P-AR Denver, CO 80202-1129

Chris's Phone number (303) 312-6648

Tim Rogers, Environmental Manager Black Hills Corporation P.O. Box 1400 Rapid City, SD 57709 (605) 721-2286 - work (605) 484-0134 - cell

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further reading.2012-01-23\_Report\_CPGS Cultural Resouce Survey.pdf

Ante



Re: Also sending word version of letter in the event you want to extract verbiage from it. Christopher Razzazian to: Rogers, Tim 03/05/2012 09:35 AM

 From:
 Christopher Razzazian/R8/USEPA/US

 To:
 "Rogers, Tim" <Tim.Rogers@blackhillscorp.com>

Excellent! Thanks Tim,

Will review and call you. Have a wonderful day.

Chris

Date:	03/02/2012 03:40 PM	of latter in the event you want to extract verbiage from it	
To:	Christopher Razzazian/R8/U	hristopher Razzazian/R8/USEPA/US@EPA	
From:	"Rogers, Tim" <tim.rogers@< th=""><th>@blackhillscorp.com&gt;</th></tim.rogers@<>	@blackhillscorp.com>	
"Rogers,	Tim" Tim Rogers Envi	vironmental Services 03/02/2012 03:40:50 PI	

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

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Also sending word version of letter in the event you want to extract verbiage from it. Rogers, Tim to: Christopher Razzazian 03/02/2012 03:40 PM

From: "Rogers, Tim" <Tim.Rogers@blackhillscorp.com> To: Christopher Razzazian/R8/USEPA/US@EPA History:

This message has been replied to and forwarded.

**Tim Rogers Environmental Services** (605) 721-2286 - work (605) 484-0134 - cell

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further reading.2012-03-01\_Draft\_CPGS EPA Cover Letter (final).docx

111



 BHC Cheyenne Prairie Generating Station - ESA Biological Assessment for

 EPA GHG PSD Permit

 Rogers, Tim to: Christopher Razzazian

 03/02/2012 03:39 PM

 Cc:

 "Rogers, Tim", "Joe.Hammond@ch2m.com"

 ..."Matt.Kizlinski@CH2M.com", "Tatar, George", "Hartman, Jason"

 "Rogers, Tim" <Tim.Rogers@blackhillscorp.com>

 Christopher Razzazian/R8/USEPA/US@EPA

 "Rogers, Tim" <Tim.Rogers@blackhillscorp.com>, "Joe.Hammond@ch2m.com"

 <Joe.Hammond@ch2m.com>, "Matt.Kizlinski@CH2M.com"

 <Joe.Hammond@ch2m.com>, "Matt.Kizlinski@CH2M.com"

 <Joe.Hammond@ch2m.com>, "Matt.Kizlinski@CH2M.com>, "Tatar, George" <George.Tatar@blackhillscorp.com>, "Hartman, Jason"

 This message has been forwarded.

History:

Chris,

From:

To: Cc:

This is the Biological Assessment for the BHC Cheyenne Prairie Generating Station. The cover letter ties together the ESA BA report, BHC WY Avian Protection Plan, and discussions/resolutions with USFWS. We hope this information is useful in your ESA consultation with the Service. If you have any questions, please call. Thanks.

P.S. The attached information has been sent hard copy.

PDF

E-01-01-02-WY Avian Protection FINAL 2011-09-06 Revised.pdf

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

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PDF

further reading.2012-03-02\_Letter\_ESA BA Study to EPA.pdf2012-02-14\_Final Report\_West ESA.pdf



RE: Black Hills Corporation - Cheyenne Prairie Generating Station -EPA-GHG Permit - SF6 electrical containing equipment Rogers, Tim to: Christopher Razzazian 02/17

02/17/2012 12:11 PM

From: To: "Rogers, Tim" <Tim.Rogers@blackhillscorp.com> Christopher Razzazian/R8/USEPA/US@EPA

Chris,

It was good. Definitely provided a clearer direction on what they are looking for and what they want. The word for the day was "avoidance". I am working with my operations people to see if can make "avoidance" happen. If we can, that is what we will transmit to you with the report.

Have a good weekend as well - don't believe we have President's Day off - need to check.

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

-----Original Message-----From: Christopher Razzazian [mailto:Razzazian.Christopher@epamail.epa.gov] Sent: Friday, February 17, 2012 11:04 AM To: Rogers, Tim Subject: Re: Black Hills Corporation - Cheyenne Prairie Generating Station -EPA-GHG Permit - SF6 electrical containing equipment

Thank you very much Tim. How did your meeting go yesterday?

Have a good weekend and Presidents' Day.

Chris

From:	"Rogers, Tim" <tim.rogers@blackhillscorp.com></tim.rogers@blackhillscorp.com>
To:	Christopher Razzazian/R8/USEPA/US@EPA
Cc:	"Joe.Hammond@CH2M.com" <joe.hammond@ch2m.com>, "Tatar,</joe.hammond@ch2m.com>
	George" <george.tatar@blackhillscorp.com>, "Hartman, Jason" <jason.hartman@blackhillscorp.com>, "Tatar, George" <george tatar@blackhillscorp.com="">, "Rogers, Tim"</george></jason.hartman@blackhillscorp.com></george.tatar@blackhillscorp.com>
	<tim.rogers@blackhillscorp.com></tim.rogers@blackhillscorp.com>
Date:	02/17/2012 10:52 AM
Subject:	Black Hills Corporation - Cheyenne Prairie Generating
	Station - EPA-GHG Permit - SF6 electrical containing equipment

## Chris,

There will be 9 breakers containing SF6 associated with the switchyard at the Cheyenne Prairie Generating Station. All breakers associated with the generators are vacuum breakers (no SF6). Therefore all SF6 breakers are associated with the switchyard. Each switchyard breaker will have 60 pounds (9 breakers X 60 lbs) of SF6 for a total of 540 lbs. The manufacturer guaranteed leak rate is 1%. This would correlate to a leakage rate of 5.4 lbs per year.

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

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Black Hills Corporation - Cheyenne Prairie Generating Station - EPA-G Permit - SF6 electrical containing equipment		
(Bread)	Rogers, Tim to: Christopher Razzazian 02/17/2012 10:52 AM	
	Cc: "Joe.Hammond@CH2M.com", "Tatar, George", "Hartman,	
	Jason", "Tatar, George", "Rogers, Tim"	
From:	"Rogers, Tim" <tim.rogers@blackhillscorp.com></tim.rogers@blackhillscorp.com>	
To:	Christopher Razzazian/R8/USEPA/US@EPA	
Cc:	"Joe.Hammond@CH2M.com" <joe.hammond@ch2m.com>, "Tatar, George" <george.tatar@blackhillscorp.com>, "Hartman, Jason" <jason.hartman@blackhillscorp.com>, "Tatar, George" <george.tatar@blackhillscorp.com>,</george.tatar@blackhillscorp.com></jason.hartman@blackhillscorp.com></george.tatar@blackhillscorp.com></joe.hammond@ch2m.com>	
History:	This message has been replied to.	

Chris,

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Tim Rogers **Environmental Services** (605) 721-2286 - work (605) 484-0134 - cell

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RE: Cheyenne Prairie Generating Station - Environmental Justice Study and Cultural Resources Report Rogers, Tim to: Christopher Razzazian 02/07/2012 04:46 PM

From:"Rogers, Tim" <Tim.Rogers@blackhillscorp.com>To:Christopher Razzazian/R8/USEPA/US@EPA

History: This message has been replied to.

#### Chris,

You are welcome. Avian will be addressed in the ESA and transmittal letter with ESA - coming soon.

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

----Original Message----From: Christopher Razzazian [mailto:Razzazian.Christopher@epamail.epa.gov] Sent: Tuesday, February 07, 2012 4:39 PM To: Rogers, Tim Subject: Re: Cheyenne Prairie Generating Station - Environmental Justice Study and Cultural Resources Report

Thanks Tim,

I will be looking at this as soon as I can. Does this include the avian plan as well?

Thanks so much Tim!

Chris

From:	"Rogers, Tim" <tim.rogers@blackhillscorp.com></tim.rogers@blackhillscorp.com>
To:	Christopher Razzazian/R8/USEPA/US@EPA
Cc:	"Joe.Hammond@CH2M.com" <joe.hammond@ch2m.com>,</joe.hammond@ch2m.com>
	"Matt.Kizlinski@CH2M.com" <matt.kizlinski@ch2m.com>, "Tatar,</matt.kizlinski@ch2m.com>
	George" <george.tatar@blackhillscorp.com>, "Hartman, Jason"</george.tatar@blackhillscorp.com>
	<pre><jason.hartman@blackhillscorp.com>, "Carl, Fred"</jason.hartman@blackhillscorp.com></pre>
	<fred.carl@blackhillscorp.com></fred.carl@blackhillscorp.com>
Date:	02/07/2012 02:48 PM
Subject:	Cheyenne Prairie Generating Station - Environmental Justice
	Study and Cultural Resources Report

### Chris,

Enclosed, you will find the Environmental Justice Study and the Cultural Resources Report (and the transmittal letter) for the Cheyenne Prairie Generating Station in Cheyenne. In the very near future, we will send the ESA report with a transmittal letter discussing how we will address the findings in the report.

FYI - All of the documents in this email have been sent in today's mail.

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

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Cheyenne Prairie Generating Station - Environmental Justice Study and Cultural Resources Report	
Rogers, Tim       to: Christopher Razzazian       02/07/2012 02:48 PM         Cc:       "Joe.Hammond@CH2M.com", "Matt.Kizlinski@CH2M.com"       02/07/2012 02:48 PM         ., "Tatar, George", "Hartman, Jason", "Carl, Fred"       02/07/2012 02:48 PM	
"Rogers, Tim" <tim.rogers@blackhillscorp.com></tim.rogers@blackhillscorp.com>	
Christopher Razzazian/R8/USEPA/US@EPA	
"Joe.Hammond@CH2M.com" <joe.hammond@ch2m.com>, "Matt.Kizlinski@CH2M.com" <matt.kizlinski@ch2m.com>, "Tatar, George" <george.tatar@blackhillscorp.com>, "Hartman, Jason" <jason.hartman@blackhillscorp.com>, "Carl, Fred" <fred.carl@blackhillscorp.com></fred.carl@blackhillscorp.com></jason.hartman@blackhillscorp.com></george.tatar@blackhillscorp.com></matt.kizlinski@ch2m.com></joe.hammond@ch2m.com>	
This message has been replied to and forwarded.	

Chris,

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FYI - All of the documents in this email have been sent in today's mail.

PDF

2012-01-23\_Report\_CPGS Cultural Resouce Survey.pdf

Tim Rogers **Environmental Services** (605) 721-2286 - work (605) 484-0134 - cell

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further reading.2012-02-07\_Letter\_EJ and Cultural Study to EPA.pdf2012-02-01\_Memo\_CPGS EJ Study.pdf



Re: Black Hills - Cheyenne Prairie Generating Station - Response to inquires on general information Christopher Razzazian to: Rogers, Tim 01/24/2012 05:47 PM Bcc: Sara Laumann, Mike Owens

From:	Christopher Razzazian/R8/USEPA/US
To:	"Rogers, Tim" < Tim.Rogers@blackhillscorp.com>
Bcc:	Sara Laumann/R8/USEPA/US@EPA, Mike Owens/R8/USEPA/US@EPA

Thanks Tim, really appreciate. Will get back to you if anything comes up with this info during the data entry. Also Carl touched base with WDEQ about your timing question, but Steve D. wasn't available to chat at the time. Hold tight if you can, I'll let you know as soon as I do.

Thanks again,

## Chris

"Rogers, Tim"		Chris, Below are the responses to some of the g	01/24/2012 05:25:18 PM
From:	"Roge	rs, Tim" <tim.rogers@blackhillscorp.com></tim.rogers@blackhillscorp.com>	
To:	Christe	opher Razzazian/R8/USEPA/US@EPA	
Cc:	"Roge	rs, Tim" <tim.rogers@blackhillscorp.com></tim.rogers@blackhillscorp.com>	
Date:	01/24/	2012 05:25 PM	
Subject:	Black Hills - Cheyenne Prairie Generating Station - Response to inquires on general information		

## Chris,

Below are the responses to some of the general information for the facility you asked for at our January 17, 2012 meeting. There will be a joint ownership of this facility between two subsidiaries of Black Hills Corporation (Black Hills Power, Inc. and Cheyenne Light, Fuel and Power Company). We would prefer that the joint ownership be represented. Understanding that the database may not accept this – then Black Hills Corporation should be listed. If you have guestions, please call.

/er
pid City,
\$8-3241

**Tim Rogers** 

Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

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Black Hills - Cheyenne Prairie Generating Station - Response to inquires on general information Rogers, Tim to: Christopher Razzazian 01/24/2012 05:25 PM Cc: "Rogers, Tim" Hide Details From: "Rogers, Tim" <Tim.Rogers@blackhillscorp.com>

To: Christopher Razzazian/R8/USEPA/US@EPA

Cc: "Rogers, Tim" <Tim.Rogers@blackhillscorp.com>

# History: This message has been replied to.

## Chris,

Below are the responses to some of the general information for the facility you asked for at our January 17, 2012 meeting. There will be a joint ownership of this facility between two subsidiaries of Black Hills Corporation (Black Hills Power, Inc. and Cheyenne Light, Fuel and Power Company). We would prefer that the joint ownership be represented. Understanding that the database may not accept this – then Black Hills Corporation should be listed. If you have questions, please call.

Facility ID: AFS:	Assigned by EPA or State Assigned by EPA or State
Facility Name:	Chevenne Prairie Generating Station
NAICS:	221112
SIC:	4911
State:	Wyoming
Reservation:	NA
Lat Long:	41° 07' 27.83" N, 104° 43' 13.34" W, Center of facility
Section, T, R:	T13N, R66W, Section 1, Laramie County, - centroid
Operator:	Black Hills Service Company, LLC
Owner:	Joint Ownership: Black Hills Power, Inc. and Cheyenne Light, Fuel and Power Company
Owner Address:	P.O. Box 1400, Rapid City, SD 57709, physical address 629 9th Street, Rapid City, SD
57701	
Contact (permit):	Tim Rogers, 605-721-2286
Operator (facility):	Not known at this time
Responsible Official:	Mark Lux, Vice President and General Manager of Power Delivery 303-568-3241
Alternate:	George Tater, Director of Generation Operations II

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

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Marker and American Strikes in anti-Still the granited volume and its and filled as a short for at Stat domain of a linear transference of the state of the st
	Re: Cheyenne Prairie Generating Station - EPA GHG - Question on Operational Situations		
Line and the second	Christopher Razzazian to: Rogers, Tim	01/11/2012 10:17 AM	
	Bcc: Sara Laumann, Mike Owens, Deirdre Rothery		
From:	Christopher Razzazian/R8/USEPA/US		
To:	"Rogers, Tim" <tim.rogers@blackhillscorp.com></tim.rogers@blackhillscorp.com>		
Bcc:	Sara Laumann/R8/USEPA/US@EPA, Mike Owens/R8/USEPA/US@EPA, Deirdre Rothery/R8/USEPA/US@EPA		

# Thank you Tim,

I think I can address the scenario. I'm glad the conversation came up earlier rather than later.

Thanks again,

Chris

"Rogers, Tim"		Chris, In our last conversation, you asked wheth	01/11/2012 09:52:00 AM
From:	"Rogers,	Tim" <tim.rogers@blackhillscorp.com></tim.rogers@blackhillscorp.com>	
To:	Christopher Razzazian/R8/USEPA/US@EPA		
Cc:	"Rogers, Tim" < Tim.Rogers@blackhillscorp.com>, "Joe.Hammond@CH2M.com"		
	<joe.ha< td=""><td>mmond@CH2M.com&gt;, "Hartman, Jason" <jason.hartman@b< td=""><td>lackhillscorp.com&gt;</td></jason.hartman@b<></td></joe.ha<>	mmond@CH2M.com>, "Hartman, Jason" <jason.hartman@b< td=""><td>lackhillscorp.com&gt;</td></jason.hartman@b<>	lackhillscorp.com>
Date:	01/11/20	12 09:52 AM	
Subject:	Cheyenne Prairie Generating Station - EPA GHG - Question on Operational Situations		

## Chris,

In our last conversation, you asked whether we would operate the simple cycle combustion turbine units associated with the combined cycle steam generator in simple cycle mode. The response is yes. If there was a problem with the steam turbine generator, the steam generated by the HRSGs (Heat Recovery Steam Generator), using heat from the gas turbine exhaust, would be diverted to the water-cooled condenser. Thus, there would be no MW generation from the steam turbine generator. This essentially would be equivalent to simple cycle operation.

The question was in reference to our CO2 (GHG) lb/MWhr proposed efficiency limit. The proposed limit for the combined cycle operation is 1100 lb/MWhr and the proposed limit for the simple cycle units is 1600 lb/MWhr.

Issue: Due to the loss of the megawatts from the steam turbine generator not operating, we may potentially be in violation with a combined cycle limit of 1100 lb/MWhr, in this scenario, due to the loss of megawatts from the steam turbine generator in the denominator of the equation for the CO2 limit. A smaller denominator will make our emissions higher.

Requested Remedy: Black Hills proposes to incorporate an Alternative Operating Scenario in the permit to specify the combined cycle combustion turbines will be subject to the 1600 lb/MWhr limit when the steam turbine generator is not operational or is not capable of generating megawatts.

Notes

- We will still be generating the same amount of CO2 in mass regardless of whether the combined cycle steam turbine is operating or not.
- 2. It is actually to our disadvantage not to be operating the steam turbine generator due to the loss of

MW generation (something we would want to avoid), but we need to account for this scenario if the steam turbine generator is not operational.

I will follow-up with a call. Thanks.

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

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Cheyenne Prairie Generating Station - Combined Cycle Question Rogers, Tim to:

Christopher Razzazian 12/22/2011 07:08 AM Cc: "Rogers, Tim" Hide Details From: "Rogers, Tim" <Tim.Rogers@blackhillscorp.com>

To: Christopher Razzazian/R8/USEPA/US@EPA

Cc: "Rogers, Tim" <Tim.Rogers@blackhillscorp.com>

## History: This message has been replied to.

Chris,

In a conversation we had a week ago, you asked a question about the operation of the combined cycle. If I recall correctly, the question was – can the combined cycle system operate with just one LM6000 turbine operating. This was discussed with our operations staff and the answer is yes. The combined cycle system can operate with just one LM6000 turbine operating. Let me know if that answers the question or if this sparks any other questions.

My plans were to get down to Denver before years end to meet and discuss any further issues and timing of permit actions (your internal review, our review, and PN), but that is not going to happen – just running out of time with end of the year deadlines. I would like to shoot for the first part of January – if that would work for you. I guess I am assuming we will get to review your proposed permit before going out to PN. This process is new to us. Will that be the case?

I will call today to open discussions on the reason I would like to meet on permit actions.

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

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RE: turbine heat rate Rogers, Tim to: Christopher Razzazian Cc: "Joe.Hammond@CH2M.com"

12/13/2011 11:14 AM

History:	This message has been replied to.	
Cc:	"Joe.Hammond@CH2M.com" <joe.hammond@ch2m.com></joe.hammond@ch2m.com>	
To:	Christopher Razzazian/R8/USEPA/US@EPA	
From:	"Rogers, Tim" < Tim.Rogers@blackhillscorp.com>	

Chris,

It should have been 366 MMBtu/hr instead of 366 btu/hr for Heat Input on page 5.3 table 5-2.

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

-----Original Message-----From: Razzazian.Christopher@epamail.epa.gov [ mailto:Razzazian.Christopher@epamail.epa.gov] Sent: Tuesday, December 13, 2011 10:41 AM To: Rogers, Tim Subject: turbine heat rate

Hi Tim,

I'm writing limits this morning :)

Do you think the application meant to list the turbines at 366 MBtu/hr or is it really 366 Btu/hr (page 5-3 of the revised version)?

I did a calculation of 9263 Btu/kWh (your requested heat rate limit) and multiplied that by the gen capacity of 37100 kWh/hr to get 343 MBtu/hr, so I would assume you meant million Btu (MBtu).

Also, since your heat rate limit in Btu/kWh results in a lower heat rate in Btu/hr than 366, would it be safe to say that your heat rate limit (of 9263 Btu/kWh or equivalently 343 MBtu/hr) is below the capacity of the turbine at 366 MBtu/hr?

Thanks Tim,

Chris

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RE: Response to Inquires Rogers, Tim to: Christopher Razzazian Cc: "Carl, Fred", "Joe.Hammond@CH2M.com" "Doug.Huxley@CH2M.com", "Tatar, George", "Hartman, Jason"

12/01/2011 09:59 AM

From: "Rogers, Tim" <Tim.Rogers@blackhillscorp.com>

# To: Christopher Razzazian/R8/USEPA/US@EPA

Cc:

"Carl, Fred" <Fred.Carl@blackhillscorp.com>, "Joe.Hammond@CH2M.com" <Joe.Hammond@CH2M.com>, "Doug.Huxley@CH2M.com" <Doug.Huxley@CH2M.com>, "Tatar, George" <George.Tatar@blackhillscorp.com>, "Hartman, Jason"

Chris - responses to your questions below.

1. In-let Heater: We need to bring the unit up to zero degrees F, when the ambient temperature is below zero degrees F, in order for GE emission limit guarantees to apply. A unit operator may operate the in-let heater to eliminate suspected icing on the unit at anytime for safety and to protect the integrity unit.

2. The 327 HP unit identified is the size needed for this facility. We don't anticipate the size of this unit changing, but if it does - we understand that we will need to submit an amendment to the permit or application. We appreciate your insight on the impacts with permitting in going with a higher HP unit. This has been brought to our operations awareness and they verified the 327 HP level needs.

We are still plugging away with the ESA and Cultural Assessment. I will keep you posted on progress and will forward final work products as received. We will also make a concerted effort to engage the SHPO with the EPA GHG permit requirements/approvals that we will need to obtain with our Industrial Siting Permit with the State of Wyoming on the cultural piece.

Thanks

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

-----Original Message-----From: Razzazian.Christopher@epamail.epa.gov [ mailto:Razzazian.Christopher@epamail.epa.gov] Sent: Wednesday, November 23, 2011 9:48 AM To: Rogers, Tim Subject: Re: Response to Inquires

Thanks Tim. Hope you have a good Holiday as well.

I appreciate your letter.

I have to say there are two questions that stem from this response letter though:

1. Regarding the use of the air heaters. It sounds like they are used anytime the outside air is less than zero degrees F. Is that what you meant?

2. With regard to the emergency generator, the info I need is more along the lines of - after considering all your options in the size ranges available what would the maximum power be (recall you have 327hp now). If all your options are at or below 327, then no change is necessary, I just need to know that. If any option would be above 327hp then we should quote that hp as a possibility.

Thanks for going through the LCRA permit. I agree with all of your comments.

Do you have any thoughts on the timing of your info responding to the expanded species listing for ESA, or news on contact with the SHPO? I know you mention in your letter that these will be coming.

Sincerely,

Christopher Razzazian US EPA (303)312-6648

From: "Rogers, Tim" <Tim.Rogers@blackhillscorp.com> To: Christopher Razzazian/R8/USEPA/US@EPA Date: 11/22/2011 02:28 PM Subject: Response to Inquires

Chris,

I have been keeping a cache of questions and discussions that we have had over the past two months. I wanted to follow-up in writing with responses to create a paper trail. The hard copy is in the mail, but I am sending a pdf version with the email.

Happy Thanksgiving - have a good weekend

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

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3. With regard to the amergency generator, the rafoll need to more slong the linus of - nhin considering of your options in the asse tangen available what would the maximum powerbe (recall you have 327hb now) and your coulons are stor below, 327. Then no change suprecision (1 list need to know that. If 369, quitare of the suprecision are store to the second 327. The more suprecision (1 list need to know that.

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Do you have any thoughts on the Sining of you into asymptotic to the expanding for ESA, ay nove on context with the SUPO 2.7 know you mouther, in your lease that there will be coming.

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Harry Thursdriving - Next a road weekend

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Re: Response to Inquires Christopher Razzazian to: Rogers, Tim Bcc: Sara Laumann, Deirdre Rothery

11/23/2011 09:48 AM

 From:
 Christopher Razzazian/R8/USEPA/US

 To:
 "Rogers, Tim" <Tim.Rogers@blackhillscorp.com>

 Bcc:
 Sara Laumann/R8/USEPA/US@EPA, Deirdre Rothery/R8/USEPA/US@EPA

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Sincerely,

Christopher Razzazian US EPA (303)312-6648

"Rogers, Tim"		Chris, I have been keeping a cache of questions	11/22/2011 02:28:16 PM	
From:	"Roge	ers, Tim" <tim.rogers@blackhillscorp.com></tim.rogers@blackhillscorp.com>		
To:	Christ	topher Razzazian/R8/USEPA/US@EPA		
Date:	11/22	/2011 02:28 PM		
Subject:	Resp	onse to Inquires		

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Happy Thanksgiving - have a good weekend

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

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Response to Inquires Rogers, Tim to: Christopher Razzazian

11/22/2011 02:28 PM

"Rogers, Tim" <Tim.Rogers@blackhillscorp.com> From: Christopher Razzazian/R8/USEPA/US@EPA To: History:

This message has been replied to and forwarded.

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Happy Thanksgiving - have a good weekend

Tim Rogers **Environmental Services** (605) 721-2286 - work (605) 484-0134 - cell

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further reading. 2011-11-22\_Letter\_Response to EPA Inquires.pdf



RE: Black Hills Cheyenne Generating Station - EPA-PSD-GHG permit Rogers, Tim to: Christopher Razzazian 10/12/2011 10:43 PM

From: "Rogers, Tim" <Tim.Rogers@blackhillscorp.com> To: Christopher Razzazian/R8/USEPA/US@EPA

Chris,

Will call tomorrow - Out all day with required supervision training today.

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

-----Original Message-----From: Razzazian.Christopher@epamail.epa.gov [ mailto:Razzazian.Christopher@epamail.epa.gov] Sent: Tuesday, October 11, 2011 8:10 AM To: Rogers, Tim Subject: Re: Black Hills Cheyenne Generating Station - EPA-PSD-GHG permit

Sure does - I will remain consistent with your numbering.

Can we talk about fugitive methane sometime? I've been looking at a pre-draft permit that EPA is writing in another Region, and to be consistent I think we might want to say something about fugitive methane.

Is that something you've already thought about as far as piping, connections, etc., etc., - or - is it still a bit early to quantify?

Hope you're doing well.

Chris Razzazian U.S. EPA (303)312-6648

From: "Rogers, Tim" <Tim.Rogers@blackhillscorp.com>
To: Christopher Razzazian/R8/USEPA/US@EPA
Cc: "Rogers, Tim" <Tim.Rogers@blackhillscorp.com>
Date: 10/09/2011 09:37 AM
Subject: Black Hills Cheyenne Generating Station - EPA-PSD-GHG permit

Chris,

Sources 12-13-14 are inlet chillers. Source 17 is the wet cooling tower.

All non-greenhouse gas sources - you are correct that they will show up in the State application since they are PM sources and the GHG application is number the way it is to stay consistent with Criteria Pollutant application. Hope that answered your question, if not - let me know. Thanks. Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

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Black Hills Cheyenne Generating Station - EPA-PSD-GHG permit Rogers, Tim to: Christopher Razzazian 10/09/2011 09:37 AM Cc: "Rogers, Tim"

 From:
 "Rogers, Tim" <Tim.Rogers@blackhillscorp.com>

 To:
 Christopher Razzazian/R8/USEPA/US@EPA

 Cc:
 "Rogers, Tim" <Tim.Rogers@blackhillscorp.com>

 History:
 This message has been replied to.

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Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

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RE: ESA Species List Rogers, Tim to: Christopher Razzazian

09/26/2011 12:06 PM

From: "Rogers, Tim" <Tim.Rogers@blackhillscorp.com> To: Christopher Razzazian/R8/USEPA/US@EPA

Anytime - give me a call.

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

-----Original Message-----From: Razzazian.Christopher@epamail.epa.gov [ mailto:Razzazian.Christopher@epamail.epa.gov] Sent: Monday, September 26, 2011 11:08 AM To: Rogers, Tim Cc: Rothery.Deirdre@epamail.epa.gov; Owens.Mike@epamail.epa.gov; Laumann.Sara@epamail.epa.gov Subject: RE: ESA Species List

Thanks Tim,

I'm wondering if there might be a need to have a quick conference call after our meeting tomorrow? I'll be getting back to you shortly.

thanks,

Chris

Chris,

Thank you. As we discussed, we plan to have our consultant conduct an informal ESA assessment with intent to identify if we are going to run into any issues. Obviously, we will want to know if there are any issues and what we have to do to mitigate the issue - if possible. The work will be done in a Section 7 format. As this work product is completed, we will forward to you.

We understand EPA is the entity preparing the Section 7 review to Wyoming USFWS. Hopefully, this document will be of some use to you in preparing your analysis for the Wyoming USFWS.

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

-----Original Message-----From: Razzazian.Christopher@epamail.epa.gov [ mailto:Razzazian.Christopher@epamail.epa.gov] Sent: Monday, September 26, 2011 10:24 AM To: Rogers, Tim Cc: Laumann.Sara@epamail.epa.gov; Owens.Mike@epamail.epa.gov; Rothery.Deirdre@epamail.epa.gov Subject: ESA Species List

Hi Tim,

I received this species list from FWS several days ago. We are meeting tomorrow with several programs to discuss procedure.

Let's be in touch over the next few days.

Thanks so much,

Chris

(See attached file: Cheyenne Light, Fuel & Power - CGS - ESA Section 7 SPECIES LIST.pdf) (this is without signature, but the sent version has it, I just haven't pdfed that one as well yet. Let me know if you need the signed version).

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RE: ESA Species List Rogers, Tim to: Christopher Razzazian Cc: Sara Laumann, Mike Owens, Deirdre Rothery

09/26/2011 10:49 AM

 From:
 "Rogers, Tim" <Tim.Rogers@blackhillscorp.com>

 To:
 Christopher Razzazian/R8/USEPA/US@EPA

 Cc:
 Sara Laumann/R8/USEPA/US@EPA, Mike Owens/R8/USEPA/US@EPA, Deirdre Rothery/R8/USEPA/US@EPA

History: This message has been replied to.

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Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

-----Original Message-----From: Razzazian.Christopher@epamail.epa.gov [ mailto:Razzazian.Christopher@epamail.epa.gov] Sent: Monday, September 26, 2011 10:24 AM To: Rogers, Tim Cc: Laumann.Sara@epamail.epa.gov; Owens.Mike@epamail.epa.gov; Rothery.Deirdre@epamail.epa.gov Subject: ESA Species List

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ESA Species List Christopher Razzazian to: Rogers, Tim Cc: Sara Laumann, Mike Owens, Deirdre Rothery

09/26/2011 10:24 AM

 From:
 Christopher Razzazian/R8/USEPA/US

 To:
 "Rogers, Tim" <Tim.Rogers@blackhillscorp.com>

 Cc:
 Sara Laumann/R8/USEPA/US@EPA, Mike Owens/R8/USEPA/US@EPA, Deirdre Rothery/R8/USEPA/US@EPA

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Chris

Cheyenne Light, Fuel & Power - CGS - ESA Section 7 SPECIES LIST.pdf (this is without signature, but the sent version has it, I just haven't pdfed that one as well yet. Let me know if you need the signed version).

	BHC -Cheyenne Generating Station - Revised EPA-PSD-GHG Application         Rogers, Tim       to: Christopher Razzazian       09/26/2011 09:40 AM         Cc:       "Carl, Fred", "Joe.Hammond@CH2M.com"       , "Lux, Mark",         Tatar, George", "Hartman, Jason"       , Carl Daly		
From:	"Rogers, Tim" <tim.rogers@blackhillscorp.com></tim.rogers@blackhillscorp.com>		
To:	Christopher Razzazian/R8/USEPA/US@EPA		
Cc:	"Carl, Fred" <fred.carl@blackhillscorp.com>, "Joe.Hammond@CH2M.com" <joe.hammond@ch2m.com>, "Lux, Mark" <mark.lux@blackhillscorp.com>, "Tatar, George" <george.tatar@blackhillscorp.com>, "Hartman, Jason"</george.tatar@blackhillscorp.com></mark.lux@blackhillscorp.com></joe.hammond@ch2m.com></fred.carl@blackhillscorp.com>		
History:	This message has been replied to and forwarded.	10	

# Good morning Chris,

Attached please find the revised BHC Cheyenne Generating Station EPA-PSD-GHG Application. I am also attaching a tracked changes application that shows the changes made to the original application.

Joe Hammond with CH2MHill submitted hard copies via Fedex that should be in your office today. Five copies will be delivered to Carl Daly.

Our goal was to address items discussed in our face-to-face meeting and phone conversations – hopefully, we achieved that goal. Please call if you have questions.

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

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further reading.2011-09-23\_Application\_EPA GHG - Revised - Combined.pdf

2011-09-23\_Application\_Comparison between Original and Revised.pdf

POF

BHO Chayming Garanzano Station - Revised EPA-PSD-GHG Application Rugan Tim ta Christopher Receivated C Title Revi "Jointamino)@ChEM.com" June Mati C Title Revis "Jointamino)@ChEM.com" Contents

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#### Sood maming Chris

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Re: CGS ESA Julie\_Proell to: Christopher Razzazian

09/14/2011 08:04 AM

 From:
 Julie\_Proell@fws.gov

 To:
 Christopher Razzazian/R8/USEPA/US@EPA

 History:
 This message has been forwarded.

Hi, Chris,

Sorry about the delay. Here is the pdf without a signature. The official letter (with signature) is in the mail. Let me know if you have any questions.

Julie M. Proell Fish and Wildlife Biologist (Energy) 5353 Yellowstone Road, Suite 308A Cheyenne, WY 82009 (307) 772-2374 x 232 (307) 772-2358 fax Julie\_Proell@fws.gov

~~~~~~~~~~

Razzazian.Christopher@epamail.epa.gov

09/13/2011 04:27 PM

To julie\_proell@fws.gov cc Subject CGS ESA

Hi Julie,

Just wanted to make sure you had my email correctly. I don't see an email from you, so wanted to check.

Thanks again so much for all your time and effort in preparing this.

Yours,

Chris



WY11SL0365\_jpCheyenneGeneratingStationBlackHillsPower.pdf



# CGS ESA

Christopher Razzazian to: julie\_proell

09/13/2011 04:27 PM

From:Christopher Razzazian/R8/USEPA/USTo:julie\_proell@fws.gov

Hi Julie,

Just wanted to make sure you had my email correctly. I don't see an email from you, so wanted to check.

Thanks again so much for all your time and effort in preparing this.

Yours,

Chris



Cheyenne Generating Station - EPA/GHG/PSD CO2 CEM issue - 9:30 am meeting 9-2-2011 Rogers, Tim to: Christopher Razzazian, Mordhorst, Tim , Finley, Steven , Carl, Fred 09/01/2011 02:43 PM

 From:
 "Rogers, Tim" <Tim.Rogers@blackhillscorp.com>

 To:
 Christopher Razzazian/R8/USEPA/US@EPA, "Mordhorst, Tim"

 <Tim.Mordhorst@blackhillscorp.com>, "Finley, Steven" <Steven.Finley@blackhillscorp.com>, "Carl, Fred" <Fred.Carl@blackhillscorp.com>

 History:
 This message has been replied to and forwarded.

All – I sent out a meeting invite, but it came back as undeliverable. Our system may be having issues. Regardless, the meeting is scheduled for 9:30 am tomorrow. The call in number is below.

Call in number: 866-242-5249 Participant Code

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

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Portions of this document redacted. Personal privacy.

ONlygeme Generating Station - REA/OHC/PSD 002 SIGN Name - 9.30 cm method 9-2-2011

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RE: ESA question Christopher Razzazian to: Rogers, Tim Bcc: julie\_proell

08/23/2011 02:04 PM

From:Christopher Razzazian/R8/USEPA/USTo:"Rogers, Tim" <Tim.Rogers@blackhillscorp.com>Bcc:julie\_proell@fws.gov

Thanks Tim,

I'll get back to you on whether we need anything further. Appreciate your quick response!

Chris

| "Rogers, Tim" |        | Chris, There are no existing infrastructure utilitie                     | 08/23/2011 01:56:01 PM |  |
|---------------|--------|--------------------------------------------------------------------------|------------------------|--|
| From:         | "Roge  | rs, Tim" <tim.rogers@blackhillscorp.com></tim.rogers@blackhillscorp.com> |                        |  |
| To:           | Christ | opher Razzazian/R8/USEPA/US@EPA                                          |                        |  |
| Date:         | 08/23/ | 2011 01:56 PM                                                            |                        |  |
| Subject:      | RE: E  | SA question                                                              |                        |  |

#### Chris,

There are no existing infrastructure utilities powerlines, natural gas pipelines, or wastewater lines. We will be installing electrical transmission lines, natural gas pipeline (underground), and wastewater line (underground) to the wastewater treatment plant adjacent to the plant. We are 90% sure we are going to the wastewater plant at this time. One other option is to obtain a NPDES discharge permit and discharge to Crow Creek. We are investigating the ability to comply with in-stream standards on this one vs wastewater treatment plant standards - as well as cost.

We plan to use either Cit water or Wastewater plant water.

Let me know if you have any further questions. Thanks.

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell -----Original Message-----From: Razzazian.Christopher@epamail.epa.gov [ mailto:Razzazian.Christopher@epamail.epa.gov] Sent: Monday, August 22, 2011 9:33 AM To: Rogers, Tim Subject: ESA question

Hi Tim,

US FWS has a question with regard to the ESA consultation, which I can't answer - can you? Thanks so much - Chris

Q: Are there existing electrical lines/gas pipelines or will that

infrastructure be constructed with the facility? If you plan on constructing that, would you be able to provide some information on what will go in and where?

Thanks so much!

Chris

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Re: ESA question Rogers, Tim to: Christopher Razzazian

08/22/2011 10:55 AM

From:"Rogers, Tim" <Tim.Rogers@blackhillscorp.com>To:Christopher Razzazian/R8/USEPA/US@EPAHistory:This message has been forwarded.

Chris. I am on it. Tim.

----- Original Message -----From: Razzazian.Christopher@epamail.epa.gov [ mailto:Razzazian.Christopher@epamail.epa.gov] Sent: Monday, August 22, 2011 09:32 AM To: Rogers, Tim Subject: ESA question

Hi Tim,

US FWS has a question with regard to the ESA consultation, which I can't answer - can you? Thanks so much - Chris

Q: Are there existing electrical lines/gas pipelines or will that infrastructure be constructed with the facility? If you plan on constructing that, would you be able to provide some information on what will go in and where?

Thanks so much!

Chris

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Re: Black Hills Section 7 ESA - Location from google earth with lat long Julie Proell to: Christopher Razzazian 08/22/2011 08:53 AM

 From:
 Julie\_Proell@fws.gov

 To:
 Christopher Razzazian/R8/USEPA/US@EPA

Hi, Christopher,

One more thing - As I was reviewing the project site information, I realized that I am unaware of the existing or proposed infrastructure that will connect to and from the proposed facility. Do you know if there are existing electrical transmission lines and natural gas pipelines in the project area that the proposed facility will tie in to? If not, do you know of proposed lines?

Thanks!

Julie M. Proell Fish and Wildlife Biologist (Energy) 5353 Yellowstone Road, Suite 308A Cheyenne, WY 82009 (307) 772-2374 x 232 (307) 772-2358 fax Julie\_Proell@fws.gov

Razzazian.Christopher@epamail.epa. gov

08/17/2011 09:17 AM

To Julie\_Proell@fws.gov cc Subject Re: Black Hills Section 7 ESA - Location from google earth with lat long

Thanks so much Julie,

That sounds good to me.

As far as current land use/habitat - I believe it is grassland with highway on one side and creek/river to the south. Keep in mind this source may or may not want to discharge water to the river before the treatment plant (I believe). At this point I don't have enough info to really assess temperature/flow impacts.

Thanks again,

Christopher Razzazian Mechanical/Environmental Engineer U.S. EPA, Region 8 Air Program (303)312-6648

From: Julie\_Proell@fws.gov To: Christopher Razzazian/R8/USEPA/US@EPA Date: 08/17/2011 07:57 AM Subject: Re: Black Hills Section 7 ESA - Location from google earth with lat long

Hi, Christopher,

Sorry I missed your call - I was pulled into a meeting about a couple of wind development projects in the state. Donna and Jim in my office gave me the information that you gave to them yesterday.

Based on the address that you gave to Jim and the close-up maps that were included with the project description, I was able to determine the exact location of the project. That should be sufficient for me to determine which species might be within the proposed project area and generate a species list for you.

Then, based on the information that I provide to you, you or your biologists should make determinations of effects for each species that might be within the project area, and send that determination, with justification, to me so that I may concur or not concur with your determinations.

I may be pulled into another meeting today, but otherwise, I should be in the office until 3:15 and all day tomorrow. Please let me know if you have any more information to add, such as a description of the current land usage or habitat on-site, or questions regarding consultation under Section 7 of the ESA.

#### Thanks!

Julie M. Proell Fish and Wildlife Biologist (Energy) 5353 Yellowstone Road, Suite 308A Cheyenne, WY 82009 (307) 772-2374 x 232 (307) 772-2358 fax Julie\_Proell@fws.gov

-----

Razzazian.Christopher@epama il.epa.gov

08/16/2011 02:10 PM

To julie\_proell@fws.gov cc

Subject Black Hills Section 7 ESA -Location from google earth with lat long

## Hi Julie,

Got your message - mine was a bit long. Give me a call and I can straighten out the location for you. Here it is below (the white area along the highway). The lat long listed in the window was for the center of the rectangle, but I suggest you verify for yourself. I could almost see the fence line in google earth that Black Hills shows in the application I sent. Anyway - give a call and we'll make sure you have the right location.

Thanks a bunch,

Chris(Embedded image moved to file: pic05000.gif)[attachment "pic05000.gif" deleted by Julie Proell/R6/FWS/DOI] Para a como de la como Averta a sucretaria

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# Wyoming State Historic Preservation Office Rogers, Tim to: Christopher Razzazian

08/18/2011 12:16 PM

From: To: "Rogers, Tim" <Tim.Rogers@blackhillscorp.com> Christopher Razzazian/R8/USEPA/US@EPA

Mary Hopkins Wyoming State Historic Preservation Office Barrett Building - 3rd Floor 2301 Central Avenue Cheyenne, WY 82002 (307) 777-7697

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

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Re: Black Hills Section 7 ESA - Location from google earth with lat long Christopher Razzazian to: Julie\_Proell 08/17/2011 09:17 AM

| From: | Christopher Razzazian/R8/USEPA/US |  |
|-------|-----------------------------------|--|
| To:   | Julie_Proell@fws.gov              |  |

Thanks so much Julie,

That sounds good to me.

As far as current land use/habitat - I believe it is grassland with highway on one side and creek/river to the south. Keep in mind this source may or may not want to discharge water to the river before the treatment plant (I believe). At this point I don't have enough info to really assess temperature/flow impacts.

Thanks again,

Christopher Razzazian Mechanical/Environmental Engineer U.S. EPA, Region 8 Air Program (303)312-6648

| ell Hi, Christopher, Sorry I missed your call - I was                    | 08/17/2011 07:57:20 AM                                                                                                                                           |
|--------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| Julie Proell@fws.gov                                                     |                                                                                                                                                                  |
| Christopher Razzazian/R8/USEPA/US@EPA                                    |                                                                                                                                                                  |
| 08/17/2011 07:57 AM                                                      |                                                                                                                                                                  |
| Re: Black Hills Section 7 ESA - Location from google earth with lat long | g                                                                                                                                                                |
|                                                                          | Julie_Proell@fws.gov<br>Christopher Razzazian/R8/USEPA/US@EPA<br>08/17/2011 07:57 AM<br>Re: Black Hills Section 7 ESA - Location from google earth with lat long |

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Thanks!

~~~~~~~

Julie M. Proell Fish and Wildlife Biologist (Energy) 5353 Yellowstone Road, Suite 308A Cheyenne, WY 82009 (307) 772-2374 x 232 (307) 772-2358 fax Julie\_Proell@fws.gov

Razzazian.Christopher@epamail.epa.gov

To julie\_proell@fws.gov

08/16/2011 02:10 PM

Subject Black Hills Section 7 ESA - Location from google earth with lat long

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Hi Julie,

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CC

Thanks a bunch,

Chris(Embedded image moved to file: pic05000.gif)[attachment "pic05000.gif" deleted by Julie Proell/R6/FWS/DOI]

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Re: Black Hills Section 7 ESA - Location from google earth with lat long Julie\_Proell to: Christopher Razzazian 08/17/2011 07:57 AM

| From:    | Julie_Proell@fws.gov                            |  |
|----------|---|--|
| To:      | Christopher Razzazian/R8/USEPA/US@EPA           |  |
| History: | This message has been replied to and forwarded. |  |

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Thanks!

Julie M. Proell Fish and Wildlife Biologist (Energy) 5353 Yellowstone Road, Suite 308A Cheyenne, WY 82009 (307) 772-2374 x 232 (307) 772-2358 fax Julie\_Proell@fws.gov

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Razzazian.Christopher@epamail.epa. gov

08/16/2011 02:10 PM

To julie\_proell@fws.gov

CC

Subject Black Hills Section 7 ESA - Location from google earth with lat long

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#### Thanks a bunch,

Chris(Embedded image moved to file: pic05000.gif)[attachment "pic05000.gif" deleted by Julie Proell/R6/FWS/DOI]

	Black Hills Section 7 ESA - Location from google earth with lat long			
	Christopher Razzazian to: julie_proell	08/16/2011 02:09 PM		
From:	Christopher Razzazian/R8/USEPA/US			
To:	julie_proell@fws.gov			

Hi Julie,

Got your message - mine was a bit long. Give me a call and I can straighten out the location for you. Here it is below (the white area along the highway). The lat long listed in the window was for the center of the rectangle, but I suggest you verify for yourself. I could almost see the fence line in google earth that Black Hills shows in the application I sent. Anyway - give a call and we'll make sure you have the right location.

Thanks a bunch,

Chris

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Re: BH Cheyenne Generating Station - EPA/PSD/GHG application Christopher Razzazian to: Rogers, Tim 08/16/2011 09:31 AM Bcc: Sara Laumann, Mike Owens

 From:
 Christopher Razzazian/R8/USEPA/US

 To:
 "Rogers, Tim" <Tim.Rogers@blackhillscorp.com>

 Bcc:
 Sara Laumann/R8/USEPA/US@EPA, Mike Owens/R8/USEPA/US@EPA

Hi Tim,

Here are some answers to your questions.

1. ESA - I have begun the process. You are correct that we will do this. If you already have any information for the area compiled you are free to submit that and we will consider it.

2. EJ - We will conduct an EJ analysis. Again if you have any information, it would be fine to submit that. This could include, but would not be limited to: outreach, translation, community projects, etc...

3. NHPA - I have searched the database for appropriate properties and will likely be the one to conduct any consultations.

Hopefully this answers your questions, let me know.

Have a great day.

Christopher Razzazian US EPA, Region 8 (303)312-6648

"Rogers, Tim"		Chris, At our July 8 meeting in Denver, there wer	08/16/2011 07:29:03 AM
From:	"Roge	ers, Tim" <tim.rogers@blackhillscorp.com></tim.rogers@blackhillscorp.com>	
To:	Christ	topher Razzazian/R8/USEPA/US@EPA	
Date:	08/16	/2011 07:29 AM	
Subject:	BH CI	heyenne Generating Station - EPA/PSD/GHG application	

Chris,

At our July 8 meeting in Denver, there were three items that we discussed that we would like to follow-up on.

- 1. Endangered Species Act;
- 2. Environmental Justice disadvantaged areas; and
- 3. National Historic Preservation Act.

If I recall correctly, EPA was going to determine if these requirements applied with this permit. Here is my understanding on these items.

1. ESA – I was not certain on whether this was something EPA would conduct or whether we would conduct the analysis. If it is our responsibility, we would consider just moving forward with the review to make it a non-issue. We would just need to know what is expected.

2. Environmental Justice - I believe it was stated that EPA would make the call on Environmental Justice in the sense if you would identify any disadvantaged areas near the facility that needed to be taken into

#### consideration.

3. NHPA – if this applies, we would initiate the process. It is my understanding that this approval goes through the National agency and is then approved at the State level. Again, if this is something we would conduct, we would move forward with it to make it a non-issue.

Could you provide an update on these items? Again, if it appears that it will take a while to obtain an answer, we would like to move forward with the study or review to make them a non-issue in moving forward with the permitting process. Thanks.

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell



Re: I will call in a little bit - 
Christopher Razzazian to: Rogers, Tim

08/09/2011 09:45 AM

 From:
 Christopher Razzazian/R8/USEPA/US

 To:
 "Rogers, Tim" <Tim.Rogers@blackhillscorp.com>

Oh thanks Tim, I see - each.

Thanks

Chris

"Rogers, T	im" I am taking pto in the afternor	ons this week - hom	08/09/2011 08:26:52 AM
From:	"Rogers, Tim" < Tim.Rogers@blackhillscor	p.com>	
To:	Christopher Razzazian/R8/USEPA/US@F	PA	

the second s		
Subject:	I will call in a little bit -	
Date:	08/09/2011 08:26 AM	
10:	Christopher Razzazian/R8/USEPA/US@EPA	

I am taking pto in the afternoons this week - home project.

With a quick look, it appears the numbers are okay. In section three, it states the CO2 are for each turbine and section 5 combined all of the emissions – so 6 X 4,117.00 tons.

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell



I will call in a little bit -Rogers, Tim to: Christopher Razzazian

08/09/2011 08:26 AM

 From:
 "Rogers, Tim" <Tim.Rogers@blackhillscorp.com>

 To:
 Christopher Razzazian/R8/USEPA/US@EPA

 History:
 This message has been replied to.

I am taking pto in the afternoons this week - home project.

With a quick look, it appears the numbers are okay. In section three, it states the CO2 are for each turbine and section 5 combined all of the emissions – so 6 X 4,117.00 tons.

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell



RE: PSD Permitting timelines Rogers, Tim to: Christopher Razzazian

From: "Rogers, Tim" <Tim.Rogers@blackhillscorp.com> To: Christopher Razzazian/R8/USEPA/US@EPA

Chris - thanks for the clarification.

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

----Original Message----From: Christopher Razzazian [mailto:Razzazian.Christopher@epamail.epa.gov] Sent: Thursday, July 14, 2011 3:29 PM To: Rogers, Tim Subject: Re: PSD Permitting timelines

Hi Tim,

Thanks for your time today. As I mentioned on the phone, the completeness review for PSD is actually 30 days.

from 40 CFR 124.3(c):

"The Regional Administrator shall review for completeness every application for an EPA-issued permit. Each application for an EPA-issued permit submitted by a...major PSD stationary source or major PSD modification...should be reviewed for completeness by the Regional Administrator within 30 days of its receipt."

Thanks so much and hope you have safe travels.

Yours,

Christopher Razzazian U.S. EPA Region 8

Chad and Chris - I excluded the "commence construction" time period after permit issuance. Please let me know if these timeframes are accurate. Thanks.

| Process | Review Review Notice Notice Construction | (public after permit notice) issuance --| EPA 12 mo 60 days NA 30 days 30 days 18 mo --| WDEQ\* |12-18 mo | 30 days | 60 days | 30 days | 30 days? 24 mo --1

\*WDEQ does not have specified timelines in their rules Chapter 6, Section 4 for PSD permits. They attempt to following the time-lines in Section 2, but are not legally bound to these timelines.

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

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Re: PSD Permitting timelines Christopher Razzazian to: Rogers, Tim Bcc: Sara Laumann, Mike Owens, Alexis North, Carl Daly, "Schlichtemeier, Chad"

07/14/2011 03:28 PM

 From:
 Christopher Razzazian/R8/USEPA/US

 To:
 "Rogers, Tim" <Tim.Rogers@blackhillscorp.com>

 Bcc:
 Sara Laumann/R8/USEPA/US@EPA, Mike Owens/R8/USEPA/US@EPA, Alexis<br/>North/R8/USEPA/US@EPA, Carl Daly/R8/USEPA/US@EPA, "Schlichtemeier, Chad"<br/><CSchli@wyo.gov>

Hi Tim,

Thanks for your time today. As I mentioned on the phone, the completeness review for PSD is actually 30 days.

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Thanks so much and hope you have safe travels.

Yours,

Christop	her	Razzazian
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U.S. EPA R	egion 8		2
"Rogers, Tim"		Chad and Chris - I excluded the "commence con	07/13/2011 03:56:18 PM
From: To:	"Roge Chad	ers, Tim" <tim.rogers@blackhillscorp.com> Schlichtemeier <chad.schlichtemeier@wyo.gov>, Christopher</chad.schlichtemeier@wyo.gov></tim.rogers@blackhillscorp.com>	
Date:	Razza	azian/R8/USEPA/US@EPA	
Subject:	PSD F	Permitting timelines	

Chad and Chris – I excluded the "commence construction" time period after permit issuance. Please let me know if these timeframes are accurate. Thanks.

	Permit Process	Completeness Review	Technical Review	Public Notice	Hearing Notice (public notice)	Commence Construction after permit issuance
EPA	12 mo	60 days	NA	30 days	30 days	18 mo
WDEQ*	12-18 mo	30 days	60 days	30 days	30 days?	24 mo

\*WDEQ does not have specified timelines in their rules Chapter 6, Section 4 for PSD permits. They attempt to following the time-lines in Section 2, but are not legally bound to these timelines

Tim Rogers Environmental Services (605) 721-2286 - work

#### (605) 484-0134 - cell

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Ched and Chris – I excluded the "commence sonalization" hine period after pyrinit intelerion'. Plaque ler

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Trin Rognes Economotol Sympose (605) 723-2285 - work



PSD Permitting timelines Rogers, Tim to: Chad Schlichtemeier, Christopher Razzazian

07/13/2011 03:56 PM

 

 From:
 "Rogers, Tim" <Tim.Rogers@blackhillscorp.com>

 To:
 Chad Schlichtemeier <chad.schlichtemeier@wyo.gov>, Christopher Razzazian/R8/USEPA/US@EPA

History:

This message has been replied to and forwarded.

Chad and Chris – I excluded the "commence construction" time period after permit issuance. Please let me know if these timeframes are accurate. Thanks.

	Permit	Completenes	Technical	Publi	Hearing	Commence	
	Proces s	s Review	Review	c Notic e	Notice (public notice)	Construction after permit issuance	
EPA	12 mo	60 days	NA	30 days	30 days	18 mo	
WDEQ *	12-18 mo	30 days	60 days	30 days	30 days?	24 mo	

\*WDEQ does not have specified timelines in their rules Chapter 6, Section 4 for PSD permits. They attempt to following the time-lines in Section 2, but are not legally bound to these timelines.

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell



BHC Cheyenne CT Project - EPA/WDEQ Permitting timeframes Rogers, Tim to: Chad Schlichtemeier, Christopher Razzazian 07/1

07/13/2011 11:37 AM

 From:
 "Rogers, Tim" <Tim.Rogers@blackhillscorp.com>

 To:
 Chad Schlichtemeier <chad.schlichtemeier@wyo.gov>, Christopher

 Razzazian/R8/USEPA/US@EPA

History:

This message has been forwarded.

Chad and Chris,

Based upon our discussions last week, does the table below capture the PSD permitting timeframes for both your agencies?

	Permit Proces s	Completenes s Review	Technical Review	Publi c Notic e	Hearing Notice (public notice)
EPA	12 months	60 days	NA	30 days	30 days
WDEQ *	12-18 months	30 days	60 days	30 days	?

\*WDEQ does not have specified timelines in Chapter 6, Section 4 for PSD permits. Their practice is to follow the time-lines in Section 2, but they are not legally bound to these timelines.

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell



Black Hills Corporation's - Cheyenne CT Project - Meeting Agenda for Pre-application meeting with EPA on July 8, 2011 Rogers, Tim to: Carl Daly, Christopher Razzazian, Chad Schlichtemeier 07/07/2011 01:41 PM Cc: "Rogers, Tim" Hide Details From: "Rogers, Tim" <Tim.Rogers@blackhillscorp.com>

To: Carl Daly/R8/USEPA/US@EPA, Christopher Razzazian/R8/USEPA/US@EPA, Chad Schlichtemeier <chad.schlichtemeier@wyo.gov>

Cc: "Rogers, Tim" <Tim.Rogers@blackhillscorp.com>

1 Attachment

W

EPA Pre-Application Meeting Agenda\_July 8 2011\_Final.doc

Carl, Chris, and Chad,

Attached please find the meeting agenda for tomorrow. We have a PowerPoint presentation that we will give to kick off the meeting.

Chad has indicated that he will be traveling down for the meeting.

See you tomorrow.

Tim Rogers Environmental Services (605) 721-2286 - work (605) 484-0134 - cell

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# **Cheyenne Combustion Turbine Project**

EPA Pre-Application Meeting 9:00 AM – July 8, 2011 2<sup>nd</sup> Floor Conference Room, EPA Region VIII, Denver, Colorado

#### Agenda

#### 1. Introductions

# 2. Cheyenne Gas Generating Station Project Description

- Renewable Following
- Black Hills Business Purpose
- Black Hills Operating Cycle
- Combined Cycle/Simple Cycle CT Project

## 3. EPA Permitting Process – GHG

#### 4. WDEQ Permitting Process - Criteria Pollutants and HAPs

#### 5. Discussion for EPA - GHG

- No GHG Modeling
- GHG Guidance
- GHG BACT Review (5 Step BACT Review Process)
- Combined public notice and comment, combined hearing, separate application and permits.

#### 6. Other Potential Issues:

#### 7. Establish EPA, WDEQ, BHC, and CH2MHILL Point of Contacts

#### Contacts

Black Hills Corporation         frogers         Black Hills         frogers(2b)-corp.com         605-721-2286 W           Environmental Manager         Permit Lead         feat@bh-corp.com         605-721-2286 W           Fred Carl         Black Hills         feat@bh-corp.com         605-721-2286 W           Environmental Director         Black Hills         feat@bh-corp.com         605-721-2219 W           Environmental Director         Black Hills         fmordhorst@bh-corp.com         605-721-2181 W           Environmental Manager         CEM's         605-390-9033 C         605-390-9033 C           George Tatar         Black Hills         fmordhorst@bh-corp.com         719-696-3217 W           Operations         Jason hartman@blackhillscorp.com         719-696-3217 W           Jason Hartman         Black Hills         Jason hartman@blackhillscorp.com         720-413-9199 C           CH2MHILL         Permit Consultants         720-286-5919 W         720-413-9199 C           Joe Hammond         CH2MHILL         Joe.hammond@ch2m.com         720-286-5919 W           Permit Consultant         Joe.hammond@ch2m.com         720-286-5919 W           Joe Hammond         CH2MHILL         Sobert.Pearson@ch2m.com         720-286-5919 W           Gordon Schott         CH2MHILL         Sobert.Pearson@ch2m.com
Tim Rogers       Black Hills       trogers@bh-corp.com       605-721-2286 W         Environmental Manager       Permit Lead       605-484-0134 C         Fred Cari       Black Hills       fcat(@bh-corp.com       605-721-2219 W         Environmental Director       605-739-8056 C       605-739-8056 C         Tim Mordhorst       Black Hills       fmordhorst@bh-corp.com       605-721-2181 W         Environmental Manager       CEM's       605-390-9933 C         George Tatar       Black Hills       george tatar@blackhillscorp.com       719-696-3217 W         Operations       303-945-6619 C       303-945-6619 C         Jason Hartman       Black Hills       Jason hartman@blackhillscorp.com       720-413-9199 C         CH2MHILL - Permitting Consultants       Joe.hammond@ch2m.com       720-286-5919 W         Joe Hammond       CH2MHILL       Robert Pearson@ch2m.com       720-286-5919 W         Permit Consultant       303-517-9102 C       Gordon Schott@ch2m.com       720-286-5056 W         Gordon Schott       CH2MHILL       Bobert Pearson@ch2m.com       720-286-5134 W         BACT       Bradley.nyan@ch2m.com       720-286-5134 W       303-726-5629 C         Wyoming Department of Environmental Quality       Thad schlichtemeier@wyo.gov       307-777-5924 W         PSD
Environmental Manager     Permit Lead     605-484-0134 C       Fred Carl     Black Hills     fcarl@bh-corp.com     605-721-2219 W       Environmental Director     605-390-8056 C     605-390-8056 C       Tim Mordhorst     Black Hills     fmordhorst@bh-corp.com     605-721-2181 W       Environmental Manager     CEM's     605-390-9933 C     605-390-9933 C       George Tatar     Black Hills     George tatar@blackhillscorp.com     719-696-3217 W       Operations     303-945-6619 C     303-945-6619 C       Jason Hartman     Black Hills     Jason hartman@blackhillscorp.com     720-413-9199 C       CH2MHILL - Permitting Consultants     Joe.hammond@ch2m.com     720-286-5919 W       Joe Hammond     CH2MHILL     Robert Pearson@ch2m.com     720-286-5056 W       Bob Pearson     CH2MHILL     Robert Pearson@ch2m.com     720-286-5056 W       Gordon Schott     CH2MHILL     Gordon Schott@ch2m.com     720-286-5134 W       BACT     Schott@ch2m.com     720-286-5134 W       BACT     Bradley_nyan@ch2m.com     720-286-5134 W       ME Manager     Engineering     303-726-5629 C       Wyoming Department of Environmental Quality     720-286-5121 W       Chad Schlichterneier     WDEQ     chad schlichterneier@wyo.gov     307-777-5924 W       PSD Permit Director     WDEQ
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Operations303-945-6619 CJason HartmanBlack HillsJason hartman@blackhillscorp.com303-566-3445 WOperations720-413-9199 CCH2MHILL – Permitting ConsultantsJoe.hammond@ch2m.com720-286-5919 WJoe HammondCH2MHILLJoe.hammond@ch2m.com720-286-5919 WPermit ConsultantPermit Consultant719-330-1771 CBob PearsonCH2MHILLRobert.Pearson@ch2m.com720-286-5056 WPermit ConsultantGordon.Schott@ch2m.com720-286-5013 WGordon SchottCH2MHILLGordon.Schott@ch2m.com720-286-5134 WBACTBACT720-286-5110 WBrad RyanCH2MHILLBradley.ryan@ch2m.com720-286-5121 WME ManagerEngineering303-726-5629 CWyoming Department of Environmental QualityS00307-777-5924 WChad SchlichtemeierWDEQchad.schlichtemeier@wyo.gov307-777-5924 WAndy KeyfauverWDEQInterventionIntervention
Jason HartmanBlack Hills OperationsJason.hartman@blackhillscorp.com303-566-3445 W 720-413-9199 CCH2MHILL – Permitting ConsultantsJoe.hammond@ch2m.com720-286-5919 W 719-330-1771 CJoe HammondCH2MHILL Permit ConsultantJoe.hammond@ch2m.com720-286-5956 W 303-517-9102 CBob PearsonCH2MHILL Permit ConsultantRobert.Pearson@ch2m.com720-286-5056 W 303-517-9102 CGordon SchottCH2MHILL Permit ConsultantGordon.Schott@ch2m.com720-286-5134 W 720-286-5134 W 720-586-6116 CBrad RyanCH2MHILL BACTBradley.ryan@ch2m.com720-286-5121 W 303-726-5629 CWyoming Department of Environmental QualitySold schlichtemeier@wyo.gov307-777-5924 WChad Schlichtemeier ModelingWDEQChad.schlichtemeier@wyo.gov307-777-5924 WAndy KeyfauverWDEQIntervintion of the section
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Joe HammondCH2MHILLJoe.hammond@ch2m.com720-286-5919 WPermit ConsultantPermit Consultant719-330-1771 CBob PearsonCH2MHILLRobert.Pearson@ch2m.com720-286-5056 WBod PearsonCH2MHILLGordon.Schott@ch2m.com720-286-5134 WGordon SchottCH2MHILLGordon.Schott@ch2m.com720-286-5134 WBACTBACT720-286-5116 C8Brad RyanCH2MHILLBradley.ryan@ch2m.com720-286-5121 WME ManagerEngineering303-726-5629 CWyoming Department of Environmental QualityChad SchlichtemeierWDEQChad.schlichtemeier@wyo.gov307-777-5924 WPSD Permit DirectorWDEQChad.schlichtemeier@wyo.gov307-777-5924 WAndy KeyfauverWDEQImage: MDEQImage: MDEQModelingMDEQImage: MDEQImage: MDEQAndy KeyfauverWDEQImage: MDEQImage: MDEQ
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Permit Writer
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Permit Writer
EPA
Legal



#### UNITED STATES ENVIRONMENTAL PROTECTION AGENCY REGION 8 1595 Wynkoop Street DENVER, CO 80202-1129 Phone 800-227-8917

http://www.epa.gov/region08

May 23, 2012

# **MEMORANDUM**

- SUBJECT: Record of Communication conference call regarding Draft GHG PSD permit for Black Hills Corp./Cheyenne Light Fuel & Power Cheyenn Prairie Generating Station
- FROM: Christopher Razzazian

TO: Cheyenne Prairie Generating Station GHG PSD permit docket

This memorandum is to serve as a record of communication for a conference call that occurred on 5/22/2012 from 1:30 p.m. - 2:30 p.m.

# Attendees:

- <u>EPA</u> Christopher Razzazian Air Program Deirdre Rothery - Air Program, Unit Chief Sara Laumann - Office of Regional Council
- <u>Black Hills Corp.</u> Tim Rogers - Black Hills Corp. Fred Carl - Black Hills Corp. Tim Mordhorst - Black Hills Corp. Dennis Arfmann - legal council

# Summary of phone call

# **Environmental Justice (EJ)**

Black Hills notes that this is discussed in the Statement of Basis (SOB) and wonders why ESA and NHPA were not touched upon in the SOB. EPA responded that the SOB provides the current EPA policy for EJ in GHG PSD permitting and went on to explain ESA and NHPA requirements (see below).

# **Endangered Species Act (ESA)**

Black Hills would like the public record available for public comment to include the efforts to date submitted to EPA with regard to ESA compliance. EPA responded that efforts are underway to provide the information to the Laramie County Clerk and to include the information on the EPA website with the draft permit documents. However, EPA notes that ESA requirements are not open for public comment at this stage and EPA must fulfill its obligations under the ESA before the issuance of the final GHG PSD permit.

# National Historic Preservation Act (NHPA)

Black Hills would like the public record available for public comment to include the efforts to date submitted to EPA with regard to NHPA compliance. EPA responded that efforts are underway to provide the cultural resources report to the Laramie County Clerk and to post that information on the EPA website with the draft permit documents. However, EPA is still analyzing the requirements of the statute and will comply with any public participation requirements in the NHPA in order to show compliance with those requirements prior to issuance of the final permit.

## **Permit Questions**

Black Hills asked whether EPA Region 8 could provide a full rationale of draft permit Condition III.B.3.b. and noted a typographical error. EPA responded that the correct citation in Condition III.B.3.b. should be to III.B.1.b.ii, not III.B.1.c. EPA also indicated that it would not be able to speak to the intent of Condition III.B.3.b. at this time without further representation from others within the agency.



UNITED STATES ENVIRONMENTAL PROTECTION AGENCY REGION 8 1595 WYNKOOP STREET DENVER, CO 80202-1129 Phone 800-227-8917 http://www.epa.gov/region08

Ref: 8P-AR

# MAY 1 7 2012

#### <u>CERTIFIED MAIL</u> <u>RETURN RECEIPT REQUESTED</u>

Mr. Mark L. Lux Vice President and General Manager, Power Delivery Black Hills Corporation P.O. Box 1400 625 Ninth Street Rapid City, South Dakota 57709

> Re: Greenhouse Gas Prevention of Significant Deterioration Draft Permit # PSD-WY-000001-2011.001

Dear Mr. Lux:

The U.S. Environmental Protection Agency (EPA), Region 8, has completed its initial review of Black Hills Corporation/Cheyenne Light Fuel & Power's permit application dated September 23, 2011, for a Greenhouse Gas (GHG) Prevention of Significant Deterioration (PSD) permit to allow construction and operation of a new 220 MW natural gas fired combustion turbine electric generating utility to be known as the Cheyenne Prairie Generating Station.

Enclosed is the draft PSD permit and corresponding Statement of Basis, along with a copy of the public notice. A copy of these materials (in addition to the PSD application submitted to the EPA) are also being sent to the Laramie County Clerk's office. These documents are also available on the EPA's website at: <u>http://www.epa.gov/region8/pubnotice.html</u>, under the heading "Region 8 Air Permitting comment opportunities" within the "PSD Permits" heading.

A copy of the administrative record for the draft permit, which consists of the draft permit, the draft Statement of Basis, the permit application and addendums, all data submitted by the permit applicant, and all permit-related correspondence, is available for public inspection through June 21, 2012, at the Region 8 office Monday through Friday, from 8:00 a.m. to 4:00 p.m. (excluding federal holidays).

The public notice will be published in the <u>Wyoming Tribune Eagle</u> on Monday, May 21, 2012. The public comment period will end on June 21, 2012, at 8:30 p.m. All written or emailed comments submitted by the close of the public comment period will be considered by the EPA in making its final permit decision. Please refer to the enclosed copy of the public notice for details on the public comment period.

The Wyoming Department of Environmental Quality (WDEQ) will issue a draft PSD permit for PSD pollutants other than GHGs for this facility. The WDEQ will conduct a public comment period concurrent with the EPA's for its draft PSD permit.

The conditions contained in the permit will become effective and enforceable if the permit is issued as a final permit. If you are unable to accept any term or condition of the draft permit, please submit your written comments, along with the reason(s) for non-acceptance, to:

Christopher Razzazian - Permit Contact U.S. EPA, Region 8 Air Program (8P-AR) 1595 Wynkoop Street Denver, Colorado 80202-1129

If you have any questions concerning the enclosed materials, you may contact Mr. Razzazian at (303) 312-6648.

Sincerely,

Vichha

Callie A.Videtich Acting Assistant Regional Administrator Office of Partnerships and Regulatory Assistance

Enclosures (3)

#### **Statement of Basis**

Greenhouse Gas Prevention of Significant Deterioration Pre-Construction Permit for the Black Hills Corporation/Cheyenne Light Fuel & Power, Cheyenne Prairie Generating Station

Permit Number: PSD-WY-000001-2011.001

May 21, 2012

This document serves as the Statement of Basis (SOB) required by 40 CFR 124.7. This document sets forth the legal and factual basis for the draft permit conditions and provides references to the statutory or regulatory provisions, including provisions under 40 CFR 52.21, and 40 CFR 52.37 (FIP to issue permits under the PSD requirements to sources that emit greenhouse gases), that would apply if the permit is issued. This document is intended for use by all parties interested in the permit.

#### I. Executive Summary

On September 23, 2011, Black Hills Corporation/Cheyenne Light Fuel & Power (BHC/CLF&P) submitted to the Environmental Protection Agency Region 8 (EPA) a Prevention of Significant Deterioration (PSD) permit application for Greenhouse Gas (GHG) emissions associated with the construction and operation of a new power generation facility to be known as the Cheyenne Prairie Generating Station (CPGS). In connection with the same proposed project, BHC/CLF&P submitted a PSD permit application for non-GHG pollutants to the Wyoming Department of Environmental Quality (WDEQ) Air Quality Division (AQD) on October 19, 2011. The new proposed plant would be a 220 megawatt (MW) natural gas fired combustion turbine (CT) electric utility power generating facility including five CTs each rated at 40 MW. Two of the CTs will be operated in a 2-on-1 combined cycle mode with two CTs feeding two heat recovery steam generators (HRSG) and then combining to drive a single 20 MW electric generating steam turbine. After reviewing the application, EPA has prepared the following SOB and draft New Source Review (NSR)/PSD pre-construction air permit to authorize construction of GHG air emission sources at the BHC/CLF&P, CPGS.

This SOB documents the information and analysis EPA used to support decisions made in drafting the air permit. It includes a description of the proposed facility, the applicable air permit requirements, and an analysis showing how the applicant complied with the requirements.

EPA concludes that BHC/CLF&P's application is complete and provides the necessary information to demonstrate that the proposed project meets the applicable PSD air permit regulations for GHG. EPA's conclusions rely upon information provided in the permit application, supplemental information EPA requested and provided by BHC/CLF&P, and EPA's own technical analysis. EPA is making all of this information available as part of the public record.

# II. Applicant

Black Hills Power Corporation/Cheyenne Light, Fuel & Power P.O. Box 1400 625 Ninth Street Rapid City, South Dakota 57709

Physical Location: Cheyenne Prairie Generating Station Section 1, Township 13 North, Range 66 West Latitude: 41° 07' 27.83" North Longitude: 104° 43' 13.34" West Cheyenne, Laramie County, Wyoming

Operator: Black Hills Service Company, LLC Owner: Joint Ownership - Black Hills Power, Inc. and Cheyenne Light, Fuel and Power Company Responsible Official: Mark Lux, Vice President and General Manager of Power Delivery, 303-568-3241 Alternate: George Tater, Director of Generation Operations II, 719-696-3217 Permit Contact: Tim Rogers, Environmental Services, 605-721-2286

## III. Permitting Authority

On December 30, 2010, EPA published a Federal Implementation Plan (FIP) making EPA the GHG PSD permitting authority for states that do not have the authority to implement GHG PSD permitting. 75 FR 82246 (promulgating 40 CFR 52.37). Wyoming still retains approval of its State Implementation Plan (SIP) and PSD program for pollutants that were subject to regulation before January 2, 2011, i.e., regulated NSR pollutants other than GHGs.

The GHG PSD permitting authority for the state of Wyoming is:

EPA, Region 8 1595 Wynkoop St. Denver, CO 80202

Permit Author: Christopher Razzazian Air Permitting Monitoring and Modeling Unit (8P-AR) (303) 312-6648

The non-GHG PSD permitting authority for the state of Wyoming is:

Air Quality Division Wyoming Dept. of Environmental Quality 122 West 25<sup>th</sup> Street Cheyenne, WY 82002

#### IV. Public Notice, Comment, Hearings and Appeals

Public notice for the draft PSD GHG permit will be published on May 21, 2012, in the Wyoming Tribune. The public comment period will begin on May 21, 2012 and close on June 21, 2012, at 8:30 p.m. During the public comment period, the public will be given the opportunity to review a copy of the permit application, the draft permit prepared by EPA, the SOB, and permit-related correspondence. The draft permit, SOB, and Administrative Record for the draft permit will be available for review at EPA Region 8's office Monday through Friday, from 8:00 a.m. to 4:00 p.m. (excluding federal holidays). The permit application, draft permit and SOB will also be available for review on EPA's website at <u>http://www.epa.gov/region8/pubnotice.html</u>, under the heading "Region 8 Air Permitting comment opportunities" within the "PSD Permits" heading. A hardcopy of these documents will also be available for review at the Laramie County Clerk's Office in Cheyenne, Wyoming, Monday through Friday from 8:00 a.m. to 5:00 p.m. until the close of the public comment period.

In accordance with 40 CFR 52.21(q), *Public participation*, any interested person is afforded the opportunity to submit written comments on the draft permit during the public comment period and to request a hearing. A public hearing will be held for this action on June 21, 2012 from 7:00 p.m. to 8:30 p.m. in the Cottonwood Room of the Laramie County Library located at 2200 Pioneer Avenue, Cheyenne, WY 82001. The purpose of the hearing is to gather comments concerning the issuance of the EPA GHG PSD permit. The scope of the hearing will be limited to such issues in order for the EPA to determine whether or not the applicable PSD Regulations have been appropriately applied to the construction and operation of the proposed generating station. Oral statements will be accepted at the time of the hearing or prior thereto. Since the EPA is not the permitting authority for the remainder of the NSR pollutants there will be a hearing held prior to the EPA GHG permit hearing from 5:30 p.m. to 7:00 p.m. at the aforementioned date and location regarding the WDEQ draft PSD permit. All comments regarding pollutants other than GHGs from the proposed facility must be submitted to the WDEQ, which is running a concurrent public comment period for this facility.

In accordance with 40 CFR 124.13, *Obligation to raise issues and provide information during the public comment period*, anyone, including the permit applicant, who believes any condition of the draft permit is inappropriate, or that EPA's tentative decision to prepare a draft permit for the project is inappropriate, must raise all reasonably ascertainable issues and submit all arguments supporting the commenter's decision, by the close of the public comment period.

Any supporting materials submitted must be included in full and may not be incorporated by reference, unless the material has been already submitted as part of the administrative record in the same proceeding or consists of state or federal statutes and regulations, EPA documents of general applicability, or other generally available reference material. An extension of the 30-day public comment period may be granted if the request for an extension adequately explains why more time is needed to prepare comments.

In accordance with 40 CFR 124.15, *Issuance and Effective Date of Permit*, the permit shall become effective immediately upon issuance as a final permit, if no comments request a change in the draft

permit. If changes are requested, the permit shall become effective thirty days after issuance of a final permit decision. Notice of the final permit decision shall be provided to the permit applicant and to each person who submitted written comments or requested notice of the final permit decision.

In accordance with 40 CFR 124.19, *Appeal of RCRA, UIC, and PSD Permits*, any person who filed comments on the draft permit or participated in the public hearing may petition the Environmental Appeals Board, within 30 days after the final permit decision, to review any condition of the permit decision. Any person who failed to file comments or failed to participate in the public hearing on the draft permit may petition for administrative review only on changes from the draft to the final permit decision.

# V. Facility Location

The CPGS is located in Laramie County, Wyoming, which is currently considered to be in attainment for all of the National Ambient Air Quality Standards (NAAQS). The nearest federal Class 1 area is Rocky Mountain National Park, which is located approximately 60 miles southwest from the proposed site. Savage Run Wilderness Area is a Class I area recognized by the state of Wyoming located approximately 83 miles west from the proposed site. The geographic coordinates for this facility are as follows:

Latitude: 41° 07' 27.83" North Longitude: 104° 43' 13.34" West



# Figure 1 – Proposed Facility Location/Layout

# VI. Applicability of Prevention of Significant Deterioration (PSD) Regulations

Under EPA's Clean Air Act permitting rules, the term "greenhouse gas" means an air pollutant consisting of the aggregate of six gases with atmospheric warming potential: carbon dioxide (CO<sub>2</sub>), methane (CH<sub>4</sub>), nitrous oxide (N<sub>2</sub>O), hydrofluorocarbons (HFCs), perfluorocarbons (PFCs), and sulfur hexafluoride (SF<sub>6</sub>). GHG emissions are determined by multiplying the mass emissions of each of these gases, in tons per year (tpy) by its respective Global Warming Potential (GWP) and summing the result, which is referred to as the "CO<sub>2</sub>-equivalent" (CO<sub>2</sub>e). The GWPs (from 40 CFR 98, Table A-1) are 1.0 for CO<sub>2</sub>, 21 for CH<sub>4</sub>, 310 for N<sub>2</sub>O, and 23,900 for SF<sub>6</sub>. No emissions of HFCs or PFCs are expected from this project.

EPA concludes that BHC/CLF&P's application is subject to PSD review for GHG, because the project would lead to a facility GHG emissions increase as described at 40 CFR § 52.21(b)(49)(iv) and (v). The proposed project emissions would result in increased GHG emissions above both of the PSD thresholds, which are 250 tpy on a mass basis and 75,000 tpy on a CO<sub>2e</sub> basis. BHC/CLF&P has presented CO<sub>2e</sub> potential emissions of 964,289 tpy. The potential GHG emissions on a mass basis are 962,965 tpy. EPA is the permitting authority responsible for implementing a GHG PSD FIP for Wyoming under the provisions of 40 CFR § 52.21 (except paragraph (a)(1)). See 40 CFR § 52.37.

As the permitting authority for regulated NSR pollutants other than GHGs, WDEQ has determined the proposed new source is subject to PSD review for non-GHG pollutants. Specifically, the PSD application submitted to WDEQ explains the proposed facility will be a new "major stationary source" as defined in PSD rules, which will emit the following pollutants above PSD significant emission rates: nitrogen oxides (NO<sub>x</sub>), carbon monoxide (CO), volatile organic compounds (VOC), particulate matter less than 10 microns in aerodynamic diameter (PM<sub>10</sub>), and particulate matter less than 2.5 microns in aerodynamic diameter (PM<sub>2.5</sub>). Accordingly, WDEQ is proposing to issue the non-GHG portion of the PSD permit and EPA is proposing to issue the GHG portion.<sup>1</sup>

EPA applies the policies and practices reflected in the EPA document entitled "PSD and Title V Permitting Guidance for Greenhouse Gases" (March 2011) (Guidance), available on EPA website at: <u>www.epa.gov/nsr/ghgdocs/ghgpermittingguidance.pdf</u>. Consistent with the Guidance, we have not required the applicant to model or conduct ambient monitoring for GHG, since there are no ambient air quality standards for GHGs, and we have not required any assessment of impacts of GHG in the context of the additional impacts analysis or Class I area provisions. Instead, EPA has determined that compliance with the Best Available Control Technology (BACT) analysis is the best technique that can be employed, at present, to satisfy the additional impacts analysis and Class I area requirements of the rules related to GHG. We note again, however, that the project has triggered review for regulated NSR pollutants that are non-GHG pollutants under the PSD permit sought from WDEQ.

<sup>&</sup>lt;sup>1</sup> See EPA, Question and Answer Document: Issuing Permits for Sources with Dual PSD Permitting authorities (April 19, 2011).

Available online at: http://www.epa.gov/nsr/ghgdocs/ghgissuedualpermitting.pdf.

For a description of the five-step process involved in making a PSD BACT determination for GHGs, please refer to the aforementioned Guidance. EPA has followed those steps in making the GHG BACT determination for this project.

# VII. Project Description

The proposed GHG PSD permit, if finalized, will allow BHC/CLF&P to construct a new nominal 220 MW gross simple and combined cycle natural gas-fired CT electric utility power plant in Laramie County, Wyoming. The plant, the CPGS, will be located five miles southeast of downtown Cheyenne along Interstate 80. CLF&P is a wholly owned subsidiary of BHC and was acquired from Xcel Energy in 2005. CLF&P provides electric utility service to Laramie County, Wyoming. CPGS will include three simple cycle General Electric (GE) LM6000PF SPRINT natural gas CTs, and two GE LM6000PF SPRINT CTs operated in a 2-on-1 combined cycle configuration (each turbine exhausts to its own HRSG and that steam is routed to a single steam turbine electric generator). In addition to the CTs, the facility will include the following: one wet cooling tower for the combined cycle steam turbine; three electric chiller units, each with cooling towers, for inlet air cooling for the CT inlet air; six natural gas-fired inlet air heaters to heat the CT inlet air; two natural gas-fired fuel gas heaters; one diesel emergency generator; and one diesel fire pump.

Equipment	Description	$CO_2$ (tpy)	CH <sub>4</sub> (tpy)	N <sub>2</sub> O (tpy)	SF <sub>6</sub> (tpy)	CO <sub>2e</sub> (tpy)
EP01 - EP02	CT01A - GE LM6000PF SPRINT Combined Cycle Combustion Turbine (366 MBtu/hr) with HRSG #1, SCR and CatOx	374268 (187,134 each)	7.1 (3.53 each)	0.7 (0.35 each)	0	374,635
EP03 - EP05	CT02A - GE LM6000PF SPRINT Simple Cycle Combustion Turbine (366 MBtu/hr) with SCR and CatOx	561,402 (187,134 each)	10.6 (3.53 each)	1.1 (0.35 each)	0	561,966
EP06 - EP11	Natural Gas-Fired Inlet Air Heaters #1 - #6	24,679 (4,113.13 each)	0.5 (0.08 each)	0.06 (0.01 each)	0	24,708
EP12 - EP14	Inlet Air Chillers	0	0	0	0	0
EP15	Diesel Emergency/Standby Generator	225.01	0.01	0	0	225
EP16	Diesel Fire Pump Engine	50.95	0	0	0	51
EP17	Wet Cooling Tower	0	0	0	0	N/A
EP18 - EP19	Natural Gas-Fired Fuel Gas Heater #1 and #2	2,304 (1,151.92 each)	0.04 (0.02 each)	0	0	2,305
NG-FUG	Fugitive natural gas emissions from valves, flanges, nad on-site compressor	0	16	0	0	336
SF <sub>6</sub> -FUG1 through SF <sub>6</sub> -FUG9	Nine SF <sub>6</sub> Capacitors in circuit breakers, 60 lbs SF6 each breaker, maximum 1% leak rate assumed	0	0	0	0.0027	64.5
TOTALS		962,929	34.25	1.86	0.0027	964,289

Table 1 – Potential to Emit for CPGS Emission Sources

## VIII. BACT Analysis

The BACT analysis provided by the applicant included the assumptions described below, which have been considered and adopted and modified by EPA in its own BACT analysis.

1. Table 1 above presents estimated CPGS GHG emissions in terms of  $CO_{2e}$  emissions, and only includes emissions of  $CO_2$ ,  $CH_4$ , and  $N_2O$  and  $SF_6$  (which was considered due to the potential for leaks from equipment containing  $SF_6$ ). The CPGS is not expected to emit HFCs or PFCs because these manmade gases are primarily used as cooling, cleaning, or propellant agents.  $SF_6$  is also a man-made gas that may be used as an insulating gas for high-voltage equipment, such as capacitors, and circuit breakers.

2. From the GHG emissions inventory presented in Table 1 above,  $CH_4$  and  $N_2O$  total only approximately 1,296 tpy of  $CO_{2e}$  emissions, which is about 0.13% of total  $CO_{2e}$  emissions. Due to the small contribution of  $CH_4$  and  $N_2O$  emissions to the total, the CPGS GHG BACT analysis includes the full five-step BACT determination process only for  $CO_2$  emissions from combustion sources. With regard to SF<sub>6</sub> emissions, the only emissions included in Table 1 are those that would result from leaks from the nine SF<sub>6</sub> circuit breakers at the CPGS; an abbreviate BACT analysis for those emissions is included near the end of this document.

3. The WDEQ's BACT analysis for criteria pollutants proposes the installation of a selective catalytic reduction (SCR) system for NO<sub>x</sub> emissions reduction, and an oxidation catalyst (CatOx) for control of CO and VOCs for each CT.

4. During actual CT operation, the CatOx may result in minimal increases in  $CO_2$  from the oxidation of any CO and  $CH_4$  in the flue gas. However, the EPA's Final Mandatory Reporting of Greenhouse Gases Rule (Mandatory Reporting Rule or MRR) (40 CFR 98) includes factors for estimating  $CO_{2e}$  emissions from the combustion of natural gas and assumes complete combustion of the fuel. While the oxidation catalyst has the potential of incrementally increasing  $CO_2$  emissions, these emissions are already accounted for in the MRR factors and included in the  $CO_{2e}$  totals.

5. Similarly, the SCR catalyst may result in an increase in  $N_2O$  emissions. Although quantifying the increase is difficult, it is generally estimated to be minimal under proper operating scenarios. From Table 1, above, the estimated  $N_2O$  emissions from all combustion sources total only 1.86 tpy on a mass basis, or 576 tpy  $CO_{2e}$ . Therefore, even if there were an order of magnitude increase in  $N_2O$  as a result of the SCR, the impact to  $CO_{2e}$  emissions would be small as compared to facility  $CO_{2e}$  emissions.

Use of the SCR and CatOx slightly decreases the project's thermal efficiency due to backpressure on the CTs (these impacts are already included in the emission inventory presented in Table 1) and, as noted above, may create a marginal increase to  $N_2O$  emissions. While elimination of the  $NO_x$  and CO/VOC controls could conceivably be considered as an option within the GHG BACT analysis, the environmental benefits of the  $NO_x$ , CO, and VOC control are assumed to outweigh the marginal increase to GHG emissions. Therefore, in accordance with section III.E., of the Guidance, EPA has concluded that the potential marginal increase in  $N_2O$  emissions does not warrant elimination of these controls for other pollutants, which are anticipated to be required by the state as part of its BACT determination for those other pollutants.

#### A. Natural Gas-Fired Combined Cycle Combustion Turbines

The new power plant will have a generating capacity of approximately 220 MW. This generating capacity is divided between five identical CTs each rated at 40 MW for a total generating capacity from the CTs of 200 MW. The remaining 20 MW will be generated by the combined cycle steam turbine generator, which will be fed by the two CT combined cycle HRSGs. The CTs chosen for the project are GE Energy Aeroderivative LM6000 PF SPRINT CTs.

The GHG permit application from BHC/CLF&P included a 5-step top-down BACT analysis for the CT emission units (EP01-EP05). EPA has considered the information submitted by BHC/CLF&P and presents the following BACT analysis for the CTs.

#### 1. Step 1 - Identify All Control Technologies

The applicant identified two alternatives to limit GHG emissions from the proposed project: (1) carbon capture and storage/sequestration (CCS); and (2) electrical generation efficiency. We describe these below.

<u>CCS</u> - CCS systems involve the use of adsorption or absorption processes to remove  $CO_2$  from flue gas, with subsequent desorption to produce a concentrated  $CO_2$  stream. The concentrated  $CO_2$  is then compressed to supercritical temperature and pressure, a state in which  $CO_2$  exists neither as a liquid nor a gas, but instead has physical properties of both liquids and gases. The supercritical  $CO_2$  would then be transported to an appropriate location for underground injection into a suitable geological storage reservoir, such as a deep saline aquifer or depleted coal seam, or used in crude oil production for enhanced oil recovery (EOR). Three fundamental types of carbon capture systems are employed throughout different process and energy industries: sorbent adsorption; physical absorption; and chemical absorption.

<u>Electrical generation efficiency</u> - Other than capture and sequestration of GHG emitted by combustion, the only known option for reducing GHG emissions is through maximization of the energy released during the combustion process and then through the maximization of the use or capture of that energy. To minimize GHG emissions, it is desirable to use less fuel to generate a given amount of electrical energy. There are several factors that may be examined that affect the amount of GHG produced per MW-hr of energy produced. These include low carbon fuels (those fuels that inherently produce less GHG, or  $CO_{2e}$ , per unit of energy released when combusted), and the thermodynamic and mechanical efficiency of the combustion unit (CT in this case).

The applicant has stated that their Business Plan and Integrated Resource Plan (Plans) have determined that the proposed mix of natural gas combined cycle and simple cycle power generation is the only alternative that meets all of the Plan requirements to generate economically viable and reliable electrical power 8,760 hours per year in all weather conditions. CPGS is intended to provide supplemental and backup electrical generation for solar and wind projects within the region. In order to serve that purpose, any power generation built would need to be capable of generating power during periods when wind or solar energy sources are not available, necessitating fuel-based generation. Additionally, the applicant has stated that as a peaking power plant simple cycle operation is necessary to accommodate short term load fluctuations. However, the applicant has acknowledged that future expansion of the facility could include build-out of the simple cycle CTs into combined cycle systems to provide additional thermal

efficiency. The primary energy efficiency option presented by Black Hills focuses on choosing a highly efficient low emitting CT, highly efficient HRSGs, and electric generating steam turbine.

The first aspect to evaluate with regard to an energy efficient process is the source of fuel. To compare the emission factors for GHG from the combustion of various fuels, we have provided Table 2 through Table 4 below (which have been extracted from Tables C-1 (Table 2) and C-2 (Tables 3 and 4) of 40 CFR part 98, subpart C to the MRR). In order to facilitate this analysis, the tables have been reorganized from the order listed in the CFR to show lower emitting fuels at the top of the tables and the higher emitting (less attractive) fuels at the bottom. BHC/CLF&P has proposed to use natural gas as the fuel for the CTs. Natural gas is listed as the third cleanest fuel with respect to  $CO_2$  emissions, the third cleanest fuel with respect to  $CH_4$  emissions, and the cleanest fuel with respect to  $N_2O$  emissions. The two cleaner fuels with respect to  $CO_2$  emissions (coke oven gas and biogas) cannot be utilized by a CT. With regard to fuels that can be utilized by a CT, natural gas produces the lowest GHG emissions profile.

(extracted from 40 CTA part 50, 545part C, Table C I)				
Fuel type	Default CO <sub>2</sub> emission factor (Kg/MMBtu)			
Coke Oven Gas	46.85			
Biogas (Captured methane)	52.07			
Natural Gas (Weighted U.S. Average)	53.02			
Fuel Gas	59			
Propane	61.46			
Propane Gas	61.46			
Ethane	62.64			
Liquefied petroleum gases (LPG)	62.98			
Isobutane	64.91			
Butane	65.15			
Propylene	65.95			
Natural Gasoline	66.83			
Ethylene	67.43			
Butylene	67.73			
Isobutylene	67.74			
Naphtha (<401 deg F)	68.02			
Ethanol	68.44			
Ethanol	68.44			
Aviation Gasoline	69.25			
Pentanes Plus	70.02			

Table 2 – Default CO<sub>2</sub> Emission Factors by Fuel Type (extracted from 40 CFR part 98, Subpart C, Table C-1)
Motor Gasoline	70.22
Petrochemical Feedstocks	70.97
Rendered Animal Fat	71.06
Kerosene-Type Jet Fuel	72.22
Special Naphtha	72.34
Residual Fuel Oil No. 5	72.93
Distillate Fuel Oil No. 1	73.25
Biodiesel	73.84
Biodiesel (100%)	73.84
Distillate Fuel Oil No. 2	73.96
Used Oil	74
Lubricants	74.27
Unfinished Oils	74.49
Crude Oil	74.49
Heavy Gas Oils	74.92
Plastics	75
Distillate Fuel Oil No. 4	75.04
Residual Fuel Oil No. 6	75.1
Kerosene	75.2
Asphalt and Road Oil	75.36
Other Oil (>401 deg F)	76.22
Vegetable Oil	81.55
Tires	85.97
Municipal Solid Waste	90.7
Bituminous - Coal	93.4
Mixed (Industrial coking) - Coal and coke	93.65
Wood and Wood Residuals - solid fuel	93.8
Mixed (Industrial sector) - Coal and coke	93.91
Mixed (Electric Power sector) - Coal and coke	94.38
Mixed (Commercial sector) - Coal and coke	95.26
Lignite - Coal	96.36
Subbituminous - Coal	97.02
Coke	102
Petroleum Coke	102.4

Petroleum Coke	102.4
Anthracite Coal	103.5
Biomass Solid Byproducts	105.5
Peat - solid fuel	111.8
Agricultural Byproducts - solid fuel	118.2
Blast Furnace Gas	274.3

# Table 3 – Default CH4 Emission Factors by Fuel Type(extracted from 40 CFR part 98, Subpart C, Table C-2)

Fuel type	Default CH <sub>4</sub> emission factor (kg CH <sub>4</sub> /MMBtu)
Blast Furnace Gas	2.2E-05
Coke Oven Gas	4.8E-04
Natural Gas	1.0E-03
Biomass Fuels—Liquid (All fuel types in Table C-1)	1.1E-03
Petroleum (All fuel types in Table C–1)	3.0E-03
Biogas	3.2E-03
Coal and Coke (All fuel types in Table C–1)	1.1E-02
Municipal Solid Waste	3.2E-02
Tires	3.2E-02
Biomass Fuels—Solid (All fuel types in Table C–1)	3.2E-02

# Table 4 – Default N2O Emission Factors by Fuel Type(extracted from 40 CFR part 98, Subpart C, Table C-2)

Fuel type	$\begin{array}{c} \text{Default $N_2O$ emission factor (kg} \\ N_2O/MMBtu) \end{array}$
Natural Gas	1.0E-04
Blast Furnace Gas	1.0E-04
Coke Oven Gas	1.0E-04
Biomass Fuels—Liquid (All fuel types in Table C– 1)	1.1E-04
Petroleum (All fuel types in Table C–1)	6.0E-04
Biogas	6.3E-04
Coal and Coke (All fuel types in Table C–1)	1.6E-03
Municipal Solid Waste	4.2E-03
Tires	4.2E-03
Biomass Fuels—Solid (All fuel types in Table C-1)	4.2E-03

The second aspect of the energy generation process to evaluate with regard to energy efficiency is the mode by which the fuel will be combusted. In this case, the applicant's Business Plan calls for generation of electricity utilizing CTs, which represent the most efficient mode of natural gas combustion to generate mechanical (and thermal) energy. CTs utilize compressed air to maximize the amount of energy that can be released during the expansion of the hot combustion products.

BHC/CLF&P provided the following information in their application with regard to available turbines that would meet plant requirements, including calculations of each turbine's efficiency. BHC/CLF&P has proposed to use the GE Energy Aeroderivative LM6000PF SPRINT CT because it best meets its Business Plan, its system, and operational criteria. Business Plan considerations for turbine selection include: combustion efficiency; exhaust characteristics that impact combined cycle system efficiency; size range; and consistency with other locations. Selection of a fleet of like turbines for different locations provides advantages with knowledge of maintenance and operations, stocking of spare parts, and ability to swap turbines between locations. The CT calculated efficiency for the GE LM6000PF SPRINT is 37.6%. Using a conversion factor of 3,412.14245 Btu = 1 kW-hr, the calculated efficiency would be 37.58%. The only commercially available turbines surpassing this efficiency are the Rolls-Royce Trent 60 DLE and DLE ISI model turbines (37.7% and 38.3%, respectively).

Turbine <sup>1</sup>	Production (kW)	Gross Heat Rate	Efficiency <sup>2</sup>
		(Btu/kWh)	(%)
		Higher Heating Value	
		(HHV)	
Dresser-Rand			
DR-63G PC	35,150	9,095	37.5
GE Energy Aeroder	rivative		
LM6000PC	39,253	9,487	36.0
LM6000PC Sprint	40,605	9,419	36.2
LM6000PD	34,612	9,103	37.5
LM6000PD Sprint	38,079	9,091	37.5
LM6000PF	34,612	9,103	37.5
LM6000PF Sprint	38,649	9,079	37.6
LM6000PG	42,995	9,556	35.7
GE Energy Oil & G	as		
LM6000PD	33,964	9,283	36.8
IHI Power Systems			
LM6000PC	34,306	9,198	37.1
LM6000PC Sprint	37,129	9,228	37.0
LM6000PD	33,800	9,231	37.0
LM6000PD Sprint	37,236	9,213	37.0

Table 5 Combustion Turbing Efficiency Comparison

LM6000PG	40,084	9,157	37.3
Pratt & Whitney Po	ower Systems	· · ·	
FT8 TwinPac	41,267	9,898	34.5
SwiftPac 50 DLN	41,175	9,914	34.4
Rolls-Royce			
Trent 60 DLE	41,537	9,064	37.7
Trent 60 DLE ISI	46,612	8,913	38.3
Siemens Energy	·	· · ·	
SGT-800	37,772	10,126	33.7
SGT-900	39,781	11,626	29.4

<sup>1</sup> Specifications for simple-cycle production output at 59°F, 5,950-Foot Altitude, Gross Output, HHV. <sup>2</sup> Calculation: Efficiency= [3,413 Btu/kWh divided by Gross Heat Rate] x 100

The information presented in Table 5, above was not adjusted for site specific conditions applicable to the proposed CPGS. In Table 6 below, BHC/CLF&P has provided site-specific CT criteria for the GE LM6000PF SPRINT turbine based upon GE provided information, including consideration for parasitic auxiliary loads at CPGS site conditions. With these considerations in place, the adjusted Gross Heat Rates are as shown in Table 6 below, for simple cycle and combined cycle. The calculated efficiency of the turbine is 36.8% in simple-cycle mode (versus 37.6% in Table 5 above) and 48.3% in combined-cycle mode.

Combustion Turbine Criteria	Value <sup>1</sup>
Simple-Cycle Combustion Turbine Gross Output (MW)	37.1
2x1 Combined-Cycle Combustion Gross Turbine Output (MW)	97.4
Simple-Cycle Gross Heat Rate (Btu/KWh) HHV	9,263
Combined-Cycle Gross Heat Rate (Btu/KWh) HHV	7,062
Heat Input (Btu/hr) HHV	366

Table 0 = 012 Lintovovi i Di Kinti Combastion i ai bine Attributes	Та	ble	6 -	GE	$\mathbf{L}$	M60	00 <b>P</b> F	SP	RIN	T	Com	bus	tion	Tu	ırbine	Att	ributes
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<sup>1</sup> 60° F at site elevation

#### 2. Step 2 - Eliminate Technically Infeasible Options

**CCS** - BHC/CLF&P has provided an analysis asserting that post-combustion CCS should be considered technically infeasible for the CPGS project based on a variety of technical and logistical barriers, and thus they argue that CCS should be eliminated from further consideration (Application, pg. 5-7 through 5-11). Given that EPA plans to propose this permit concurrently with the WDEQ non-GHG PSD permit, there is not time to perform an in-depth analysis of the applicant's claims regarding the technical and logistical barriers to implementing CCS for this project. Accordingly, we have assumed, for purposes of this permitting action, that potential technical or logistical barriers do not make CCS technically infeasible for the CPGS project, and have asked the applicant to address economic feasibility issues in Step 4 of the BACT analysis in order to address any arguments that CCS is BACT for this project.

## 3. Step 3 - Rank Remaining Control Technologies

Both CCS and electrical generation efficiency will be carried forward to Step 4 of the analysis and are ranked below. As part of electrical generation efficiency BHC/CLF&P has proposed to utilize natural gas, which, as explained above, is the cleanest source of fuel available.

1. CCS

2. Electrical Generation Efficiency

# 4. Step 4 - Energy, Environmental, and Economic Impacts

# **CCS - Cost of Compliance**

EPA requested that BHC/CLF&P provide an evaluation of the economic feasibility of CCS as part of Step 4 of the CT BACT analysis. Control options considered in this step therefore include application of CCS technology, and plant energy efficiency. On Page 42 of the EPA PSD and Title V Guidance, it is suggested that detailed cost estimates and vendor quotes should not be required where it can be determined from a qualitative standpoint that a control strategy would not be cost effective, where the Guidance explained that, "[w]ith respect to the valuation of the economic impacts of GHG control strategies, it may be appropriate in some cases to assess the cost effectiveness of a control option in a less detailed quantitative (or even qualitative) manner. For instance, when evaluating the cost effectiveness of CCS as a GHG control option, if the cost of building a new pipeline to transport the CO<sub>2</sub> is extraordinarily high and by itself would be considered cost prohibitive, it would not be necessary for the applicant to obtain a vendor quote and evaluate the cost effectiveness of a CO<sub>2</sub> capture system."

The Guidance also acknowledges that construction and utilization of CSS at this time can result in high costs. See Guidance at 42-43. With regard to the CPGS project, the costs of constructing and operating CCS technology are projected to be extraordinarily high based on current technology. Even with the assumption that appropriate EOR opportunities could be identified in order to lower costs as compared to sequestration in deep saline aquifers or depleted coal seams, additional costs to the CPGS would include the following:

- Licensing of scrubber technology and construction of carbon capture systems;
- Significant reduction to plant output due to the high energy consumption of capture and compression systems;
- Identification of oil and gas companies holding depleted oil reservoirs with appropriate characteristics for effective use of CO<sub>2</sub> for tertiary oil recovery, and negotiation with those parties for long term contracts for CO<sub>2</sub> purchases;
- Construction of compression systems and pipelines to deliver CO<sub>2</sub> to EOR locations;
- Labor to operate, maintain, and monitor the capture, compression, and transport systems; and
- Issues regarding current project risk that would jeopardize ability to finance construction and to obtain Public Utility Commission (PUC) approval.

(BHC/CLR&P PSD Application, pg. 5-16)

The August 2010 Report of the Interagency Task Force on Carbon Capture and Storage<sup>2</sup> provides an estimate of capital and operating costs for carbon capture from natural gas systems, "[f]or a [550 MWe net output] natural gas combined cycle (NGCC) plant, the capital cost would increase by \$340 million

<sup>&</sup>lt;sup>2</sup> Available online at: <u>http://www.fe.doe.gov/programs/sequestration/ccstf/CCSTaskForceReport2010.pdf</u>.

and an energy penalty of 15% would result from the inclusion of  $CO_2$  capture." (August 2010 Report of the Interagency Task Force on Carbon Capture and Storage, pg. 33) Using the "Capacity Factor Method" for prorating capital costs for similar systems of different sizes as suggested by the Association for the Advancement of Cost Engineering (AACE),  $CO_2$  capture system capital cost for the CPGS is estimated to require an additional \$196 million. Based on an estimated CPGS plant capital cost of \$300 million, the capture system alone would thus be expected to add approximately 65% to the overall plant capital cost.

Actual cost per MW associated with CCS would likely be higher for CPGS than the referenced plant in the Interagency Task Force report due to the inclusion of simple cycle units in the CPGS design, which pose additional challenges. Simple cycle units would require capture systems to handle a much higher temperature gas flow for which there exists little or no pilot test data. Also, modifications to the absorption process may be required, including different materials of construction.

The energy penalty would also be higher for simple cycle systems that will be utilized in the CPGS design than for the combined cycle systems examined in the Interagency Task Force report. This is due to scrubber and compressors sized based on CT output, but overall unit output is lower for simple cycle turbines, causing the fractional energy penalty to be higher than for combined cycle units. BHC/CFL&P stated that whether plant size would remain the same with output reduced, or plant size were to be increased to account for lost output, the energy penalty alone represents at least a 15% increase to the fuel component of the cost of electricity. BHC/CFL&P estimates that at a cost of 8.9¢/kWh residential retail price for electricity, and assuming an annual average of 50% capacity factor for plant operation and 15% energy penalty, the value of lost electricity sales from the project is \$12.9 million per year (BHC/CLF&P PSD Application, pg. 5-17).

The effort required to identify and negotiate with oil and gas companies who may be able to utilize the  $CO_2$  in EOR would be substantial according to BHC/CLF&P. BHC/CLF&P is aware that the proposed Greencore pipeline is being substantially oversized, versus what would be required for only the Belle Creek EOR operation, so it is reasonable to assume project developers are planning that there will be a future need for  $CO_2$  in the Powder River Basin or other locations in Wyoming or Montana. The location and timing of those sites, however, is not public information, and due to the patchwork of oil well ownership, many parties could potentially be involved in negotiations over  $CO_2$  value (BHC/CLF&P PSD Application, pg. 5-17).

Due to the extremely high pressures required to transport and inject  $CO_2$  under supercritical conditions, the compressors required are very specialized. For example, the compressors for the Dakota Gasification Company system are of a unique eight stage design. It is unclear whether the Interagency Task Force cost estimate noted above includes the required compression systems, but if not this represents another substantial capital cost. Pipelines must be designed to withstand the very high pressures (over 2000 psig), and the potential for corrosion if any water is introduced to the system. The most realistic scenario for CPGS would be to construct a pipeline from Cheyenne to tie into the proposed Greencore pipeline. At its closest point, the Greencore pipeline would be approximately 175 miles from Cheyenne. Based on engineering analysis done by the designers of that pipeline, costs for an eight inch  $CO_2$  pipeline to connect the Cheyenne project to the Greencore pipeline are estimated at \$600,000 per mile, for a total cost of \$105 million. Thus, the cost to install the connecting pipeline alone would represent a 35% increase to the project cost, and the pipeline and capture system together would double the project capital cost (BHC/CLF&P PSD Application, pg. 5-17).

BHC/CLF&P believes it is unlikely that financing could be approved for CPGS if it were to combine electrical generation with CCS, given the technical and financial risks listed above. Also, as evidenced with utilities' inability to obtain PUC approval for integrated gasification / combined cycle (IGCC) projects due to unacceptable cost and risk to rate-payers, such as Wisconsin's disapproval of the We Energy project, BHC/CLF&P believes it is reasonable to assume that the same issues would apply in this case before the Wyoming PUC (BHC/CLF&P PSD Application, pg. 5-17, 5-18).

If BHC/CLF&P were to construct or pay for construction of the pipeline to deliver some (or all) captured  $CO_2$  for use in EOR, it is possible that revenue from sale of the  $CO_2$  could be realized. However, current market pricing for  $CO_2$  delivered for EOR is proprietary and confidential, and reliable sources of information could not be identified within the scope of this BACT analysis.

In summary, capital cost for capture system and pipeline construction are estimated at \$300 million, and the retail value of lost power sales due to the CCS system energy penalty is estimated at \$12.9 million per year, assuming only 50% plant capacity factor. Other costs, such as identification, negotiation, and engineering of EOR opportunities; operating labor and maintenance costs for capture, compression, and pipeline systems; less favorable financing terms or inability to finance; and difficulty in obtaining PUC approval would also impact the project. As stated earlier, it is unclear if compression systems are included in the Interagency Task Force estimate of capture system costs, which could pose additional costs. A fraction of these costs could possibly be offset through the sale of CO<sub>2</sub>, but BHC/CLF&P has stated that the addition of CCS, with or without EOR opportunity, would make the CPGS project economically unviable. Therefore, for the reasons presented above, CCS is eliminated as an economically unviable control option for the CPGS project and will not be considered further.

Accordingly, the only control option left for the CTs is electrical generation efficiency.

#### 5. Step 5 - Select BACT

The CT proposed by BHC/CLF&P is the third most efficient turbine identified in Table 5 above and Table 7 below. While both Rolls-Royce turbines providing slightly higher efficiencies, they are not chosen as BACT technology for this project, for reasons explained below. As explained in the review of the three evaluation metrics presented below, the heat rate for the CPGS GE LM6000PF SPRINT CT, selected pursuant to the CPGS Business Plan, was found to favorably compare with other CTs and projects.

#### **Turbine Energy Efficiency Comparison**

Energy Impacts - The following table, Table 7, provides a direct comparison of the GE and Rolls-Royce CTs, which was also presented in Table 5, above. Although the Rolls-Royce CTs provide better efficiency there are other considerations that resulted in BHC/CLF&P's proposal to use the GE turbine. These were listed above in Step 1 and include the turbine's ability to meet its Business Plan (combustion efficiency, exhaust characteristics, size range, and consistency with other locations allowing for fleet experience, stocking of spare parts and turbine swap-outs), the plant system, and operational criteria.

Turbine	Production (kW)	Gross Heat Rate (Btu/kWh) HHV	Efficiency (%)
GE LM6000PF Sprint	38,649	9,079	37.6
Rolls-Royce Trent 60 DLE	41,537	9,064	37.7
Rolls-Royce Trent 60 DLE ISI	46,612	8,913	38.3

 Table 7 – Comparison of Selected Turbine with Higher Efficiency Turbines

 of Comparable Electrical Production

#### **General Electric Combustion Turbine Design Elements**

As demonstrated above, the GE LM6000PF SPRINT CT has high efficiency which is equal to or greater than the majority of other turbines with comparable electrical production capacity. However, the differences in efficiency from offerings of other vendors are in some cases very small. The design elements of those turbines that result in high efficiency undoubtedly vary between vendors, and in many cases are proprietary and confidential. However the issue was discussed by BHC/CLF&P with the selected turbine vendor, GE, and they offered comments on the unique elements of their design. This information is provided in Appendix B-4 of the application submitted to EPA by BHC/CLF&P.

Some of the key elements noted by GE are dual shaft architecture, low shaft speed, modulation of shaft speed and air flow with power, and high operating pressure ratio. It should be noted that the electrical generator is provided as a combined unit with the GE LM6000PF SPRINT CT package, and has been engineered to match CT operating characteristics. Preliminary information gathered by BHC/CLF&P provided in their application indicates that the generator is greater than 98% efficient, so overall system efficiency is driven by the CT characteristics. The CPGS 2-on-1 combined cycle system will also utilize a steam turbine and HRSG. Steam turbines manufactured today for small combined cycle plants have efficiencies limited by the metal design temperatures and pressures. The steam turbine is custom engineered rotating machinery where the efficiency is optimized in the blade path design, which maximizes the energy extracted from the steam. HRSG efficiency is maximized in the design by selecting aggressive approach and pinch points to extract the maximum heat out of the gas turbine exhaust stream. The efficiency is further improved by tube bundle arrangement, finned tubing and back end recirculation and or condensate preheating.

#### **RACT/BACT/LAER Clearinghouse (RBLC) Efficiency Comparison**

The RBLC information presented in Table 8 below, provided by BHC/CLF&P, compares efficiencies for projects with CTs in the same nominal 40 MW size range as the CPGS project. The information presented is for CTs operating in simple cycle. No information was found by BHC/CLF&P or EPA for comparable 40 MW combined cycle units without duct burning.

	111	DLC Lincichcy in	or mation of	imple Cyc		
Facility	State	Description	Heat Capacity MMBtu/hr (HHV)	Net MW	Heat Rate Btu/kWh (HHV)	Calculated Efficiency (%)
Western Farmers Electric	Oklahoma	Simple Cycle Combustion Turbine	462.7	50	9,254	36.9
El Colton, LLC	California	LM6000 (Enhanced Sprint)	456.5	48.7	9,374	36.4
Bayonne Energy Center	New Jersey	Rolls Royce Trent 60WLE	603	64	9,422	36.2
Creole Trail LNG	Louisiana	Simple Cycle Combustion Turbine	290	30	9,667	35.3
Arvah B. Hopkins Generating Station	Florida	GE LM6000PC, Simple Cycle	489.5	50	9,790	35
Indigo Energy Facility	California	LM6000 (Enhanced Sprint)	450	45	10,000	34.1
Lambie Energy Center	California	GE LM6000PC, Simple Cycle	500	49.9	10,020	34.1

 Table 8

 RBLC Efficiency Information – Simple Cycle

Note: 1.108 was used for the HHV/LHV conversion factor.

The CTs compared above are similar in size to those planned for the CPGS project. This analysis and the resulting CPGS proposed permit limits are based on use of a turbine with simple cycle gross heat rate of 9,263 Btu/kWh (HHV). An exact comparison cannot be made between the CPGS CTs and those listed in Table 8 above because each project has unique equipment and site conditions, primarily elevation and temperature. However, the CPGS heat rate compares very favorably with all of the reviewed comparable projects listed above, which demonstrates the high-efficiency attributes of the CPGS project. The only project listed above with a lower heat rate is Western Farmers Electric, which is a slightly larger CT (approximately 10 MW larger). Therefore it is not surprising that this project is slightly more efficient on a CT heat rate basis.

#### CO<sub>2e</sub> Emission Rate Comparison

In simple-cycle operation, the CPGS turbines are estimated to produce 1,102 pounds of  $CO_{2e}/MWh$  at average ambient conditions and full-load operation. Considering the range of normal operating loads (50% to 100% generator output), and ambient temperatures (0 degrees Fahrenheit to 108 degrees Fahrenheit), GHG emissions for the CPGS simple-cycle CTs range from 1,072 to 1,603 pounds of  $CO_{2e}$  for new and clean CT prior to any degradation.

In combined-cycle operation, GHG emissions for the CPGS 2x1 combined-cycle system ranges from 833 to 985 lb CO<sub>2e</sub>/MWh for a new or clean CT prior to any degradation (again considering the range of normal operating loads, 50% to 100% output, and ambient temperature, 0 degrees Fahrenheit to 108 degrees Fahrenheit).

The information below, in Table 9, was provided by BHC/CLF&P and presents operating information from the EPA Acid Rain database, and was developed using actual comparable operating unit information from 2010.

			Operating	Net Load	CO2	
State	Facility Name	Unit ID	Time (hr)	(MWh)	(Tons)	lb CO <sub>2</sub> /MWh
CA	El Cajon Energy Center	1	242	9450	5652	1196
ОК	Horseshoe Lake	10	710	29,293	18,142	1,239
ОК	Horseshoe Lake	9	174	6,851	4,248	1,240
CA	Orange Grove Project	CTG1	632	25,017	15,734	1,258
CA	Orange Grove Project	CTG2	654	24,954	15,847	1,270
FL	Arvah B Hopkins	HC4	903	27,627	17,623	1,276
FL	Polk*	2	249	27,652	18,500	1,338
FL	Arvah B Hopkins	HC3	662	18,283	12,529	1,371
FL	Polk*	5	476	51,662	36,111	1,398
FL	Polk*	4	563	60,221	42,443	1,410
FL	Polk*	3	204	23,176	16,600	1,432
NJ	Bayonne Plant Holding, LLC	2001	1,055	35,582	28,385	1,595
NJ	Bayonne Plant Holding, LLC	1001	1,208	39,061	32,004	1,639
NJ	Bayonne Plant Holding, LLC	4001	1,134	36,629	30,200	1,649
NE	C W Burdick	GT-3	24	426	399	1,871
NE	C W Burdick	GT-2	33	606	579	1,912
CA	Escondido Energy Center, LLC	CT1A	28	345	466	2,702
CA	Escondido Energy Center, LLC	CT1B	28	345	468	2,718

Table 9CPGS Comparable Unit GHG Emissions

Notes: \*Net load 5% lower than gross load

Data based on EPA Clean Air Markets - Data and Maps (available online at:http://www.epa.gov/airmarkets) Based on 2010 data

The proposed CPGS combined cycle CT GHG limit of 1,100 lb/MWh (see Table 10 below) compares favorably with the facilities shown Table 9 above. The proposed simple cycle GHG limit of 1,600 lb/MWh (also in Table 10 below) does not appear to be as favorable when compared to Polk, Arvah B Hopkins, Horseshoe Lake, or El Cajon Energy Center; however, BHC/CLF&P provided the following explanation.

Allowance must be given for load variances, impact of ambient conditions, startup and shutdown, and equipment degradation over time. In reviewing the information from Table 9, a large variance in  $CO_2$  lb/MWh emission can be seen (1,196 to 2,718 lb/MWh). All of the units listed in Table 9 can be considered to be "peaking" units, due to the low number of annual operating hours. The resultant wide variance in pounds of  $CO_2$ /MWh may likely be attributed to the significant proportion of time in startup and shutdown and/or reduced load operation.

Based on explanations from BHC/CLF&P described above, EPA proposes the following emission limits:

Tuble 10 Troposed et 65 combustion Turbine co22 Termit Emilis							
Emission Unit	Annual CO <sub>2e</sub> Limit (Pounds/MWhr)	Annual CO <sub>2e</sub> Limit (Tons/Year)					
Combined Cycle Combustion Turbine CT01A	1,100	187,318					
Combined Cycle Combustion Turbine CT01B	1,100	187,318					
Simple Cycle Combustion Turbine CT02A	1,600	187,318					
Simple Cycle Combustion Turbine CT02B	1,600	187,318					
Simple Cycle Combustion Turbine CT03A	1,600	187,318					

Table 10 - Proposed CPGS Combustion Turbine CO<sub>2e</sub> Permit Limits

We note that on April 13, 2012, EPA published a Federal Register notice (77 FR 22392) which proposes a GHG emission standard , under a new subpart TTTT of 40 CFR Part 60 (New Source Performance Standards), of 1,000 lb/MWh for combined cycle CTs, on a 12-month annual average basis, at electric utility power plants. Simple cycle CTs are proposed to be exempted from NSPS GHG emission standards. The definition of BACT in PSD rules at 40 CFR 52.21(b)(12) states that "In no event shall application of best available control technology result in emissions of any pollutant which would exceed the emissions allowed by any applicable standard under 40 CFR parts 60 and 61." In light of this relationship between the NSPS and BACT and emissions limits that had been examined for this permit, BHC/CLF&P wrote to EPA on May 3, 2012 to explain that if the combined cycle CTs at this project are operated at less than 75% of maximum load (which is an expected operating scenario for this proposed facility, given the peaking role it is intended to serve), then the proposed NSPS emission limit will be exceeded. However, in that same letter, BHC/CLF&P indicates that they understand they will have to comply with the standards established in the final NSPS rule.

#### **B.** Auxiliary Combustion Equipment

In addition to the five CTs planned for the CPGS project, there are several other small combustion sources associated with auxiliary equipment which will operate at the plant. The GHG calculations for these small combustion sources are located in Appendix B-1 to BHC/CLF&P's GHG PSD permit application.

- EP06 EP11 (6) Natural gas-fired inlet air heaters (nominal 16-MMBtu/hr air heater with estimated emissions of 4,117 CO<sub>2e</sub> tpy each), required for safety to prevent icing of air handling systems
- EP18, EP19 (2) Natural gas-fired fuel gas heaters (nominal 4.5-MMBtu/hr gas heater with estimated emissions of 1,153 CO<sub>2e</sub> tpy each)
- EP15 (1) Diesel-fired emergency generator (nominal 839-BHP engine with estimated emissions of 225 CO<sub>2e</sub> tpy)
- EP16 (1) Diesel-fired fire pump (nominal 327-BHP engine with estimated 51 CO<sub>2e</sub> tpy)

The total GHG emissions from the above small combustion sources are minor as compared to the emissions from the CTs. Therefore, the auxiliary combustion equipment GHG emission sources were evaluated in aggregate below.

#### 1. Step 1 - Identify All Control Technologies

The available control technologies for the CPGS auxiliary combustion equipment GHG sources are identical to those identified for the CTs, with the exception that there is the potential for fugitive emissions of  $SF_6$  and  $CH_4$  at the auxiliary equipment, so fugitive emissions are considered here. These options include:

- CCS;
- Small Combustion Source Efficiency;
- Efficient Use of Energy; and
- Minimization of fugitive emissions (SF<sub>6</sub> and CH<sub>4</sub>).

#### **Small Combustion Source Efficiency**

#### EP06 - EP11, Inlet Air Heaters

The inlet air anti-icing heater is similar to a conventional natural gas fired watertube boiler, and is required for safety reasons to prevent icing during winter weather. However, the water does not reach the boiling point in this system and a mixture of water and glycol is used for its thermodynamic advantages over water. The unit is designed for quick load response eliminating the requirement for a stored energy system and associated efficiency losses. Combusted natural gas is used to directly heat the incoming water/glycol mixture. Other technologies available for heating the water/glycol mixture include an indirect fired water bath heater or fire tube boiler. The fire tube boiler has similar efficiency but a much higher capital cost. The indirect fired water bath heater has a lower efficiency resulting in higher operating costs and increased emissions. With both cost and environmental operations considered, these two options are not economical for this application.

#### EP18 - EP19, Fuel Gas Heaters

Indirect water/glycol bath heaters were selected for heating of high-pressure natural gas. The natural gas is heated to ensure a measure of superheat before reaching the CT generator. Indirect heaters use a fire tube to transfer heat from the fired natural gas (fuel) to the water/glycol solution. The heat is then transferred from the water/glycol bath to the natural gas coil (product) in a safe manner.

#### EP15, Diesel Emergency/Standby Generator & EP16, Diesel Fire Pump Engine

While BHC/CLF&P has not made the final selection of CPGS emergency diesel equipment, BHC/CLF&P has informed EPA that the potential choices of diesel equipment comply with relevant NSPS emissions standards for these types of equipment and be will evaluated to ensure that the final selection has a high efficiency design. Regardless of specific equipment selected, the potential GHG emissions from these units would be minimal, and the available control options will be evaluated in light of that fact.

#### **Efficient Use of Energy**

The small combustion sources will not be operated continuously, but only during conditions when they are needed. For example, the inlet air heaters and fuel gas heaters will be operated only when required

for safety reasons to protect against icing of the turbines or condensation within the fuel lines. Therefore, energy will be utilized in an efficient manner.

#### 2. Step 2 - Eliminate Technically Infeasible Options

#### **CCS - Auxiliary Combustion Equipment**

For the same reasons as those presented for the turbines, CCS is considered economically unviable for such small combustion sources at a plant not otherwise equipped to capture and compress CO<sub>2</sub>.

#### Fuel Gas Heater - Direct Heating

Although direct heating of natural gas is more efficient than indirect heat when considering heating technology for the fuel gas heaters, it is extremely dangerous and not recommended. With direct heating, any small manufacturing defect, failure, or leak may result in catastrophic explosions as the product (natural gas) is exposed to an open flame/heat source. Accordingly, indirect heating is considered the only technically feasible option due to the safety reasons with direct heating.

#### 3. Step 3 - Rank Remaining Control Technologies

The remaining technically feasible GHG control technologies for auxiliary combustion equipment at the CPGS project are "Small Combustion Source Efficiency" and "Efficient Use of Energy."

#### 4. Step 4 - Energy, Environmental, and Economic Impacts and Level of Control

"Small Combustion Source Efficiency" and "Efficient Use of Energy" will both be implemented. Neither option is eliminated at Step 4.

#### 5. Step 5 - Select BACT

GHG BACT for the CPGS auxiliary combustion equipment consists of selecting equipment with consideration for high design efficiency, and operation of that equipment in an energy-efficient manner. To ensure energy-efficient operation, the BACT limits in Table 11 below shall apply. These limits have been calculated based on information provided by BHC/CLF&P and equipment vendors. For detailed information see BHC/CLF&P's permit application, Appendix B-8 and B-9 for the inlet air heaters; Appendix B-10 and B-11 for the fuel gas heaters; Appendix B-12 for the diesel emergency/standby generator; and Appendix B-13 for the diesel fire pump engine.

The following BACT limits apply to the auxiliary combustion equipment:

meric limits are based on a 365-day rolling average)
4,117 tpy $CO_{2e}$ per heater
Fuel: pipeline quality natural gas
1,153 tpy CO <sub>2e</sub> per heater
Fuel: pipeline quality natural gas
226 tpy CO <sub>2e</sub>
Not to exceed 500 hours of operation per
12-month period
EPA Tier 2 (or Better) Certified Engine
Rated at $\leq 839$ bhp
Diesel fuel (#2 grade fuel oil or better)
51 tpy CO <sub>2e</sub>
Not to exceed 250 hours of operation per
12month period
EPA Tier 3 (or Better) Certified Engine
Rated at $\leq$ 327 bhp
Diesel fuel (#2 grade fuel oil or better)

Table 11 – Proposed BACT limits for CO<sub>2e</sub> from Auxiliary Combustion Equipment

#### C. Fugitive Emission Sources

EPA has reviewed and concurs with BHC/CLF&P's Fugitive Emission Sources BACT analysis. Based on Black Hills' BACT analysis for fugitive emissions, EPA concludes that using state-of-the-art enclosed-pressure SF<sub>6</sub> circuit breakers with leak detection is the appropriate BACT control technology option, with a leak rate of 1% or less, which BHC/CLF&P stated is an industry standard leak rate. The proposed GHG PSD permit, if finalized, includes nine new 60 lb SF<sub>6</sub> insulated circuit breakers for a total of 540 lbs of SF<sub>6</sub>. Assuming that the leak rate is 1% or less, this equates to 5.4 lbs/year (0.0027 tpy) of SF<sub>6</sub> that will be leaked or emitted to the atmosphere. The global warming potential of SF<sub>6</sub> is 23,900 from 40 CFR Part 98, which equates to 64.5 tpy CO<sub>2e</sub> from the SF<sub>6</sub> equipment. BHC/CLF&P will monitor the SF<sub>6</sub> emissions annually in accordance with the requirements of the Mandatory Greenhouse Gas Reporting rules for Electrical Transmission and Distribution Equipment Use.

The annual  $SF_6$  emissions will be calculated according to the mass balance approach in Equation DD1 of 40 CFR Part 98, Subpart DD.

Sources of fugitive methane (CH<sub>4</sub>) emissions include the emissions from piping, valves, flanges and on site compression totaling 16 tpy CH<sub>4</sub>, or 336 tpy  $CO_{2e}$  (see November 22, 2011 letter from BHC/CLF&P responding to questions from EPA). The annual CH<sub>4</sub> emissions will be calculated according to the emission factors from Table W-1A of 40 CFR Part 98, Subpart W, Petroleum and Natural Gas Systems.

EPA concurs with and adopts BHC/CLF&P's proposed best work practice standards as BACT for control of CH<sub>4</sub> emissions from fugitive emission sources; and these work practice standards are included in the draft permit at Section III.D.2.

		GHG Pollutar	GHG CO <sub>2e</sub>	
Unit ID. No.	Unit Description	Pollutant	ТРҮ	ТРҮ
NG-FUG	Fugitive natural gas emissions from valves,	CH4	16	336
	flanges and on site compressor			
SF6-FUG1	9 SF <sub>6</sub> circuit breakers	SF <sub>6</sub>	0.0027	64.5
through SF6-	$60 \text{ lbs SF}_6$ each breaker		(5.4 lbpy)	
FUG9	1% SF <sub>6</sub> leak rate or better			
	With leak detection			

Table 12 – Proposed BACT Limits for CH4 and SF6 from Fugitive Emission Sources

#### IX. Environmental Justice (EJ)

Executive Order (EO) 12898 (59 FR 7629 (Feb. 16, 1994)) establishes the federal executive policy on EJ. Its main provision directs federal agencies, to the greatest extent practicable and permitted by law, to make EJ part of their mission by identifying and addressing, as appropriate, disproportionately high and adverse human health or environmental effects of their programs, policies, and activities on minority populations and low-income populations in the United States. EPA maintains an ongoing commitment to ensure EJ for all people, regardless of race, color, national origin, or income. Ensuring EJ means not only protecting human health and the environment for everyone, but also ensuring that all people are treated fairly and are given the opportunity to participate meaningfully in the development, implementation, and enforcement of environmental laws, regulations, and policies.

Based on the EO, the EPA's Environmental Appeals Board (EAB) has held that EJ issues must be considered in connection with the issuance of federal PSD permits issued by EPA Regional Offices. *See, e.g., In re Prairie State Generating Co.,* 13 E.A.D. 1, 123 (EAB 2006); *In re Knauf Fiber Glass, GmbH,* 8 E.A.D. 121, 174-75 (EAB 1999). This permitting action, if finalized, only authorizes emissions of GHGs and does not select environmental controls for any other pollutants. Climate change modeling and evaluations of risks and impacts is typically conducted for changes in emissions orders of magnitude larger than the emissions from individual projects that might be analyzed in PSD permit reviews. As a result, quantifying the exact impacts in specific places and points attributable to a specific GHG source obtaining a permit would not be possible (Guidance, pg. 48). Thus, we conclude it would not be meaningful to evaluate impacts of GHG emissions on a local community in the context of a single permit. Accordingly, we have determined an EJ analysis is not necessary for this permitting record.

#### X. Conclusion and Proposed Action

Based on the information supplied by BHC/CLF&P, our review of the analyses contained in the WDEQ PSD Permit Application and in the GHG PSD Permit Application, and our independent evaluation of the information contained in our Administrative Record, it is our determination that the proposed facility would employ BACT for GHG under the terms contained in the draft permit. Therefore, EPA is proposing to issue BHC/CLF&P, a PSD permit for GHG for the CPGS, subject to the PSD permit conditions specified therein. This permit is subject to review and comments. A final decision on issuance of the permit will be made by EPA after considering comments received (if any) during the public comment period.

United States Environmental Protection Agency Region 8 Air Program 1595 Wynkoop Street Denver, Colorado 80202-1129 May 21, 2012



# Draft Air Pollution Control Prevention of Significant Deterioration (PSD) Permit to Construct

PSD-WY-000001-2011.001

Permittee: Cheyenne Light, Fuel & Power / Black Hills Corporation P.O. Box 1400 625 Ninth Street Rapid City, South Dakota 57709

> <u>Permitted Facility</u>: Cheyenne Generating Station Laramie County, Wyoming

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# **Table of Acronyms**

BACT	Best Available Control Technology
bhp	Brake Horse Power
Btu/hr	British Thermal Units per Hour
CatOx	Catalytic Oxidation
CEMS	Continuous Emission Monitoring System
CFR	Code of Federal Regulations
CGS	Cheyenne Generating Station
CH <sub>4</sub>	Methane
CLF&P	Cheyenne Light, Fuel & Power
CO	Carbon Monoxide
$CO_2$	Carbon Dioxide
$CO_{2e}$	Carbon Dioxide Equivalent
dscf	Dry Standard Cubic Foot
EP	Emission Point
FIP	Federal Implementation Plan
FR	Federal Register
FTIR	Fourier Transform Infra-Red Spectroscopy
GC-FID	Gas Chromatograph-Flame Ionization Detector
GE	General Electric
GHG	Greenhouse Gas
gr	Grains
HHV	High Heating Value
hr	Hour
HRSG	Heat Recovery Steam Generator
kWh	Killowatt-Hour
lb	Pound
lbpy	Pounds Per Year
MMBtu/hr	Million British Thermal Units per Hour
MW	Megawatt
MWh	Megawatt-Hour
N <sub>2</sub> O	Nitrous Oxide
NSPS	New Source Performance Standards
NO <sub>x</sub>	Nitrogen Oxides
PSD	Prevention of Significant Deterioration
PTE	Potential to Emit
QA/QC	Quality Assurance and/or Quality Control
RATA	Relative Accuracy Test Audit
Scf/hr	Standard Cubic Feet per Hour
SCR	Selective Catalytic Reduction
SF <sub>6</sub>	Sulfur Hexafluoride
tpy	Tons Per Year
VOC	Volatile Organic Compounds
%	Percent

# I. <u>INTRODUCTION</u>

This Federal PSD permit is being issued under authority of 40 CFR 52.21 (PSD) and 52.37 (FIP to issue permits under the PSD requirements to sources that emit GHG). Cheyenne Light, Fuel & Power (hereinafter the "Permittee") proposes to construct a new nominal 220 MW gross simple and combined cycle natural gas-fired combustion turbine power plant in Laramie County, Wyoming. The plant, the Cheyenne Plains Generating Station, will be located five miles southeast of downtown Cheyenne along Interstate 80. Cheyenne Light, Fuel and Power Company is a wholly owned subsidiary of Black Hills Corporation and was acquired from Xcel Energy in 2005. Cheyenne Light, Fuel and Power Company provides electric utility service to Laramie County, Wyoming. The Cheyenne Prairie Generating Station will include three simple cycle General Electric LM6000 PF SPRINT natural gas turbines, and two General Electric LM6000 PF SPRINT turbines operated in a 2-on-1 combined cycle configuration (each turbine exhausts to its own HRSG and that steam is routed to a single steam turbine electric generator). In addition to the turbines the facility will include one wet cooling tower for the combined cycle steam turbine; three electric chiller units, each with cooling towers, for inlet air cooling for the turbine inlet air; six natural gas-fired inlet air heaters to heat the turbine inlet air, two natural gas-fired fuel gas heaters, one diesel emergency generator, and one diesel fire pump.

# II. <u>GENERAL PERMIT CONDITIONS</u>

On the basis of findings set forth in Section III Special Permit Conditions, of this permit, and pursuant to the authority (as delegated by the Administrator) of 52.21(u), EPA hereby conditionally authorizes Black Hills Corporation to construct the Cheyenne Prairie Generating Station. The authorization is expressly conditioned as follows:

# A. PERMIT EFFECTIVE DATE AND EXPIRATION

As provided in 40 CFR 124.15(b), this PSD permit shall become effective 30 days after the service of notice of the permit decision, unless:

- 1. a later effective date is specified in the decision;
- 2. review is requested on the permit under §124.19; or
- **3.** no comments requested a change in the draft permit, in which case the permit shall become effective immediately upon issuance.

As provided in 40 CFR 52.21(r), this PSD Permit shall become invalid if construction:

- 1. is not commenced (as defined in 40 CFR §52.21(b)(9)) within 18 months after the approval takes effect; or
- 2. is discontinued for a period of 18 months or more; or
- 3. is not completed within a reasonable time; and,
- 4. EPA may extend the 18 month period upon a satisfactory showing that an extension is justified.

#### **B. PERMIT NOTIFICATION REQUIREMENTS**

The Permittee shall notify EPA in writing of:

- 1. the date construction is commenced, postmarked within 30 days of such date;
- 2. the actual date of initial startup, postmarked within 15 days of such date. Startup means the setting in operation of an affected facility for any purpose;
- **3.** the date upon which initial performance tests will commence, in accordance with the provisions of Section V., Shakedown Periods, of this permit, postmarked not less than 30 days prior to such date. Notification may be provided with the submittal of the performance test protocol required pursuant to Condition V.B.; and
- **4.** the date upon which certification tests of the CO<sub>2</sub> CEMS will commence in accordance with 40 CFR § 75.61(a)(1)(i) and 40 CFR Part 60, Appendix B, Performance Specification 3. Additionally, the initial certification or recertification application shall be submitted for the CO<sub>2</sub> CEMS as required by 40 CFR 75.63.

# C. FACILITY OPERATION

At all times, including periods of startup, shutdown, and malfunction, Permittee shall maintain and operate the facility including associated air pollution control equipment (including SCR and CatOx) in a manner consistent with good air pollution control practice for minimizing GHG emissions. Determination of whether acceptable operating and maintenance procedures are being used will be based on information available to the EPA, which may include, but is not limited to, monitoring results, review of operating maintenance procedures and inspection of the facility.

# D. MALFUNCTION REPORTING

1. The Permittee shall notify EPA by mail within two working days following the discovery of any failure of air pollution control equipment, process equipment, or of a process to operate in a normal manner, which results in an increase in  $CO_{2e}$  emissions above the allowable emission limits stated in Condition III.A., of this permit.

- 2. In addition, the Permittee shall notify EPA in writing within 15 days of any such failure described under Section IV Recordkeeping Requirements. This notification shall include a description of the malfunctioning equipment or abnormal operation, the date of the initial malfunction, the period of time over which emissions were increased due to the failure, the cause of the failure, the estimated resultant emissions in excess of those allowed in Condition III.A., and the methods utilized to mitigate emissions and restore normal operations.
- **3.** Compliance with this malfunction notification provision shall not excuse or otherwise constitute a defense to any violation of this permit or any law or regulation such malfunction may cause.

#### E. RIGHT OF ENTRY

EPA authorized representatives, upon the presentation of credentials, shall be permitted:

- 1. to enter the premises where the facility is located or where any records are required to be kept under the terms and conditions of this PSD Permit;
- **2.** during normal business hours, to have access to and to copy any records required to be kept under the terms and conditions of this PSD Permit;
- 3. to inspect any equipment, operation, or method subject to requirements in this PSD Permit; and,
- 4. to sample materials and emissions from the source(s).

# F. TRANSFER OF OWNERSHIP

In the event of any changes in control or ownership of the facilities to be constructed under this permit, this PSD Permit is binding on all subsequent owners and operators. The Permittee shall notify, by letter, the succeeding owner and operator of the existence of this PSD Permit and its conditions. A copy of the letter shall be provided to EPA within 30-days of the letter signature. Permit transfers shall be made in accordance with 40 CFR Part 122, Subpart D.

# G. SEVERABILITY

The provisions of this PSD Permit are severable, and, if any provision of the PSD Permit is held invalid, the remainder of this PSD Permit shall not be affected.

# H. ADHERENCE TO APPLICATION AND COMPLIANCE WITH OTHER ENVIRONMENTAL LAWS

The Permittee shall construct and operate this project in compliance with this PSD Permit, the application on which this permit is based, and all other applicable federal, state, and local air quality regulations. This

PSD permit does not release the Permittee from any liability for compliance with other applicable federal, state and local environmental laws and regulations, including the Clean Air Act.

# I. BINDING APPLICATION

This permit is issued in reliance upon the accuracy and completeness of the information set forth in the Permittee's application to EPA dated September 23, 2011, and subsequent information provided by the Permittee to EPA, as listed in the Administrative Record for issuance of this permit.

The Permittee shall abide by all representations, statements of intent and agreements contained in the permit application and subsequent submittals as listed in the Administrative Record. EPA shall be notified no less than 10 days in advance of any significant deviation from the permit application as well as any plans, specifications or supporting data furnished. The issuance of this PSD Permit to Construct and Operate may be suspended or revoked if EPA determines that a significant deviation from the permit application, specifications, and supporting data furnished has been, or is to be, made.

# J. ENFORCEABILITY OF PERMIT

On the effective date of this permit, the conditions herein become enforceable by EPA pursuant to any remedies it now has or may have in the future, under the Clean Air Act.

# K. TREATMENT OF EMISSIONS

Emissions in excess of the limits specified in this permit shall constitute a violation.

# III. SPECIAL PERMIT CONDITIONS

# A. POINT SOURCE EMISSION LIMITS

At all times, including during startup, shutdown and malfunction, the Permittee shall not allow the discharge of GHG emissions from each unit into the atmosphere, in excess of the following:

Source ID.	<b>Emission Point/Equipment</b>	Limitations			
		(All numeric limits are based on a 365-day rolling average)			
EP01 - EP02	CT01A and CT01B -	• $1100 \text{ lb } \text{CO}_{2e}$ /MWh per turbine			
	GE LM6000PF SPRINT	• 187,318 tpy CO <sub>2e</sub> per turbine			
	Combined Cycle Combustion	• Fuel: pipeline quality natural gas			
	Turbine (366 MMBtu/hr) with				
	HRSG #1, SCR and CatOx				
EP03 - EP05	СТ02А, СТ02В, СТ03А -	• 1600 lb $CO_{2e}$ /MWh per turbine			
	GE LM6000PF SPRINT Simple	• 187,318 tpy per turbine			
	Cycle Combustion Turbine (366	• Fuel: pipeline quality natural gas			
	MMBtu/hr) with SCR and CatOx				
EP06 - EP11	Natural Gas-Fired Inlet Air	• 4,117 tpy CO <sub>2e</sub> per heater			
	Heaters #1 - #6	• Fuel: pipeline quality natural gas			
EP12 - EP14	Inlet Air Chillers	N/A			
EP15	Diesel Emergency/Standby	• 226 tpy CO <sub>2e</sub>			
	Generator	• Not to exceed 500 hours of operation per			
		12-month period			
		• EPA Tier 2 (or Better) Certified Engine			
		• Rated at < 839 bhp			
		• Diesel fuel (#2 grade fuel oil or better)			
EP16	Diesel Fire Pump Engine	• 51 tpy CO <sub>2e</sub>			
		• Not to exceed 250 hours of operation per			
		12-month period			
		• EPA Tier 3 (or Better) Certified Engine			
		• Rated at $\leq$ 327 bhp			
		• Diesel fuel (#2 grade fuel oil or better)			
EP17	Wet Cooling Tower	N/A			
EP18 - EP19	Natural Gas-Fired Fuel Gas	• 1,153 tpy CO <sub>2e</sub> per heater			
	Heater #1 and #2	• Fuel: pipeline quality natural gas			

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#### **B. REQUIREMENTS FOR COMBUSTION TURBINE**

#### 1. Compliance with Combustion Turbine Generator (CTG) BACT Emission Limits

- a. To demonstrate compliance with the lb  $CO_{2e}/MWh$  BACT emission limits (for Units EP01-EP05), the Permittee shall calculate the pounds of  $CO_{2e}$  emitted hourly from the equations provided in 40 CFR Part 75 Appendix G or the  $CO_2$  emissions CEMS data, and divide the emissions value by the measured net hourly energy output (MWh (net)). The result shall be expressed on a 365-day rolling average.
- b. The Permittee shall determine the hourly stack gas volumetric flow rate using one of the following methods:
  - i. Using 40 CFR Part 75, Appendix G, using F<sub>c</sub> factors updated monthly from fuel analysis; or
  - ii. Installing and operating a volumetric stack gas flow monitor and associated data acquisition and handling system in accordance with the  $CO_2$  CEMS system requirements provided in 40 CFR § 75.10(a)(3) and (a)(5).

#### 2. CO<sub>2</sub> Emission Monitor or CO<sub>2</sub> CEMS

- a. The Permittee shall install, calibrate, and operate a CO<sub>2</sub> emission monitor for each emission unit, EP01-EP05, and shall meet the applicable requirements, including certification testing, of 40 CFR Part 60, Appendix B, Performance Specification 3, and 40 CFR Part 75. This monitor shall be used in conjunction with the F<sub>c</sub> factor and conversion procedures in 40 CFR Part 75, Appendix F, to calculate the volumetric stack gas flow rate.
- b. As an alternative to Condition III.B.2.a., the Permittee may install a CO<sub>2</sub> CEMS and volumetric stack gas flow monitoring system with an automated data acquisition and handling system for measuring and recording CO<sub>2</sub> emissions.
- c. In accordance with 40 CFR § 75.4(b), the Permittee shall ensure that all required CO<sub>2</sub> monitoring system/equipment are installed, and all certification tests are completed, on or before the earlier of 90 unit operating days or 180 calendar days after the date the unit commences commercial operation (as defined in 40 CFR § 72.2).
- d. The Permittee shall comply with the specifications and test procedures for  $CO_2$  CEMS at 40 CFR 75.13 and related requirements in Appendices A, B and G of Part 75.
- e. The Permittee shall comply with the appropriate quality assurance requirements specified in 40 CFR Part 60, Appendix F for the CO<sub>2</sub> CEMS.

#### 3. Combustion Turbine Work Practice and Operational Requirements

- a. The Permittee shall calculate the amount of CO<sub>2</sub> emitted from CTG EP01-EP05 in tons/hr, averaged daily and converted to tpy on a 365-day rolling average, based on equation G-4 of 40 CFR Part 75 and the average net heat rate on an hourly basis based on the heat input calculation procedures contained in 40 CFR Part 75, Appendix F, equation F-20.
- b. The Permittee shall compare the calculated  $CO_2$  emissions from Special Condition III.B.3.a. to the measured  $CO_2$  emissions from the  $CO_2$  emission monitor, required in Condition III.B.1.c., on a daily basis. If the Permittee finds that the mean difference between the calculated and measured  $CO_2$  emission monitor result is greater than 10% of measured  $CO_2$  concentration, the Permittee shall review the operational performance of the emission units and monitoring instrumentation. From this review, any necessary corrective measures to restore the difference to less than 10% shall be identified and recorded by the Permittee, including the reason for the  $CO_2$  emissions difference. The Permittee shall complete corrective measures within 48 hours of identification of a difference of greater than 10%, to restore the difference to less than 10%. If the Permittee chooses to install and operate a  $CO_2$  CEMS equipped with a volumetric stack gas monitoring system, then the  $CO_2$  emission calculation from Condition II.B.3.a and the mean difference comparison shall not be required, and the Permittee shall rely instead on the data from the  $CO_2$ CEMS for compliance purposes.
- c. The Permittee shall calculate the CH<sub>4</sub> and N<sub>2</sub>O emissions on a 365-day rolling average. The Permittee shall determine compliance with the CO<sub>2e</sub> emissions limits in Condition III.A., using the default CH<sub>4</sub> and N<sub>2</sub>O emission factors contained in Table C-2 of 40 CFR Part 98 and the measured actual hourly heat input (HHV).
- d. The Permittee shall calculate the CO<sub>2e</sub> emissions on a 365-day rolling average, based on the procedures contained in Greenhouse Gas Regulations, 40 CFR Part 98, Subpart A using the Global Warming Potentials (GWP) listed in Table A-1 of 40 CFR Part 98, Subpart A.
- e. The Permittee shall determine the gross calorific value of the fuel monthly using the procedures contained in 40 CFR Part 75, Appendix F, § 5.5.2, and shall maintain records of the monthly fuel gross calorific value for a period of five years. Upon request by EPA, the Permittee shall provide a sample and/or analysis of the fuel fired in the Combustion Turbines, or shall allow a sample to be taken by EPA for analysis.
- f. The Permittee shall install, maintain and operate a non-resettable elapsed flow meter, to measure the flow rate of the fuel combusted in emission units EP01-EP05.
- g. The Permittee shall measure and record the net energy output (MWh<sub>net</sub>) on an hourly basis.

h. The Permittee shall maintain and operate units EP01 and EP02, each with HRSGs equipped with SCR and CatOx, and EP03-EP05 each equipped with SCR and CatOx, to ensure the GHG emissions are continuously at or below the emissions limits specified in this permit.

#### C. REQUIREMENTS FOR AUXILIARY COMBUSTION EQUIPMENT

- 1. The Permittee shall install, maintain and operate a non-resettable elapsed time meter for the Diesel Emergency/Standby Generator (EP15) and the Diesel Fire Pump Engine (EP16).
- 2. The Permittee shall maintain a file of all records, data measurements, reports and documents related to the operation of the diesel fired engines, EP15 and EP16. This may include, but is not limited to, the following: all records or reports pertaining to maintenance performed, all records relating to performance tests and monitoring of EP15 and/or EP16; for each diesel fuel oil delivery, documents from the fuel supplier certifying the fuel heat input values required to show compliance with the heat rate limitations in Condition III.A., hours of operation; and all other information required by this permit recorded in a permanent form suitable for inspection. The Permittee must retain the file for not less than five years following the date of such measurements, maintenance, reports, and/or records.

#### D. FUGITIVE EMISSION SOURCES

#### 1. Fugitive Emission Sources Emission Limits

At all times the Permittee shall not discharge from the source, or cause the discharge, of fugitive emissions from each unit into the atmosphere in excess of the following:

Unit ID. No.	Unit Description	<b>GHG Pollutants</b>	(Mass Basis)	GHG CO <sub>2e</sub>
		Pollutant	TPY	TPY
NG-FUG	Fugitive natural gas emissions	$CH_4$	16	336
	from valves, flanges and on site			
	compressor			
SF <sub>6</sub> -FUG1 through	9 SF <sub>6</sub> circuit breakers	SF <sub>6</sub>	0.0027	64.5
SF <sub>6</sub> -FUG9	$60 \text{ lbs } SF_6 \text{ each breaker}$		(5.4 lbpy)	
	1% SF <sub>6</sub> leak rate or better			
	With leak detection			

 Table 2: Fugitive Emission Sources Emission Limits

#### 2. Fugitive Emission Sources Work Practice and Operational Requirements

- a. For CH<sub>4</sub> emissions from sources NG-FUG, emissions shall be calculated by the Permittee annually (calendar year). Emissions shall be calculated based on the emission factors from Table W-1A of 40 CFR Part 98, Subpart W, Petroleum and Natural Gas Systems.
- b. For SF<sub>6</sub> emissions from sources SF<sub>6</sub>-FUG1 through SF<sub>6</sub>-FUG9, emissions shall be calculated by

the Permittee annually (calendar year) in accordance with the mass balance approach provided in equation DD-1 of the Mandatory Greenhouse Gas Reporting Rule for Electrical Transmission and Distribution Equipment Use, 40 CFR Part 98, Subpart DD.

c. The Permittee shall maintain a file of all records, data measurements, reports and documents related to the fugitive emissions sources (NG-FUG and SF<sub>6</sub>-FUG1 through SF<sub>6</sub>-FUG9) including, but not limited to, the following: all records or reports pertaining to maintenance performed, equipment replacement, and all records relating to compliance with the Monitoring and Quality Assurance and Quality Control (QA/QC) procedures outlined in 40 CFR 98.304.

#### IV. <u>RECORDKEEPING REQUIREMENTS</u>

- A. Including any recordkeeping requirements specified elsewhere in this permit, the Permittee shall maintain a file of all records, data, measurements, reports, and documents related to the operation of the facility, including, but not limited to, the following: all records or reports pertaining to significant maintenance performed on any system or device at the facility; all records relating to performance tests and monitoring of auxiliary combustion equipment; for each diesel fuel oil delivery, documents from the fuel supplier certifying compliance with the limitation to burn diesel fuel in Condition III.A.; and other information required by this permit recorded in a permanent form suitable for inspection. The file must be retained for not less than five years following the date of such measurements, maintenance, reports, and/or records.
- **B.** The Permittee shall maintain the following records for at least five years, including:
  - 1. the occurrence and duration of any startup, shutdown, malfunction;
  - 2. duration of any initial shakedown period for the emission units, pollution control units and CEMS;
  - 3. performance testing of emission units for demonstrating compliance with this permit;
  - 4. CEMS emission measurements;
  - 5. CEMS testing, maintenance and calibration checks conducted to satisfy quality assurance requirements;
  - 6. the time and duration of any periods that monitoring devices are not operating; and
  - 7. any emission data required by this permit.
- **C.** The Permittee shall maintain records of all GHG emission units and CO<sub>2</sub> emission CEMS certification tests and monitoring and compliance information required by this permit.
- **D.** The Permittee shall maintain records of any exceedance of limitations in this permit and submit a

written report of all exceedances to EPA semi-annually, except when: more frequent reporting is specifically required by an applicable subpart; or the Administrator of authorized representative, on a case-by-case basis, determines that more frequent reporting is necessary to accurately assess the compliance status of the source. The report is due on the 30<sup>th</sup> day following the end of each semi-annual period and shall include the following:

- 1. time intervals, data and magnitude of the exceedance, the nature and cause (if known), corrective actions taken and preventative measures adopted;
- 2. applicable time and date of each period during which the monitoring equipment was inoperative (monitoring down-time);
- 3. if no exceedances of a permit limit occurred during the reporting period or the monitoring equipment has not been inoperative, repaired or adjusted, a statement that no exceedance of that limit occurred, and/or that the monitoring equipment has not been inoperative, repaired or adjusted (as applicable), shall be submitted;
- 4. any failure to conduct any required source testing, monitoring, or other compliance activities; and
- 5. any violation of limitations on operation, including but not limited to restrictions on hours of operation of the emergency generator of fire pump.
- **E.** Exceedance shall be defined as any period in which the facility emissions or other parameter of operation exceed a maximum limit set forth in this permit.
- **F.** Excess emissions indicated by GHG emission source certification testing or compliance monitoring shall be considered violations of the applicable emission limit for the purpose of this permit.
- **G.** All records required by this PSD Permit shall be retained for not less than five years following the date of such measurements, maintenance, and reports.

#### V. <u>SHAKEDOWN PERIODS</u>

The shakedown period is defined as the period beginning with initial startup and ending no later than initial performance testing, during which the Permittee conducts operational and contractual testing and tuning to ensure the safe, efficient and reliable operation of the plant. The shakedown period shall not exceed the time period between initial startup and the deadline for initial performance testing specified in Condition VI.A.

## VI. <u>PERFORMANCE TESTING REQUIREMENTS</u>

- A. The Permittee shall conduct a performance test to establish the actual quantities of  $CO_{2e}$  being emitted into the atmosphere from one of the five identical combustion turbines and to determine compliance with the annual  $CO_{2e}$  emission limits established in this permit. Sampling shall be conducted in accordance with 40 CFR § 60.8 and EPA Method 3a or 3b for the concentration of  $CO_2$ . The test shall be conducted by the Permittee within one calendar year of initial startup and a written report of the performance testing results shall be furnished by the Permittee to the EPA.
- **B.** The Permittee shall submit a performance test protocol to EPA no later than 30 days prior to the test to allow review of the test plan and to arrange for an observer to be present at the test. The performance test shall be conducted by the Permittee in accordance with the submitted protocol, and any changes required by EPA.
- C. Fuel sampling for emission units EP01-EP05 shall be conducted by the Permittee in accordance with 40 CFR Part 75 and Part 98.
- **D.** Each turbine tested by the Permittee shall be at or above 90% of maximum load operations. Tested turbine load shall be identified by the Permittee in the sampling report. The Permittee shall present at the pretest meeting the manner in which stack sampling will be executed in order to demonstrate compliance with the emissions limits contained in Condition III.A.
- **E.** The Permittee shall conduct performance tests under conditions that are representative of normal operation of the affected facility. The Permittee shall make available to the EPA such records as may be necessary to determine the conditions of the performance tests.
- **F.** The Permittee shall provide the EPA at least 30 days prior notice of any performance test, to afford the EPA the opportunity to have an observer present and/or to attend a pre-test meeting. If there is a delay in the original test date, the Permittee must provide at least 7 days prior notice of the rescheduled date of the performance test.
- G. The Permittee shall provide, or cause to be provided, performance testing facilities as follows:
  - 1. sampling ports adequate for test methods applicable to this facility;
  - 2. safe sampling platform(s);
  - 3. safe access to sampling platform(s); and
  - 4. utilities for sampling and testing equipment.
- **H.** Unless otherwise specified, each performance test conducted by the Permittee shall consist of three separate runs using the applicable test method. Each run shall be conducted by the Permittee for the

time, and under the conditions, specified in the applicable standard. For purposes of determining compliance with an applicable standard, the arithmetic mean of the results of the three runs shall apply.

#### VII. AGENCY NOTIFICATIONS

The Permittee shall submit GHG permit applications, permit amendments, and other applicable permit information to:

Air Program (8P-AR) US EPA Region 8 1595 Wynkoop St. Denver, CO 80202

The Permittee shall submit a copy of all compliance and enforcement correspondence as required by this permit to:

Air Technical Enforcement Program (8ENF-AT) US EPA Region 8 1595 Wynkoop St. Denver, CO 80202

Authorized By: United States Environmental Protection Agency, Region 8

Callie A.Videtich Acting Assistant Regional Administrator Office of Partnerships and Regulatory Assistance

Date:



# **BLACK HILLS POWER & LIGHT CO. BLACK HILLS GENERATION**

A Black Hills Corporation Enterprise

**Tim Rogers** Environmental Manager 605•721•2286

November 22, 2011

Chris Razzazian **USEPA Region 8** 1595 Wynkoop Street Mail Code 8P-AR Denver, CO 80201-1129

RE: Black Hills Corporation: Chevenne Generating Station - Response to Questions

Dear Mr. Razzazian:

Over the past couple of months, Black Hills Corporation and EPA exchanged phone conversations and emails discussing specific aspects of our Cheyenne Generating Station Greenhouse Gas PSD application submitted to EPA. This purpose of this correspondence is to respond to questions that were not answered and to provide a paper trail for the responses.

Question 1: In regards to the combustion turbine, can we propose how we will comply with limit? Response: Black Hills will calculate hourly CO2 emissions using methodologies required by EPA's Clean Air Markets Division under 40CFR75 Appendix G and EPA's Mandatory Greenhouse Gas Reporting rule under 40CFR98 Subpart D.

CO2e Lb/MWhr Limit: To determine compliance with the 365 rolling day CO2e BACT emission limit for each combustion turbine, Black Hills will measure gross hourly energy output (MWh) from the generator and the hourly CO2 mass (tons) calculated using the 40CFR60/40CFR75 onsite continuous emission monitoring system (CEMS). For each operating hour the CO2 ton/hr emission rate will be determined according to 40CFR75 Appendix G, Section 2.3, Eq. G-4. Heat input shall be determined hourly using 40CFR75 Appendix F Section 5. At the end of each unit operating day, a new 365 day rolling average will be calculated by summing all valid hourly CO2 mass ton/hr data, multiplying by 2000 lbs/ton, and then dividing by the sum of all valid hourly gross MWh data generated. All valid CO2 lb/hr data in the 365 day period will be used and all valid gross megawatt hours will be used. Missing heat input (CO2 lb/hr) will be substituted according to the methodologies of 40CFR75 Appendix D Section 2.4. Megawatt substitution will follow a similar approach to 40CFR75 methods. The 365 day data availability will be maintained according to the typical 40CFR60 requirement target of greater than ninety percent. This CEMS 365 day rolling CO2 lb/MWh calculated average would be compared to the permit limit to determine compliance.

CO2e Ton/Year Limit: To determine compliance with the mass CO2e BACT emission limit (tons/year) for each combustion turbine, the limit will be calculated as noted above, except that the annual CO2 mass emission sum would not be multiplied by 2000 and would not be divided by the medawatt production sum. thus yielding tons of CO2 per calendar year.

Question 2: In regards to the inlet heater, Black Hills stated that the heaters will heat combustion air to prevent icing. Is the purpose of this device to maintain the 49 degree F ideal/optimal inlet air temperature for performance purposes?

Response: The inlet air heater is designed to raise the inlet air from -40 degrees F (worse case temperature scenario) to 0 degrees to meet GE emission guarantees. It will also provide the side benefit to prevent icing.

> ----- P.O. Box 1400 • 409 Deadwood Avenue ------Rapid City, SD 57709-1400

**Question 3:** In regards to the combustion turbine, inlet air heaters, and gas-line heaters, do these sources have separate stacks?

**Response:** These sources do have separate stacks.

**Question 4**: In regards to the diesel emergency generator and diesel fire water pump, has Black Hills locked into specific equipment yet?

**Response:** No, Black Hills does not plan on locking into specific equipment until the Spring/Summer of 2012. There are several reasons for not locking into equipment at this time such as technology advancements, prices, budgeting, and changes in site requirements.

EPA forwarded Region VI's proposed GHG permit for the Lower Colorado River Authority (LCRA) and were interested in Black Hills thoughts on some of the approaches taken in this permit. Black Hills is providing the following observations on the permit.

**Fugitive emission requirements**: The estimated fugitive emissions from the valves, flanges and compressor on site appear to be insignificant (16 ton/year – methane and 327 ton/year CO2e). Black Hills suggests that the sources be identified and emissions calculated annually, but there should not be a limitation on the number of devices.

**Start-up and Shut-down limits**: A lb/hr limitation was set for CO2e emissions for start-up and shut-down on combustion turbines. EPA's PSD and Title V Permitting Guidance for Greenhouse Guidance notes that longer-term averages are more appropriate than short-term averages for emission limits. For a naturalgas fired combustion turbine, the mass emission rate of  $CO_2$  will in all cases be less than or equal to the full load emission rate during normal operation. Furthermore, the permit limits (lb/MWh and tpy) proposed by Black Hills for the CGS incorporate startup and shutdown emissions. A short-term permit limit serves no logical purpose and we suggest that it not be included in the CGS permit.

**Auxiliary Combustion Equipment Emission Limits**. The LCRA permit includes short-term (lb/hr) and annual (tpy) emission limits for the fire water pump and emergency generator. Again, the short term limit is contrary to the EPA guidance and serves no useful purpose. Such emissions would be calculated from fuel consumption and/or hours of operation. We suggest that the CGS permit include only longer-term emission limits and/or limits on hours of operation for auxiliary equipment.

**Sulfur content limit in natural gas:** The proposed permit appears to expound outside the Greenhouse Gas arena with establishing sulfur limits in the natural gas used (condition B.3(e) and C.2(a)). These limits will be addressed in the State Criteria Pollutant permit.

On a closing note, we continue to work on the Endangered Species Act and Cultural Heritage Assessments and will provide to you as soon as they are completed. Black Hills appreciates the open dialogue in this permit process and is certain it aid in developing sound and timely permit for this project.

If you have any questions related to our responses or with our observations on the LCRA, please contact me at 605-721-2286.

Sincerely,

Cc Fred Carl, BHC (email) Tim Mordhorst, BHC (email) Joe Hammond, CH2MHill (email) Dennis Arfmann, Legal Counsel

----- P.O. Box 1400 • 409 Deadwood Avenue ------ Rapid City, SD 57709-1400



Tim Rogers Environmental Manager 605•721•2286

May 3, 2012

Chris Razzazian USEPA Region 8 1595 Wynkoop Street Mail Code 8P-AR Denver, CO 80202-1129

# RE: Cheyenne Prairie Generating Station (CPGS) site – CO2 BACT Limit

Dear Mr. Razzazian,

Black Hills Corporation (Black Hills) submitted a permit to construct application to EPA for a natural gas combustion turbine electrical generating facility to be located in Cheyenne, Wyoming. The facility is designed for five GE LM6000 PF Sprint combustion turbines with two of the turbines in a Combined Cycle Combustion Turbine (CCCT) configuration and three in Simple Cycle Combustion Turbine (SCCT) mode. The facility would nominally generate 220 megawatts.

The facility is being constructed to provide peak electrical demand in the Summer for our Cheyenne Light Fuel Power electrical utility, assist with the regulation of wind energy by supplementing this renewable energy, and to replace generation from three coal-fired power plants being retired in the Black Hills Power, Inc. electrical utility. The planned capacity factor for the units in the first couple of years of operation will fluctuate as we phase in the retirement of the coal generating units. Load fluctuation will also result from increasing renewable generation, commonly called renewable generation load following. As we explain below, and as you can see from the attached spreadsheet, such load fluctuating operation has an influence on the CO2 production per MWh generated for both the simple cycle and the combined cycle turbines.

In the application, Black Hills proposed a BACT limit of 1600 CO2 lb/MWh for the SCCT and 1100 CO2 lb/MWh for the CCCT. Please see the application for a full BACT analysis to support these requested limits. During the permit development process, EPA proposed a CO2 New Source Performance Standard (NSPS) rule for Electrical Generating Utilities (Subpart TTTT) that "EPA is proposing a standard of 1000 CO2 lbs/MWh, but...taking comment on a range from 950 lb CO2/MWh to 1,100 lb CO2/MWh." See 77 Fed. Reg. 22392, at page 22406. The proposed rule excluded SCCT from the limit due to the peaking nature of SCCT units and their inability to comply with this limit.

On April 24, 2012, Black Hills met with EPA Region VIII and EPA Headquarters staff to discuss the BACT CO2 limit as it would apply to this facility. Black Hills explained the business need for the proposed facility and provided more details on the manner in which the facility would be operated. EPA asked for this submittal. The following are the CPGS operating scenarios, more fully described in the attached spreadsheet:

# CCCT:

- 1. Two on One two combustion turbines operating with the steam turbine generator at various loads;
- 2. One on One one combustion turbine operating with the steam turbine generator at various loads; and
- 3. One or Two on None Either one or two combustion turbines operating at various loads when the steam turbine generator is malfunctioning and in a planned or unplanned outage.

# SCCT:

1. These units would be operated in simple cycle mode, at various loads.

# Load:

1. All combustion turbines could be operated from 50 to100 percent load, during normal operation, dependent upon the required electrical dispatch needs (i.e. replacing coal generation, renewable generation load following, etc.).

Black Hills conducted the attached analysis to assist in determining the proper CO2 BACT limits, considering the recently proposed NSPS.

The analysis involved calculating CO2 emissions based upon the operating scenarios described above using the manufacturer's performance runs on the combustion turbines at the following operating loads (50%, 75%, and 100%). The analysis also assessed CO2 emissions with no equipment degradation and a 10% degradation factor. The following are Black Hills observations of the attached analysis:

**SCCT:** In all of the cases analyzed, the SCCT could not meet the proposed NSPS 1000 lb/MWh limit, however the calculations indicate that the proposed 1,600 lb/MWh permit limit for simple cycle is appropriate on a 12-month rolling average. Compliance is possible with the proposed 12-month rolling average proposed in the NSPS rule. As noted in our application on page 5-13 in table 5-5, there is a wide range of CO2 lb/MWh emission rates for SCCT reviewed (1196 to 2718 CO2 lb/MWh).

**CCCT**: All of the combined cycle cases at 100% and 75% load points met the proposed NSPS limit of 1,000 lb/MW-hr, however some of the combined cycle cases at 50% load exceeded the limit. The proposed 1,100 lb/MWh on a 12-month rolling average limit would allow compliance for all cases from 50% to 100%. It is also important to note that the 1000 and 1100 lb/MWh limits would be exceeded when the steam turbine generator is malfunctioning or being repaired.

# Conclusion and Requested CO2 BACT Limits:

## SCCT -

- There is a wide range of CO2 emissions from 1196 to 2718 lb/MWh for SCCT turbines described in the BACT review section of the application. This provides the rationale why SCCT were excluded from the limit in EPA's proposed CO2 NSPS rule.
- Based upon the manufacturer's performance runs in this analysis, Black Hills believes the proposed BACT limit in the application of 1600 CO2 lb/MWh with a 12-month rolling average is the proper BACT limit. The averaging period is critical to Black Hills compliance.

## CCCT-

- If the CCCT is operated with one or two combustion turbines with the steam turbine generator unit operating at higher operating loads 75-100%, Black Hills could comply with the proposed NSPS limit of 1000 CO2 lb/MWh. When the CCCT and steam units are operated at 50-75% load, the proposed NSPS limit will be exceeded. Of course, operating below 50% load will result in noncompliance as well.
- There will be times when Black Hills may need to operate the combustion turbines when the steam unit is malfunctioning or in outage. In this mode, the proposed NSPS limit (1000 CO2 lb/MWh) will be exceeded. The proposed permit limit (1100 lb/MWh) for CCCT would be exceeded during this time as well.
- There will be several SUSD that will result in significantly higher CO2 lb/MWh limits based upon the lack of power generation during SUSD. These will be short periods, but there will be several hours operating in this mode due to the operating nature of this unit. These emissions will be averaged in the number evaluated against the limit, but nonetheless, the emissions are higher and will increase the recorded value.
- With these observations noted, Black Hills is comfortable with the limit proposed in the application (1100 lb/MWh on a 12-month rolling average) as it will provide the margin needed to deal with the operating scenarios described above. The averaging period is critical to Black Hills compliance.

**EPA's Proposed Base-load NSPS Limit based upon Operating Capacity**: The proposed NSPS limit was designed for base load operation according to the proposal. As stated above, Black Hills anticipates the generating load for this facility to fluctuate for the first 2-3 years.

The CPGS (both SCCT and CCCT) will be a multi-purpose electrical generating facility.

- 1. It will replace three coal generating plants in the short term. As such, it will provide intermittent base load demand service,
- 2. It will provide peaking service during the summer months, and
- 3. It will chase/supplement/enable renewable (primarily wind) electrical generation year round.

Under all three scenarios, the combustion turbines will also be operated at varying loads (50-100%). As the attached spreadsheet demonstrates, complying with the proposed

base load designed NSPS limit will be difficult for this facility. This will be especially true for the CCCT as it will be utilized as much as, if not more than, the SCCT for these scenarios as it will provide a greater efficiency than the SCCT.

Black Hills would propose to set the limits for the CCCT and SCCT at the levels identified in the application with a paragraph stating that the CPGS will comply with the limits in EPA's final NSPS rule. Black Hills plans to comment on the rule. This would include addressing emissions at partial loads and the EGU definition addressing capacity factor.

Black Hills believes the results of the analysis demonstrate that the operating nature of this facility will have difficulty meeting the proposed NSPS CO2 limit. We respectfully request that this information be taken into account in developing the Project's PSD permit CO2 BACT limit and the proposed CO2 EGU NSPS rule. Black Hills understands the facility will have to comply with the limits and requirements of the CO2 NSPS for EGU when it becomes final regardless of the limits established in this permit negotiation.

If you have any questions, please contact me at (605) 721-2286 or <u>Tim.Rogers@blackhillscorp.com</u>.

Sincerely,

Tim Rogers Environmental Manager

cc: Fred Carl, BHC Mark Lux, BHC George Tatar, BHC Dennis Arfmann, Legal Counsel

Enclosures:
Black Hills - Cheyenne Priarie Generating Station - Estimated Performance (CO2 Emissions) 2x1 GE LM6000 Water Cooled CC Plant



 53.02
 kg/MMBtu HHV EPA emission factor for pipeline average natural gas (from GHG MRR)

 2.205
 lb/kg
 conversion factor

1.1 Btu HHV / Btu L assumed conversion

10% Degradation

Combined Cycle Plant

	Black Hills	<u>BH-1</u>	<u>BH-2</u>	<u>BH-3</u>	<u>BH-4</u>	<u>BH-5</u>	<u>BH-6</u>	<u>BH-7</u>	<u>BH-8</u>	<u>BH-9</u>
Plant configuration	2x1									
CTG Load Point	100%	100%	75%	50%	100%	75%	50%	100%	75%	50%
Ambient Temperature, oF	95	108	108	108	60	60	60	0	0	0
Relative Humidity, %	20	10	10	10	60	60	60	60	60	60
Inlet Chilling Tons	885	0	0	0	0	0	0	0	0	0
Fuel Heating Value, Btu/Lb (LHV)	21,000	21,000	21,000	21,000	21,000	21,000	21,000	21,000	21,000	21,000

								the second se		
CT Generators terminal power, kW	77,640	52,930	39,730	26,510	74,300	55,750	37,180	81,180	60,900	36,460
ST Generator terminal power, kW	23,370	20,842	18,680	17,879	23,140	20,230	18,355	24,330	21,020	18,930
Gross Plant Power, kW	101,010	73,772	58,410	44,389	97,440	75,980	55,535	105,510	81,920	55,390
Gas Turbine Fuel Input, Btu/Hr	643,019,998	474,222,015	395,765,928	322,265,990	621,096,051	492,911,948	385,392,034	659,610,107	528,612,022	409,122,021
Gross Plant Heat Rate, Btu/kWH (LHV)	6,366	6,428	6,776	7,260	6,374	6,487	6,940	6,252	6,453	7,386
Plant Auxiliary Loads, kW	4,155	2,582	2,044	1,554	3,410	2,659	1,944	3,693	2,867	1,939
Net Plant Power, kW	96,855	71,190	56,366	42,835	94,030	73,321	53,591	101,817	79,053	53,451
Net Plant Heat Rate, Btu/kWH (LHV)	6,639	6,661	7,021	7,523	6,605	6,723	7,191	6,478	6,687	7,654

#### **Exhaust Parameters**

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Flow, Lb/Hr	846,706	658,668	557,107	476,406	822,616	720,003	538,316	875871	723236	609906
Temperature, F	220	204	195	186	218	211	193	214	203	195
		CO2 Emission Rates, No Turbine Degradation, Ib / MWh								
Combined Cycle 2x1	819	827	871	934	820	834	892	804	830	950
Combined Cycle 2x1 (10% Degradation)	910	919	968	1037	911	927	992	893	922	1055

#### Simple Cycle Gas Turbine

Plant configuration	1x0	1x0	1x0	1x0						
CTG Load Point	100%	100%	75%	50%	100%	75%	50%	100%	75%	50%
Ambient Temperature, oF	95	108	108	108	60	60	60	0	0	0
Relative Humidity, %	20	10	10	10	60	60	60	60	60	60
Inlet Chilling Tons	885	0	0	0	0	0	0	0	0	0
Fuel Heating Value, Btu/Lb (LHV)	21,000	21,000	21,000	21,000	21,000	21,000	21,000	21,000	21,000	21,000
CT Generators terminal power, kW	38820	26467	19,864	13,256	37,149	27,873	18,590	40,588	30,450	18,229
Total Fuel Input, Btu/Hr	321,507,240	237,091,386	197,865,304	161,126,680	310,565,640	246,453,066	192,703,940	329818088	264306000	204547609
Gross Plant Heat Rate, Btu/kWH (LHV)	8,282	8,958	9,961	12,155	8,360	8,842	10,366	8,126	8,680	11,221
Plant Auxiliary Loads, kW	1,590	662	497	331	929	697	465	1,015	761	456
Net Plant Power, kW	37,230	25,805	19,367	12,925	36,220	27,176	18,125	39,573	29,689	17,773
Net Plant Heat Rate, Btu/kWH (LHV)	8,636	9,188	10,216	12,467	8,574	9,069	10,632	8,334	8,903	11,509

#### **Exhaust Parameters**

Flow, Lb/Hr	846,706	658,668	557,107	476,406	822,616	720,000	538,316	875872	723236	609906
Temperature, F	856	912	938	997	864	860	947	842	854	882
		CO2 Emission Rates, Ib / MWh								
Simple Cycle - 1x0 or 2x0	1065	1152	1281	1563	1075	1137	1333	1045	1116	1443
Simple Cycle - 1x0 or 2x0 (10% Degradation)	1183	1280	1423	1737	1195	1263	1481	1161	1240	1603
Combined Cycle 1x1	819	827	871	934	820	834	892	804	830	950
Combined Cycle 1x1 (10% Degradation)	910	918	968	1037	911	927	992	893	922	1055

#### All Scenarios Summary Table

		CO2 Emission Rates, No Turbine Degradation, Ib / MWh								
CTG Load Point	100%	100%	75%	50%	100%	75%	50%	100%	75%	50%
Ambient Temperature, oF	95	108	108	108	60	60	60	0	0	0
Combined Cycle 2x1	819	827	871	934	820	834	892	804	830	950
Simple Cycle - 1x0 or 2x0	1065	1152	1281	1563	1075	1137	1333	1045	1116	1443
Combined Cycle 1x1	819	827	871	934	820	834	892	804	830	950

	CO2 Emission Rates, Assume 10% Degradation both CTG and STG, lb / MWh									
CTG Load Point	100%	100%	75%	50%	100%	75%	50%	100%	75%	50%
Ambient Temperature, oF	95	108	108	108	60	60	60	0	0	0
Combined Cycle 2x1	910	919	968	1037	911	927	992	893	922	1055
Simple Cycle - 1x0 or 2x0	1183	1280	1423	1737	1195	1263	1481	1161	1240	1603
Combined Cycle 1x1	910	918	968	1037	911	927	992	893	922	1055

NOTE: Combined cycle 2X1 or 1X1 configurations without the steam turbine are equivalent to the simple cycle 2X0 and 1X0 configurations.

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# Acronyms and Abbreviations

BACT	best available control technology		Formatted: Space After: 6 pt
Black HillsBHC	Black Hills Corporation		Formatted: Space After: 6 pt
<u>BHP</u>	Black Hills Power		
CAA	Clean Air Act		Formatted: Space After: 6 pt
CatOx	Catalytic Oxidation		Formatted: Space After: 6 pt
CEM	continuous emissions monitor		Formatted: Space After: 6 pt
CFR	Code of Federal Regulations		Formatted: Space After: 6 pt
CGS	Cheyenne Generating Station		Formatted: Space After: 6 pt
$CH_4$	methane <u>Methane</u>		Formatted: Space After: 6 pt
Cheyenne	Cheyenne Light, Fuel and Power Company		Formatted: Space After: 6 pt
Light <u>CLFP</u>			
СО	carbon monoxide		Formatted: Space After: 6 pt
CO <sub>2</sub>	carbon dioxide		Formatted: Space After: 6 pt
CO <sub>2</sub> e	carbon dioxide equivalent		Formatted: Space After: 6 pt
CTG	combustion turbine generator		Formatted: Space After: 6 pt
°F	degrees Fahrenheit		Formatted: Space After: 6 pt
EPA	U.S. Environmental Protection Agency		Formatted: Space After: 6 pt
FIP	Federal Implementation Plan	←	Formatted: Space After: 6 pt
FR	Federal Register	-	Formatted: Space After: 6 pt
GHG	greenhouse gas	-	Formatted: Font: Not Italic
GWP	global warming potential	-	Formatted: Space After: 6 pt
HFC	hydrofluorocarbon		Formatted: Space After: 6 pt
HHV	higher heating value		Formatted: Space After: 6 pt
HRSG	heat recovery steam generator		Formatted: Space After: 6 pt
IPCC	Intergovernmental Panel on Climate Change		Formatted: Space After: 6 pt
IRP	Intergovernmentar rate on ennate enange		Formatted: Space After: 6 pt
kW	kilowatt		Formatted: Space After: 6 pt
kWb	kilowatt hour		Formatted: Space After: 6 pt
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LAEK	Lowest Achievable Emission Kate	-	Formatted: Tab stops: Not at 3"
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lb	poundPound	(	Formatted: Space After: 6 pt
lb/hr	pound per hour	(	Formatted: Space After: 6 pt
LHV	lower heating value	←(	Formatted: Space After: 6 pt
MACT	maximum achievable control technology	(	Formatted: Space After: 6 pt
MRR	Final Mandatory Reporting of Greenhouse Gases Rule <del>, or Mandatory</del> <del>Reporting Rule</del>	←(	Formatted: Space After: 6 pt
MMBtu	million British thermal units per hour	(	Formatted: Space After: 6 pt
MW	<del>megawatt<u>Meg</u>awatt</del>	(	Formatted: Space After: 6 pt
N <sub>2</sub> O	nitrous oxide	(	Formatted: Space After: 6 pt
NAAQS	National Ambient Air Quality Standards	(	Formatted: Space After: 6 pt
NO <sub>X</sub>	nitrogen oxide	(	Formatted: Space After: 6 pt
NSR	New Source Review	(	Formatted: Space After: 6 pt
N <sub>2</sub> O	nitrous oxide	▲(	Formatted: Space After: 6 pt
O <sub>2</sub>	<del>oxygen</del> Oxygen	←(	Formatted: Space After: 6 pt
PFC	perfluorocarbonPerfluorocarbon	(	Formatted: Space After: 6 pt
$PM_{10}$	particulate matter less than 10 microns in diameter	(	Formatted: Space After: 6 pt
ppm	parts per million	(	Formatted: Space After: 6 pt
PTE	potential to emit	(	Formatted: Space After: 6 pt
PSD	Prevention of Significant Deterioration	←(	Formatted: Space After: 6 pt
RACT	Reasonably Available Control Technology	(	Formatted: Space After: 6 pt
RBLC	RACT/BACT/LAER Clearinghouse	(	Formatted: Space After: 6 pt
SCR	Selective Catalytic Reduction	(	Formatted: Space After: 6 pt
SF <sub>6</sub>	sulfur hexafluoride	←───(	Formatted: Space After: 6 pt
SIP	State Implementation Plan	(	Formatted: Space After: 6 pt
SO <sub>2</sub>	sulfur dioxide	(	Formatted: Space After: 6 pt
STG	steam turbine generator	(	Formatted: Space After: 6 pt
tpy	tons per year	(	Formatted: Space After: 6 pt
WDEQ	Wyoming Department of Environmental Quality	(	Formatted: Space After: 6 pt
VOC	volatile organic compound	←(	Formatted: Space After: 6 pt
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# **Executive Summary**

Black Hills Corporation (Black HillsBHC) plans to construct a new nominal 220-megawatt (MW) gross simple--and combined-cycle natural gas-fired combustion turbine power plant in Laramie County, Wyoming. The project, named the Cheyenne Generating Station (CGS), will be located within the city limits of the City of Cheyenne, Wyoming, approximately 5 miles southeast of the downtown area.

Cheyenne Light, Fuel and Power Company (Cheyenne Light<u>CLFP</u>) is a wholly owned subsidiary of <u>Black HillsBHC</u>. It was acquired from Xcel Energy on January 1, 2005, and provides electric utility service to Laramie County, Wyoming, including the City of Cheyenne.

Presently, electricity sold by <u>Chevenne LightCLFP</u> is generated elsewhere (primarily the Gillette, Wyoming, area) and is transmitted to Chevenne for retail delivery. There is currently no local generation capability in the Chevenne area. The CGS will provide a local source of electricity to increase the amount of available electricity and to improve reliability of power delivery in the Chevenne area.

The CGS project will include the following:

- Five 40 <u>MWGeneral Electric (GE) LM6000 PF SPRINT</u> combustion turbine generators (CTGs) fired by <u>clean-burningpipeline quality</u> natural gas. Two of the turbines will be operated in combined-cycle mode and three will be operated in simple-cycle mode.
- One wet cooling tower for the combined-cycle steam turbine
- Three electric chiller units, each with cooling towers, for inlet air cooling for all of the CTGs
- Six natural gas inlet air heaters for inlet air heating for all of the CTGs
- Two fuel gas heaters, natural gas-fired
- One diesel emergency generator
- One diesel fire pump

In accordance with the terms of federal regulations, <u>Black HillsBHC</u> is applying to U.S. Environmental Protection Agency (EPA) Region 8 for a permit to construct the CGS. The application is limited to requesting a permit for the emissions of greenhouse gases (GHGs) from the CGS and contains a description of the project, a review of applicable federal regulations, a listing of the emissions, and a best available control technology analysis.

The CGS will have potential emissions of 963,874 tons per year (tpy) of GHGs expressed as carbon dioxide equivalent (CO<sub>2</sub>e). This is comprised of 962,929 tpy of carbon dioxide (CO<sub>2</sub>), or CO2e of 962,929 tpy, 1.8 tpy of nitrous oxide (N<sub>2</sub>O), or CO2e of 564 tpy, and 18.2 tpy of methane (CH<sub>4</sub>), or a CO2e of 381 tpy. Because the emissions of CO<sub>2</sub>e exceed 100,000 tpy,

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this plant will be a major new source and will be subject to the Prevention of Significant Deterioration (PSD) rules.

Because the emission rate of GHG exceeds the 100,000-tpy limit specified in the Final Prevention of Significant Deterioration and Title V Greenhouse Gas Tailoring Rule (Tailoring Rule), a best available control technology (BACT) analysis was performed. The BACT analysis concludes that the CGS project operating at its design energy conversion efficiency is BACT for GHGs.

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# SECTION 1.0

Black Hills Corporation (Black Hills)<u>BHC</u> plans to construct a new nominal 220-megawatt (MW) gross simple and combined-cycle combustion turbine power plant located in Laramie County, Wyoming. The project, named the Cheyenne Generating Station (CGS), will be located in the City of Cheyenne approximately 5 miles southeast of the downtown area.

The facility will produce electrical power for Cheyenne Light, Fuel and Power Company (Cheyenne Light), CLFP, a wholly owned subsidiary of Black Hills. Cheyenne LightBHC. CLFP provides electric service to Laramie County, Wyoming, and the City of Cheyenne, with more than 38,000 customers.

Presently, electricity sold by <u>Chevenne LightCLFP</u> is generated elsewhere (primarily the Gillette, Wyoming, area) and is transmitted to Chevenne for retail delivery. There is presently no local generation capability in the Chevenne area. The CGS will provide a local source of electricity to increase the amount of available electricity and to improve reliability of power delivery in the Chevenne area.

The power plant will include the following:

- Five 40-MW combustion turbine generators (CTGs) fired by <u>clean-burningpipeline</u> <u>quality</u> natural gas. Two of the turbines will be operated in combined-cycle mode and three will be operated in simple-cycle mode. Operating in combined-cycle will provide approximately 20-MW.
- One wet cooling tower for the combined-cycle steam turbine
- Three electric chiller units, each with cooling towers, for inlet air cooling for all of the CTGs
- Six natural gas inlet air heaters for inlet air heating for all of the CTGs
- Two fuel gas heaters, natural gas-fired
- One diesel emergency generator
- One diesel fire pump

In accordance with the terms of federal regulations, <u>Black HillsBHC</u> is applying to U.S. Environmental Protection Agency (EPA) Region 8 for a permit to construct the CGS. The application is limited to requesting a permit for the emissions of greenhouse gases (GHGs) and contains a description of the project, a review of applicable regulations, a listing of the emissions, and a best available control technology (BACT) analysis.

Section 1.1 provides project contacts and an overview of the documentation being submitted with the application for a permit to construct the CGS.

## 1.1 Project Contacts

The following individuals may be contacted for additional information on this project:

Applicant	Tim Rogers Environmental Manager Black Hills Corporation 625 Ninth Street Rapid City, SD 57709 (605) 721-2286 <del>TRogers@bh-corp.com<u>TRogers@bh-corp.com</u></del>
Permitting Consultant	Joe Hammond <u>SeniorPrincipal</u> Project Manager CH2M HILL <u>Engineers</u> , Inc. 9193 South Jamaica Street Englewood, CO 80112 (720) 286-5919 <u>joe.hammond@ch2m.comjoe.hammond@ch2m.</u> <u>com</u>

## 1.2 Document Overview

The following is an overview of the information included in this permit application.

- Section 1.0 Introduction. This section provides an overview of the project and describes the application organization.
- Section 2.0 Project Description. This section includes a general description of the proposed project including equipment and operations of the project. Information regarding non-emitting processes and equipment is provided for a general understanding of plant operations.
- Section 3.0 Greenhouse Gas Emissions Summary. This section provides a summary of emissions-related information.
- Section 4.0 Greenhouse Gas Regulatory Review. This section contains a detailed regulatory review of federal GHG air regulations that may impact the permitting, construction, or operation of the proposed project.
- Section 5.0 BACT Analysis. This section includes a BACT analysis for GHG pollutants. This analysis follows the EPA-prescribed five-step top-down approach. Requested permit limits are also included in this section.
- Appendix A Location Map and Plot Plan. This appendix includes a location map, plot plan, and general equipment arrangement drawing for the proposed project.
- —Appendix B Greenhouse Gas Supporting Documentation. This appendix contains the calculations used to determine the GHG emissions for this permit application.

• and additional information on the GE combustion turbines and auxiliary equipment.

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# Project Description

Black Hills<u>BHC</u> proposes to construct and operate the CGS in Cheyenne, Wyoming. A plot plan of the facility and a map detailing the location of the proposed facility can be found in Appendix A. The facility will be a nominal 220-MW gross output power plant that will produce electrical power for the <u>Black HillsBHC</u>-owned <u>Cheyenne Light</u>, Fuel and Power (CLFP) electric retail service territory in Laramie County, Wyoming, including the City of Cheyenne and Black Hills Power (BHP) service territory in Wyoming and South Dakota. Facility output varies with ambient temperature, with higher output at lower ambient temperatures. A general arrangement of the turbine layout and associated equipment can be found in Appendix A.

The CGS facility configuration was selected based upon the needs identified in the CLFP *Integrated Resource Plan* (IRP).<sup>1</sup> The CLFP Certificate of Public Convenience and Necessity (CPCN) was filed with the Wyoming Public Service Commission (August 1, 2011 – Docket Number 20003-112-EA11) and was based upon CLFP IRP that identified three simple-cycle combustion turbines (nominally 120 MW gross output). The CLFP CPCN further identifies the potential build-out of the site to accommodate future generation needs. <u>Black HillsBHC</u> plans to submit a BHP CPCN in fall 2011 and will be based upon the BHP IRP that tentatively (plan has not been finalized) identifies the need for two <u>simple cycle</u> combustion turbines configured in combined cycle mode (nominally 100 MW gross output). The <u>Black Hills'BHC's</u> Integrated Resource Plans will show the public need for increased capacity requirements in the CLFP and BHP service areas, reserve generation requirements, and generation within the service area of Cheyenne for reliability reasons. The necessary generation (wind, solar, and other renewable resources).

The proposed CGS facility will consist of five combustion turbines. Combustion turbines CT01A and CT01B will operate in a 2 X 1 combined-cycle design consisting of two 40-MW CTGs with one heat recovery steam generator (HRSG) for each CTG with no duct burners. Steam from the HRSGs will be combined to flow to a steam turbine that will produce additional electricity. The total generating capacity of the combined-cycle configuration will be approximately 100 MW. Combustion turbines CT02A, CT02B, and CT03A, will each be high-efficiency 40-MW CTGs, operating in simple-cycle mode.

Inlet air chillers with wet cooling towers will be provided for each CTG to cool the combustion air, which will enhance overall plant output during times of higher ambient temperature. Inlet air heaters will also be provided for each CTG to heat the combustion air, which will prevent icing during times of lower ambient temperature.

The proposed CGS facility will also have fuel gas pre-heaters, an emergency generator, and a fire pump.

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<sup>&</sup>lt;sup>1</sup> The IRP determines the capacity expansion, which takes into consideration the size of the electrical systems' demand, and further defines the size of combustion turbines selected.

# 2.1 Power Generation

Power will be produced in the plant by a total of six generators, one for each of the five 40-MW CTGs plus one steam turbine generator (STG). All other facility operations ancillary to the primary generation function are described below.

## 2.2 Emission Sources

### 2.2.1 Combined-Cycle Combustion Turbine Generators

The CGS will use two 40-MW combustion turbines CT01A and CT01B-will be operated in a 2 X 1 combined-cycle design with two CTGs and one steam turbine. The combustion turbines will be fired exclusively with pipeline-quality natural gas and are very similar to large aircraft jet engines in function and design. The combustion turbines will be equipped with unfired (no duct burner) HRSGs to extract heat from each combustion turbine exhaust to make steam. The steam will be used in an STG to produce more electricity. The combined-cycle configuration will consist of two CTGs, two HRSGs (one for each CTG), and one STG.

## 2.2.2 Simple-Cycle Combustion Turbine Generators

The CGS will use three 40-MW combustion turbines operated in simple-cycle mode, without heat recovery from the turbine exhaust. These combustion turbines, designated as CT02A, CT02B, and CT03A, will be fired exclusively with pipeline-quality natural gas and are very similar to large aircraft jet engines in function and design. The combustion turbines have the capability to reach full-load operation quickly after initiation of startup, thereby reducing overall startup emissions.

Each combustion turbine consists of a compressor, combustor, and expansion turbine. After filtration, air passes through the compressor before combining with the fuel and entering the low nitrogen oxide (NO<sub>X</sub>) combustor. The combustion products and compressed air pass through the expansion turbine, which drives both the compressor and the generator. Up to approximately 40 MW of gross electrical power are produced by each CTG over and above the work required by the compressor. The exhaust gas from each combustion turbine enters the Selective Catalytic Reduction (SCR) and Catalytic Oxidation (CatOx) catalysts at high temperature (approximately 850 degrees Fahrenheit [°F] at full load).

### 2.2.3 Wet Cooling Towers

### 2.2.3.1 Inlet Chiller Cooling Towers

An inlet air chilling system will be installed at the compressor inlet of each CTG, downstream of the inlet air filter. The inlet air chilling system serves to enhance the overall output of the plant by lowering the temperature of the ambient air entering the CTGs during periods of high air temperature. The cooling process takes place at the cooling coils where air is cooled before entering the compressor section of the turbine. At low temperatures, the air becomes denser and, therefore, more air flows though the CTGs. The net increase in airflow results in higher power output for each of the CTGs at high ambient temperatures. Three inlet chiller cooling towers will be used to serve the inlet chilling system at CGS.

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#### 2.2.3.2 Unit 1 Cooling Tower

One wet cooling tower will be installed to provide cooling to condense the steam that is exhausted from the steam turbine on the combined cycle configuration-<u>in order to increase system efficiency</u>. The steam condensers will have circulating cooling water flow through tubes that will absorb the heat from the condensing steam that is exhausted from the steam turbines. The warmed circulating water is then pumped to the cooling tower where it flows down through the tower and is cooled through evaporation, in a manner similar to other cooling towers. The cooled circulating water then flows back to the steam condensers to pick up more heat.

## 2.2.4 Inlet Air Heaters

An inlet air heating system will be installed at the compressor inlet of each CTG, upstream of the inlet air filter. The inlet air heating system <u>raises the temperature of the ambient air</u> entering the CTGs during periods of low air temperature to prevent icing <u>for safety reasons</u>.

## 2.2.5 Fuel Gas Heaters

A fuel gas pre-heat system will be utilized on each CTG to raise the temperature of the natural gas above the saturation temperature. <u>for safety reasons</u>. Natural gas fired fuel gas heaters will be used on the five combustion turbines.

## 2.2.6 Diesel Fire Pump

One diesel fire pump will be used to provide fire protection water for the plant. This engine will fire only ultra-low-sulfur diesel fuel, and will operate only during testing that is anticipated to occur once per week. Total operating hours for the fire pump are 250 hours per year or less.

### 2.2.7 Emergency Generator

One diesel emergency generator will be used to provide emergency power for the plant. This engine will fire only ultra-low-sulfur diesel fuel, and will operate only during testing that is anticipated to occur once per week. Total operating hours for the emergency generator are 250500 hours per year or less.

## 2.2.8 Storage Tanks

Storage tanks at the site will include diesel tanks for the fire water pump and emergency generator, aqueous ammonia storage tanks for the SCR NO<sub>x</sub> emissions control unit, and several water storage tanks. <u>No GHG emissions will result from these tanks</u>.

## 2.3 Non-Emitting Major Facility Components

## 2.3.1 Ancillary Facilities

Other facilities used to support power generation at the CGS will include the following:

- Water treatment system to remove solids and hardness from plant makeup water
- Wastewater treatment system to allow recycle of cooling tower blowdown and other plant wastewater

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- · Plant and instrument air compressors (electric-driven) and auxiliary equipment
- Plant sumps, sump pumps, and oily water separator
- Miscellaneous fire protection equipment

Septic system for sanitary waste

- Steam and water sampling systems
- Administration and warehouse/maintenance buildings

## 2.4 Emission Controls

The CGS will include the following emission controls:

- Dry low NO<sub>X</sub> burners on the CTGs, and a SCR system to reduce NO<sub>X</sub> emissions on all CTGs
- An oxidation catalyst to reduce carbon monoxide (CO) and volatile organic compound (VOC) emissions from theon all CTGs
- Good combustion design and operation to reduce particulate matter of 10 microns in diameter (PM<sub>10</sub>) emissions from the CTGs
- Use of pipeline-quality natural gas to minimize sulfur dioxide (SO<sub>2</sub>) emissions from the CTGs
- High-efficiency drift eliminators on the steam condenser cooling towers to reduce  $PM_{10}$  emissions in the cooling tower drift

## 2.5 Emissions Monitoring

As required by Title 40 of the Code of Federal Regulations (CFR) Parts 60 and 75, the CGS will use continuous emissions monitors (CEMs) for NO<sub>X</sub>, CO, and oxygen (O<sub>2</sub>) for all five CTGs. These CEMs will average and record data on frequencies consistent with state and federal acid rain rules. The plant will also monitor and record the natural gas flow rate and will analyze natural gas fuel quality as required by the acid rain rules.

CGS will use these continuous emissions monitors (CEMs) to determine compliance with the CO<sub>2</sub> emission limits established in the PSD permit. CEMS will be installed and operated for each turbine according to 40CFR75 requirements. Accordingly, these CEMS will calculate CO<sub>2</sub> emissions from each source according to the 40CFR75 Appendix F and G methodologies. The calculated CO<sub>2</sub> emissions follow a strict calculation requirement to determine CO<sub>2</sub> emissions for each minute of fuel combustion typically. The minute data is converted to hourly emissions for reporting per 40CFR75 data reduction requirements. All CO<sub>2</sub> emissions are accounted for in the reported values, including startup and shutdown.

The CO<sub>2</sub> emissions data generated from the CEMS, per 40CFR75 requirements, are used to report emissions for 40CFR98 (Mandatory Greenhouse Gas Reporting rule). Specifically, Subpart D – Electricity Generation, guide the CO<sub>2</sub> emissions reporting requirements. Black

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Hill currently uses this methodology for its natural gas fired combustion turbines. The calculation methodology is defined simply as:

"(a)...continue to monitor and report CO<sub>2</sub> mass emissions as required under §75.13 or section 2.3 of appendix G to 40 CFR part 75, and §75.64. Calculate CO<sub>2</sub> emissions as follows: (1) Convert the cumulative annual CO<sub>2</sub> mass emissions reported in the fourth quarter electronic data report required under §75.64 from units of short tons to metric tons. To convert tons to metric tons, divide by 1.1023."

This calculation, as required by EPA's Greenhouse Gas MMR rule simply uses the 40CFR75 fourth quarter, or end of year, CO<sub>2</sub> emission and coverts the short tons to metric tons (Nitrous Oxide and Methane emissions are calculated from Green House Gas emission factors). Additionally, the CO<sub>2</sub> data will follow quality assurance/control requirements as well as missing data substitution routines according to 40CFR75 rules. Therefore, since EPA's long standing Acid Rain Program regulations (40CFR75) and the recently released Greenhouse Gas MMR rule (40CFR98) both recognize the 40CFR75 methodology as an accurate and complete method to monitor CO<sub>2</sub> emissions, the CGS will use the methodology to determine compliance with CO<sub>2</sub> emission limits identified in this permit.

In a recent permit application with the Bay Area Air Quality Management District (BAAQMD) for the Russell Energy Center in California, the agency made the following determination regarding CEMS versus the Fuel Meter (heat input ) method:

"The Air District has also considered whether to require the facility to use a Continuous Emissions Monitor (CEM) to measure greenhouse gas emissions directly (as  $CO_2$ ), but has concluded that calculating emissions from heat input is preferable. Unlike some other pollutants such as  $NO_3$  or carbon monoxide whose formation is heavily dependent on conditions of combustion and/or performance of add-on emissions controls, greenhouse gases are a direct and unavoidable byproduct of the combustion process. The amount of carbon within the fuel will all ultimately be emitted as greenhouse gases in a manner that is easily determined using well-established emissions factors. One can therefore determine with great accuracy what greenhouse gases are being emitted by measuring the amount of hydrocarbon fuel being burned (measured as heat input). For this reason, the test methods for measuring heat rate and capacity can achieve an accuracy of  $\pm 1.5\%$  <sup>55</sup>, which is better than the relative accuracy of CEMs which typically ranges as high as  $\pm 10\%$ .<sup>56</sup> The Air District is therefore proposing to require surrogate monitoring for greenhouse gas emissions using heat rate instead of a CEM."

<sup>55</sup> American Society of Mechanical Engineers (ASME), Performance Test Code on Overall Plant Performance, (PTC 46-1996), December 15, 1997, Table 1.1, "Largest Expected Test Uncertainties", at p. 4 (providing 1.5% variance in the corrected heat rate for "combined gas turbine and steam turbine cycles with or without supplemental firing to steam generator"). <sup>56</sup> See, e.g., 40 C.F.R. Part 75, Appendix A, § 3.3.3 ("The relative accuracy for CO<sub>2</sub> and O<sub>2</sub> monitors shall not exceed 10.0 percent.")

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# 2.6 Operating Schedule

The exact annual operating schedule of the CGS will be dependent on the demand for electric power-within Cheyenne Light's electric system. Thus, the exact operating schedule cannot be accurately predicted at this time.

For this reason, the permit limits requested in this application, and the resulting assumptions used in the <u>ambient impact analysis</u> <u>emissions inventory</u> and BACT analysis, are as follows:

- Up to 8,760 hours per turbine per year of CTG operation (both simple and combined cycle) at 100 percent load or at any lesser load rate
- Up to 600 startups for each simple-cycle combustion turbine per year
- Up to 600 startups for each combined-cycle combustion turbine per year
- Up to 5,330 hours per tower per year of inlet chiller cooling tower operation
- Up to 8,760 hours per year of combined-cycle cooling tower operation
- Up to 4,380 hours of operation per year for each inlet air heater
- Up to 4,380 hours of operation per year for each fuel gas heater

These hours could be based on continuous short-term or long-term operation. In other words, the plant could operate up to 8,760 hours per year (counting startup episodes) and could operate 24 hours per day, 7 days per week, and 365 days per year.

# 2.7 Permitting and Construction Schedule

The planned permitting and construction timeline is shown in Table 2-1.

TABLE 2-1 Permitting and Construction Schedule	
Event	Date
AirGHG PSD Permit Application Filed with EPA	August <del>5,</del> 2011
Air <u>Revised GHG PSD</u> Permit Application Filed with ₩DEQEPA	September <del>1,</del> 2011
PSD Air Permit Application Filed with WDEQ	October 2011
Air Permits Issued by EPA and WDEQ	SummerSeptember 2012
Begin Purchase Major Pieces of Equipment	SummerSeptember 2012
Start of Construction	SummerApril 2013
Commercial Operation	SummerJune 2014

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# GHG Emissions Summary

GHG emission estimates were prepared for all point emissions sources from the CGS, including the combustion turbines and auxiliary equipment. The annual carbon dioxide (CO<sub>2</sub>) equivalent (CO<sub>2</sub>e) emissions were estimated based on 100 percent capacity factor (full-load operation for 8,760 hours per year) for each of the combustion turbines. More detailed GHGNote that instantaneous fuel flow is always lower during turbine startup than normal turbine operations; therefore, unlike for criteria air pollutants, instantaneous GHG emissions are always lower during startup than normal operations, and 8760 hours per year at full load is a conservative assumption for calculating GHG emissions. More detailed emission calculations are provided in Appendix B.

## 3.1 Combustion Turbines

The CGS project consists of two nominal 40 MWGE LM6000PF SPRINT combustion turbines operating in a 2 X 1 combined-cycle configuration, designated as CT01A and CT01B. There will also be three nominal 40 MWGE LM6000PF SPRINT combustion turbines operating in simple cycle identified as CT02A, CT02B, and CT03A. EachAll five combustion turbine has aturbines will have separate stackstacks, which will be a separate emission pointpoints.

# 3.2 Auxiliary Equipment

In addition to the five <u>GE LM6000PF SPRINT</u> combustion turbines planned for the CGS project, there are several other small GHG combustion sources associated with auxiliary equipment that will operate at the CGS:

- (6) Natural gas-fired inlet air heaters (nominal 16-million-British-thermal-units-per hour [MMBtu/hr] air heater with estimated emissions of 4,117 CO<sub>2</sub>e tons/year each)
- (2) Natural gas-fired fuel gas heaters (nominal 4.5-MMBtu/hr gas heater with estimated emissions of 1,153 CO<sub>2</sub>e tons/year each)
- (1) Diesel-fired emergency generator (nominal 839-BHP engine with estimated emissions of 226 CO<sub>2</sub>e tons/year-each)
- (1) Diesel-fired fire pumps (nominal 327-BHP engine with estimated 51 CO<sub>2</sub>e tons/year each)

# 3.3 GHG Emission Summary

The GHG emission sources for the project are shown in Table 3-1, along with estimated annual  $CO_{2}e$  emissions.

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SECTION 3.0 - GHG EMISSIONS SUMMARY

#### TABLE 3-1 GHG Emission Source Summary Source Number **Emission Point** Estimated Annual CO<sub>2</sub>e Emissions EP01 and EP02 (2) Nominal 40-MWGE LM6000PF SPRINT Combined-Cycle Combustion Turbines 374,635 CT01A and CT01B (3) Nominal 40-MW CombinedGE LM6000 <u>PF SPRINT Simple</u>-Cycle Combustion TurbinesCT02A, CT02B, and CT03A EP03, EP04, and EP05 561,953 24,703 EP06 through EP11 Six (6) Inlet Air Heaters EP18 and EP19 Two (2) Fuel Gas Heaters 2,306 EP16 One (1) Diesel Fire Pump 51 226 EP15 One (1) Diesel Standby Generator

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# Regulatory Review

This section provides a regulatory review of the applicability of federal air quality permitting requirements for GHGs and GHG air pollution control regulations for the CGS project proposed by <u>Black HillsBHC</u>. The purpose of this section is to provide appropriate explanation and rationale regarding the applicability of these regulations to the CGS project. The review is limited to federal regulations for GHG because there are no State of Wyoming regulations for GHG that apply to the permitting of CGS.

Because the Wyoming Department of Environmental Quality (WDEQ) has a SIP-approved PSD program for all criteria pollutants but has not adopted regulations under the Tailoring Rule, WDEQ is the permitting authority for the CGS non-GHG pollutants (other regulated NSR pollutants), while EPA Region 8 is the permitting authority for the CGS GHG pollutants. Both agencies have agreed to work together to process these two air permits for CGS.

# 4.1 Federal Regulations

The proposed project was evaluated to determine compliance with applicable federal GHG air quality regulations. Potentially applicable federal GHG regulations include the following:

- Final Prevention of Significant Deterioration and Title V Greenhouse Gas Tailoring Rule (Tailoring Rule) 40 CFR 51.166, 52.21, as published in the *Federal Register* (FR) June 3, 2010 (75 FR 31514)
- Federal Implementation Plan (FIP) for State of Wyoming GHG 40 CFR 52.37, as published in the *Federal Register* December 30, 2010 (75 FR 82246)
- New Source Review (NSR) 40 CFR 51 and 52

On April 2, 2007, the U.S. Supreme Court found that GHGs are air pollutants under Clean Air Act (CAA) section 302(g) (*Massachusetts* v. *EPA*, 549 U.S. 497 [2007]). GHG includes the six gases of  $CO_2$ , nitrous oxide (N<sub>2</sub>O), methane (CH<sub>4</sub>), hydrofluorocarbons (HFCs), perfluorocarbons (PFCs), and sulfur hexafluoride (SF<sub>6</sub>). Of these, the first three will be emitted from the CGS. These gases have different potential to affect global warming, termed the global warming potential (GWP). The GWP of the three emitted gases are  $CO_2$  (1), N<sub>2</sub>O (310), and CH<sub>4</sub> (21).

Based on the series of legal and regulatory actions that culminated in the Tailoring Rule, regulation of major increases of GHG emissions through the Prevention of Significant Deterioration (PSD) permit program was required. EPA recognized that the major source threshold levels for the criteria pollutants for PSD pollutants of 100 or 250 tons per year (tpy) would make virtually every new project a major source. Accordingly, in June, 2010, EPA adopted the Tailoring Rule to raise the major source thresholds for GHG to 75,000 or 100,000 tons of GHG per year.

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The State of Wyoming has an approved State Implementation Plan (SIP) based program for the criteria pollutants for the PSD permitting of new major sources. However, Wyoming has decided to not include GHG in the state PSD permitting program. Accordingly, the GHG PSD program is being implemented by the EPA for major sources of GHG within the State of Wyoming through the federally approved FIP.

#### 4.1.1 Greenhouse Gas Tailoring Rule

On June 3, 2010, EPA issued the final Tailoring Rule (75 FR 31514), which allowed the phasing in of the PSD permitting process for new major sources of GHGs such as the CGS project. Step 2 of the Tailoring Rule requires that beginning July 1, 2011, all new sources with the potential to emit (PTE) greater than 100,000 tpy of CO<sub>2</sub>e (including the statutory threshold of 100 or 250 tons on a mass basis) comply with PSD and Title V requirements. All references to "tons" are provided in terms of short tons (2,000 pounds/ton) instead of metric tonnes, in accordance with EPA GHG PSD permitting guidance.

As shown in Table 4-1, under the Tailoring Rule, the CGS will be a major source subject to PSD permitting because the total emissions of CO<sub>2</sub>e exceed 100,000 tpy. The CGS project will result in an increase in CO<sub>2</sub>e emissions of 963,874 tpy, and more than 100 tpy <u>inof</u> certain criteria pollutants. Therefore, the project is classified as a major source for PSD applicability determination.

#### TABLE 4-1

GHG Pollutants Expected to be Emitted, Annual Emission Rates, Global Warming Potential, and Annual Emissions Rates Adjusted for Global Warming Potential

Pollutant	Proposed Facility GHG Emissions (TPY)	Global Warming Potential (GWP)	GHG Emissions Adjusted for GWP (TPY)
Carbon Dioxide (CO <sub>2</sub> )	962,929	1	962,929
Nitrous Oxide (N <sub>2</sub> O)	1.82	310	564
Methane (CH <sub>4</sub> )	18.17	21	381
Total GHG as CO2e			963,874

#### 4.1.2 Federal Implementation Plan for Wyoming

EPA has determined that the Wyoming SIP is deficient for purposes of the PSD permitting of GHG. Accordingly, EPA adopted a FIP in which it retains the authority to issue a PSD permit for GHG. Thus, this application is being filed with EPA Region 8 for the sole purpose of obtaining a PSD permit for the emissions of GHG from the CGS. The permit for the emissions of the criteria and hazardous pollutants from CGS will be obtained from the State of Wyoming.

EPA has not adopted ambient air quality standards or new source performance standards for GHG. Accordingly, this application only contains a BACT analysis for GHG.

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### 4.1.3 New Source Review

PSD is the portion of NSR that applies to pollutants that are in attainment of National Ambient Air Quality Standards (NAAQS). Because there are no ambient air quality standards for GHG, all portions of the United States are in attainment for GHG. Major new or modified air emission sources locating in Laramie County are, therefore, potentially subject to PSD review for these GHG pollutants.

The first step in PSD review is determining whether the proposed facility is a major PSD source. As noted above, the CGS will be a major source. Therefore, CGS is subject to PSD review for GHG. The primary elements of PSD requirements are as follows: is application of BACT to emissions of GHG

Application of BACT to emissions of GHG

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# Greenhouse Gas BACT Analysis

## 5.1 Background

Black HillsAs described above, BHC plans to build a natural gas-fired combustion turbine generating facility in the southeast section of the City of Cheyenne in Laramie County, Wyoming, pursuant to its approved <u>CLFP</u> *Integrated Resource Plan* filed before the Wyoming Public Service Commission (described in Section 2.0, Project Description). The proposed site is immediately west of the Dry Creek Water Reclamation Facility, which is located approximately 5 miles southeast of the downtown area.

The CGS will consist of a total of five natural gas-fired CTGs sized at a nominalapproximately 40-MW capacity each. Two CTGs will be configured for combinedcycle operation and will each be equipped with dry-low NO<sub>x</sub> combustors and a HRSG without duct burners, with steam flowing from the two HRSGs to one condensing STG with condenser in a "2x1" configuration. The combined-cycle generation capacity is nominally 100 MW. All of the CTGs will be equipped with SCR for NO<sub>x</sub> control and Catalytic Oxidation for CO and VOC control. Three CTGs will operate in simple cycle. CGS auxiliary equipment includes one mechanical draft condenser wet cooling tower, three electric inlet air chiller units with mechanical draft cooling towers, six natural gas-fired inlet air heaters, two natural gas-fired fuel heaters, one diesel-fired fire pump, and one diesel-fired emergency generator.

### 5.1.1 CGS Business Plan and Combustion Turbine Selection

The Cheyenne LightCLFP CPCN and associated IRP (Docket Number 20003-112-EA11), were filed August 1, 2011, with the Wyoming Public Service Commission, and present the business plan in detail. The Black Hills PowerBHP CPCN and associated IRP will be submitted to the Commission in fall 2011. Generally, Black Hills'BHC's CPCN and associated IRP show the public need for increased capacity requirements, reserve generation requirements, and generation within the service area of Cheyenne for reliability reasons. The necessary generation will be primarily peaking for CLFP, with baseload capabilities for BHP, and will further enable renewable generation (wind, solar, and other renewable resources). Black HillsBHC identified natural gas simple-/combined-cycle gas turbines to be the best-suited generation source to meet this CGS business plan-

While Black Hills<u>BHC</u> has determined<u>selected</u> the <u>nominal output of eachGeneral Electric</u> <u>LM 6000PF SPRINT</u> combustion turbine to be 40 MW, for the combustion turbine manufacturer has not been selected. CGS project. Table 5-1 lists <u>potentialcomparable</u> combustion turbine manufacturers and a comparison of estimated performance efficiency at the CGS site conditions.-<u>This information was compiled from published data from Gas</u> <u>Turbine World magazine</u>, and is presented only for comparative purposes. Gross heat rate and efficiencies are based on power output at the combustion turbine generator terminals, and does not include consideration of parasitic unit auxiliary loads.

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Combustion Turbine Comparison				
Turbine <sup>1</sup>	Production (kW)	Gross Heat Rate (Btu/kWh) HHV	EfficiencyEfficiency	
Dresser-Rand				
DR-63G PC	35,150	9,095	37.5%	
GE Energy AeorderivativeAe	roderivative			
LM6000PC	39,253	9,487	36.0%	
LM6000PC Sprint	40,605	9,419	36.2%	
LM6000PD	34,612	9,103	37.5%	
LM6000PD Sprint	38,079	9,091	37.5%	
LM6000PF	34,612	9,103	37.5%	
LM6000PF Sprint	38,649	9,079	37.6%	
LM6000PG	42,995	9,556	35.7%	
GE Energy Oil & Gas				
LM6000PD	33,964	9,283	36.8%	
IHI Power Systems				
LM6000PC	34,306	9,198	37.1%	
LM6000PC Sprint	37,129	9,228	37.0%	
LM6000PD	33,800	9,231	37.0%	
LM6000PD Sprint	37,236	9,213	37.0%	
LM6000PG	40,084	9,157	37.3%	
Pratt & Whitney Power Syste	ms			
FT8 TwinPac	41,267 9,898		34.5%	
SwiftPac 50 DLN	41,175	9,914	34.4%	
Rolls-Royce				
Trent 60 DLE	41,537	9,064	37.7%	
Trent 60 DLE ISI	46,612	8,913	38.3%	
Siemens Energy				
SGT-800	37,772	10,126	33.7%	
SGT-900	39,781	11,626	29.4%	
	•	*		

# TABLE 5-1

<sup>1</sup> Specifications for production output at 59°F, 5,950-Foot Altitude, Gross Output, HHV.

-<sup>2</sup>Calculation: Efficiency= 3,413 Btu/kWh/Gross Heat Rate

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Black Hills will select a combustion turbine that best meets its business plan, its system, and operational criteria, with possible selection of any combustion turbine from Table 5.1. A key consideration is that installation of combustion turbines from only one manufacturer is desired, and both simple cycle and combined cycle operational considerations must be evaluated. Due to differences in exhaust temperatures and other factors, turbines with lower efficiency than others in simple cycle operation. As will be demonstrated below, Black Hills proposes to establish annual GHG mass and output based limits assuming use of a turbine from the top of the possible efficiency range, and will agree to comply with those limits regardless of actual turbine selection. Black Hills will perform a complete competitive bidding process to select the combustion turbine for the CGS project, and the selected combustion turbine will be subject to the GHG BACT permit limits established by EPA as part of this permitting process.

Therefore, BHC selected the GE LM6000PF SPRINT combustion turbine because it best meets its business plan, its system, and operational criteria. Business plan considerations for turbine selection include combustion efficiency, exhaust characteristics that impact combined cycle system efficiency, size range, and consistency with other locations. Selection of a "fleet" of like turbines for different locations provides advantages with knowledge of maintenance and operations, stocking of spare parts, and ability to "swap" turbines between locations. The combustion turbine calculated efficiency for this turbine (37.6%) compares favorably with other combustion turbines listed in Table 5.1.

Table 5-2 below lists the assumedGE LM6000PF SPRINT combustion turbine attributes to be used within the GHG BACT analysis, and represents high-efficiency operation in both simple- and combined-cycle operation. The information included in Table 5-2 is based upon GE provided information, and summarizes the estimated combustion turbine performance at site conditions including consideration for parasitic auxiliary loads. Therefore, since Table 5-1 does not consider unit auxiliary loads in the efficiency calculation, and Table 5-2 includes allowance for auxiliary loads, the values are slightly different between the two tables.

#### TABLE 5-2

EfficientGE LM6000PF SPRINT Combustion Turbine DefinitionAttributes

Combustion Turbine Criteria	Assumed Value <sup>1</sup>
Simple-Cycle Combustion Turbine Gross Output (MW)	37 <u>.1</u>
2x1 Combined-Cycle Combustion Gross Turbine Output (MW)	97 <u>.4</u>
Simple-Cycle Gross Heat Rate (Btu/KWh) HHV	9, <del>300<u>263</u></del>
Combined-Cycle Gross Heat Rate (Btu/KWh) HHV	7, <del>200<u>062</u></del>
Heat Input (Btu/hr) HHV	366

<sup>1</sup> 60<sup>0</sup> F at site elevation.

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## 5.2 Regulatory Basis

GHGs have become subject to emission permitting through PSD and Title V programs. On June 3, 2010, EPA issued the final Tailoring Rule (75 FR 31514), which allowed phasing in the PSD permitting process for new sources of GHGs such as the CGS project. Step 2 of the Tailoring Rule requires that beginning July 1, 2011, all new sources with PTE greater than 100,000 tpy of GHGs on a CO<sub>2</sub>e basis, and with a GHG PTE of 100 or 250 tpy, depending on source type, on a mass basis will become subject to PSD and Title V requirements. All references to tons within the table and in this BACT analysis are provided in terms of short tons (2,000 pounds/ton) instead of metric tonnes, in accordance with EPA GHG PSD permitting guidance.

The CGS project will be a new source with a GHG PTE of greater than 100,000 tpy CO<sub>2</sub>e and greater than the 100-tpy mass basis for listed sources, and will also have a PTE of greater than 100 tpy for certain criteria pollutants. Because the Wyoming Department of Environmental Quality (WDEQ) has a SIP-approved PSD program for all criteria pollutants but has not adopted regulations under the Tailoring Rule, WDEQ is the permitting authority for the CGS non-GHG pollutants (other regulated NSR pollutants), while EPA Region 8 is the permitting authority for the CGS GHG pollutants. Therefore, this GHG BACT analysis was prepared for presentation to EPA Region 8 as part of the CGS permit application process.

## 5.3 Emissions Summary

Per EPA Tailoring Rule definitions, GHGs consist of the following gases:

- Carbon Dioxide (CO<sub>2</sub>)
- Methane (CH<sub>4</sub>)
- Nitrous oxide (N<sub>2</sub>O)
- Hydrofluorocarbons (HFCs)
- Perfluorocarbons (PFCs)
- Sulfur hexafluoride (SF<sub>6</sub>)

To determine  $CO_{2e}$  emissions, mass flows of each individual gas are multiplied by the appropriate GWP as referenced to the Intergovernmental Panel on Climate Change (IPCC) Second Assessment Report, and the results are summed.

The combustion turbines, inlet air heaters, and fuel gas heaters will be fired with pipelinequality natural gas, and complete combustion will result <u>primarily</u> in water and  $CO_2$ byproducts. However, incomplete combustion will result in some unburned natural gas or  $CH_4$  emissions. Additionally, due to the presence of nitrogen in the combustion air, some small quantities of N<sub>2</sub>O will also be emitted. The standby generator and fire pump engines will be fired with diesel fuel, again resulting in  $CO_2$  emissions from oxidation of the fuel and with minor quantities of  $CH_4$  emissions resulting from incomplete combustion and N<sub>2</sub>O emissions from conversion of nitrogen from the atmosphere and fuel.

Table 5-3 represents potential sources and estimated quantities of GHG emissions from CGS project equipment.

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#### TABLE 5-3

CGS Estimated GHG Emissions by Equipment Category

Equipment	Description	Total CO <sub>2</sub> e Emissions (t/yr)
Two (2) Combustion Turbines in Combined-Cycle Operation with no HRSG Duct Burner	Maximum Heat Input Each 366 MMBtu/hr Higher Heating Value (HHV)	374,635
Three (3) Simple-Cycle Combustion Turbines	Maximum Heat Input Each 366 MMBtu/hr Higher Heating Value (HHV)	561,953
Two (2) Fuel Gas Heaters	Maximum Heat Input 4.5 MMBtu/hr each	2,306
One (1) Diesel Fire Pump	Maximum Heat Input 2.5 MMBtu/hr	51
One (1) Diesel Standby Generator	Maximum Heat Input 5.52 MMBtu/hr	226
Six (6) Inlet Air Heaters	Maximum Heat Input 16.07 MMBtu/hr each	24,703
Total		963,874

#### 5.3.1 GHG BACT Analysis Assumptions

During the completion of GHG BACT analysis, the following assumptions were made:

- Table 5-3 above presents estimated CGS GHG emissions in terms of CO<sub>2</sub>e emissions, and only includes emissions of CO<sub>2</sub>, CH<sub>4</sub>, and N<sub>2</sub>O. The CGS is not expected to emit HFCs or PFCs because these man-made gases are primarily used as cooling, cleaning, or propellant agents. SF<sub>6</sub> is also a man-made gas that may be used as an insulating gas for high-voltage equipment and circuit breakers; however, <u>Black HillsBHC</u> does not plan to install electrical equipment containing SF<sub>6</sub> at the CGS. Therefore, only CO<sub>2</sub>, CH<sub>4</sub>, and N<sub>2</sub>O will be included in CO<sub>2</sub>e totals.
- 2. From the GHG emissions inventory presented in Appendix <u>AB-1</u>, the relative quantities of CH<sub>4</sub> and N<sub>2</sub>O total only approximately <u>20945</u> tpy of <u>CO<sub>2</sub>e emissions</u>, or less than 0.0021 percent of total CO<sub>2</sub>e emissions. Due to the extremely small contribution of CH<sub>4</sub> and N<sub>2</sub>O emissions to the total, the CGS GHG BACT analysis only <u>included\_includes</u> the five-step process for CO<sub>2</sub> emissions.
- 3. Completion of the BACT analysis for criteria pollutants will result in the installation of an SCR system for  $NO_x$  emissions reduction, and an oxidation catalyst for control of CO and VOCs for each turbine.
- 4. During actual combustion turbine operation, the oxidation catalyst may result in minimal increases in CO<sub>2</sub> from the oxidation of any CO and CH<sub>4</sub> in the flue gas. However, the EPA Final Mandatory Reporting of Greenhouse Gases Rule (Mandatory Reporting Rule or MRR) (40 CFR 98) factors for estimating CO<sub>2</sub>e emissions from the combustion of natural gas assume complete combustion of the fuel. While the oxidation catalyst has the potential of incrementally increasing CO<sub>2</sub> emissions, these emissions are already accounted for in the MRR factors and included in the CO<sub>2</sub>e totals.
- 5. Similarly, the SCR catalyst may result in an increase in N<sub>2</sub>O emissions. Although quantifying the increase is difficult, it is generally estimated to be very small or

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negligible. From the GHG emissions inventory, the estimated  $N_2O$  emissions from all combustion turbines total only 1.5 tpy. Therefore, even if there were an order-of-magnitude increase in  $N_2O$  as a result of the SCR, the impact to  $CO_2e$  emissions would be insignificant.

Use of the SCR and oxidation catalyst slightly decreases the project thermal efficiency due to backpressure on the turbines (these impacts are already included in the emission inventory) and, as noted above, may create a marginal but unquantifiable increase to N<sub>2</sub>O emissions. The combustion turbine SCR systems will be designed to reduce NO<sub>\*</sub> from the combustion turbine low-NO<sub>\*</sub> burners (LNBs) from 25 parts per million (ppm) to 3 ppm. Similarly, the oxidation catalyst systems have the benefits of reducing both CO and VOCs. The oxidation catalyst reduces CO and VOC emissions from 70 ppm to 6 ppm, and from 8.4 ppm to 3 ppm, respectively.

\_While elimination of the NO<sub>x</sub> and CO/VOC controls could conceivably be considered as an option within the GHG BACT, the environmental benefits of the NO<sub>x</sub>, CO, and VOC control are assumed to outweigh the marginal increase to GHG emissions. Thus, even if carried forward through the GHG BACT analysis, they would be eliminated in Step 4 due to other environmental impacts. Therefore, we have not considered omission of these controls within the BACT analysis.

## 5.4 Top-Down BACT Process

The EPA has developed a recommended process for conducting BACT analyses, referred to as the "top-down" method. The following steps to conducting a top-down analysis are listed in the EPA's *New Source Review Workshop Manual* (EPA, 1990):

- Step 1: Identify all control technologies
- Step 2: Eliminate technically infeasible options
- Step 3: Rank remaining control technologies by control effectiveness
- Step 4: Evaluate most effective controls and document results
- Step 5: Select BACT

Each of these steps, described in the following sections, has been conducted for GHG emissions for the CGS project. The following top-down BACT analysis for CO<sub>2</sub>e has been prepared in accordance with the EPA's *New Source Review Workshop Manual* (EPA, 1990). A top-down BACT analysis takes into account energy, environmental, economic, and other costs associated with each alternative technology.

## 5.5 Combustion Turbine BACT for GHGs

### Step 1: Identify All Control Technologies

The combustion turbines will be <u>nominal 40 MW machinesGE LM6000PF SPRINT</u> <u>combustion turbines</u> that utilize the latest emissions control technology. There are two basic alternatives identified to limit the GHG emissions of this project. These options include

- Carbon Capture and Storage (CCS)
- Electrical Generation Efficiency

GREENHOUSE GAS PSD PERMIT APPLICATION REVISION 1 - SEPTIMBER 2011 5-6 Black Hills'BHC's CGS Business Plan and IRP have determined that the proposed mix of natural gas combined-cycle and simple-cycle power generation is the only alternative that meets all of the CGS requirements for economic and reliable power 24 hours per day and in all weather conditions. As such, other generation technologies such as coal, wind, and solar were not evaluated in this BACT analysis. This is consistent with EPA's March 2011 *PSD and Title V Permitting Guidance for Greenhouse Gases*, which states, "EPA has recognized that a Step 1 list of options need not necessarily include inherently lower polluting processes that would fundamentally redefine the nature of the source proposed by the permit applicant...", and "...the permitting authority should keep in mind that BACT, in most cases, should not regulate the applicant's purpose or objective for the proposed facility..." (p. 26) Nonetheless, it should be noted that the CGS is intended to provide supplemental and backup generation for solar and wind projects, and renewable generation is not an adequate supplement and backup for other renewable generation; a fuel-based alternative is required.

The only identified <u>alternativesGHG emission "control" options</u> are post-combustion CCS and energy efficiency of the proposed generation facility.

## Step 2: Eliminate Technically Infeasible Options Effectiveness

#### Carbon Capture and Storage Systems

CCS systems involve use of adsorption or absorption processes to remove  $CO_2$  from flue gas, with subsequent desorption to produce a concentrated  $CO_2$  stream. The concentrated  $CO_2$  is then compressed to "supercritical" temperature and pressure, a state in which  $CO_2$  exists neither as a liquid nor a gas, but instead has physical properties of both liquids and gases. The supercritical  $CO_2$  would then be transported to an appropriate location for underground injection into a suitable geological storage reservoir, such as a deep saline aquifer or depleted coal seam, or used in crude oil production for enhanced oil recovery.

The concentration of CO<sub>2</sub> is required because injection of exhaust streams containing high levels of nitrogen, oxygen and dilute CO<sub>2</sub> is not technically feasible. Research into technically and economically feasible capture systems is ongoing and is the focus of many large-scale grants from the U.S. Department of Energy (DOE). Adequate techniques for compression of CO<sub>2</sub> exist, but such compression systems require large amounts of energy. Furthermore, the capture process is energy intensive. It is estimated that a significant portion of power plant output would be required for CO<sub>2</sub> capture and subsequent compression. As stated in the August 2010 *Report of the Interagency Tack Force on Carbon Capture and Storage*, "For a [550 MWe net output] natural gas combined cycle (NGCC) plant, the capital cost would increase by \$340 million and an energy penalty of 15 percent would result from the inclusion of CO<sub>2</sub> capture."

Research into geologic storage requirements is also ongoing. DOE research programs are investigating the reliability, permanence, risks, required monitoring, verification, and other issues to be addressed before geologic storage can proceed on a large commercial scale. Many regulatory issues remain to be resolved, such as pore space ownership, financial responsibility requirements, long term risk following closure of the sequestration site, and issues regarding CO<sub>2</sub> purity and potential contamination of aquifers.

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CCS systems are not currently available on a commercial basis. Large-scale demonstration projects are currently being planned or are in early stages of development, but no company or vendor currently offers a commercially available turn-key, integrated CCS system. While many believe that CCS will allow the future use of fossil fuels while minimizing GHG emissions, there are a number of technical barriers concerning the use of this technology for the CGS:

- No full scale systems are currently in operation for capture of CO<sub>2</sub> from dilute exhaust steams such as that from natural gas fired electrical generation systems,
- Lack of pilot scale experience with capture systems for high-temperature streams such
   as simple cycle combustion turbine exhaust currently exists,
- Use of captured CO<sub>2</sub> for enhanced oil recovery (EOR) is widely believed to represent the practical first opportunity for CCS deployment; however identification of suitable oil reservoirs with willing and able owners and operators is beyond the capability for most electric utilities. Owners of oil fields generally closely guard information regarding production volumes and reservoir status,
- Little experience exists with other types of storage systems such as deep saline aquifers
   or depleted coal seams,
- Because of the developmental nature of CCS technology, vendors and contractors do not offer turn-key offerings; separate contracting would be required for capture system design and construction; compression and pipeline system routing, siting and licensing, engineering and construction; and geologic storage system design, deployment, operations, and monitoring,
- Significant legal uncertainties still exist regarding relationship between land surface ownership rights and subsurface (pore space) ownership, potential conflicts with other uses of land such as exploitation of mineral rights, management of risks and liabilities, etc, and
- Potential for frequent startup and shutdown of generation units at the CGS make CCS impractical for two reasons – inability of capture systems to startup in the same short time frame as combustion turbines, and infeasibility for potential users of the CO<sub>2</sub> such as EOR systems to use uncertain and intermittent flows. The simple cycle units at the CGS are designed for peaking operation and as such the ability to rapidly startup the units and to operate them for short durations is critical. While the combined cycle units are being designed for baseload operation, under many operational scenarios rapid response may also be needed for these units.

These issues are discussed in more detail below.

As suggested in the 1990 Draft EPA New Source Review Workshop Manual, control technologies should be demonstrated in practice on full scale operations in order to be considered available within a BACT analysis. "Technologies which have not yet been applied to (or permitted for) full scale operations need not be considered available; an applicant should be able to purchase or construct a process or control device that has already been demonstrated in practice." As will be discussed in more detail below, carbon

S-CHEYENNE GENERATING STATION GREENHOUSE GAS PSD PERMIT APPLICATION REVISION 1 - SEPTIMBER 2011 5-8 capture technology has not been demonstrated in practice in power plant applications. Other process industries do have carbon capture systems that are demonstrated in practice, but the technology used for these processes cannot be applied to power plants.

Three fundamental types of carbon capture systems are employed throughout different process and energy industries: sorbent adsorption, physical absorption, and chemical absorption. Use of carbon capture systems on power plant exhaust is inherently different from other commercial scale systems currently in operation, due in large part to concentration of CO<sub>2</sub> and other constituents in the gas streams.

For example,  $CO_2$  is separated from petroleum refinery hydrogen plants in a number of locations, but this is typically accomplished on the product gas from a steam methane reforming process which contains primarily hydrogen (H<sub>2</sub>), unreacted methane (CH<sub>4</sub>) and CO<sub>2</sub>. Based on the stoichiometry of the reforming process the CO<sub>2</sub> concentration is approximately 80 percent by weight, and the gas pressure is approximately 350 pounds per square inch, gauge (psig). Because of the high concentration and high pressure a pressure swing adsorption (PSA) process is used for the separation. In the PSA process, all non-H<sub>2</sub> components including CO<sub>2</sub> and CH<sub>4</sub> are adsorbed onto the solid media under high pressure. After the sorbent becomes saturated the pressure is reduced to near atmospheric conditions to desorb these components. The  $CO_2/CH_4$  mixture in the PSA tail gas is then typically recycled to the reformer process boilers to recover the heating value; but where the  $CO_2$  is to be sold offset an additional amine absorption process would be required to separate the CO<sub>2</sub> from CH<sub>4</sub>. In its May 2011 "DOE/NETL Advanced Carbon Dioxide Capture R&D Program: Technology Update", NETL notes the different applications for chemical solvent absorption, physical solvent absorption, and sorbent adsorption processes. From Section 4.B, "When the fluid component has a high concentration in the feed stream (e.g., 10 percent or more), a pressure swing adsorption (PSA) mechanism is more appropriate."

In another example, at the Dakota Gasification Company's Great Plains Synfuels Plant (GPSP) in North Dakota, CO<sub>2</sub> is separated from intermediate fuel streams produced from gasification of coal. The gas from which the CO<sub>2</sub> is separated is a mixture of primarily hydrogen (H<sub>2</sub>), methane (CH<sub>4</sub>), and 30 to 35 percent CO<sub>2</sub> and a physical absorption process (Rectisol) is used. In contrast, as shown in the GE Guarantee in Appendix B-3, and as noted on Page 29 of the August 2010 *Report of the Interagency Task Force on Carbon Capture and Storage*, CO<sub>2</sub> concentrations for natural-gas fired systems are in the range of 3 to 5 percent. This adds significant technical challenges to separation of CO<sub>2</sub> from power plant exhaust as compared to other systems.

In Section 4.A of the above-referenced Technology Update, NETL notes this difference between pre-combustion CO<sub>2</sub> capture such as that from the GPSP versus the postcombustion capture such as that required from a natural-gas fired power plant, "Physical solvents are well suited for pre-combustion capture of CO<sub>2</sub> from syngas at elevated pressures; whereas, chemical solvents are more attractive for CO<sub>2</sub> capture from dilute lowpressure post-combustion flue gas."

The Interagency Task Force on Carbon Capture and Storage consists of 14 executive departments and federal agencies, co-chaired by the DOE and EPA. In the 2010 report noted above, the task force discusses four currently operating post-combustion CO<sub>2</sub> capture systems associated with power production. All four are on coal-based power plants where

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CO<sub>2</sub> concentrations are higher (typically 12 to 15 percent), with none noted for natural gasbased power plants (typically 3 to 5 percent).

The Department of Energy's (DOE) National Energy Technology Laboratory (NETL) is a key player in the nation's efforts to realize commercial deployment of CCS technology. A downloadable database of worldwide CCS projects is available on the NETL website (http://www.netl.doe.gov/technologies/carbon\_seq/global/database/index.html). Filtering this database for projects that involve both capture and storage, which are based on post-combustion capture technology (the only technology applicable to natural gas turbine systems), which are shown as "active" with "injection ongoing" or "plant in operation", yields four projects. Three projects, one of which is a pilot-scale process noted in the Interagency Task Force report as described above, are listed at a capacity of 274 tons per day (100,000 tons per year) and the fourth has a capacity of only 50 tons per day. Postcombustion CCS has not been accomplished on a scale of even the modestly-sized CGS facility, which could produce up to 964,000 tons per year or 2,600 tons per day. Furthermore, scale-up involving a 10x increase in size from pilot scale to commercial scale is unusual in chemical processes and would represent significant technical risk.

As detailed in its the August 2010 report, one goal of the task force Task Force is to bring five to 10 commercial demonstration projects online by 2016. With demonstration projects still years away, clearly the technology is not currently commercially available.- It is notable that several projects, including those with DOE funding or loan guarantees, have been cancelled in recent months, making it further unlikely that technical information required to scale up these processes can be accomplished in the near future. For example, at the AEP Mountaineer site noted above, the commercial scale project was to expand capture capacity to 100,000 tpy, but to date only the "Project Validation Facility" was completed and only accomplished capture of a total of 50,000 metric tons and storage of 37,000 metric tons of CO<sub>2</sub>. AEP recently announced that the larger project will be cancelled after completion of the front end engineering design due to uncertain economic and policy conditions.

The Interagency Task Force report notes the lack of demonstration in practice: "Current technologies could be used to capture CO<sub>2</sub> from new and existing fossil energy power plants; however, they are not ready for widespread implementation primarily because they have not been demonstrated at the scale necessary to establish confidence for power plant application. Since the CO<sub>2</sub> capture capacities used in current industrial processes are generally much smaller than the capacity required for the purposes of GHG emissions mitigation at a typical power plant, there is considerable uncertainty associated with capacities at volumes necessary for commercial deployment."

One of the many technical challenges with carbon capture systems is the temperature of the exhaust steams. For coal-based plants, where most of the post-combustion capture technology research has been accomplished, typical exhaust temperatures are in the range of 300 degrees F. For the three simple cycle systems planned for the CGS, exhaust temperature will be up to 900 degrees F. To our knowledge, CCS pilot tests have not been accomplished on a simple cycle gas turbine system anywhere in the world. This would represent another major technical uncertainty associated with CCS implementation at the CGS. Chemical absorption of CO<sub>2</sub>, such as that accomplished by most amine-based carbon capture processes, is an exothermic reaction, meaning that heat is released during absorption; high temperature of the exhaust and solvent would therefore inhibit the carbon capture.

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GREENHOUSE GAS PSD PERMIT APPLICATION REVISION 1 – SEPTMBER 2011 5-10 Furthermore, the regeneration of the sorbent to release the CO<sub>2</sub> for compression requires heating of the sorbent, so high temperature of the solution would clearly inhibit the chemical reaction required for absorption.

BHC is aware of the planned construction of a CO<sub>2</sub> pipeline, intended to transport byproduct CO<sub>2</sub> from oil and gas operations to an EOR location in Montana. This project will be used as a CCS large-scale demonstration project by the DOE-funded Plains CO<sub>2</sub> Reduction Partnership. From review of publicly available documentation, the pipeline is being designed with excess capacity, presumably to provide future capability to transport CO<sub>2</sub> from other sources to EOR locations in the region. At its closest point the pipeline is estimated to be 175 miles away from the power plant location. However the location, time frame, and needed flowrates for those future EOR operations are closely guarded trade secrets. Thus BHC, as developer of this power generation facilities, has no way of knowing when and if those future needs will be realized. At the current time, the only known CO<sub>2</sub>based tertiary oil recovery system operating in the region is the Salt Creek Field (also approximately 175 miles from the power plant location),for which current CO<sub>2</sub> needs are being served from current separation systems in the Shute Creek Field of southwest Wyoming, with CO<sub>2</sub> being transported by existing pipeline.

Ability to inject into deep saline aquifers as an alternative to EOR reservoirs is a major focus of the NETL research program. While it is believed that saline aquifers are a viable opportunity, many uncertainties exist. Risk of mobilization of natural elements such as manganese, cobalt, nickel, iron, uranium, and barium into potable aquifers is of concern. Technical considerations for site selection include geologic siting, monitoring and verification programs, post injection site care, long term stewardship, property rights, and other issues. In regards to CO<sub>2</sub> storage security, the CCS Task Force Report notes such uncertainties, "The technical community believes that many aspects of the science related to geologic storage security are relatively well understood. For example, IPCC concluded that "it is considered likely that 99 percent or more of the injected CO<sub>2</sub> will be retained for 1,000 years" (IPCC, 2005). However, additional information (including data from large-scale field projects with comprehensive monitoring) is needed to confirm predictions of the behavior of natural systems in response to introduced CO<sub>2</sub> and to quantify rates for long-term processes that contribute to trapping and, hence, risk profiles (e.g., IPCC, 2005)."

<u>CCS technology development is dominated by vendors who are attempting to</u> <u>commercialize carbon capture technologies and academia-lead teams (largely funded by</u> <u>DOE) who are leading research into the geologic systems. Ability for electric utilities to</u> <u>contract for turn-key CCS systems simply does not exist at this time.</u>

Most current carbon capture systems are based on amine or chilled ammonia technology, which are chemical absorption processes. While capture system startup and shutdown time of vendor processes could not be confirmed within this BACT analysis, clearly both types of processes would require durations which exceed the turbine startup time. The simple cycle generation systems are designed to be able to produce electricity at full load within 10 minutes of cold start, and the combined cycle systems designed to be able to produce electricity at full load with SCR and oxidation catalysts controlling criteria air pollutants within 40 minutes of startup. Durations of plant operation may be short, depending on needs to serve peak power loads. In contrast, both amine and chilled ammonia systems require startup of countercurrent liquid-gas absorption towers and either chilling of the

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GREENHOUSE GAS PSD PERMIT APPLICATION REVISION 1 - SEPTIMBER 2011 5-11 ammonia solution or heating of regeneration columns for the amine systems. It is technically infeasible for the carbon capture systems to startup and shutdown in the time frames required to effectively serve this type of operation, meaning that significant portions of at least the simple cycle operations would run without CO<sub>2</sub> capture even with implementation of a CCS system.

Finally, the potential to sell CO<sub>2</sub> to industrial or oil & gas operations is infeasible for an operation such as this, where daily operation of both simple cycle and combined cycle systems may depend on grid dispatch needs. Even if a potential EOR opportunity could be identified by the power plant developers, such an operation would typically need a steady supply of CO<sub>2</sub> year-round. Intermittent CO<sub>2</sub> supply from potentially short-duration with uncertain daily operation would be virtually impossible to sell on the market, making the EOR option unviable. Therefore, CCS technology would be better suited on applications which have low variability in operating conditions.

In the EPA PSD and Title V GHG permitting guidance, it is acknowledged that the issues noted above are summarized, "A number of ongoing research, development, and demonstration projects may make CCS technologies more widely applicable in the future" (italics added). From Page 36 of this guidance, "While CCS is a promising technology<sub>72</sub> EPA does not believe that at this time CCS will be a technically feasible BACT option in certain cases.". As noted above, to establish that an option is technically infeasible, the permitting record should show that an available control option has neither been demonstrated in practice nor is available and applicable to the source type under review. EPA recognizes the significant logistical hurdles that the installation and operation of a CCS system presents and that sets it apart from other add-on controls that are typically used to reduce emissions of other regulated pollutants and already have an existing reasonably accessible infrastructure in place to address waste disposal and other offsite needs. Logistical hurdles for CCS may include obtaining contracts for offsite land acquisition (including the availability of land), the need for funding (including, for example, government subsidies), timing of available transportation infrastructure, and developing a site for secure long-term storage. Not every source has the resources to overcome the offsite logistical barriers necessary to apply CCS technology to its operations, and smaller sources will likely be more constrained in this regard..."

The Interagency Task Force report notes the lack of demonstration in practice: "Current technologies could be used to capture CO<sub>2</sub>-from new and existing fossil energy power plants; however, they are not ready for widespread implementation primarily because they have not been demonstrated at the scale necessary to establish confidence for power plant application. Since the CO<sub>2</sub>-capture capacities used in current industrial processes are generally much smaller than the capacity required for the purposes of GHG emissions mitigation at a typical power plant, there is considerable uncertainty associated with capacities at volumes necessary for commercial deployment."

Therefore, the CCS alternative is not considered technically feasible for the CGS project, and is eliminated from further consideration. While it is being eliminated based on technical feasibility in Step 2, it should be acknowledged that even if carried forward for further analysis, it would undoubtedly be eliminated in Step 4 based on cost effectiveness. The technical risks associated with the technologies would make the project un-financeable. The energy requirements for the capture and compression systems alone would dramatically

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GREENHOUSE GAS PSD PERMIT APPLICATION REVISION 1 – SEPTMBER 2011 increase the overall cost of generation for the project, and the cost of capture and compression systems, pipelines, development of storage reservoirs, and monitoring systems is very high as well.at the suggestion of USEPA team members, economic feasibility issues will be covered in Step 4.

#### **Electrical Generation Efficiency**

EPA's *PSD and Title V Permitting Guidance for Greenhouse Gases* (EPA, 2011) identifies three categories of control technologies (p. 25):

- 1. Inherently lower-emitting processes/practices/designs
- 2. Add-on controls, and
- 3. Combinations of lower-emitting process/practices/designs and add-on controls

Because there are no demonstrated add-on controls, only those processes, practices, and designs that result in lower GHG emissions are applicable for this BACT analysis. As noted above, the project includes both simple-cycle and combined-cycle generation in this phase of the project, and possible<sub>z</sub> but unplanned future expansion of the facility could include build-out of the simple-cycle combustion turbines into combined-cycle systems- providing added thermal efficiencies. The CGS project as proposed will utilize a high-efficiency, state-of-the-art, combustion turbine, generator, and HRSG design. OperationOperations will use good combustion practices and result in energy efficient operation to provide steam to a new steam turbine generator.

In addition, installation of two combustion turbines in a combined cycle configuration results in a lower resultant plant heat rate as compared to only simple cycle combustion turbines. In some cases, the turbine which is most efficient in simple cycle mode will result in a less efficient turbine for combined cycle operations.

Furthermore, inlet air chillers will be used to prevent loss of turbine efficiency that results during hot weather-<u>, and a wet cooling tower will be used to improve the thermal efficiency</u> of the combined cycle system.

The following analysis will demonstrate that the overall generation efficiency meets or exceeds that of other recently implemented projects.

The permit limits proposed in this application are based on assumed use of a GE LM 6000PF SPRINT combustion turbine of 37.1 MW gross output and a gross heat rate of 9,300263 Btu/kWh (HHV) for simple-cycle operation. This results in an estimated net output of approximately 97.4 MW at a netgross heat rate of 7,200062 Btu/kWh (HHV) for the 2x1 combined-cycle system, which results in an efficiency of 36.8% and 48.3% for simple cycle and combined cycle operation respectively. These efficiencies include consideration of parasitic auxiliary loads. The combined-cycle system will not have duct firing. All noted performance information is based upon CGS site conditions at 60°F; the high altitude of the area results in marginal decreases to turbine efficiency compared to other locations. The CGS project will utilize all new equipment.

#### **Combustion Turbine Generator Comparable Permitted Emissions**

A search of the EPA's RACT/BACT/LAER Clearinghouse (RBLC) was performed for simple- and combined-cycle projects with combustion turbines similar to those proposed for the CGS project. No GHG permit information was limits were found in searching the RBLC

for comparable units. Information from other recent combustion turbine projects was researched for this BACT analysis, even though this information has not yet been posted to the RBLC, thermal efficiency data was available.

#### Efficiency Review

An efficiency review of the proposed CGS project was completed with two metrics: 1) RBLC comparable unit heat rates and 2) comparison of CO<sub>2</sub>e emission rates.

#### **RBLC Efficiency Comparison**

The RBLC information presented in Table 5-4 below provides a comparison of efficiencies for projects with combustion turbines in the same nominal 40-MW size range as the CGS project. The information presented is for combustion turbines operating in simple cycle. No information was found for comparable 40-MW combined-cycle units without duct burning.

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RBLC Efficiency Info	ormation – Simu	ble Cycle					$\sim$	Formatted Table
Facility	State	Description	Heat Capacity MMBtu/hr (HHV)	Net MW	Heat Rate Btu/kWh (HHV)	Calculated Efficiency (%)		
Arvah B. Hopkins Generating StationWestern Farmers Electric	FloridaOkl ahoma	GE LM6000PCCombus tion Turbine Simple Cycle	4 <u>89.5462.7</u>	50	9, <del>790<u>254</u></del>	<u>36.9</u>		
Lambie Energy Center <u>El Colton,</u> LLC	California	GE LM6000PC Simple Cycle LM6000 (Enhanced Sprint)	<del>500<u>456.5</u></del>	4 <del>9.9<u>48.7</u></del>	<del>10,020<u>9,374</u></del>	<u>36.4</u>		Formatted: Keep with next, Keep lines together
Creole Trail LNGBayonne Energy Center	Louisiana <u>N</u> ew Jersey	Combustion Turbine Simple CycleRolls Royce Trent 60WLE	<del>290<u>603</u></del>	<del>30<u>64</u></del>	9, <del>667<u>422</u></del>	<u>36.2</u>		
Western Farmers ElectricCreole Trail LNG	Oklahoma Louisiana	Combustion Turbine Simple Cycle	4 <del>62.7<u>290</u></del>	<del>50<u>30</u></del>	9, <del>25</del> 4 <u>667</u>	<u>35.3</u>		
El Colton, LLCArvah B. Hopkins Generating	California <u>FI</u> orida	LM6000 (Enhanced Sprint) <u>GE</u> LM6000PC Simple Cycle⊾	4 <del>56<u>489</u>.5</del>	4 <u>8.7</u> 50	9, <del>374<u>790</u></del>	<u>35.0</u>		Formatted: Don't keep with next, Don't keep lines together Formatted: Font color: Auto
Station							-	,
Indigo Energy Facility	California	LM6000 (Enhanced Sprint)	450	45	10,000	<u>34.1</u>		Formatted: Font color: Auto
BayonneLambie Energy Center	New JerseyCalif ornia	Rolls Royce Trent 60WLEGE LM6000PC Simple	<del>603<u>500</u></del>	64 <u>49.9</u>	<del>9,422<u>10.020</u></del>	34.1		

Notes: Used 1.108 for HHV/LHV conversion factor.

The combustion turbines compared above are similar in size to those planned for the CGS project. As noted above, this analysis and resulting CGS proposed permit limits are based on use of a turbine with simple-cycle gross heat rate of 9,<del>300263</del> Btu/kWh (HHV). An exact comparison cannot be made between the CGS combustion turbines and those listed in Table 5-14 above because each project has unique equipment and site conditions, primarily elevation and temperature. However, the CGS heat rate compares very favorably with all of the reviewed comparable projects listed above, which demonstrates the high-efficiency attributes of the CGS project.

#### CO2e Emission Rate Comparison

In simple-cycle operation, the CGS turbines are estimated to produce 1,102 pounds of  $CO_{2e}/MWh$  at average ambient conditions and full-load operation. Considering the range of normal operating loads (50 to 100 percent generator output), and ambient temperature (0°F to 108°F), GHG output for the CGS simple-cycle combustion turbines range from 1,072 to 1,603 pounds of CO<sub>2</sub>e for new and clean combustion turbine prior to any degradation.

Table 5-5 below presents operating information from the EPA Acid Rain database, and was developed using actual comparable operating unit information from 2010.

TABLE 5-5 CGS Comparable Unit GHG Emissions

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State	Facility Name	Unit ID	Operating Time (Hr)	Net Load (MWh)	CO₂ Tons	lb CO₂/MWh
CA	El Cajon Energy Center	1	242	9450	5652	1196
ОК	Horseshoe Lake	10	710	29293	18142	1239
OK	Horseshoe Lake	9	174	6851	4248	1240
CA	Orange Grove Project	CTG1	632	25017	15734	1258
CA	Orange Grove Project	CTG2	654	24954	15847	1270
FL	Arvah B Hopkins	HC4	903	27627	17623	1276
FL	Polk	**2	249	27652	18500	1338
FL	Arvah B Hopkins	HC3	662	18283	12529	1371
FL	Polk	**5	476	51662	36111	1398
FL	Polk	**4	563	60221	42443	1410
FL	Polk	**3	204	23176	16600	1432
NJ	Bayonne Plant Holding, LLC	2001	1055	35582	28385	1595
NJ	Bayonne Plant Holding, LLC	1001	1208	39061	32004	1639
NJ	Bayonne Plant Holding, LLC	4001	1134	36629	30200	1649
NE	C W Burdick	GT-3	24	426	399	1871
NE	C W Burdick	GT-2	33	606	579	1912
CA	Escondido Energy Center, LLC	CT1A	28	345	466	2702
CA	Escondido Energy Center, LLC	CT1B	28	345	468	2718

Notes:

Net load 5% lower than gross load.

Data as per EPA Clean Air Markets - Data and Maps.

Based on 2010 data.

The CGS combustion turbine GHG output compares favorably with the facilities shown Table 5-5 above. It is recognized that in establishing any permit limit, allowance must be given for load variances, impact of ambient conditions, startup and shutdown, and equipment degradation over time. This is exemplified by reviewing the information from Table 5-5, because all of these units can be considered as "peaking" due to the low number of annual operating hours. The resultant wide variance in pounds of  $CO_2e/MWh$  may likely be attributed to the significant proportion of time in startup and shutdown and/or reduced load operation, as well as lower thermal efficiency for older units.

Note that, based on the combustion turbine defined above, and considering the range of normal operating loads (50 to 100 percent output), and ambient temperature (0°F to 108°F), GHG output for the CGS 2x1 combined-cycle system ranges from 833 to 985 pounds of CO<sub>2</sub>e for a new or clean combustion turbine prior to any degradation.

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<u>Step 3: Rank Remaining Control Technologies by Control Effectiveness</u> <u>The only remaining technically feasible GHG control technology for the CGS</u> <u>project is the electrical generation efficiency</u>. Step 3: Rank Remaining <u>Control Technologies by Control Effectiveness</u>

The only remaining technically feasible GHC control technology for the CCS project is the electrical generation efficiency. This option is presented in Table 5-6 based on their energy efficiencies expressed in terms of heat rate.

TABLE 5-6 CGS Project GHG Control Technology Ranking

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#### TABLE 5-6 CGS Project GHG Control Technology Ranking

Configuration	Gross Plant Heat Rate (HHV) (Btu/kWh) <sup>1</sup>
Electrical Generation Combined-Cycle Efficiency (without duct firing)	<del>7,200</del>
Electrical Generation Simple-Cycle Efficiency	<del>9,300</del>
Electrical Generation Combined-Cycle Efficiency	<u>7,062</u>
Electrical Generation Simple-Cycle Efficiency	<u>9,263</u>

Note: <sup>1</sup>At CGS site conditions.

#### **Combustion Turbine Design Elements**

As demonstrated above, the GE LM6000PF SPRINT combustion turbine has high efficiency which is equal or greater the majority of other turbines of the same nominal capacity. However the differences in efficiency from offerings of other vendors are in some cases trivial. The design elements of those turbines that result in high efficiency undoubtedly vary between vendors, and in many cases are proprietary and confidential. Thus an extensive analysis of what design considerations are needed to have an efficient turbine design is beyond the scope of this permit application.

<u>However the issue was discussed with the selected turbine vendor, GE, and they offered</u> comments on the unique elements of their design. This information is provided in Appendix <u>B-4. Some of the key elements noted by GE are dual shaft architecture, low shaft speed,</u> modulation of shaft speed and air flow with power, and high operating pressure ratio.

It should be noted that the electrical generator is provided as a combined unit with the GE LM6000PF SPRINT combustion turbine package, and has been engineered to match combustion turbine operating characteristics. Preliminary information indicates that the generator is 98%+ efficient, so overall system efficiency is driven by the combustion turbine characteristics.

The CGS 2x1 combined cycle system will also utilize a steam turbine and Heat Recovery. Steam Generators (HRSG). Steam turbines manufactured today for small combined cycle plants have efficiencies limited by the metal design temperatures and pressures. The steam turbine is custom engineered rotating machinery where the efficiency is optimized in the blade path design, which maximizes the energy extracted from the steam. HRSG efficiency is maximized in the design by selecting aggressive approach and pinch points to extract the maximum heat out of the gas turbine exhaust stream. The efficiency is further improved by tube bundle arrangement, finned tubing and back end recirculation and or condensate preheating.

#### Step 4: Evaluate Most Effective Controls and Document Results

The <u>As</u> demonstrated in Step 2 above, CCS is not a technically feasible alternative for the <u>CGS</u> project. Nonetheless, at the suggestion of USEPA team members, economic feasibility of CCS technology is reviewed in this Step 4. Control options considered in this step

S-CHEVENNE GENERATING STATION REVISION 1 - SEPTIMBER 2011 5-18 therefore include application of CCS technology, and plant energy efficiency. As demonstrated below, CCS is clearly not economically feasible for the CGS.

On Page 42 of the EPA PSD and Title V Permitting Guidance, it is suggested that detailed cost estimates and vendor quotes should not be required where it can be determined from a qualitative standpoint that a control strategy would not be cost effective: "With respect to the valuation of the economic impacts of GHG control strategies, it may be appropriate in some cases to assess the cost effectiveness of a control option in a less detailed quantitative (or even qualitative) manner. For instance, when evaluating the cost effectiveness of CCS as a GHG control option, if the cost of building a new pipeline to transport the CO<sub>2</sub> is extraordinarily high and by itself would be considered cost prohibitive, it would not be necessary for the applicant to obtain a vendor quote and evaluate the cost effectiveness of a CO<sub>2</sub> capture system."

The guidance document also acknowledges the high costs of CCS technology at the current time: "EPA recognizes that at present CCS is an expensive technology, largely because of the costs associated with CO<sub>2</sub> capture and compression, and these costs will generally make the price of electricity from power plants with CCS uncompetitive compared to electricity from plants with other GHG controls. Even if not eliminated in Step 2 of the technical feasibility of the BACT analysis, on the basis of the current costs of CCS, we expect that CCS will often be eliminated from consideration in Step 4 of the economical feasibility of the BACT analysis, even in some cases where underground storage of the captured CO<sub>2</sub> near the power plant is feasible."

The costs of constructing and operating CCS technology are indeed extraordinarily high based on current technology. Even with the optimistic assumption that appropriate EOR opportunities could be identified in order to lower costs as compared to "pure" sequestration in deep saline aquifers or depleted coal seams, additional costs to the CGS would include the following:

- Licensing of scrubber technology and construction of carbon capture systems,
- Significant reduction to plant output due to the high energy consumption of capture and compression systems,
- Identification of oil & gas companies holding depleted oil reservoirs with appropriate characteristics for effective use of CO<sub>2</sub> for tertiary oil recovery, and negotiation with those parties for long term contracts for CO<sub>2</sub> purchases,
- Construction of compression systems and pipelines to deliver CO<sub>2</sub> to EOR locations,
- Labor to operate, maintain, and monitor the capture, compression, and transport systems, and
- Issues regarding project risk that would jeopardize ability to finance construction and to obtain PUC approval.

The interagency task force report provides an estimate of capital and operating costs for carbon capture from natural gas systems: "For a [550 MWe net output] natural gas combined cycle (NGCC) plant, the capital cost would increase by \$340 million and an energy penalty of 15 percent would result from the inclusion of CO<sub>2</sub> capture." Using the

SCHEVENUE GENERATING STATION GREENHOUSE GAS PSD PERMIT APPLICATION REVISION 1 - SEPTIMBER 2011 5-19 "Capacity Factor Method" for prorating capital costs for similar systems of different sizes as suggested by the Association for the Advancement of Cost Engineering (AACE) and other organizations, CO<sub>2</sub> capture system capital cost for the CGS is estimated as at least \$196 million. Based on an estimated CGS plant capital cost of \$300 million, the capture system alone would thus be expected to add approximately 65 percent to the overall plant capital cost.

Actual cost per megawatt would likely be higher for CGS than the reference plant in the Task Force report due to the inclusion of simple cycle units; this would require capture systems to handle a much higher temperature gas flow; little or no pilot test data is available for this situation, different materials of construction may be required, and modifications to the absorption process may be required.

Similarly, the energy penalty would be higher for simple cycle systems than for combined cycle; since scrubber and compressors are sized based on combustion turbine output, but overall unit output is lower for simple cycle, the fractional penalty would be higher. Whether plant size would remain the same with output reduced, or plant size increased to account for lost output, the energy penalty alone represents at least a 15% increase to the fuel component of the cost of electricity. At an estimated 8.9¢/kWh residential retail price for electricity, and assuming an annual average of 50% capacity factor for plant operation and 15% energy penalty, the value of lost electricity sales from the project is \$12.9 million per year.

As noted above, the effort required to identify and negotiate with oil & gas companies who may be able to utilize the  $CO_2$  would be substantial. BHC is aware that the proposed Greencore pipeline is being substantially oversized, versus what would be required for only the Belle Creek EOR operation, so it is reasonable to assume project developers are planning that there will be a future need for  $CO_2$  in the Powder River Basin or other locations in Wyoming or Montana. The location and timing of those sites, however, is not public information, and due to the patchwork of oil well ownership many parties could potentially be involved in negotiations over  $CO_2$  value.

Due to the extremely high pressures required to transport and inject CO<sub>2</sub> under supercritical conditions, the compressors required are very specialized. For example, the compressors for the Dakota Gasification Company system are of a unique eight stage design. It is unclear whether the Task Force NGCC cost estimate noted above includes the required compression systems, but if not this represents another substantial capital cost.

Pipelines must be designed to withstand the very high pressures (over 2000 pounds per square inch, gauge) and potential for corrosion if any water is introduced to the system. As noted above, if CCS were otherwise technically and economically feasible for the CGS, the most realistic scenario could be to construct a pipeline from Cheyenne to tie into the proposed Greencore pipeline. At its closest point, the Greencore pipeline would be approximately 175 miles from Cheyenne. Based on engineering analysis done by the designers of that pipeline, costs for an 8" CO<sub>2</sub> pipeline to connect the Cheyenne project to the Greencore pipeline are estimated at \$600,000 per mile, for a total cost of \$105 million. Thus the pipeline alone would represent a 35 percent increase to the project cost, and the pipeline and capture system together would double the project capital cost.

GEENHOUSE GAS PSD PERMIT APPLICATION REVISION 1 - SEPTIMBER 2011 5-20 It is unlikely that financing could be approved for a project which combines CCS in conjunction with generation, given the technical and financial risks. Also, as evidenced with utilities' inability to obtain PUC approval for integrated gasification / combined cycle (IGCC) projects due to unacceptable cost and risk to ratepayers, such as Wisconsin's disapproval of the We Energy project, it is reasonable to assume that the same issues would apply in this case before the Wyoming PUC.

Sale of the CO<sub>2</sub> for EOR could be the one positive direct economic impact of CCS. If BHC were to construct or pay for construction of the pipeline to deliver captured  $CO_2$ , it is possible that revenue from sale of the CO<sub>2</sub> could be realized. Current market pricing for CO<sub>2</sub> delivered for EOR is however proprietary and confidential, and reliable sources of information could not be identified within this scope of this BACT analysis.

In summary, capital cost for capture system and pipeline construction are estimated at \$300 million, and retail value of lost power sales due to the CCS system energy penalty is estimated at \$12.9 million per year assuming only 50% plant capacity factor. Other costs such as identification, negotiation, and engineering of EOR opportunities; operating labor and maintenance costs for capture, compression, and pipeline systems; less favorable financing terms or inability to finance; and difficulty in obtaining PSC approval would also impact the project, and it is unclear if compression systems are included in the Task Force estimate of capture system costs. A fraction of these impacts could possibly be offset through sale of the CO<sub>2</sub>, but overall addition of CCS with or without EOR opportunity would make the project unviable.

CCS is clearly not economically feasible for natural gas fired power plants at the current time. Since CCS is not considered technically or economically feasible, the proposed CGS electrical generation efficiency is determined to be the most effective GHG control technology.

From a review of the three evaluation metrics presented above, the CCS combustion turbine net heat rate for the CGS GE LM6000 PF Sprint combustion turbine, selected pursuant to the CGS business plan, was found to favorably compare with other combustion turbines and projects.

#### Step 5: Select BACT

The only remaining option is the "Electrical Generation Efficiency" option, which, therefore, is selected as BACT. This option determined to consist of the CGS project as proposed with new state-of-the-art combustion turbines. Consistent with the review criteria presented above, the CGS project evaluated combustion turbine exhibits comparable efficiency with most of the evaluated alternative combustion turbines, and superior efficiency over the Pratt & Whitney and Siemensother comparable machines. Therefore, Black Hills BHC proposes that CGS GHG BACT consist of installation of GE LM6000PF SPRINT combustion turbines from any manufacturer with a rating of nominal 40 MW. However, and the annual CO2 emissions limit for the five new combustion turbines will be based upon the BACT emission limits proposed below, which are based upon a combustion turbine from the top of the efficiency range shown. The proposed permit limit of annual total tons of CO2e and Ib/MWh would remain fixed regardless of the combustion turbine selected.

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\_The estimated total annual CO<sub>2</sub>e emissions from the combustion turbines are 936,588 tpy, and this value is proposed to be the annual CO<sub>2</sub>e permit limit for the five combustion turbines.

EPA's PSD permitting guidance for GHGs suggests use of output-based BACT emission limits and longer-term averaging periods for GHGs. Based on <u>Black Hills'BHC</u> analysis of conservative scenarios for number of turbine startups and shutdowns, partial load operation, and ambient temperature during operations, and considering the range of normalized GHG emissions noted above and eventual turbine degradation, proposed BACT permit limits are 1,100 lb/MWh for each combined-cycle combustion turbine and 1,600 lb/MWh for each simple-cycle combustion turbine on an annual average basis. If the averaging time is less than 1 year, these permit limits should be increased accordingly.

### 5.6 Small Combustion Sources BACT for GHGs

In addition to the five combustion turbines planned for the CGS project, there are several other small combustion sources associated with auxiliary equipment which will operate at the plant. The GHG calculations for these small combustion sources are located in Appendix B-1.

- (6) Natural gas-fired inlet air heaters (nominal 16-MMBtu/hr air heater with estimated emissions of 4,117 CO<sub>2</sub>e tons/year each<del>)), required for safety to prevent icing of air handling systems</del>
- (2) Natural gas-fired fuel gas heaters (nominal 4.5-MMBtu/hr gas heater with estimated emissions of 1,153 CO<sub>2</sub>e tons/year each)
- (1) Diesel-fired emergency generator (nominal 839-BHP engine with estimated emissions of 226 CO<sub>2</sub>e tons/year-each)
- (1) Diesel-fired fire <u>pumpspump</u> (nominal 327-BHP engine with estimated 51 CO<sub>2</sub>e tons/year-<u>each</u>)

The total GHG emissions from the above small combustion sources are very minor as compared to the emissions from the combustion turbines. However, for completeness, these minor GHG emission sources were evaluated in aggregate below.

#### Step 1: Identify All Control Technologies

The available control technologies for the CGS minor GHG sources are identical to those identified for the combustion turbines. These options include

- Carbon Capture and Storage Systems (CCS
- Small Combustion Source Efficiency
- Efficient Use of Energy

## Step 2: Eliminate Technically Infeasible Options Effectiveness

#### Carbon Capture and Storage Systems

As discussed above, CCS for GHG control is not considered a technically feasible control option <u>for the combustion turbines</u>. <u>Stand-alone capture systems for the small sources</u>

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would be even further from technical feasibility. Therefore, CCS is eliminated from further consideration for <del>auxiliary boilersmall combustion source</del> GHG reduction.

#### Small Combustion Source Efficiency

This<u>The</u> small combustion sources for the CGS project will incorporate a high-efficiency design.

#### Efficiency Background Information

In support of small combustion source design, additional background information is assembled in Appendix B-8 through B-14 regarding efficiency attributes of the auxiliary equipment; i.e., inlet air heater, inlet chiller units, fuel gas heaters, diesel fire pump, and diesel emergency generator.

#### Inlet Air Heater

The inlet air anti-icing heater is similar to a conventional natural gas fired watertube boiler, and is required for safety reasons to prevent icing during winter weather. However, the water does not reach the boiling point in this system and a mixture of water and glycol is used for its thermodynamic advantages over water. The unit is designed for quick load response eliminating the requirement for a stored energy system and associated efficiency losses. Combusted natural gas is used to directly heat the incoming water/glycol mixture.

Other technologies available for heating the water/glycol mixture include an indirect fired water bath heater or fire tube boiler. The fire tube boiler has similar efficiency but a much higher capital cost. The indirect fired water bath heater has a lower efficiency resulting in higher operating costs and increased emissions. With both cost and environmental operations considered, these two options are not economical for this application.

#### Fuel Gas Heater

Indirect water/glycol bath heaters were selected for heating of high-pressure natural gas. The natural gas is heated to ensure a measure of superheat before reaching the combustion turbine generator. Indirect heaters use a fire tube to transfer heat from the fired natural gas (fuel) to the water/glycol solution. The heat is then transferred from the water/glycol bath to the natural gas coil (product) in a safe manner. Although this heating technology is not as efficient as direct heating, it is considered the only acceptable option due to safety reasons as noted below.

Direct heating of natural gas would result in a slightly more efficient process; however, direct heating of natural gas is extremely dangerous and not recommended. Any small manufacturing defect, failure, or leak may result in catastrophic explosions as the product (natural gas) is exposed to an open heat source.

#### Diesel Fire Pump & Standby Generator

While preliminary review of the CGS emergency diesel equipment has been initiated, the final equipment selection has not been completed. However, the diesel equipment will be evaluated to ensure a high efficiency design.

#### Efficient Use of Energy

The small combustion sources will not be operated continuously, but only during conditions when they are needed. For example, the inlet air heaters and fuel gas heaters will be

S-CHEVENNE GENERATING STATION REVISION 1 - SEPTIMBER 2011 5-23 operated only when required for safety reasons to protect against icing of the turbines or <u>condensation within the</u> fuel lines. Therefore, energy will be utilized in an efficient manner.

#### Step 3: Rank Remaining Control Technologies by Control Effectiveness

The remaining technically feasible GHG control technologies for the CGS project are "Small Combustion Source Efficiency "and "Efficient Use of Energy." Both technologies are equally important toward minimizing GHG emissions.

#### Step 4: Evaluate most effective controls and document results

The remaining technically feasible GHG control technologies for the CGS project are "Small Combustion Source Efficiency "and "Efficient Use of Energy." Both technologies will be implemented for the CGS project.

#### Step 5: Select BACT

GHG BACT for the CGS small equipment are "Small Combustion Source Efficiency "and "Efficient Use of Energy." All auxiliary equipment will be selected with consideration for high design efficiency, and will be operated in an efficient manner. Due to the <u>estimated</u> minor CO<sub>2</sub>e emissions contribution from these small combustion sources, no <u>efficiency or</u> <u>output-based</u> GHG permit <u>limit is limit are</u> recommended for the CGS auxiliary equipment.

#### 5.7 Requested Permit Limits

The following Tables 5-7 and Table 5-8 list the recommended permit limits for the combustion turbines and auxiliary equipment respectively:

#### TABLE 5-7

CGS Combustion Turbine Recommended CO2e Permit Limits

Emission Unit	<u>Annual CO₂e Limit</u> (Pounds/MWhr)	<u>Annual CO₂e Limit</u> (Tons/Year)
Combined Cycle Combustion Turbine CT01A	<u>1,100</u>	<u>187,318</u>
Combined Cycle Combustion Turbine CT01B	<u>1,100</u>	<u>187,318</u>
Simple Cycle Combustion Turbine CT02A	<u>1.600</u>	<u>187,318</u>
Simple Cycle Combustion Turbine CT02B	<u>1,600</u>	<u>187,318</u>
Simple Cycle Combustion Turbine CT03A	<u>1,600</u>	<u>187,318</u>

TABLE 5-8

Emission Unit	<u>Annual CO<sub>2</sub>e Limit (Tons/Year)</u>	
Six (6) Inlet Air Heaters	24,703	
Two (2) Fuel Gas Heaters	<u>2,306</u>	
One (1) Diesel Fire Pump	<u>51</u>	
One (1) Diesel Standby Generator	226	

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PO Box 1400. 625 Ninth Street Rapid City, South Dakota 57709

September 23, 2011

Mr. Carl Daly Director of Air Programs EPA Region 8 1595 Wynkoop Street Denver, CO 80202-1129

RE: Black Hills Corporation - Cheyenne Generating Station Submittal of Greenhouse Gas PSD Construction Air Permit Application **Revision 1 – Sept. 2011** 

Dear Mr. Daly,

Black Hills Corporation (BHC) is submitting a revised Greenhouse Gas PSD Construction Permit Application for the Cheyenne Generating Station in the City of Cheyenne in Laramie County, Wyoming. Revisions have been made to the original application submitted on August 5, 2011 to respond to comments made during several telephone conversations and meetings between EPA and BHC staff. For your convenience, we have enclosed five (5) copies of the complete revised application including divider tabs that can be inserted in the original 3-ring binders. As we discussed in the pre-application meeting for this project held in your offices on July 8, 2011, the application for the PSD permit for the criteria pollutant emissions will be submitted to the Wyoming Department of Environmental Quality.

The Cheyenne Generating Station (CGS) will be a nominal 220 MW gross electric generating facility that includes five (5) 40 MW combustion turbines. Two of the turbines will operate in combined cycle mode and three will operate in simple cycle mode. The planned start of construction is summer 2012.

Please contact Tim Rogers, Black Hills Corporation at (605) 721-2286 or Joe Hammond, CH2M HILL at (720) 286-5919 on any questions that EPA may have during the application review. We appreciate your assistance on this important project.

Sincerely, Fred Carles

Director, Environmental Services Black Hills Corporation

C: Chris Razzazian, Deirdre Rothery; EPA Region 8 Mark Lux, Tim Rogers; BHC Chad Schlichtemeier, Wyoming DEQ



#### Signature of Responsible Official

I have reviewed this application and based on information and belief formed after reasonable inquiry, I certify that the statements and information contained in this application are true, accurate and complete.

Printed or Typed Name	Title
Mark L. Lux	Vice President and General Manager Power Delivery
Signature	Date Signed
Think	09/23/2011

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# **Acronyms and Abbreviations**

BACT	best available control technology
ВНС	Black Hills Corporation
BHP	Black Hills Power
CAA	Clean Air Act
CatOx	Catalytic Oxidation
CEM	continuous emissions monitor
CFR	Code of Federal Regulations
CGS	Cheyenne Generating Station
CH <sub>4</sub>	Methane
CLFP	Cheyenne Light, Fuel and Power Company
СО	carbon monoxide
CO <sub>2</sub>	carbon dioxide
CO <sub>2</sub> e	carbon dioxide equivalent
CTG	combustion turbine generator
°F	degrees Fahrenheit
EPA	U.S. Environmental Protection Agency
FIP	Federal Implementation Plan
FR	Federal Register
GHG	greenhouse gas
GWP	global warming potential
HFC	Hydrofluorocarbon
HHV	higher heating value
HRSG	heat recovery steam generator
IPCC	Intergovernmental Panel on Climate Change
IRP	Integrated Resource Plan
kW	Kilowatt
kWh	kilowatt-hour
LAER	Lowest Achievable Emission Rate
lb	Pound

lb/hr	pound per hour
LHV	lower heating value
MACT	maximum achievable control technology
MRR	Final Mandatory Reporting of Greenhouse Gases Rule
MMBtu	million British thermal units per hour
MW	Megawatt
$N_2O$	nitrous oxide
NAAQS	National Ambient Air Quality Standards
NO <sub>X</sub>	nitrogen oxide
NSR	New Source Review
$N_2O$	nitrous oxide
O <sub>2</sub>	Oxygen
PFC	Perfluorocarbon
$PM_{10}$	particulate matter less than 10 microns in diameter
ppm	parts per million
PTE	potential to emit
PSD	Prevention of Significant Deterioration
RACT	Reasonably Available Control Technology
RBLC	RACT/BACT/LAER Clearinghouse
SCR	Selective Catalytic Reduction
SF <sub>6</sub>	sulfur hexafluoride
SIP	State Implementation Plan
$SO_2$	sulfur dioxide
STG	steam turbine generator
tpy	tons per year
WDEQ	Wyoming Department of Environmental Quality
VOC	volatile organic compound

Black Hills Corporation (BHC) plans to construct a new nominal 220-megawatt (MW) gross simple-and combined-cycle natural gas-fired combustion turbine power plant in Laramie County, Wyoming. The project, named the Cheyenne Generating Station (CGS), will be located within the city limits of the City of Cheyenne, Wyoming, approximately 5 miles southeast of the downtown area.

Cheyenne Light, Fuel and Power Company (CLFP) is a wholly owned subsidiary of BHC. It was acquired from Xcel Energy on January 1, 2005, and provides electric utility service to Laramie County, Wyoming, including the City of Cheyenne.

Presently, electricity sold by CLFP is generated elsewhere (primarily the Gillette, Wyoming, area) and is transmitted to Cheyenne for retail delivery. There is currently no local generation capability in the Cheyenne area. The CGS will provide a local source of electricity to increase the amount of available electricity and to improve reliability of power delivery in the Cheyenne area.

The CGS project will include the following:

- Five General Electric (GE) LM6000 PF SPRINT combustion turbine generators (CTGs) fired by pipeline quality natural gas. Two of the turbines will be operated in combined-cycle mode and three will be operated in simple-cycle mode.
- One wet cooling tower for the combined-cycle steam turbine
- Three electric chiller units, each with cooling towers, for inlet air cooling for all of the CTGs
- Six natural gas inlet air heaters for inlet air heating for all of the CTGs
- Two fuel gas heaters, natural gas-fired
- One diesel emergency generator
- One diesel fire pump

In accordance with the terms of federal regulations, BHC is applying to U.S. Environmental Protection Agency (EPA) Region 8 for a permit to construct the CGS. The application is limited to requesting a permit for the emissions of greenhouse gases (GHGs) from the CGS and contains a description of the project, a review of applicable federal regulations, a listing of the emissions, and a best available control technology analysis.

The CGS will have potential emissions of 963,874 tons per year (tpy) of GHGs expressed as carbon dioxide equivalent ( $CO_2e$ ). This is comprised of 962,929 tpy of carbon dioxide ( $CO_2$ ) or CO2e of 962,929 tpy, 1.8 tpy of nitrous oxide ( $N_2O$ ) or CO2e of 564 tpy, and 18.2 tpy of methane ( $CH_4$ ) or a CO2e of 381 tpy. Because the emissions of CO<sub>2</sub>e exceed 100,000 tpy, this plant will be a major new source and will be subject to the Prevention of Significant Deterioration (PSD) rules.

Because the emission rate of GHG exceeds the 100,000-tpy limit specified in the Final Prevention of Significant Deterioration and Title V Greenhouse Gas Tailoring Rule (Tailoring Rule), a best available control technology (BACT) analysis was performed. The BACT analysis concludes that the CGS project operating at its design energy conversion efficiency is BACT for GHGs.

# section 1.0

BHC plans to construct a new nominal 220-megawatt (MW) gross simple and combinedcycle combustion turbine power plant located in Laramie County, Wyoming. The project, named the Cheyenne Generating Station (CGS), will be located in the City of Cheyenne approximately 5 miles southeast of the downtown area.

The facility will produce electrical power for CLFP, a wholly owned subsidiary of Black BHC. CLFP provides electric service to Laramie County, Wyoming, and the City of Cheyenne, with more than 38,000 customers.

Presently, electricity sold by CLFP is generated elsewhere (primarily the Gillette, Wyoming, area) and is transmitted to Cheyenne for retail delivery. There is presently no local generation capability in the Cheyenne area. The CGS will provide a local source of electricity to increase the amount of available electricity and to improve reliability of power delivery in the Cheyenne area.

The power plant will include the following:

- Five 40-MW combustion turbine generators (CTGs) fired by pipeline quality natural gas. Two of the turbines will be operated in combined-cycle mode and three will be operated in simple-cycle mode. Operating in combined-cycle will provide approximately 20-MW.
- One wet cooling tower for the combined-cycle steam turbine
- Three electric chiller units, each with cooling towers, for inlet air cooling for all of the CTGs
- Six natural gas inlet air heaters for inlet air heating for all of the CTGs
- Two fuel gas heaters, natural gas-fired
- One diesel emergency generator
- One diesel fire pump

In accordance with the terms of federal regulations, BHC is applying to U.S. Environmental Protection Agency (EPA) Region 8 for a permit to construct the CGS. The application is limited to requesting a permit for the emissions of greenhouse gases (GHGs) and contains a description of the project, a review of applicable regulations, a listing of the emissions, and a best available control technology (BACT) analysis.

Section 1.1 provides project contacts and an overview of the documentation being submitted with the application for a permit to construct the CGS.

# 1.1 Project Contacts

The following individuals may be contacted for additional information on this project:

Applicant	Tim Rogers Environmental Manager Black Hills Corporation 625 Ninth Street Rapid City, SD 57709 (605) 721-2286 <u>TRogers@bh-corp.com</u>
Permitting Consultant	Joe Hammond Principal Project Manager CH2M HILL Engineers, Inc. 9193 South Jamaica Street Englewood, CO 80112 (720) 286-5919 joe.hammond@ch2m.com

# 1.2 Document Overview

The following is an overview of the information included in this permit application.

- **Section 1.0 Introduction.** This section provides an overview of the project and describes the application organization.
- Section 2.0 Project Description. This section includes a general description of the proposed project including equipment and operations of the project. Information regarding non-emitting processes and equipment is provided for a general understanding of plant operations.
- Section 3.0 Greenhouse Gas Emissions Summary. This section provides a summary of emissions-related information.
- Section 4.0 Greenhouse Gas Regulatory Review. This section contains a detailed regulatory review of federal GHG air regulations that may impact the permitting, construction, or operation of the proposed project.
- Section 5.0 BACT Analysis. This section includes a BACT analysis for GHG pollutants. This analysis follows the EPA-prescribed five-step top-down approach. Requested permit limits are also included in this section.
- **Appendix A Location Map and Plot Plan.** This appendix includes a location map, plot plan, and general equipment arrangement drawing for the proposed project.
- **Appendix B Greenhouse Gas Supporting Documentation.** This appendix contains the calculations used to determine the GHG emissions for this permit application and additional information on the GE combustion turbines and auxiliary equipment.

# SECTION 2.0 Project Description

BHC proposes to construct and operate the CGS in Cheyenne, Wyoming. A plot plan of the facility and a map detailing the location of the proposed facility can be found in Appendix A. The facility will be a nominal 220-MW gross output power plant that will produce electrical power for the BHC-owned CLFP electric retail service territory in Laramie County, Wyoming, including the City of Cheyenne and Black Hills Power (BHP) service territory in Wyoming and South Dakota. Facility output varies with ambient temperature, with higher output at lower ambient temperatures. A general arrangement of the turbine layout and associated equipment can be found in Appendix A.

The CGS facility configuration was selected based upon the needs identified in the CLFP *Integrated Resource Plan* (IRP).<sup>1</sup> The CLFP Certificate of Public Convenience and Necessity (CPCN) was filed with the Wyoming Public Service Commission (August 1, 2011 – Docket Number 20003-112-EA11) and was based upon CLFP IRP that identified three simple-cycle combustion turbines (nominally 120 MW gross output). The CLFP CPCN further identifies the potential build-out of the site to accommodate future generation needs. BHC plans to submit a BHP CPCN in fall 2011 and will be based upon the BHP IRP that tentatively (plan has not been finalized) identifies the need for two combustion turbines configured in combined cycle mode (nominally 100 MW gross output). The BHC's Integrated Resource Plans will show the public need for increased capacity requirements in the CLFP and BHP service areas, reserve generation requirements, and generation within the service area of Cheyenne for reliability reasons. The necessary generation (wind, solar, and other renewable resources).

The proposed CGS facility will consist of five combustion turbines. Combustion turbines CT01A and CT01B will operate in a 2 X 1 combined-cycle design consisting of two 40-MW CTGs with one heat recovery steam generator (HRSG) for each CTG with no duct burners. Steam from the HRSGs will be combined to flow to a steam turbine that will produce additional electricity. The total generating capacity of the combined-cycle configuration will be approximately 100 MW. Combustion turbines CT02A, CT02B, and CT03A, will each be high-efficiency 40-MW CTGs, operating in simple-cycle mode.

Inlet air chillers with wet cooling towers will be provided for each CTG to cool the combustion air, which will enhance overall plant output during times of higher ambient temperature. Inlet air heaters will also be provided for each CTG to heat the combustion air, which will prevent icing during times of lower ambient temperature.

The proposed CGS facility will also have fuel gas pre-heaters, an emergency generator, and a fire pump.

<sup>&</sup>lt;sup>1</sup> The IRP determines the capacity expansion, which takes into consideration the size of the electrical systems' demand, and further defines the size of combustion turbines selected.

# 2.1 Power Generation

Power will be produced in the plant by a total of six generators, one for each of the five 40-MW CTGs plus one steam turbine generator (STG). All other facility operations ancillary to the primary generation function are described below.

# 2.2 Emission Sources

## 2.2.1 Combined-Cycle Combustion Turbine Generators

The CGS will use two 40-MW combustion turbines CT01A and CT01B operated in a 2 X 1 combined-cycle design with two CTGs and one steam turbine. The combustion turbines will be fired exclusively with pipeline-quality natural gas and are very similar to large aircraft jet engines in function and design. The combustion turbines will be equipped with unfired (no duct burner) HRSGs to extract heat from each combustion turbine exhaust to make steam. The steam will be used in an STG to produce more electricity. The combined-cycle configuration will consist of two CTGs, two HRSGs (one for each CTG), and one STG.

## 2.2.2 Simple-Cycle Combustion Turbine Generators

The CGS will use three 40-MW combustion turbines operated in simple-cycle mode, without heat recovery from the turbine exhaust. These combustion turbines, designated as CT02A, CT02B, and CT03A, will be fired exclusively with pipeline-quality natural gas and are very similar to large aircraft jet engines in function and design. The combustion turbines have the capability to reach full-load operation quickly after initiation of startup, thereby reducing overall startup emissions.

Each combustion turbine consists of a compressor, combustor, and expansion turbine. After filtration, air passes through the compressor before combining with the fuel and entering the low nitrogen oxide (NO<sub>X</sub>) combustor. The combustion products and compressed air pass through the expansion turbine, which drives both the compressor and the generator. Up to approximately 40 MW of gross electrical power are produced by each CTG over and above the work required by the compressor. The exhaust gas from each combustion turbine enters the Selective Catalytic Reduction (SCR) and Catalytic Oxidation (CatOx) catalysts at high temperature (approximately 850 degrees Fahrenheit [°F] at full load).

## 2.2.3 Wet Cooling Towers

## 2.2.3.1 Inlet Chiller Cooling Towers

An inlet air chilling system will be installed at the compressor inlet of each CTG, downstream of the inlet air filter. The inlet air chilling system serves to enhance the overall output of the plant by lowering the temperature of the ambient air entering the CTGs during periods of high air temperature. The cooling process takes place at the cooling coils where air is cooled before entering the compressor section of the turbine. At low temperatures, the air becomes denser and, therefore, more air flows though the CTGs. The net increase in airflow results in higher power output for each of the CTGs at high ambient temperatures. Three inlet chiller cooling towers will be used to serve the inlet chilling system at CGS.

#### 2.2.3.2 Unit 1 Cooling Tower

One wet cooling tower will be installed to provide cooling to condense the steam that is exhausted from the steam turbine on the combined cycle configuration in order to increase system efficiency. The steam condensers will have circulating cooling water flow through tubes that will absorb the heat from the condensing steam that is exhausted from the steam turbines. The warmed circulating water is then pumped to the cooling tower where it flows down through the tower and is cooled through evaporation, in a manner similar to other cooling towers. The cooled circulating water then flows back to the steam condensers to pick up more heat.

### 2.2.4 Inlet Air Heaters

An inlet air heating system will be installed at the compressor inlet of each CTG, upstream of the inlet air filter. The inlet air heating system raises the temperature of the ambient air entering the CTGs during periods of low air temperature to prevent icing for safety reasons.

## 2.2.5 Fuel Gas Heaters

A fuel gas pre-heat system will be utilized on each CTG to raise the temperature of the natural gas above the saturation temperature for safety reasons. Natural gas fired fuel gas heaters will be used on the five combustion turbines.

## 2.2.6 Diesel Fire Pump

One diesel fire pump will be used to provide fire protection water for the plant. This engine will fire only ultra-low-sulfur diesel fuel, and will operate only during testing that is anticipated to occur once per week. Total operating hours for the fire pump are 250 hours per year or less.

## 2.2.7 Emergency Generator

One diesel emergency generator will be used to provide emergency power for the plant. This engine will fire only ultra-low-sulfur diesel fuel, and will operate only during testing that is anticipated to occur once per week. Total operating hours for the emergency generator are 500 hours per year or less.

## 2.2.8 Storage Tanks

Storage tanks at the site will include diesel tanks for the fire water pump and emergency generator, aqueous ammonia storage tanks for the SCR NO<sub>x</sub> emissions control unit, and several water storage tanks. No GHG emissions will result from these tanks.

## 2.3 Non-Emitting Major Facility Components

## 2.3.1 Ancillary Facilities

Other facilities used to support power generation at the CGS will include the following:

- Water treatment system to remove solids and hardness from plant makeup water
- Wastewater treatment system to allow recycle of cooling tower blowdown and other plant wastewater

- Plant and instrument air compressors (electric-driven) and auxiliary equipment
- Plant sumps, sump pumps, and oily water separator
- Miscellaneous fire protection equipment
- Steam and water sampling systems
- Administration and warehouse/maintenance buildings

## 2.4 Emission Controls

The CGS will include the following emission controls:

- Dry low NO<sub>X</sub> burners on the CTGs, and a SCR system to reduce NO<sub>X</sub> emissions on all CTGs
- An oxidation catalyst to reduce carbon monoxide (CO) and volatile organic compound (VOC) emissions on all CTGs
- Good combustion design and operation to reduce particulate matter of 10 microns in diameter (PM<sub>10</sub>) emissions from the CTGs
- Use of pipeline-quality natural gas to minimize sulfur dioxide (SO<sub>2</sub>) emissions from the CTGs
- High-efficiency drift eliminators on the steam condenser cooling towers to reduce PM<sub>10</sub> emissions in the cooling tower drift

# 2.5 Emissions Monitoring

As required by Title 40 of the Code of Federal Regulations (CFR) Parts 60 and 75, the CGS will use continuous emissions monitors (CEMs) for NO<sub>X</sub>, CO, and oxygen (O<sub>2</sub>) for all five CTGs. These CEMs will average and record data on frequencies consistent with state and federal acid rain rules. The plant will also monitor and record the natural gas flow rate and will analyze natural gas fuel quality as required by the acid rain rules.

CGS will use these continuous emissions monitors (CEMs) to determine compliance with the CO<sub>2</sub> emission limits established in the PSD permit. CEMS will be installed and operated for each turbine according to 40CFR75 requirements. Accordingly, these CEMS will calculate CO<sub>2</sub> emissions from each source according to the 40CFR75 Appendix F and G methodologies. The calculated CO<sub>2</sub> emissions follow a strict calculation requirement to determine CO<sub>2</sub> emissions for each minute of fuel combustion typically. The minute data is converted to hourly emissions for reporting per 40CFR75 data reduction requirements. All CO<sub>2</sub> emissions are accounted for in the reported values, including startup and shutdown.

The  $CO_2$  emissions data generated from the CEMS, per 40CFR75 requirements, are used to report emissions for 40CFR98 (Mandatory Greenhouse Gas Reporting rule). Specifically, Subpart D – Electricity Generation, guide the  $CO_2$  emissions reporting requirements. Black Hill currently uses this methodology for its natural gas fired combustion turbines. The calculation methodology is defined simply as:

"(a)...continue to monitor and report  $CO_2$  mass emissions as required under §75.13 or section 2.3 of appendix G to 40 CFR part 75, and §75.64. Calculate  $CO_2$  emissions as follows: (1) Convert the cumulative annual  $CO_2$  mass emissions reported in the fourth quarter electronic data report required under §75.64 from units of short tons to metric tons. To convert tons to metric tons, divide by 1.1023."

This calculation, as required by EPA's Greenhouse Gas MMR rule simply uses the 40CFR75 fourth quarter, or end of year,  $CO_2$  emission and coverts the short tons to metric tons (Nitrous Oxide and Methane emissions are calculated from Green House Gas emission factors). Additionally, the  $CO_2$  data will follow quality assurance/control requirements as well as missing data substitution routines according to 40CFR75 rules. Therefore, since EPA's long standing Acid Rain Program regulations (40CFR75) and the recently released Greenhouse Gas MMR rule (40CFR98) both recognize the 40CFR75 methodology as an accurate and complete method to monitor  $CO_2$  emissions, the CGS will use the methodology to determine compliance with  $CO_2$  emission limits identified in this permit.

In a recent permit application with the Bay Area Air Quality Management District (BAAQMD) for the Russell Energy Center in California, the agency made the following determination regarding CEMS versus the Fuel Meter (heat input ) method:

"The Air District has also considered whether to require the facility to use a Continuous Emissions Monitor (CEM) to measure greenhouse gas emissions directly (as CO<sub>2</sub>), but has concluded that calculating emissions from heat input is preferable. Unlike some other pollutants such as NO<sub>x</sub> or carbon monoxide whose formation is heavily dependent on conditions of combustion and/or performance of add-on emissions controls, greenhouse gases are a direct and unavoidable byproduct of the combustion process. The amount of carbon within the fuel will all ultimately be emitted as greenhouse gases in a manner that is easily determined using well-established emissions factors. One can therefore determine with great accuracy what greenhouse gases are being emitted by measuring the amount of hydrocarbon fuel being burned (measured as heat input). For this reason, the test methods for measuring heat rate and capacity can achieve an accuracy of ±1.5% <sup>55</sup>, which is better than the relative accuracy of CEMs which typically ranges as high as ±10%.<sup>56</sup> The Air District is therefore proposing to require surrogate monitoring for greenhouse gas emissions using heat rate instead of a CEM."

<sup>55</sup> American Society of Mechanical Engineers (ASME), Performance Test Code on Overall Plant Performance, (PTC 46-1996), December 15, 1997, Table 1.1, "Largest Expected Test Uncertainties", at p. 4 (providing 1.5% variance in the corrected heat rate for "combined gas turbine and steam turbine cycles with or without supplemental firing to steam generator"). <sup>56</sup> See, e.g., 40 C.F.R. Part 75, Appendix A, § 3.3.3 ("The relative accuracy for CO<sub>2</sub> and O<sub>2</sub> monitors shall not exceed 10.0 percent.")

# 2.6 Operating Schedule

The annual operating schedule of the CGS will be dependent on the demand for electric power. Thus, the exact operating schedule cannot be accurately predicted at this time.

For this reason, the permit limits requested in this application, and the resulting assumptions used in the emissions inventory and BACT analysis, are as follows:

- Up to 8,760 hours per turbine per year of CTG operation (both simple and combined cycle) at 100 percent load or at any lesser load rate
- Up to 600 startups for each simple-cycle combustion turbine per year
- Up to 600 startups for each combined-cycle combustion turbine per year
- Up to 5,330 hours per tower per year of inlet chiller cooling tower operation
- Up to 8,760 hours per year of combined-cycle cooling tower operation
- Up to 4,380 hours of operation per year for each inlet air heater
- Up to 4,380 hours of operation per year for each fuel gas heater

These hours could be based on continuous short-term or long-term operation. In other words, the plant could operate up to 8,760 hours per year (counting startup episodes) and could operate 24 hours per day, 7 days per week, and 365 days per year.

# 2.7 Permitting and Construction Schedule

The planned permitting and construction timeline is shown in Table 2-1.

#### TABLE 2-1

Permitting and Construction Schedule

Event	Date
GHG PSD Permit Application Filed with EPA	August 2011
Revised GHG PSD Permit Application Filed with EPA	September 2011
PSD Air Permit Application Filed with WDEQ	October 2011
Air Permits Issued by EPA and WDEQ	September 2012
Begin Purchase Major Pieces of Equipment	September 2012
Start of Construction	April 2013
Commercial Operation	June 2014

# GHG Emissions Summary

GHG emission estimates were prepared for all point emissions sources from the CGS, including the combustion turbines and auxiliary equipment. The annual carbon dioxide (CO<sub>2</sub>) equivalent (CO<sub>2</sub>e) emissions were estimated based on 100 percent capacity factor (full-load operation for 8,760 hours per year) for each of the combustion turbines. Note that instantaneous fuel flow is always lower during turbine startup than normal turbine operations; therefore, unlike for criteria air pollutants, instantaneous GHG emissions are always lower during startup than normal operations, and 8760 hours per year at full load is a conservative assumption for calculating GHG emissions. More detailed emission calculations are provided in Appendix B.

# 3.1 Combustion Turbines

The CGS project consists of two GE LM6000PF SPRINT combustion turbines operating in a 2 X 1 combined-cycle configuration, designated as CT01A and CT01B. There will also be three GE LM6000PF SPRINT combustion turbines operating in simple cycle identified as CT02A, CT02B, and CT03A. All five combustion turbines will have separate stacks, which will be a separate emission points.

# 3.2 Auxiliary Equipment

In addition to the five GE LM6000PF SPRINT combustion turbines planned for the CGS project, there are several other small GHG combustion sources associated with auxiliary equipment that will operate at the CGS:

- (6) Natural gas-fired inlet air heaters (nominal 16-million-British-thermal-units-per hour [MMBtu/hr] air heater with estimated emissions of 4,117 CO<sub>2</sub>e tons/year each)
- (2) Natural gas-fired fuel gas heaters (nominal 4.5-MMBtu/hr gas heater with estimated emissions of 1,153 CO<sub>2</sub>e tons/year each)
- (1) Diesel-fired emergency generator (nominal 839-BHP engine with estimated emissions of 226 CO<sub>2</sub>e tons/year)
- (1) Diesel-fired fire pumps (nominal 327-BHP engine with estimated 51 CO<sub>2</sub>e tons/year)

# 3.3 GHG Emission Summary

The GHG emission sources for the project are shown in Table 3-1, along with estimated annual  $CO_2e$  emissions.

TABLE 3-1GHG Emission Source Summary

Source Number	Emission Point	Estimated Annual CO <sub>2</sub> e Emissions
EP01 and EP02	(2) GE LM6000PF SPRINT Combined-Cycle Combustion Turbines CT01A and CT01B	374,635
EP03, EP04, and EP05	(3) GE LM6000 PF SPRINT Simple-Cycle Combustion TurbinesCT02A, CT02B, and CT03A	561,953
EP06 through EP11	Six (6) Inlet Air Heaters	24,703
EP18 and EP19	Two (2) Fuel Gas Heaters	2,306
EP16	One (1) Diesel Fire Pump	51
EP15	One (1) Diesel Standby Generator	226

# Regulatory Review

This section provides a regulatory review of the applicability of federal air quality permitting requirements for GHGs and GHG air pollution control regulations for the CGS project proposed by BHC. The purpose of this section is to provide appropriate explanation and rationale regarding the applicability of these regulations to the CGS project. The review is limited to federal regulations for GHG because there are no State of Wyoming regulations for GHG that apply to the permitting of CGS.

Because the Wyoming Department of Environmental Quality (WDEQ) has a SIP-approved PSD program for all criteria pollutants but has not adopted regulations under the Tailoring Rule, WDEQ is the permitting authority for the CGS non-GHG pollutants (other regulated NSR pollutants), while EPA Region 8 is the permitting authority for the CGS GHG pollutants. Both agencies have agreed to work together to process these two air permits for CGS.

# 4.1 Federal Regulations

The proposed project was evaluated to determine compliance with applicable federal GHG air quality regulations. Potentially applicable federal GHG regulations include the following:

- Final Prevention of Significant Deterioration and Title V Greenhouse Gas Tailoring Rule (Tailoring Rule) 40 CFR 51.166, 52.21, as published in the *Federal Register* (FR) June 3, 2010 (75 FR 31514)
- Federal Implementation Plan (FIP) for State of Wyoming GHG 40 CFR 52.37, as published in the *Federal Register* December 30, 2010 (75 FR 82246)
- New Source Review (NSR) 40 CFR 51 and 52

On April 2, 2007, the U.S. Supreme Court found that GHGs are air pollutants under Clean Air Act (CAA) section 302(g) (*Massachusetts* v. *EPA*, 549 U.S. 497 [2007]). GHG includes the six gases of CO<sub>2</sub>, nitrous oxide (N<sub>2</sub>O), methane (CH<sub>4</sub>), hydrofluorocarbons (HFCs), perfluorocarbons (PFCs), and sulfur hexafluoride (SF<sub>6</sub>). Of these, the first three will be emitted from the CGS. These gases have different potential to affect global warming, termed the global warming potential (GWP). The GWP of the three emitted gases are CO<sub>2</sub> (1), N<sub>2</sub>O (310), and CH<sub>4</sub> (21).

Based on the series of legal and regulatory actions that culminated in the Tailoring Rule, regulation of major increases of GHG emissions through the Prevention of Significant Deterioration (PSD) permit program was required. EPA recognized that the major source threshold levels for the criteria pollutants for PSD pollutants of 100 or 250 tons per year (tpy) would make virtually every new project a major source. Accordingly, in June, 2010, EPA adopted the Tailoring Rule to raise the major source thresholds for GHG to 75,000 or 100,000 tons of GHG per year.

The State of Wyoming has an approved State Implementation Plan (SIP) based program for the criteria pollutants for the PSD permitting of new major sources. However, Wyoming has decided to not include GHG in the state PSD permitting program. Accordingly, the GHG PSD program is being implemented by the EPA for major sources of GHG within the State of Wyoming through the federally approved FIP.

## 4.1.1 Greenhouse Gas Tailoring Rule

On June 3, 2010, EPA issued the final Tailoring Rule (75 FR 31514), which allowed the phasing in of the PSD permitting process for new major sources of GHGs such as the CGS project. Step 2 of the Tailoring Rule requires that beginning July 1, 2011, all new sources with the potential to emit (PTE) greater than 100,000 tpy of CO<sub>2</sub>e (including the statutory threshold of 100 or 250 tons on a mass basis) comply with PSD and Title V requirements. All references to "tons" are provided in terms of short tons (2,000 pounds/ton) instead of metric tonnes, in accordance with EPA GHG PSD permitting guidance.

As shown in Table 4-1, under the Tailoring Rule, the CGS will be a major source subject to PSD permitting because the total emissions of CO<sub>2</sub>e exceed 100,000 tpy. The CGS project will result in an increase in CO<sub>2</sub>e emissions of 963,874 tpy, and more than 100 tpy of certain criteria pollutants. Therefore, the project is classified as a major source for PSD applicability determination.

#### TABLE 4-1

GHG Pollutants Expected to be Emitted, Annual Emission Rates, Global Warming Potential, and Annual Emissions Rates Adjusted for Global Warming Potential

Pollutant	Proposed Facility GHG Emissions (TPY)	Global Warming Potential (GWP)	GHG Emissions Adjusted for GWP (TPY)
Carbon Dioxide (CO <sub>2</sub> )	962,929	1	962,929
Nitrous Oxide (N <sub>2</sub> O)	1.82	310	564
Methane (CH <sub>4</sub> )	18.17	21	381
Total GHG as CO <sub>2</sub> e			963,874

## 4.1.2 Federal Implementation Plan for Wyoming

EPA has determined that the Wyoming SIP is deficient for purposes of the PSD permitting of GHG. Accordingly, EPA adopted a FIP in which it retains the authority to issue a PSD permit for GHG. Thus, this application is being filed with EPA Region 8 for the sole purpose of obtaining a PSD permit for the emissions of GHG from the CGS. The permit for the emissions of the criteria and hazardous pollutants from CGS will be obtained from the State of Wyoming.

EPA has not adopted ambient air quality standards or new source performance standards for GHG. Accordingly, this application only contains a BACT analysis for GHG.

#### 4.1.3 New Source Review

PSD is the portion of NSR that applies to pollutants that are in attainment of National Ambient Air Quality Standards (NAAQS). Because there are no ambient air quality standards for GHG, all portions of the United States are in attainment for GHG. Major new or modified air emission sources locating in Laramie County are, therefore, potentially subject to PSD review for these GHG pollutants.

The first step in PSD review is determining whether the proposed facility is a major PSD source. As noted above, the CGS will be a major source. Therefore, CGS is subject to PSD review for GHG. The primary elements of PSD requirements is application of BACT to emissions of GHG

# 5.1 Background

As described above, BHC plans to build a natural gas-fired combustion turbine generating facility in the southeast section of the City of Cheyenne in Laramie County, Wyoming, pursuant to its approved CLFP *Integrated Resource Plan* filed before the Wyoming Public Service Commission (described in Section 2.0, Project Description). The proposed site is immediately west of the Dry Creek Water Reclamation Facility, which is located approximately 5 miles southeast of the downtown area.

The CGS will consist of a total of five natural gas-fired CTGs sized at approximately 40-MW capacity each. Two CTGs will be configured for combined-cycle operation and will each be equipped with dry-low NO<sub>x</sub> combustors and a HRSG without duct burners, with steam flowing from the two HRSGs to one condensing STG with condenser in a "2x1" configuration. The combined-cycle generation capacity is nominally 100 MW. All of the CTGs will be equipped with SCR for NO<sub>x</sub> control and Catalytic Oxidation for CO and VOC control. Three CTGs will operate in simple cycle. CGS auxiliary equipment includes one mechanical draft condenser wet cooling tower, three electric inlet air chiller units with mechanical draft cooling towers, six natural gas-fired inlet air heaters, two natural gas-fired fuel heaters, one diesel-fired fire pump, and one diesel-fired emergency generator.

## 5.1.1 CGS Business Plan and Combustion Turbine Selection

The CLFP CPCN and associated IRP (Docket Number 20003-112-EA11), were filed August 1, 2011, with the Wyoming Public Service Commission, and present the business plan in detail. The BHP CPCN and associated IRP will be submitted to the Commission in fall 2011. Generally, BHC's CPCN and associated IRP show the public need for increased capacity requirements, reserve generation requirements, and generation within the service area of Cheyenne for reliability reasons. The necessary generation will be primarily peaking for CLFP, with baseload capabilities for BHP, and will further enable renewable generation (wind, solar, and other renewable resources). BHC identified natural gas simple/combined-cycle gas turbines to be the best-suited generation source to meet this CGS business plan-

BHC has selected the General Electric LM 6000PF SPRINT combustion turbine for the CGS project. Table 5-1 lists comparable combustion turbine manufacturers and a comparison of estimated performance efficiency at the CGS site conditions. This information was compiled from published data from Gas Turbine World magazine, and is presented only for comparative purposes. Gross heat rate and efficiencies are based on power output at the combustion turbine generator terminals, and does not include consideration of parasitic unit auxiliary loads.

#### TABLE 5-1

Combustion Turbine Comparison

Turbine <sup>1</sup>	Production (kW)	Gross Heat Rate (Btu/kWh) HHV	Efficiency <sup>2</sup>			
Dresser-Rand						
DR-63G PC	35,150	9,095	37.5%			
GE Energy Aeroderivative						
LM6000PC	39,253	9,487	36.0%			
LM6000PC Sprint	40,605	9,419	36.2%			
LM6000PD	34,612	9,103	37.5%			
LM6000PD Sprint	38,079	9,091	37.5%			
LM6000PF	34,612	9,103	37.5%			
LM6000PF Sprint	38,649	9,079	37.6%			
LM6000PG	42,995	9,556	35.7%			
GE Energy Oil & Gas						
LM6000PD	33,964	9,283	36.8%			
IHI Power Systems		·				
LM6000PC	34,306	9,198	37.1%			
LM6000PC Sprint	37,129	9,228	37.0%			
LM6000PD	33,800	9,231	37.0%			
LM6000PD Sprint	37,236	9,213	37.0%			
LM6000PG	40,084	9,157	37.3%			
Pratt & Whitney Power Systems						
FT8 TwinPac	41,267	9,898	34.5%			
SwiftPac 50 DLN	41,175	9,914	34.4%			
Rolls-Royce						
Trent 60 DLE	41,537	9,064	37.7%			
Trent 60 DLE ISI	46,612	8,913	38.3%			
Siemens Energy						
SGT-800	37,772	10,126	33.7%			
SGT-900	39,781	11,626	29.4%			

<sup>1</sup> Specifications for production output at 59°F, 5,950-Foot Altitude, Gross Output, HHV.

<sup>2</sup> Calculation: Efficiency= 3,413 Btu/kWh/Gross Heat Rate

BHC selected the GE LM6000PF SPRINT combustion turbine because it best meets its business plan, its system, and operational criteria. Business plan considerations for turbine selection include combustion efficiency, exhaust characteristics that impact combined cycle system efficiency, size range, and consistency with other locations. Selection of a "fleet" of like turbines for different locations provides advantages with knowledge of maintenance and operations, stocking of spare parts, and ability to "swap" turbines between locations. The combustion turbine calculated efficiency for this turbine (37.6%) compares favorably with other combustion turbines listed in Table 5.1.

Table 5-2 below lists the GE LM6000PF SPRINT combustion turbine attributes to be used within the GHG BACT analysis, and represents high-efficiency operation in both simpleand combined-cycle operation. The information included in Table 5-2 is based upon GE provided information, and summarizes the estimated combustion turbine performance at site conditions including consideration for parasitic auxiliary loads. Therefore, since Table 5-1 does not consider unit auxiliary loads in the efficiency calculation, and Table 5-2 includes allowance for auxiliary loads, the values are slightly different between the two tables.

Combustion Turbine Criteria	Value <sup>1</sup>
Simple-Cycle Combustion Turbine Gross Output (MW)	37.1
2x1 Combined-Cycle Combustion Gross Turbine Output (MW)	97.4
Simple-Cycle Gross Heat Rate (Btu/KWh) HHV	9,263
Combined-Cycle Gross Heat Rate (Btu/KWh) HHV	7,062
Heat Input (Btu/hr) HHV	366

TABLE 5-2

GE LM6000PF	SPRINT	Combustion	Turbine	Attributes

<sup>1</sup> 60<sup>0</sup> F at site elevation.

# 5.2 Regulatory Basis

GHGs have become subject to emission permitting through PSD and Title V programs. On June 3, 2010, EPA issued the final Tailoring Rule (75 FR 31514), which allowed phasing in the PSD permitting process for new sources of GHGs such as the CGS project. Step 2 of the Tailoring Rule requires that beginning July 1, 2011, all new sources with PTE greater than 100,000 tpy of GHGs on a CO<sub>2</sub>e basis, and with a GHG PTE of 100 or 250 tpy, depending on source type, on a mass basis will become subject to PSD and Title V requirements. All references to tons within the table and in this BACT analysis are provided in terms of short tons (2,000 pounds/ton) instead of metric tonnes, in accordance with EPA GHG PSD permitting guidance.

The CGS project will be a new source with a GHG PTE of greater than 100,000 tpy CO<sub>2</sub>e and greater than the 100-tpy mass basis for listed sources, and will also have a PTE of greater than 100 tpy for certain criteria pollutants. Because the Wyoming Department of Environmental Quality (WDEQ) has a SIP-approved PSD program for all criteria pollutants but has not adopted regulations under the Tailoring Rule, WDEQ is the permitting authority for the CGS non-GHG pollutants (other regulated NSR pollutants), while EPA Region 8 is

the permitting authority for the CGS GHG pollutants. Therefore, this GHG BACT analysis was prepared for presentation to EPA Region 8 as part of the CGS permit application process.

## 5.3 Emissions Summary

Per EPA Tailoring Rule definitions, GHGs consist of the following gases:

- Carbon Dioxide (CO<sub>2</sub>)
- Methane (CH<sub>4</sub>)
- Nitrous oxide (N<sub>2</sub>O)
- Hydrofluorocarbons (HFCs)
- Perfluorocarbons (PFCs)
- Sulfur hexafluoride (SF<sub>6</sub>)

To determine CO<sub>2</sub>e emissions, mass flows of each individual gas are multiplied by the appropriate GWP as referenced to the Intergovernmental Panel on Climate Change (IPCC) Second Assessment Report, and the results are summed.

The combustion turbines, inlet air heaters, and fuel gas heaters will be fired with pipelinequality natural gas, and complete combustion will result primarily in water and  $CO_2$ byproducts. However, incomplete combustion will result in some unburned natural gas or  $CH_4$  emissions. Additionally, due to the presence of nitrogen in the combustion air, some small quantities of N<sub>2</sub>O will also be emitted. The standby generator and fire pump engines will be fired with diesel fuel, again resulting in  $CO_2$  emissions from oxidation of the fuel and with minor quantities of  $CH_4$  emissions resulting from incomplete combustion and N<sub>2</sub>O emissions from conversion of nitrogen from the atmosphere and fuel.

Table 5-3 represents potential sources and estimated quantities of GHG emissions from CGS project equipment.

TABLE 5-3

CGS Estimated GHG Emissions by Equipm
---------------------------------------

Equipment	Description	Total CO <sub>2</sub> e Emissions (t/yr)	
Two (2) Combustion Turbines in Combined-Cycle Operation with no HRSG Duct Burner	Maximum Heat Input Each 366 MMBtu/hr Higher Heating Value (HHV)	374,635	
Three (3) Simple-Cycle Combustion Turbines	Maximum Heat Input Each 366 MMBtu/hr Higher Heating Value (HHV)	561,953	
Two (2) Fuel Gas Heaters	Maximum Heat Input 4.5 MMBtu/hr each	2,306	
One (1) Diesel Fire Pump	Maximum Heat Input 2.5 MMBtu/hr	51	
One (1) Diesel Standby Generator	Maximum Heat Input 5.52 MMBtu/hr	226	
Six (6) Inlet Air Heaters	Maximum Heat Input 16.07 MMBtu/hr each	24,703	
Total		963,874	

## 5.3.1 GHG BACT Analysis Assumptions

During the completion of GHG BACT analysis, the following assumptions were made:

- 1. Table 5-3 above presents estimated CGS GHG emissions in terms of CO<sub>2</sub>e emissions, and only includes emissions of CO<sub>2</sub>, CH<sub>4</sub>, and N<sub>2</sub>O. The CGS is not expected to emit HFCs or PFCs because these man-made gases are primarily used as cooling, cleaning, or propellant agents. SF<sub>6</sub> is also a man-made gas that may be used as an insulating gas for high-voltage equipment and circuit breakers; however, BHC does not plan to install electrical equipment containing SF<sub>6</sub> at the CGS. Therefore, only CO<sub>2</sub>, CH<sub>4</sub>, and N<sub>2</sub>O will be included in CO<sub>2</sub>e totals.
- From the GHG emissions inventory presented in Appendix B-1, the relative quantities of CH<sub>4</sub> and N<sub>2</sub>O total only approximately 945 tpy of CO<sub>2</sub>e emissions, or less than 0.1 percent of total CO<sub>2</sub>e emissions. Due to the extremely small contribution of CH<sub>4</sub> and N<sub>2</sub>O emissions to the total, the CGS GHG BACT analysis only includes the five-step process for CO<sub>2</sub> emissions.
- 3. Completion of the BACT analysis for criteria pollutants will result in the installation of an SCR system for NO<sub>x</sub> emissions reduction, and an oxidation catalyst for control of CO and VOCs for each turbine.
- 4. During actual combustion turbine operation, the oxidation catalyst may result in minimal increases in CO<sub>2</sub> from the oxidation of any CO and CH<sub>4</sub> in the flue gas. However, the EPA Final Mandatory Reporting of Greenhouse Gases Rule (Mandatory Reporting Rule or MRR) (40 CFR 98) factors for estimating CO<sub>2</sub>e emissions from the combustion of natural gas assume complete combustion of the fuel. While the oxidation catalyst has the potential of incrementally increasing CO<sub>2</sub> emissions, these emissions are already accounted for in the MRR factors and included in the CO<sub>2</sub>e totals.
- 5. Similarly, the SCR catalyst may result in an increase in N<sub>2</sub>O emissions. Although quantifying the increase is difficult, it is generally estimated to be very small or negligible. From the GHG emissions inventory, the estimated N<sub>2</sub>O emissions from all combustion turbines total only 1.5 tpy. Therefore, even if there were an order-of-magnitude increase in N<sub>2</sub>O as a result of the SCR, the impact to CO<sub>2</sub>e emissions would be insignificant.

Use of the SCR and oxidation catalyst slightly decreases the project thermal efficiency due to backpressure on the turbines (these impacts are already included in the emission inventory) and, as noted above, may create a marginal but unquantifiable increase to N<sub>2</sub>O emissions. While elimination of the NO<sub>x</sub> and CO/VOC controls could conceivably be considered as an option within the GHG BACT, the environmental benefits of the NO<sub>x</sub>, CO, and VOC control are assumed to outweigh the marginal increase to GHG emissions. Thus, even if carried forward through the GHG BACT analysis, they would be eliminated in Step 4 due to other environmental impacts. Therefore, we have not considered omission of these controls within the BACT analysis.

# 5.4 Top-Down BACT Process

The EPA has developed a recommended process for conducting BACT analyses, referred to as the "top-down" method. The following steps to conducting a top-down analysis are listed in the EPA's *New Source Review Workshop Manual* (EPA, 1990):

- Step 1: Identify all control technologies
- Step 2: Eliminate technically infeasible options
- Step 3: Rank remaining control technologies by control effectiveness
- Step 4: Evaluate most effective controls and document results
- Step 5: Select BACT

Each of these steps, described in the following sections, has been conducted for GHG emissions for the CGS project. The following top-down BACT analysis for CO<sub>2</sub>e has been prepared in accordance with the EPA's *New Source Review Workshop Manual* (EPA, 1990). A top-down BACT analysis takes into account energy, environmental, economic, and other costs associated with each alternative technology.

# 5.5 Combustion Turbine BACT for GHGs

## Step 1: Identify All Control Technologies

The combustion turbines will be GE LM6000PF SPRINT combustion turbines that utilize the latest emissions control technology. There are two basic alternatives identified to limit the GHG emissions of this project. These options include

- Carbon Capture and Storage (CCS)
- Electrical Generation Efficiency

BHC's CGS Business Plan and IRP have determined that the proposed mix of natural gas combined-cycle and simple-cycle power generation is the only alternative that meets all of the CGS requirements for economic and reliable power 24 hours per day and in all weather conditions. As such, other generation technologies such as coal, wind, and solar were not evaluated in this BACT analysis. This is consistent with EPA's March 2011 *PSD and Title V Permitting Guidance for Greenhouse Gases,* which states, "EPA has recognized that a Step 1 list of options need not necessarily include inherently lower polluting processes that would fundamentally redefine the nature of the source proposed by the permit applicant…", and "…the permitting authority should keep in mind that BACT, in most cases, should not regulate the applicant's purpose or objective for the proposed facility…" (p. 26) Nonetheless, it should be noted that the CGS is intended to provide supplemental and backup generation for solar and wind projects, and renewable generation is not an adequate supplement and backup for other renewable generation; a fuel-based alternative is required.

The only identified GHG emission "control" options are post-combustion CCS and energy efficiency of the proposed generation facility.

## Step 2: Eliminate Technically Infeasible Options Effectiveness

### Carbon Capture and Storage Systems

CCS systems involve use of adsorption or absorption processes to remove  $CO_2$  from flue gas, with subsequent desorption to produce a concentrated  $CO_2$  stream. The concentrated  $CO_2$  is then compressed to "supercritical" temperature and pressure, a state in which  $CO_2$ exists neither as a liquid nor a gas, but instead has physical properties of both liquids and gases. The supercritical  $CO_2$  would then be transported to an appropriate location for underground injection into a suitable geological storage reservoir, such as a deep saline aquifer or depleted coal seam, or used in crude oil production for enhanced oil recovery.

While many believe that CCS will allow the future use of fossil fuels while minimizing GHG emissions, there are a number of technical barriers concerning the use of this technology for the CGS:

- No full scale systems are currently in operation for capture of CO<sub>2</sub> from dilute exhaust steams such as that from natural gas fired electrical generation systems,
- Lack of pilot scale experience with capture systems for high-temperature streams such as simple cycle combustion turbine exhaust currently exists,
- Use of captured CO<sub>2</sub> for enhanced oil recovery (EOR) is widely believed to represent the practical first opportunity for CCS deployment; however identification of suitable oil reservoirs with willing and able owners and operators is beyond the capability for most electric utilities. Owners of oil fields generally closely guard information regarding production volumes and reservoir status,
- Little experience exists with other types of storage systems such as deep saline aquifers or depleted coal seams,
- Because of the developmental nature of CCS technology, vendors and contractors do not offer turn-key offerings; separate contracting would be required for capture system design and construction; compression and pipeline system routing, siting and licensing, engineering and construction; and geologic storage system design, deployment, operations, and monitoring,
- Significant legal uncertainties still exist regarding relationship between land surface ownership rights and subsurface (pore space) ownership, potential conflicts with other uses of land such as exploitation of mineral rights, management of risks and liabilities, etc, and
- Potential for frequent startup and shutdown of generation units at the CGS make CCS impractical for two reasons inability of capture systems to startup in the same short time frame as combustion turbines, and infeasibility for potential users of the CO<sub>2</sub> such as EOR systems to use uncertain and intermittent flows. The simple cycle units at the CGS are designed for peaking operation and as such the ability to rapidly startup the units and to operate them for short durations is critical. While the combined cycle units are being designed for baseload operation, under many operational scenarios rapid response may also be needed for these units.

These issues are discussed in more detail below.

As suggested in the 1990 Draft EPA New Source Review Workshop Manual, control technologies should be demonstrated in practice on full scale operations in order to be considered available within a BACT analysis. "Technologies which have not yet been applied to (or permitted for) full scale operations need not be considered available; an applicant should be able to purchase or construct a process or control device that has already been demonstrated in practice." As will be discussed in more detail below, carbon capture technology has not been demonstrated in practice in power plant applications. Other process industries do have carbon capture systems that are demonstrated in practice, but the technology used for these processes cannot be applied to power plants.

Three fundamental types of carbon capture systems are employed throughout different process and energy industries: sorbent adsorption, physical absorption, and chemical absorption. Use of carbon capture systems on power plant exhaust is inherently different from other commercial scale systems currently in operation, due in large part to concentration of  $CO_2$  and other constituents in the gas streams.

For example,  $CO_2$  is separated from petroleum refinery hydrogen plants in a number of locations, but this is typically accomplished on the product gas from a steam methane reforming process which contains primarily hydrogen (H<sub>2</sub>), unreacted methane (CH<sub>4</sub>) and  $CO_2$ . Based on the stoichiometry of the reforming process the  $CO_2$  concentration is approximately 80 percent by weight, and the gas pressure is approximately 350 pounds per square inch, gauge (psig). Because of the high concentration and high pressure a pressure swing adsorption (PSA) process is used for the separation. In the PSA process, all non-H<sub>2</sub> components including  $CO_2$  and  $CH_4$  are adsorbed onto the solid media under high pressure. After the sorbent becomes saturated the pressure is reduced to near atmospheric conditions to desorb these components. The  $CO_2/CH_4$  mixture in the PSA tail gas is then typically recycled to the reformer process boilers to recover the heating value; but where the CO<sub>2</sub> is to be sold offset an additional amine absorption process would be required to separate the CO<sub>2</sub> from CH<sub>4</sub>. In its May 2011 "DOE/NETL Advanced Carbon Dioxide Capture R&D Program: Technology Update", NETL notes the different applications for chemical solvent absorption, physical solvent absorption, and sorbent adsorption processes. From Section 4.B, "When the fluid component has a high concentration in the feed stream (e.g., 10 percent or more), a pressure swing adsorption (PSA) mechanism is more appropriate."

In another example, at the Dakota Gasification Company's Great Plains Synfuels Plant (GPSP) in North Dakota, CO<sub>2</sub> is separated from intermediate fuel streams produced from gasification of coal. The gas from which the CO<sub>2</sub> is separated is a mixture of primarily hydrogen (H<sub>2</sub>), methane (CH<sub>4</sub>), and 30 to 35 percent CO<sub>2</sub> and a physical absorption process (Rectisol) is used. In contrast, as shown in the GE Guarantee in Appendix B-3, and as noted on Page 29 of the August 2010 *Report of the Interagency Task Force on Carbon Capture and Storage*, CO<sub>2</sub> concentrations for natural-gas fired systems are in the range of 3 to 5 percent. This adds significant technical challenges to separation of CO<sub>2</sub> from power plant exhaust as compared to other systems.

In Section 4.A of the above-referenced Technology Update, NETL notes this difference between pre-combustion CO<sub>2</sub> capture such as that from the GPSP versus the postcombustion capture such as that required from a natural-gas fired power plant, "Physical solvents are well suited for pre-combustion capture of CO<sub>2</sub> from syngas at elevated
pressures; whereas, chemical solvents are more attractive for CO<sub>2</sub> capture from dilute lowpressure post-combustion flue gas."

The Interagency Task Force on Carbon Capture and Storage consists of 14 executive departments and federal agencies, co-chaired by the DOE and EPA. In the 2010 report noted above, the task force discusses four currently operating post-combustion  $CO_2$  capture systems associated with power production. All four are on coal-based power plants where  $CO_2$  concentrations are higher (typically 12 to 15 percent), with none noted for natural gas-based power plants (typically 3 to 5 percent).

The Department of Energy's (DOE) National Energy Technology Laboratory (NETL) is a key player in the nation's efforts to realize commercial deployment of CCS technology. A downloadable database of worldwide CCS projects is available on the NETL website (http://www.netl.doe.gov/technologies/carbon\_seq/global/database/index.html). Filtering this database for projects that involve both capture and storage, which are based on post-combustion capture technology (the only technology applicable to natural gas turbine systems), which are shown as "active" with "injection ongoing" or "plant in operation", yields four projects. Three projects, one of which is a pilot-scale process noted in the Interagency Task Force report as described above, are listed at a capacity of 274 tons per day (100,000 tons per year) and the fourth has a capacity of only 50 tons per day. Post-combustion CCS has not been accomplished on a scale of even the modestly-sized CGS facility, which could produce up to 964,000 tons per year or 2,600 tons per day. Furthermore, scale-up involving a 10x increase in size from pilot scale to commercial scale is unusual in chemical processes and would represent significant technical risk.

As detailed in the August 2010 report, one goal of the Task Force is to bring five to 10 commercial demonstration projects online by 2016. With demonstration projects still years away, clearly the technology is not currently commercially available. It is notable that several projects, including those with DOE funding or loan guarantees, have been cancelled in recent months, making it further unlikely that technical information required to scale up these processes can be accomplished in the near future. For example, at the AEP Mountaineer site noted above, the commercial scale project was to expand capture capacity to 100,000 tpy, but to date only the "Project Validation Facility" was completed and only accomplished capture of a total of 50,000 metric tons and storage of 37,000 metric tons of CO<sub>2</sub>. AEP recently announced that the larger project will be cancelled after completion of the front end engineering design due to uncertain economic and policy conditions.

The Interagency Task Force report notes the lack of demonstration in practice: "Current technologies could be used to capture CO<sub>2</sub> from new and existing fossil energy power plants; however, they are not ready for widespread implementation primarily because they have not been demonstrated at the scale necessary to establish confidence for power plant application. Since the CO<sub>2</sub> capture capacities used in current industrial processes are generally much smaller than the capacity required for the purposes of GHG emissions mitigation at a typical power plant, there is considerable uncertainty associated with capacities at volumes necessary for commercial deployment."

One of the many technical challenges with carbon capture systems is the temperature of the exhaust steams. For coal-based plants, where most of the post-combustion capture technology research has been accomplished, typical exhaust temperatures are in the range of

300 degrees F. For the three simple cycle systems planned for the CGS, exhaust temperature will be up to 900 degrees F. To our knowledge, CCS pilot tests have not been accomplished on a simple cycle gas turbine system anywhere in the world. This would represent another major technical uncertainty associated with CCS implementation at the CGS. Chemical absorption of CO<sub>2</sub>, such as that accomplished by most amine-based carbon capture processes, is an exothermic reaction, meaning that heat is released during absorption; high temperature of the exhaust and solvent would therefore inhibit the carbon capture. Furthermore, the regeneration of the sorbent to release the CO<sub>2</sub> for compression requires heating of the sorbent, so high temperature of the solution would clearly inhibit the chemical reaction required for absorption.

BHC is aware of the planned construction of a CO<sub>2</sub> pipeline, intended to transport byproduct CO<sub>2</sub> from oil and gas operations to an EOR location in Montana. This project will be used as a CCS large-scale demonstration project by the DOE-funded Plains CO<sub>2</sub> Reduction Partnership. From review of publicly available documentation, the pipeline is being designed with excess capacity, presumably to provide future capability to transport CO<sub>2</sub> from other sources to EOR locations in the region. At its closest point the pipeline is estimated to be 175 miles away from the power plant location. However the location, time frame, and needed flowrates for those future EOR operations are closely guarded trade secrets. Thus BHC, as developer of this power generation facilities, has no way of knowing when and if those future needs will be realized. At the current time, the only known CO<sub>2</sub>based tertiary oil recovery system operating in the region is the Salt Creek Field (also approximately 175 miles from the power plant location), for which current CO<sub>2</sub> needs are being served from current separation systems in the Shute Creek Field of southwest Wyoming, with CO<sub>2</sub> being transported by existing pipeline.

Ability to inject into deep saline aquifers as an alternative to EOR reservoirs is a major focus of the NETL research program. While it is believed that saline aquifers are a viable opportunity, many uncertainties exist. Risk of mobilization of natural elements such as manganese, cobalt, nickel, iron, uranium, and barium into potable aquifers is of concern. Technical considerations for site selection include geologic siting, monitoring and verification programs, post injection site care, long term stewardship, property rights, and other issues. In regards to CO<sub>2</sub> storage security, the CCS Task Force Report notes such uncertainties, "The technical community believes that many aspects of the science related to geologic storage security are relatively well understood. For example, IPCC concluded that "it is considered likely that 99 percent or more of the injected CO<sub>2</sub> will be retained for 1,000 years" (IPCC, 2005). However, additional information (including data from large-scale field projects with comprehensive monitoring) is needed to confirm predictions of the behavior of natural systems in response to introduced CO<sub>2</sub> and to quantify rates for long-term processes that contribute to trapping and, hence, risk profiles (e.g., IPCC, 2005)."

CCS technology development is dominated by vendors who are attempting to commercialize carbon capture technologies and academia-lead teams (largely funded by DOE) who are leading research into the geologic systems. Ability for electric utilities to contract for turn-key CCS systems simply does not exist at this time.

Most current carbon capture systems are based on amine or chilled ammonia technology, which are chemical absorption processes. While capture system startup and shutdown time of vendor processes could not be confirmed within this BACT analysis, clearly both types of

processes would require durations which exceed the turbine startup time. The simple cycle generation systems are designed to be able to produce electricity at full load within 10 minutes of cold start, and the combined cycle systems designed to be able to produce electricity at full load with SCR and oxidation catalysts controlling criteria air pollutants within 40 minutes of startup. Durations of plant operation may be short, depending on needs to serve peak power loads. In contrast, both amine and chilled ammonia systems require startup of countercurrent liquid-gas absorption towers and either chilling of the ammonia solution or heating of regeneration columns for the amine systems. It is technically infeasible for the carbon capture systems to startup and shutdown in the time frames required to effectively serve this type of operation, meaning that significant portions of at least the simple cycle operations would run without CO<sub>2</sub> capture even with implementation of a CCS system.

Finally, the potential to sell  $CO_2$  to industrial or oil & gas operations is infeasible for an operation such as this, where daily operation of both simple cycle and combined cycle systems may depend on grid dispatch needs. Even if a potential EOR opportunity could be identified by the power plant developers, such an operation would typically need a steady supply of  $CO_2$  year-round. Intermittent  $CO_2$  supply from potentially short-duration with uncertain daily operation would be virtually impossible to sell on the market, making the EOR option unviable. Therefore, CCS technology would be better suited on applications which have low variability in operating conditions.

In the EPA PSD and Title V GHG permitting guidance, the issues noted above are summarized, "A number of ongoing research, development, and demonstration projects may make CCS technologies more widely applicable in the future" (italics added). From Page 36 of this guidance, "While CCS is a promising technology; EPA does not believe that at this time CCS will be a technically feasible BACT option in certain cases. As noted above, to establish that an option is technically infeasible, the permitting record should show that an available control option has neither been demonstrated in practice nor is available and applicable to the source type under review. EPA recognizes the significant logistical hurdles that the installation and operation of a CCS system presents and that sets it apart from other add-on controls that are typically used to reduce emissions of other regulated pollutants and already have an existing reasonably accessible infrastructure in place to address waste disposal and other offsite needs. Logistical hurdles for CCS may include obtaining contracts for offsite land acquisition (including the availability of land), the need for funding (including, for example, government subsidies), timing of available transportation infrastructure, and developing a site for secure long-term storage. Not every source has the resources to overcome the offsite logistical barriers necessary to apply CCS technology to its operations, and smaller sources will likely be more constrained in this regard."

Therefore, the CCS alternative is not considered technically feasible for the CGS project, and is eliminated from further consideration. While it is being eliminated based on technical feasibility in Step 2, at the suggestion of USEPA team members, economic feasibility issues will be covered in Step 4.

#### **Electrical Generation Efficiency**

EPA's *PSD and Title V Permitting Guidance for Greenhouse Gases* (EPA, 2011) identifies three categories of control technologies (p. 25):

- 1. Inherently lower-emitting processes/practices/designs
- 2. Add-on controls, and
- 3. Combinations of lower-emitting process/practices/designs and add-on controls

Because there are no demonstrated add-on controls, only those processes, practices, and designs that result in lower GHG emissions are applicable for this BACT analysis. As noted above, the project includes both simple-cycle and combined-cycle generation in this phase of the project, and possible, but unplanned future expansion of the facility could include build-out of the simple-cycle combustion turbines into combined-cycle systems providing added thermal efficiencies. The CGS project as proposed will utilize a high-efficiency, state-of-the-art, combustion turbine, generator, and HRSG design. Operations will use good combustion practices and result in energy efficient operation to provide steam to a new steam turbine generator. Furthermore, inlet air chillers will be used to prevent loss of turbine efficiency that results during hot weather, and a wet cooling tower will be used to improve the thermal efficiency of the combined cycle system.

The following analysis will demonstrate that the overall generation efficiency meets or exceeds that of other recently implemented projects.

The permit limits proposed in this application are based on a GE LM 6000PF SPRINT combustion turbine of 37.1 MW gross output and a gross heat rate of 9,263 Btu/kWh (HHV) for simple-cycle operation. This results in an estimated net output of approximately 97.4 MW at a gross heat rate of 7,062 Btu/kWh (HHV) for the 2x1 combined-cycle system, which results in an efficiency of 36.8% and 48.3% for simple cycle and combined cycle operation respectively. These efficiencies include consideration of parasitic auxiliary loads. The combined-cycle system will not have duct firing. All noted performance information is based upon CGS site conditions at 60°F; the high altitude of the area results in marginal decreases to turbine efficiency compared to other locations. The CGS project will utilize all new equipment.

#### **Combustion Turbine Generator Comparable Permitted Emissions**

A search of the EPA's RACT/BACT/LAER Clearinghouse (RBLC) was performed for simple- and combined-cycle projects with combustion turbines similar to those proposed for the CGS project. No GHG permit limits were found in searching the RBLC for comparable units, thermal efficiency data was available.

#### Efficiency Review

An efficiency review of the proposed CGS project was completed with two metrics: 1) RBLC comparable unit heat rates and 2) comparison of  $CO_2e$  emission rates.

#### **RBLC Efficiency Comparison**

The RBLC information presented in Table 5-4 below provides a comparison of efficiencies for projects with combustion turbines in the same nominal 40-MW size range as the CGS project. The information presented is for combustion turbines operating in simple cycle. No information was found for comparable 40-MW combined-cycle units without duct burning.

Facility	State	Description	Heat Capacity MMBtu/hr (HHV)	Net MW	Heat Rate Btu/kWh (HHV)	Calculated Efficiency (%)
Western Farmers Electric	Oklahoma	Combustion Turbine Simple Cycle	462.7	50	9,254	36.9
El Colton, LLC	California	LM6000 (Enhanced Sprint)	456.5	48.7	9,374	36.4
Bayonne Energy Center	New Jersey	Rolls Royce Trent 60WLE	603	64	9,422	36.2
Creole Trail LNG	Louisiana	Combustion Turbine Simple Cycle	290	30	9,667	35.3
Arvah B. Hopkins Generating Station	Florida	GE LM6000PC Simple Cycle	489.5	50	9,790	35.0
Indigo Energy Facility	California	LM6000 (Enhanced Sprint)	450	45	10,000	34.1
Lambie Energy Center	California	GE LM6000PC Simple Cycle	500	49.9	10,020	34.1

TABLE 5-4 RBLC Efficiency Information – Simple Cycle

Notes: Used 1.108 for HHV/LHV conversion factor.

The combustion turbines compared above are similar in size to those planned for the CGS project. As noted above, this analysis and resulting CGS proposed permit limits are based on use of a turbine with simple-cycle gross heat rate of 9,263 Btu/kWh (HHV). An exact comparison cannot be made between the CGS combustion turbines and those listed in Table 5-4 above because each project has unique equipment and site conditions, primarily elevation and temperature. However, the CGS heat rate compares very favorably with all of the reviewed comparable projects listed above, which demonstrates the high-efficiency attributes of the CGS project.

#### CO2e Emission Rate Comparison

In simple-cycle operation, the CGS turbines are estimated to produce 1,102 pounds of CO<sub>2</sub>e/MWh at average ambient conditions and full-load operation. Considering the range of normal operating loads (50 to 100 percent generator output), and ambient temperature (0°F to 108°F), GHG output for the CGS simple-cycle combustion turbines range from 1,072 to 1,603 pounds of CO<sub>2</sub>e for new and clean combustion turbine prior to any degradation.

Table 5-5 below presents operating information from the EPA Acid Rain database, and was developed using actual comparable operating unit information from 2010.

State	Facility Name	Unit ID	Operating Time (Hr)	Net Load (MWh)	CO₂ Tons	lb CO₂/MWh
CA	El Cajon Energy Center	1	242	9450	5652	1196
OK	Horseshoe Lake	10	710	29293	18142	1239
ОК	Horseshoe Lake	9	174	6851	4248	1240
CA	Orange Grove Project	CTG1	632	25017	15734	1258

TABLE 5-5 CGS Comparable Unit GHG Emissions

State	Facility Name	Unit ID	Operating Time (Hr)	Net Load (MWh)	CO₂ Tons	lb CO₂/MWh
CA	Orange Grove Project	CTG2	654	24954	15847	1270
FL	Arvah B Hopkins	HC4	903	27627	17623	1276
FL	Polk	**2	249	27652	18500	1338
FL	Arvah B Hopkins	HC3	662	18283	12529	1371
FL	Polk	**5	476	51662	36111	1398
FL	Polk	**4	563	60221	42443	1410
FL	Polk	**3	204	23176	16600	1432
NJ	Bayonne Plant Holding, LLC	2001	1055	35582	28385	1595
NJ	Bayonne Plant Holding, LLC	1001	1208	39061	32004	1639
NJ	Bayonne Plant Holding, LLC	4001	1134	36629	30200	1649
NE	C W Burdick	GT-3	24	426	399	1871
NE	C W Burdick	GT-2	33	606	579	1912
CA	Escondido Energy Center, LLC	CT1A	28	345	466	2702
CA	Escondido Energy Center, LLC	CT1B	28	345	468	2718

#### TABLE 5-5

CGS Comparable Unit GHG Emissions

Notes:

Net load 5% lower than gross load.

Data as per EPA Clean Air Markets – Data and Maps. Based on 2010 data.

The CGS combustion turbine GHG output compares favorably with the facilities shown Table 5-5 above. It is recognized that in establishing any permit limit, allowance must be given for load variances, impact of ambient conditions, startup and shutdown, and equipment degradation over time. This is exemplified by reviewing the information from Table 5-5, because all of these units can be considered as "peaking" due to the low number of annual operating hours. The resultant wide variance in pounds of CO<sub>2</sub>e/MWh may likely be attributed to the significant proportion of time in startup and shutdown and/or reduced load operation, as well as lower thermal efficiency for older units.

Note that, considering the range of normal operating loads (50 to 100 percent output) and ambient temperature (0°F to 108°F), GHG output for the CGS 2x1 combined-cycle system ranges from 833 to 985 pounds of CO<sub>2</sub>e for a new or clean combustion turbine prior to any degradation.

#### Step 3: Rank Remaining Control Technologies by Control Effectiveness

The only remaining technically feasible GHG control technology for the CGS project is the electrical generation efficiency. This option is presented in Table 5-6 based on their energy efficiencies expressed in terms of heat rate.

Configuration	Gross Plant Heat Rate (HHV) (Btu/kWh) <sup>1</sup>
Electrical Generation Combined-Cycle Efficiency	7,062
Electrical Generation Simple-Cycle Efficiency	9,263

#### TABLE 5-6 CGS Project GHG Control Technology Ranking

Note: <sup>1</sup>At CGS site conditions.

#### **Combustion Turbine Design Elements**

As demonstrated above, the GE LM6000PF SPRINT combustion turbine has high efficiency which is equal or greater the majority of other turbines of the same nominal capacity. However the differences in efficiency from offerings of other vendors are in some cases trivial. The design elements of those turbines that result in high efficiency undoubtedly vary between vendors, and in many cases are proprietary and confidential. Thus an extensive analysis of what design considerations are needed to have an efficient turbine design is beyond the scope of this permit application.

However the issue was discussed with the selected turbine vendor, GE, and they offered comments on the unique elements of their design. This information is provided in Appendix B-4. Some of the key elements noted by GE are dual shaft architecture, low shaft speed, modulation of shaft speed and air flow with power, and high operating pressure ratio.

It should be noted that the electrical generator is provided as a combined unit with the GE LM6000PF SPRINT combustion turbine package, and has been engineered to match combustion turbine operating characteristics. Preliminary information indicates that the generator is 98%+ efficient, so overall system efficiency is driven by the combustion turbine characteristics.

The CGS 2x1 combined cycle system will also utilize a steam turbine and Heat Recovery Steam Generators (HRSG). Steam turbines manufactured today for small combined cycle plants have efficiencies limited by the metal design temperatures and pressures. The steam turbine is custom engineered rotating machinery where the efficiency is optimized in the blade path design, which maximizes the energy extracted from the steam. HRSG efficiency is maximized in the design by selecting aggressive approach and pinch points to extract the maximum heat out of the gas turbine exhaust stream. The efficiency is further improved by tube bundle arrangement, finned tubing and back end recirculation and or condensate preheating.

#### Step 4: Evaluate Most Effective Controls and Document Results

As demonstrated in Step 2 above, CCS is not a technically feasible alternative for the CGS project. Nonetheless, at the suggestion of USEPA team members, economic feasibility of CCS technology is reviewed in this Step 4. Control options considered in this step therefore include application of CCS technology, and plant energy efficiency. As demonstrated below, CCS is clearly not economically feasible for the CGS.

On Page 42 of the EPA PSD and Title V Permitting Guidance, it is suggested that detailed cost estimates and vendor quotes should not be required where it can be determined from a

qualitative standpoint that a control strategy would not be cost effective: "With respect to the valuation of the economic impacts of GHG control strategies, it may be appropriate in some cases to assess the cost effectiveness of a control option in a less detailed quantitative (or even qualitative) manner. For instance, when evaluating the cost effectiveness of CCS as a GHG control option, if the cost of building a new pipeline to transport the  $CO_2$  is extraordinarily high and by itself would be considered cost prohibitive, it would not be necessary for the applicant to obtain a vendor quote and evaluate the cost effectiveness of a  $CO_2$  capture system."

The guidance document also acknowledges the high costs of CCS technology at the current time: "EPA recognizes that at present CCS is an expensive technology, largely because of the costs associated with  $CO_2$  capture and compression, and these costs will generally make the price of electricity from power plants with CCS uncompetitive compared to electricity from plants with other GHG controls. Even if not eliminated in Step 2 of the technical feasibility of the BACT analysis, on the basis of the current costs of CCS, we expect that CCS will often be eliminated from consideration in Step 4 of the economical feasibility of the BACT analysis, even in some cases where underground storage of the captured  $CO_2$  near the power plant is feasible."

The costs of constructing and operating CCS technology are indeed extraordinarily high based on current technology. Even with the optimistic assumption that appropriate EOR opportunities could be identified in order to lower costs as compared to "pure" sequestration in deep saline aquifers or depleted coal seams, additional costs to the CGS would include the following:

- Licensing of scrubber technology and construction of carbon capture systems,
- Significant reduction to plant output due to the high energy consumption of capture and compression systems,
- Identification of oil & gas companies holding depleted oil reservoirs with appropriate characteristics for effective use of CO<sub>2</sub> for tertiary oil recovery, and negotiation with those parties for long term contracts for CO<sub>2</sub> purchases,
- Construction of compression systems and pipelines to deliver CO<sub>2</sub> to EOR locations,
- Labor to operate, maintain, and monitor the capture, compression, and transport systems, and
- Issues regarding project risk that would jeopardize ability to finance construction and to obtain PUC approval.

The interagency task force report provides an estimate of capital and operating costs for carbon capture from natural gas systems: "For a [550 MWe net output] natural gas combined cycle (NGCC) plant, the capital cost would increase by \$340 million and an energy penalty of 15 percent would result from the inclusion of CO<sub>2</sub> capture." Using the "Capacity Factor Method" for prorating capital costs for similar systems of different sizes as suggested by the Association for the Advancement of Cost Engineering (AACE) and other organizations, CO<sub>2</sub> capture system capital cost for the CGS is estimated as at least \$196 million. Based on an estimated CGS plant capital cost of \$300 million, the capture

system alone would thus be expected to add approximately 65 percent to the overall plant capital cost.

Actual cost per megawatt would likely be higher for CGS than the reference plant in the Task Force report due to the inclusion of simple cycle units; this would require capture systems to handle a much higher temperature gas flow; little or no pilot test data is available for this situation, different materials of construction may be required, and modifications to the absorption process may be required.

Similarly, the energy penalty would be higher for simple cycle systems than for combined cycle; since scrubber and compressors are sized based on combustion turbine output, but overall unit output is lower for simple cycle, the fractional penalty would be higher. Whether plant size would remain the same with output reduced, or plant size increased to account for lost output, the energy penalty alone represents at least a 15% increase to the fuel component of the cost of electricity. At an estimated 8.9¢/kWh residential retail price for electricity, and assuming an annual average of 50% capacity factor for plant operation and 15% energy penalty, the value of lost electricity sales from the project is \$12.9 million per year.

As noted above, the effort required to identify and negotiate with oil & gas companies who may be able to utilize the  $CO_2$  would be substantial. BHC is aware that the proposed Greencore pipeline is being substantially oversized, versus what would be required for only the Belle Creek EOR operation, so it is reasonable to assume project developers are planning that there will be a future need for  $CO_2$  in the Powder River Basin or other locations in Wyoming or Montana. The location and timing of those sites, however, is not public information, and due to the patchwork of oil well ownership many parties could potentially be involved in negotiations over  $CO_2$  value.

Due to the extremely high pressures required to transport and inject  $CO_2$  under supercritical conditions, the compressors required are very specialized. For example, the compressors for the Dakota Gasification Company system are of a unique eight stage design. It is unclear whether the Task Force NGCC cost estimate noted above includes the required compression systems, but if not this represents another substantial capital cost.

Pipelines must be designed to withstand the very high pressures (over 2000 pounds per square inch, gauge) and potential for corrosion if any water is introduced to the system. As noted above, if CCS were otherwise technically and economically feasible for the CGS, the most realistic scenario could be to construct a pipeline from Cheyenne to tie into the proposed Greencore pipeline. At its closest point, the Greencore pipeline would be approximately 175 miles from Cheyenne. Based on engineering analysis done by the designers of that pipeline, costs for an 8" CO<sub>2</sub> pipeline to connect the Cheyenne project to the Greencore pipeline are estimated at \$600,000 per mile, for a total cost of \$105 million. Thus the pipeline alone would represent a 35 percent increase to the project cost, and the pipeline and capture system together would double the project capital cost.

It is unlikely that financing could be approved for a project which combines CCS in conjunction with generation, given the technical and financial risks. Also, as evidenced with utilities' inability to obtain PUC approval for integrated gasification / combined cycle (IGCC) projects due to unacceptable cost and risk to ratepayers, such as Wisconsin's

disapproval of the We Energy project, it is reasonable to assume that the same issues would apply in this case before the Wyoming PUC.

Sale of the  $CO_2$  for EOR could be the one positive direct economic impact of CCS. If BHC were to construct or pay for construction of the pipeline to deliver captured  $CO_2$ , it is possible that revenue from sale of the  $CO_2$  could be realized. Current market pricing for  $CO_2$  delivered for EOR is however proprietary and confidential, and reliable sources of information could not be identified within this scope of this BACT analysis.

In summary, capital cost for capture system and pipeline construction are estimated at \$300 million, and retail value of lost power sales due to the CCS system energy penalty is estimated at \$12.9 million per year assuming only 50% plant capacity factor. Other costs such as identification, negotiation, and engineering of EOR opportunities; operating labor and maintenance costs for capture, compression, and pipeline systems; less favorable financing terms or inability to finance; and difficulty in obtaining PSC approval would also impact the project, and it is unclear if compression systems are included in the Task Force estimate of capture system costs. A fraction of these impacts could possibly be offset through sale of the CO<sub>2</sub>, but overall addition of CCS with or without EOR opportunity would make the project unviable.

CCS is clearly not economically feasible for natural gas fired power plants at the current time. Since CCS is not considered technically or economically feasible, the proposed CGS electrical generation efficiency is determined to be the most effective GHG control technology.

From a review of the three evaluation metrics presented above, the heat rate for the CGS GE LM6000 PF Sprint combustion turbine, selected pursuant to the CGS business plan, was found to favorably compare with other combustion turbines and projects.

### Step 5: Select BACT

The only remaining option is the "Electrical Generation Efficiency" option, which, therefore, is selected as BACT. This option determined to consist of the CGS project as proposed with new state-of-the-art combustion turbines. Consistent with the review criteria presented above, the CGS project evaluated combustion turbine exhibits comparable efficiency with most of the evaluated alternative combustion turbines, and superior efficiency over other comparable machines. Therefore, BHC proposes that CGS GHG BACT consist of installation of GE LM6000PF SPRINT combustion turbines, and the annual CO<sub>2</sub> emissions limit for the five new combustion turbines will be based upon the BACT emission limits proposed below. The estimated total annual CO<sub>2</sub>e emissions from the combustion turbines are 936,588 tpy, and this value is proposed to be the annual CO<sub>2</sub>e permit limit for the five combustion turbines.

EPA's PSD permitting guidance for GHGs suggests use of output-based BACT emission limits and longer-term averaging periods for GHGs. Based on BHC analysis of conservative scenarios for number of turbine startups and shutdowns, partial load operation, and ambient temperature during operations, and considering the range of normalized GHG emissions noted above and eventual turbine degradation, proposed BACT permit limits are 1,100 lb/MWh for each combined-cycle combustion turbine and 1,600 lb/MWh for each simple-cycle combustion turbine on an annual average basis.

## 5.6 Small Combustion Sources BACT for GHGs

In addition to the five combustion turbines planned for the CGS project, there are several other small combustion sources associated with auxiliary equipment which will operate at the plant. The GHG calculations for these small combustion sources are located in Appendix B-1.

- (6) Natural gas-fired inlet air heaters (nominal 16-MMBtu/hr air heater with estimated emissions of 4,117 CO<sub>2</sub>e tons/year each), required for safety to prevent icing of air handling systems
- (2) Natural gas-fired fuel gas heaters (nominal 4.5-MMBtu/hr gas heater with estimated emissions of 1,153 CO<sub>2</sub>e tons/year each)
- (1) Diesel-fired emergency generator (nominal 839-BHP engine with estimated emissions of 226 CO<sub>2</sub>e tons/year)
- (1) Diesel-fired fire pump (nominal 327-BHP engine with estimated 51 CO<sub>2</sub>e tons/year)

The total GHG emissions from the above small combustion sources are very minor as compared to the emissions from the combustion turbines. However, for completeness, these minor GHG emission sources were evaluated in aggregate below.

## Step 1: Identify All Control Technologies

The available control technologies for the CGS minor GHG sources are identical to those identified for the combustion turbines. These options include

- Carbon Capture and Storage Systems (CCS
- Small Combustion Source Efficiency
- Efficient Use of Energy

## Step 2: Eliminate Technically Infeasible Options Effectiveness

#### Carbon Capture and Storage Systems

As discussed above, CCS for GHG control is not considered a technically feasible control option for the combustion turbines. Stand-alone capture systems for the small sources would be even further from technical feasibility. Therefore, CCS is eliminated from further consideration for small combustion source GHG reduction.

#### Small Combustion Source Efficiency

The small combustion sources for the CGS project will incorporate a high-efficiency design.

#### Efficiency Background Information

In support of small combustion source design, additional background information is assembled in Appendix B-8 through B-14 regarding efficiency attributes of the auxiliary equipment; i.e., inlet air heater, inlet chiller units, fuel gas heaters, diesel fire pump, and diesel emergency generator.

#### Inlet Air Heater

The inlet air anti-icing heater is similar to a conventional natural gas fired watertube boiler, and is required for safety reasons to prevent icing during winter weather. However, the

water does not reach the boiling point in this system and a mixture of water and glycol is used for its thermodynamic advantages over water. The unit is designed for quick load response eliminating the requirement for a stored energy system and associated efficiency losses. Combusted natural gas is used to directly heat the incoming water/glycol mixture.

Other technologies available for heating the water/glycol mixture include an indirect fired water bath heater or fire tube boiler. The fire tube boiler has similar efficiency but a much higher capital cost. The indirect fired water bath heater has a lower efficiency resulting in higher operating costs and increased emissions. With both cost and environmental operations considered, these two options are not economical for this application.

#### Fuel Gas Heater

Indirect water/glycol bath heaters were selected for heating of high-pressure natural gas. The natural gas is heated to ensure a measure of superheat before reaching the combustion turbine generator. Indirect heaters use a fire tube to transfer heat from the fired natural gas (fuel) to the water/glycol solution. The heat is then transferred from the water/glycol bath to the natural gas coil (product) in a safe manner. Although this heating technology is not as efficient as direct heating, it is considered the only acceptable option due to safety reasons as noted below.

Direct heating of natural gas would result in a slightly more efficient process; however, direct heating of natural gas is extremely dangerous and not recommended. Any small manufacturing defect, failure, or leak may result in catastrophic explosions as the product (natural gas) is exposed to an open heat source.

#### Diesel Fire Pump & Standby Generator

While preliminary review of the CGS emergency diesel equipment has been initiated, the final equipment selection has not been completed. However, the diesel equipment will be evaluated to ensure a high efficiency design.

#### Efficient Use of Energy

The small combustion sources will not be operated continuously, but only during conditions when they are needed. For example, the inlet air heaters and fuel gas heaters will be operated only when required for safety reasons to protect against icing of the turbines or condensation within the fuel lines. Therefore, energy will be utilized in an efficient manner.

## Step 3: Rank Remaining Control Technologies by Control Effectiveness

The remaining technically feasible GHG control technologies for the CGS project are "Small Combustion Source Efficiency "and "Efficient Use of Energy." Both technologies are equally important toward minimizing GHG emissions.

## Step 4: Evaluate most effective controls and document results

The remaining technically feasible GHG control technologies for the CGS project are "Small Combustion Source Efficiency "and "Efficient Use of Energy." Both technologies will be implemented for the CGS project.

## Step 5: Select BACT

GHG BACT for the CGS small equipment are "Small Combustion Source Efficiency "and "Efficient Use of Energy." All auxiliary equipment will be selected with consideration for

high design efficiency, and will be operated in an efficient manner. Due to the minor CO<sub>2</sub>e emissions contribution from these small combustion sources, no efficiency or output-based GHG permit limits are recommended for the CGS auxiliary equipment.

## 5.7 Requested Permit Limits

The following Tables 5-7 and Table 5-8 list the recommended permit limits for the combustion turbines and auxiliary equipment respectively:

#### TABLE 5-7

CGS Combustion Turbine Recommended CO2e Permit Limits

Emission Unit	Annual CO₂e Limit (Pounds/MWhr)	Annual CO₂e Limit (Tons/Year)
Combined Cycle Combustion Turbine CT01A	1,100	187,318
Combined Cycle Combustion Turbine CT01B	1,100	187,318
Simple Cycle Combustion Turbine CT02A	1,600	187,318
Simple Cycle Combustion Turbine CT02B	1,600	187,318
Simple Cycle Combustion Turbine CT03A	1,600	187,318

#### TABLE 5-8

CGS Auxiliary Equipment Recommended CO<sub>2</sub>e Permit Limits

Emission Unit	Annual CO <sub>2</sub> e Limit (Tons/Year)		
Six (6) Inlet Air Heaters	24,703		
Two (2) Fuel Gas Heaters	2,306		
One (1) Diesel Fire Pump	51		
One (1) Diesel Standby Generator	226		

Location Map and Plot Plans

CGS Site Location and Fenceline Map



Cheyenne Generating Station Fenceline and Power Block

CH2MHILL

CGS Structures and Emission Points





CGS Site General Arrangement



GHG Support Documentation

CGS GHG Emission Calculations

## Black Hills Corporation Cheyenne Generating Station Potential to Emit Facility Wide Greenhouse Gas Revision 07-28-11

Emission		Consumption	Emission Factors (kg/MMBtu)		Emissions (tons/year)				
Point	Description	(MMBtu/hr)	CO <sub>2</sub>	CH₄	N <sub>2</sub> O	CO <sub>2</sub>	CH₄	N <sub>2</sub> O	CO <sub>2</sub> -equivalent
EP01	Combined Cycle Combustion Turbine CT01A	366	53.02	0.001	0.0001	187,134.03	3.53	0.35	187,317.56
EP02	Combined Cycle Combustion Turbine CT01B	366	53.02	0.001	0.0001	187,134.03	3.53	0.35	187,317.56
EP03	Simple Cycle Combustion Turbine CT02A	366	53.02	0.001	0.0001	187,134.03	3.53	0.35	187,317.56
EP04	Simple Cycle Combustion Turbine CT02B	366	53.02	0.001	0.0001	187,134.03	3.53	0.35	187,317.56
EP05	Simple Cycle Combustion Turbine CT03A	366	53.02	0.001	0.0001	187,134.03	3.53	0.35	187,317.56
EP06	Inlet Air Heater 01	16.0680	<b>53.02</b>	0.001	0.0001	4,113.13	0.08	0.01	4,117.17
EP07	Inlet Air Heater 02	16.0680	53.02	0.001	0.0001	4,113.13	0.08	0.01	4,117.17
EP08	Inlet Air Heater 03	16.0680	53.02	0.001	0.0001	4,113.13	0.08	0.01	4,117.17
EP09	Inlet Air Heater 04	16.0680	53.02	0.001	0.0001	4,113.13	0.08	0.01	4,117.17
EP10	Inlet Air Heater 05	16.0680	53.02	0.001	0.0001	4,113.13	0.08	0.01	4,117.17
EP11	Inlet Air Heater 06	16.0680	53.02	0.001	0.0001	4,113.13	0.08	0.01	4,117.17
EP15	Diesel Generator	5.52	73.96	0.003	0.0006	225.01	0.01	0.00	225.77
EP16	Diesel Fire Pump	2.5	73.96	0.003	0.0006	50.95	0.00	0.00	51.13
EP18	Fuel Gas Heater 01	4.5	53.02	0.001	0.0001	1,151.92	0.02	0.00	1,153.05
EP19	Fuel Gas Heater 02	4.5	53.02	0.001	0.0001	1,151.92	0.02	0.00	1,153.05
	Total PTE for Facility					962,928.74	18.17	1.82	963,873.80
Notes: (1) $CO_2$ Emission (2) $CH_4$ and $N_2O$ (3) Global Warmin	Notes:     (1) CO2 Emission Factors from Table C-1 of the EPA's Mandatory Reporting Rule.     (2) CH4 and N2O Emission Factors from Table C-2 of the EPA's Mandatory Reporting Rule.								
( )	CO <sub>2</sub>	1							
	CH <sub>4</sub>	21							
	N <sub>2</sub> O	310							
(4) Combustion Turbines (hr/yr operation per turbine)		8760							
(5) Inlet Air Heaters (hr/yr operation per turbine)		4380							
(6) Diesel Emerge	ency Generator (hr/yr operation per turbine)	500							
(7) Diesel Fire Pu	imp (hr/yr operation per turbine)	250							
(8) Fuel Gas Heaters (hr/yr operation per turbine)		4380							

GE LM6000 Sprint Combustion Turbine Series General Information GE Power & Water Aeroderivative Gas Turbines

# Fast, Flexible Power Aeroderivative Product and Service Solutions









imagination at work



GE Power & Water's Aeroderivative Gas Turbines business is a leading supplier of aeroderivative gas turbines and packaged generator sets for industrial and marine applications. Our products and services help power the potential of customers across a wide range of operational profiles and industries by increasing efficiency while reducing environmental impact.

GE's continued investment in research and development of aircraft engine technology enables the LM series of gas turbines to maintain a leadership position in technology, performance, operational flexibility and value to the customer. With power output from 18 to 100 MW and the ability to operate with a variety of fuels and emission control technologies, GE's aeroderivative gas turbines have gained wide acceptance in the industry, with total operating experience surpassing 100 million hours.

#### Products known for...

- Operational flexibility
- High efficiency
- Superb reliability
- Fast installations

## Providing diverse solutions for...

- FPSO
- Grid Stability
- Utilities
- Oil and Gas
- Industrial
- Pipeline
- Temp Power
- Marine

# Aeroderivative Heritage



B747, B767, MD-11





A300, A310/330







-6® TF39



LM6000™



LM1800e<sup>™</sup>/LM2500<sup>™</sup> 18-24 MW



LMS100® 100 MW



LM2500+/G4T 28-34 MW

# Fast, Flexible Power

At GE, we recognize the individual operating schemes of our customers are vast and varied. That is why we are committed to providing a flexible portfolio of products to support a full spectrum of operating needs: from fast starts and load following to get peak customers on the grid quickly, to high availability and reliability to keep base load customers online for the long haul. Whatever your scenario, we can tailor a solution to meet your needs.

Operational flexibility is inherent to GE's portfolio of aeroderivative gas turbines and a critical component of our customers' success. We understand the importance of speed and flexibility when it comes to responding to power demands. Our gas turbines are designed to meet these challenges with efficiency and cost effectiveness.

#### Fast Installation with Less Interruption

GE is committed to maintaining short manufacturing cycles supported by dependable, predictable delivery times and a robust supply chain. Our modular package designs and on-going interconnect innovation allow for shorter manufacturing cycles and faster installation times with less installed and operational costs than field erected units. All of our units undergo rigorous factory testing after assembly and are ready for operation soon after arriving on site—translating into lower installation costs, shorter project schedules, and reduced financial risk for our customers.

The integration of skid-mounted support systems requires less installation work, time and expense. Fewer materials are shipped directly to the site, reducing the amount of civil works, utilizing package support systems and less foundation work than alternate generation. Our compact, lightweight package design allows for installation flexibility and less process interruption.

# Products known for operational flexibility, high efficiency, superb reliability and fast installations

#### Providing diverse solutions for various industries

- Utilities peak power, combined cycle, distributed generation, grid stability
- Oil & Gas mechanical drive, power generation
- FPSO offshore power with our compact 538 and 538e packages
- Industrial combined heat and power
- Mobile power emergency power, peak demand, mining and O&G applications
- Marine power and propulsion



## Fast Starts and Cycling Capability

The ability to go from cold iron to full power in just 10 minutes and the ability to start and stop in short, 15-minute cycles (several times per day if necessary) without impacting maintenance intervals make GE's aeroderivative gas turbines exceptionally adept at accommodating fluctuating demand with increasing efficiency across multiple industry segments. GE's aeroderivative gas turbines can be the first to respond to a peak power demand opportunity, without the costs of a spinning reserve.

## Load Following

Thanks to a two-rotor design, GE's aeroderivative portfolio provides higher part power efficiency and faster response to load changes than other similar gas turbines in the industry. This load matching allows for greater grid stability of voltage and frequency, and provides greater starting torque for mechanical drive applications.

## High Availability/Reliability

By utilizing aircraft experience and design, our aeroderivative design approach incorporates features such as split casings, modular construction, individual replacement of internal and external parts, and GE's "lease pool" engine program. Our extensive use of high quality components common with parent aircraft engines validates engine reliability and offers reduced parts cost.

Various inspections and hot section repairs can be performed on the gas turbine at site within the turbine enclosure. The "Hot Section," HPT and combustor can be removed/replaced in the field within 72 hours, allowing for greater availability during planned maintenance. Greater availability is achieved by the on-condition maintenance program, which inspects and repairs only as necessary to desired operational condition.

## Wide Fuel Range

At GE, we understand flexibility in fuel choices is a high priority. Our Alternate Fuels Center of Excellence is leading the industry in identifying, designing, and delivering fuel flexibility options—all with the high reliability, availability, and maintainability standards you expect from GE.

Our experience on liquid biofuels is proven and growing. In addition to conventional turbine fuels such as #2 diesel, jet fuel, and kerosene, aeroderivative gas turbines are designed to run on a range of alternates—from light distillates like naphtha, to greener fuels such as biodiesels and ethanol derived from various feedstocks. Our package and engine systems have over 450,000 hours of successful operations on naphtha fuel, and over 23,000 hours of operation using biodiesel.

Examples of fuel versatility for our gas turbine and package products include:

#### Gaseous fuel

- Pipeline and liquefied natural gas (LNG)
- Syngas (low and medium BTU)
- Propane, high hydrocarbon gas
- Wellhead, associated gas
- Coal bed methane (CBM)
- Landfill gas (LFG)
- Coke oven gas (COG)
- Refinery/process flare gas
- LNG for marine propulsion

#### Liquid fuel

- #2 Diesel
- Jet fuel, kerosene
- Naphtha
- Biodiesel
- Ethanol
- Liquid blends
- Butane



## GE Energy LM6000 Sprint Aeroderivative Gas Turbines

Unlike most gas turbines, the LM6000® is primarily controlled by the compressor discharge temperature in lieu of the turbine inlet temperature. Some of the compressor discharge air is then used to cool high-pressure turbine components. Sprint — which stands for "Spray Inter-cooled Turbine" — reduces compressor discharge temperature, thereby allowing advancement of the throttle to significantly enhance power and improve thermal efficiency.



## Features & Benefits

- Output increased by 12 percent @ ISO condition and over 30 percent at 90 °F (32 °C) ambient temperature
- Enhanced heat rate across the ambient range
- Exhaust conditions are also improved for combined cycle applications
- Full power in ten minutes
- Baseload, cycling, or peaking
- Dual fuel capability (distillate or gas)
- Easy on-site maintenance

## Design

The LM6000 Sprint system is composed of atomized water injection at both low-pressure compressor (LPC) and high-pressure compressor (HPC) inlet plenums. This is accomplished by using a high-pressure compressor, eighth-stage bleed air to feed two air manifolds, water-injection manifolds and sets of spray nozzles, where the water droplets are sufficiently atomized before injection at both LPC and HPC inlet plenums.

GE LM6000 CGS Performance Guarantee



#### **GE ENERGY**

	<b>GUARAN</b> PROJECT: BLACK H LOCATION: V	TEE ILLS WYOMING VY, USA
KW AT GEN TERMS BTU/KW-HR, LHV (KJ/KW-HR, LHV)	38820 8451 8916 Adesoji Dairo Performance Engineer Date: 06/30/11	EMISSIONS ARE VALID FOR T2 WITHIN 0F-120F AND A GTG LOAD DOWN TO 50% AS DEFINED IN STEADY STATE CONDITIONS NOX: 25 PPMVD AT 15% O2 (51 mg/Nm3) CO: 70 PPMVD AT 15% O2 (88 mg/Nm3) VOC: 8.4 PPMVD AT 15% O2 (6 mg/Nm3) PM10: 4 LB/HR (2 kg/hr)
NOT VALID WITHOUT SIGN	NATURE	VALID UNTIL 09/28/11
BASIS OF GUARANTEE:	BASE LOAD, GAS FUEL NO	DZZLE SYSTEM
ENGINE: FUEL: FUEL SPEC: FUEL TEMP:	NO BLEED OR EXTRACTED (1) GE LM6000PF-SPRINT-2 21000Btu/lb / (48846 kJ/kg) I MID-TD-0000-1 LATEST RE SITE FUEL TEMPERATURE	25 DLE GAS TURBINE _HV, GAS FUEL (#900-3029) VISION E OF 76.9°F(25.0°C)
GENERATOR: GENERATOR OUTPUT POWER FACTOR: AMBIENT TEMP: AMBIENT RH: INLET CONDITIONING: ALTITUDE: INLET FILTER LOSS: EXHAUST LOSS:	BDAX 7-290ERJT 13.8kV, 60 Hz ≥ 1 95.0°F / (35.0°C) 20.0% CHILL TO 47.0°F / (8.3°C) A 5950.0ft / (1813.6m) ≤ 5.00 inH <sub>2</sub> O / (127.0 mmH <sub>2</sub> C) ≤ 12.00 inH <sub>2</sub> O / (304.8 mmH <sub>2</sub> )	T 95.0% RH ጋ) ₂O)
NOX CONTROL:	DLE	
ENGINE CONDITION: FIELD TEST METHODS PERFORMANCE: NOX: CO: VOC: PM10:	NEW AND CLEAN ≤ 200 SI <sup>-</sup> GE ENERGY SGTGPTM EPA METHOD 20 EPA METHOD 10 EPA METHOD 25A/18 EPA METHOD 5 / 202	TE FIRED HOURS
BASIS OF GUARANTEE IS NOT I SI VALUES ARE FOR REFERENC	FOR DESIGN, REFER TO PROJECT DRAWING CE PURPOSES ONLY.	S FOR DESIGN REQUIREMENTS.
Γ	THIS GUARANTEE SUPERSEDES ANY PREVIOUS GUARANTEES PRESENTED	

719324-100-CGER-2011-55015508-1

## **GE ENERGY**



## **Conditions for VOC Emissions Guarantee**

- 1. Fuel must meet GE specification MID-TD-000-01.
- 2. The timing of test to coincide with lowest site ambient VOCs levels.
- 3. Gas turbine must run for a minimum of 300 total fired hours at base load prior to testing.
- 4. Gas turbine inlet and exhaust system must be free of any dirt,sand,mud,rust,oil or any other contaminates.
- 5. Re-testing (at purchaser's expense) must be allowed, if required.
- 6. GE receives a copy of the final test results.
- 7. A compressor wash prior to testing is highly recommended.

## **GE ENERGY**



## **Conditions for PM10 Emissions Guarantee**

- 1. Fuel must meet GE specification MID-TD-000-01.
- 2. The timing of test to coincide with lowest site ambient particulate levels.
- 3. Gas turbine must run for a minimum of 300 total fired hours at base load prior to testing.
- 4. Combustion turbine must be run for a minimum of 300 total fired hours prior to any particulate testing; combustion turbine must be operating a minimum of 3 4 hours at base load prior to PM / PM10 test run.
- 5. Gas turbine inlet and exhaust system must be free of any dirt,sand,mud,rust,oil or any other contaminates.
- 6. Sampling probe internal surfaces must be made of chemically inert and noncatalytic material such as quartz.
- 7. The filter material shall be quartz.
- 8. Probe wash shall be high purity acetone per EPA Method 5.
- 9. Re-testing (at purchaser's expense) must be allowed, if required.
- 10. GE receives a copy of the final test results.
- 11. A compressor wash prior to testing is highly recommended.
- 12. The area around the turbine is to be treated (e.g.sprayed down with water) to minimize airborne dust.



1. 2. 3. 4.

## **GE ENERGY**

## Conditions for Steady State Guarantee

Power Output (electrical)	±10.0% / Min
T2 Compressor Inlet air temperature	± 2.5°F / 5.0 Min
Heat Value - gaseous fuel per unit volume	±0.25% / Min
Pressure - gaseous fuel as supplied to engine	± 10 PSIG / 5.0 Min

Estimated Average Engine Performance NOT FOR GUARANTEE, REFER TO PROJECT F&ID FOR DESIGN



GE Energy

Performance By: Adesoji Dairo Project Info: Black Hills Wyoming

> Engine: LM6000 PF-SPRINT-25 Deck Info: G0125P - 8i6.scp Generator: BDAX 7-290ERJT 60Hz, 13.8kV, 1PF (35405) Fuel: Site Gas Fuel#900-3029, 21000 Btu/lb,LHV

Date: 06/30/2011 Time: 12:59:23 PM Version: 3.9.0

Case #	100
Ambient Conditions	05.0
Wet Bulb °F	95.0
RH, %	20.0
Altitude, ft	5950.0
Ambient Pressure, psia	11.799
Engine Inlet	
Comp Inlet Temp, °F	47.0
Conditioning	95.0 CHILL
Tons or kBtu/hr	885
Pressure Losses	
Inlet Loss, inH20	5.00
Volute Loss, inH20	4.00
Exhaust Loss, inH20	12.00
kW Gen Terms	38820
Est. Btu/kW-hr. LHV	8282
Guar. Btu/kW-hr, LHV	8451
Fuel Flow	
MMBtu/hr, LHV	321.5
lb/hr	15310
NOx Control	DLE
SPRINT	LPC
lb/hr	7069
Control Parameters	
HP Speed, RPM	10354
LP Speed, RPM	3600
PS3 - CDP, psia	369.5
T3CRF - CDT °F	945
T48IN, °R	2046
T48IN, °F	1587
Exhaust Parameters	
Temperature, °F	856.3
Ib/sec	235.2
D/III Energy Btu/s- Ref 0 °R	79113
Energy, Btu/s- Ref T2 °F	49517
Cp, Btu/lb-R	0.2733
Emissions (ESTIMATED, NOT FOR	GUARANTEE)
NOx ppmvd Ref 15% O2	25
NOx as NO2, lb/hr	32
CO ppmvd Ref 15% O2	25
CO2 lb/hr	19.03 41943 27
HC ppmvd Ref 15% O2	15
HC, lb/hr	673
	0.1 0



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Engine: LM6000 PF-SPRINT-25 Deck Info: G0125P - 8i6.scp Generator: BDAX 7-290ERJT 60Hz, 13.8kV, 1PF (35405) Fuel: Site Gas Fuel#900-3029, 21000 Btu/lb,LHV

Date: 06/30/2011 Time: 12:59:23 PM Version: 3.9.0

Exh Wght % Wet (NOT FOR USE IN ENVIRONMENTAL PERMITS)       AR     1.2435       N2     72.9173       O2     15.3205       CO2     4.9537       H20     5.5593       SO2     0.0000       CO     0.0023       HC     0.0008       NOX     0.0026       Exh Mole % Dry (NOT FOR USE IN ENVIRONMENTAL PERMITS)       AR     0.9650       N2     80.6950       O2     14.8437       CO2     3.4896       H20     0.0000       SO2     0.0000       CO2     3.4896       H20     0.00015       SO2     0.0000       CO2     3.1849       H20     8.7317       SO2     0.0000       CO2     3.1849       H20     8.7317       SO2     0.0000       CO     0.0023       Aero Energy Fuel Number     900-3029 (Black Hills Wyoming)       Volume %     Weight %       Hydrogen     0.0000     0.0000 </th <th>Case #</th> <th>100</th> <th></th>	Case #	100	
AR   1.2435     N2   72.9173     O2   15.3205     CO2   4.9537     H20   5.5593     SO2   0.0000     CO   0.0023     HC   0.0008     NOX   0.0026     Exh Mole % Dry (NOT FOR USE IN ENVIRONMENTAL PERMITS)     AR   0.9650     N2   80.6850     N2   80.6850     CO2   14.8437     CO2   3.4896     H20   0.0000     SO2   0.0000     SO2   0.0000     CO2   3.4896     H20   0.0026     Exh Mole % Wet (NOT FOR USE IN ENVIRONMENTAL PERMITS)     AR   0.8808     N2   73.6490     O2   13.5476     CO2   3.1849     H20   8.7317     SO2   0.0001     CO   0.0023     HC   0.0014     NOX   0.0023     HC   0.0000     Volume % Weight %     Hydrogen   0.0000	Exh Wght % Wet (NOT FOR USE	IN ENVIRON	MENTAL PERMITS)
N2     72.9173       O2     15.3205       CO2     4.9537       H20     5.5593       SO2     0.0000       CO     0.0023       HC     0.0008       NOX     0.0026       Exh Mole % Dry (NOT FOR USE IN ENVIRONMENTAL PERMITS)       AR     0.9650       O2     14.8437       CO2     3.4896       H20     0.0000       SO2     0.0000       SO2     0.0000       SO2     0.0000       SO2     0.0000       SO2     0.00015       NOX     0.0026       Exh Mole % Wet (NOT FOR USE IN ENVIRONMENTAL PERMITS)       AR     0.8806       N2     73.6490       O2     13.5476       CO2     3.1849       H20     8.7317       SO2     0.0000       CO     0.0023       HC     0.0014       NOX     0.0023       Her energy Fuel Number     900-3029 (Black Hills Wyoming)       Volume % Weig	AR	1,2435	-,
O2     15.3205       CO2     4.9537       H20     5.5593       SO2     0.0000       CO     0.0023       NCX     0.0026       Exh Mole % Dry (NOT FOR USE IN ENVIRONMENTAL PERMITS)       AR     0.9650       N2     80.6950       O2     14.8437       CO2     3.4896       H20     0.0000       SO2     0.0000       CO2     3.4896       H20     0.00015       SO2     0.0000       CO2     3.1849       H20     0.0026       Exh Mole % Wet (NOT FOR USE IN ENVIRONMENTAL PERMITS)       AR     0.8808       N2     73.6490       O2     13.5476       CO2     0.00023       HC     0.0014       NOX     0.0023       HC     0.0000       CO2     0.3675       Ethane     3.0123       Aero Energy Fuel Number     900-3029 (Black Hills Wyoming)       Varogen     0.0000       Pr	N2	72.9173	
CO2   4.9537     H20   5.5593     SO2   0.0000     CO   0.0023     HC   0.0026     Exh Mole % Dry (NOT FOR USE IN ENVIRONMENTAL PERMITS)     AR   0.9650     N2   80.6950     CO2   14.8437     CO2   3.4896     H20   0.0000     SO2   0.0000     CO2   14.8437     CO2   0.0000     SO2   0.0000     SO2   0.0000     SO2   0.00015     NOX   0.0026     Exh Mole % Wet (NOT FOR USE IN ENVIRONMENTAL PERMITS)     AR   0.8808     N2   73.6490     O2   3.1849     H20   8.7317     SO2   0.0000     CO   0.0023     Aero Energy Fuel Number   90-3029 (Black Hills Wyoming)     Volume % Weight %     Hydrogen   0.0000   0.0000     Molthane   95.5018   90.7897     Ethane   3.0123   5.3675     Ethylene   0.0000	02	15.3205	
H20   5.5593     SO2   0.0000     CO   0.0023     HC   0.0008     NOX   0.0026     Exh Mole % Dry (NOT FOR USE IN ENVIRONMENTAL PERMITS)     AR   0.9650     N2   80.6655     O2   14.8437     CO2   3.4896     H20   0.0000     SO2   0.0000     CO2   3.4896     H20   0.0026     Exh Mole % Wet (NOT FOR USE IN ENVIRONMENTAL PERMITS)     AR   0.8808     NOX   0.0026     Exh Mole % Wet (NOT FOR USE IN ENVIRONMENTAL PERMITS)     AR   0.8808     NQX   0.0023     CO2   3.1849     H20   8.7317     SO2   0.0000     CO   0.0023     Are Cenergy Fuel Number   900-3029 (Black Hills Wyoming)     Volume %   Weight %     Hydrogen   0.0000   0.0000     MOX   0.0023      Are Energy Fuel Number   90.321 (5.3675     Ethylene   0.0000   0.0000 <tr< td=""><td>CO2</td><td>4.9537</td><td></td></tr<>	CO2	4.9537	
SO2     0.0000       CO     0.0023       HC     0.0008       NOX     0.0026       Exh Mole % Dry (NOT FOR USE IN ENVIRONMENTAL PERMITS)       AR     0.9650       N2     80.6950       O2     14.8437       CO2     3.4896       H20     0.0000       SO2     0.0000       SO2     0.0000       CO2     3.4896       H20     0.00026       Exh Mole % Wet (NOT FOR USE IN ENVIRONMENTAL PERMITS)       AR     0.8808       N2     73.6490       O2     13.5476       CO2     3.1849       H20     8.7317       SO2     0.0001       CO2     3.1849       H20     8.7317       SO2     0.0000       CO2     0.0001       NOX     0.0023       Aero Energy Fuel Number     90-3029 (Black Hills Wyoming)       Volume % Weight %     Hydrogen       Hydrogen     0.0000     0.0000       NOX     0.0000 <td>H20</td> <td>5,5593</td> <td></td>	H20	5,5593	
CO     0.0023       HC     0.0008       NOX     0.0026       Exh Mole % Dry (NOT FOR USE IN ENVIRONMENTAL PERMITS)     AR       AR     0.9650       N2     80.6950       O2     14.8437       CO2     3.4896       H20     0.0000       SO2     0.0000       SO2     0.0000       CO     0.0026       Exh Mole % Wet (NOT FOR USE IN ENVIRONMENTAL PERMITS)       AR     0.8808       NOX     0.0026       Exh Mole % Wet (NOT FOR USE IN ENVIRONMENTAL PERMITS)       AR     0.8808       NOX     0.0026       Exh Mole % Wet (NOT FOR USE IN ENVIRONMENTAL PERMITS)       AR     0.8808       NOX     0.0023       CO2     3.1849       H20     8.7317       SO2     0.0000       CO     0.0023       HC     0.0014       NOX     0.0023       Here     9.03029 (Black Hills Wyoming)       Volume % Weight %       Hydrogen     0.0000	SO2	0.0000	
HC     0.0008       NOX     0.0026       Exh Mole % Dry (NOT FOR USE IN ENVIRONMENTAL PERMITS)     AR       AR     0.9650       N2     80.6950       O2     14.8437       CO2     3.4896       H20     0.0000       SO2     0.0000       CO2     0.0000       CO     0.0026       HC     0.0015       NOX     0.0026       Exh Mole % Wet (NOT FOR USE IN ENVIRONMENTAL PERMITS)       AR     0.8808       N2     73.6490       O2     13.5476       CO2     3.1849       H20     8.7317       SO2     0.0000       CO     0.0023       HC     0.0014       NOX     0.0023       Hero Energy Fuel Number     900-3029 (Black Hills Wyoming)       Volume %     Weight %       Hydrogen     0.0000     0.0000       Motane     95.5018     90.7897       Ethane     3.0123     5.3675       Ethylene     0.00	00	0.0023	
NOX     0.0026       Exh Mole % Dry (NOT FOR USE IN ENVIRONMENTAL PERMITS)     AR     0.9650       N2     80.6950     02       N2     80.6950     02       Q2     14.8437     CO2       CO2     3.4896     1420       Q2     0.0000     SO2       CO2     3.4896     1420       NOX     0.0026     14.8437       CO2     0.0000     SO2       CO2     0.0000     SO2       NOX     0.0026     14.8437       Exh Mole % Wet (NOT FOR USE IN ENVIRONMENTAL PERMITS)     AR       AR     0.8808     N2       CO2     3.1849     120       S02     0.0000     CO000       CO2     3.1849     120       S02     0.0000     0.0000       CO     0.0023     140       NOX     0.0023     140       Aero Energy Fuel Number     90-3029 (Black Hills Wyoming) Wolume %       Hydrogen     0.0000     0.0000       Methane     9.5018 <td< td=""><td>HC</td><td>0.0008</td><td></td></td<>	HC	0.0008	
Exh Mole % Dry (NOT FOR USE IN ENVIRONMENTAL PERMITS)       AR     0.9650       N2     80.6950       O2     14.8437       CO2     34.896       H20     0.0000       SO2     0.0000       SO2     0.0000       SO2     0.0006       CO2     0.0026       HC     0.0015       NOX     0.0026       Exh Mole % Wet (NOT FOR USE IN ENVIRONMENTAL PERMITS)       AR     0.8808       N2     73.6490       O2     3.1849       H20     8.7317       SO2     0.0000       CO     0.0023       HC     0.0014       NOX     0.0023       HC     0.0000       CO     0.0000       Methane     95.5018       90.7897     90       Ethane     3.0123       Solder     9.0000       Weight %     900       Propylene     0.0000       Butylene     0.0000       Butylene     0.0000 <td>NOX</td> <td>0.0026</td> <td></td>	NOX	0.0026	
AR     0.9000       N2     80.6950       O2     14.8437       CO2     3.4896       H20     0.0000       SO2     0.0000       SO2     0.0000       CO2     0.0006       CO2     0.0006       CO2     0.0006       CO2     0.0006       CO2     0.0006       CO2     0.0006       CO2     3.6490       O2     13.5476       CO2     3.1849       H20     8.7317       SO2     0.0000       CO     0.0023       HC     0.00014       NOX     0.0023       HC     0.0000       CO2     0.0000       CO3     0.0000       Volume % Weight %       Hydrogen     0.0000       MOX     0.0000       Volume % Using 1.2119       Propane     0.4638       1.2119       Propylene     0.0000       0.0000     0.00000	Exh Mole % Dry (NOT FOR USE		IENTAL PERMITS)
N2     00.0590       02     14.8437       CO2     3.4896       H20     0.0000       SO2     0.0000       CO2     3.4896       H20     0.0026       HC     0.0026       Exh Mole % Wet (NOT FOR USE IN ENVIRONMENTAL PERMITS)       AR     0.8808       N2     73.6490       O2     3.1849       H20     8.7317       SO2     0.0000       CO     0.0023       HC     0.0014       NOX     0.0023       Aero Energy Fuel Number     900-3029 (Black Hills Wyoming)       Volume % Weight %       Hydrogen     0.0000       NOX     0.0023       Aero Energy Fuel Number     900-3029 (Black Hills Wyoming)       Volume % Weight %       Hydrogen     0.0000       NOX     0.0023       Ethane     3.0123       S.3675     Ethylene       Butadiene     0.1190       Propylene     0.0000       Outoo     0.0000		0.9650	
O2     14.0437       CO2     3.4896       H20     0.0000       SO2     0.0000       CO     0.0026       HC     0.0015       NOX     0.0026       Exh Mole % Wet (NOT FOR USE IN ENVIRONMENTAL PERMITS)       AR     0.8808       N2     73.6490       O2     13.5476       CO2     3.1849       H20     8.7317       SO2     0.0000       CO     0.0023       HC     0.0014       NOX     0.0023       Aero Energy Fuel Number     900-3029 (Black Hills Wyoming)       Volume % Weight %       Hydrogen     0.0000       NOX     0.0023       Aero Energy Fuel Number     900-3029 (Black Hills Wyoming)       Volume % Weight %     NOX       Hydrogen     0.0000       Hoton     90.000       Heydrogen     0.0000       Propare     0.4638       Propare     0.4638       Propylene     0.0000       Butadiene <t< td=""><td></td><td>80.6950</td><td></td></t<>		80.6950	
CO2     3.4996       H20     0.0000       SO2     0.0000       CO     0.0026       HC     0.0015       NOX     0.0026       Exh Mole % Wet (NOT FOR USE IN ENVIRONMENTAL PERMITS)       AR     0.808       N2     73.6490       O2     13.5476       CO2     3.1849       H20     8.7317       SO2     0.0000       CO     0.0023       HC     0.0114       NOX     0.0023       Aero Energy Fuel Number     900-3029 (Black Hills Wyoming)       Volume %     Weight %       Hydrogen     0.0000       Methane     95.5018     90.7897       Ethane     3.0123     5.3675       Ethylene     0.0000     0.0000       Propane     0.4638     1.2119       Propylene     0.0000     0.0000       Butalene     0.1190     0.4099       Butylene     0.0000     0.0000       Butadiene     0.0000     0.0000	02	14.0437	
P20     0.0000       SO2     0.0000       CO     0.0026       HC     0.0026       Exh Mole % Wet (NOT FOR USE IN ENVIRONMENTAL PERMITS)       AR     0.8808       N2     73.6490       O2     13.5476       CO2     3.1849       H20     8.7317       SO2     0.0000       CO     0.0023       HC     0.0014       NOX     0.0023       Acro Energy Fuel Number     900-3029 (Black Hills Wyoming)       Volume % Weight %       Hydrogen     0.0000       Motx     0.0000       Methane     95.5018       90.7897     Ethane       Sold 12     5.3675       Ethylene     0.0000       Propylene     0.0000       Outono     0.0000       Butane     0.1190       Propylene     0.0000       Butadiene     0.0000       Porton Dioxide     0.0000       Cyclopentane     0.0000       Heptane     0.0000 <td></td> <td>3.4896</td> <td></td>		3.4896	
SO2     0.0000       CO     0.0026       HC     0.0015       NOX     0.0026       Exh Mole % Wet (NOT FOR USE IN ENVIRONMENTAL PERMITS)       AR     0.8808       N2     73.6490       O2     13.5476       CO2     3.1849       H20     8.7317       SO2     0.0000       CO     0.0023       HC     0.0014       NOX     0.0023       Aero Energy Fuel Number     900-3029 (Black Hills Wyoming)       Volume % Weight %       Hydrogen     0.0000       Mox     0.0000       Propane     0.4638       1.2119     Propylene       Butylene     0.0000       Butylene     0.0000       Butylene     0.0000       Butylene     0.0000       Ston Dioxide     0.0000       Carbon Monoxide     0.0000       Cyclopentane     0.0000       Hytergen     0.0000       Carbon Dioxide     0.6458       Nitrogen     0.220	H20	0.0000	
CO     0.0026       HC     0.0015       NOX     0.0026       Exh Mole % Wet (NOT FOR USE IN ENVIRONMENTAL PERMITS)       AR     0.8808       N2     73.6490       O2     13.5476       CO2     3.1849       H20     8.7317       SO2     0.0000       CO     0.0023       Aero Energy Fuel Number     900-3029 (Black Hills Wyoming)       Volume % Weight %       Hydrogen     0.0000       MOX     0.0000       Methane     95.5018       90.7897     Ethane       Softs     5.3675       Ethylene     0.0000       Propane     0.4638       Propylene     0.0000       Butylene     0.0000       Butylene     0.0000       Butylene     0.0000       Butylene     0.0000       Horono     0.0000       Propylene     0.0000       Butylene     0.0000       Butylene     0.0000       Olopoo     0.0000 <	SU2	0.0000	
HC     0.0015 NOX       NOX     0.0026       Exh Mole % Wet (NOT FOR USE IN ENVIRONMENTAL PERMITS) AR     0.8008       AQ     73.6490       O2     13.5476       CO2     3.1849       H20     8.7317       SO2     0.0000       CO     0.0023       HC     0.0014       NOX     0.0023       HC     0.0014       NOX     0.0023       HC     0.0000       Kero Energy Fuel Number     900-3029 (Black Hills Wyoming)       Volume %     Weight %       Hydrogen     0.0000       Methane     95.5018       90.7897     Ethane       Ethylene     0.0000       Propane     0.4638       1.2119     Propylene       Propylene     0.0000       Butalene     0.1190       Stoodo     0.0000       Pentane     0.0240       Cyclopentane     0.0000       Hylene     0.0000       Butadiene     0.0000 <td< td=""><td></td><td>0.0026</td><td></td></td<>		0.0026	
Non     0.0020       Exh Mole % Wet (NOT FOR USE IN ENVIRONMENTAL PERMITS) AR     0.8808       N2     73.6490       O2     13.5476       CO2     3.1849       H20     8.7317       SO2     0.0000       CO     0.0023       HC     0.0014       NOX     0.0023       Aero Energy Fuel Number     900-3029 (Black Hills Wyoming)       Volume % Weight %       Hydrogen     0.0000       Methane     95.5018       90.7897       Ethane     3.0123       5.3675     Ethylene       Propylene     0.0000       Methane     95.5018       Propylene     0.0000       Butatiene     0.1190       Propylene     0.0000       Butatiene     0.0135       Uppentane     0.0000       Quoto     0.0000       Pentane     0.0000       Oydopentane     0.0000       Quoto     0.0000       Cyclopentane     0.0240       Quoto	NOX	0.0015	
Exh Mole % Wet (NOT FOR USE IN ENVIRONMENTAL PERMITS)       AR     0.8808       N2     73.6490       O2     13.5476       CO2     3.1849       H20     8.7317       SO2     0.0000       CO     0.0023       HC     0.0114       NOX     0.0023       Aero Energy Fuel Number     900-3029 (Black Hills Wyoming)       Volume %     Weight %       Hydrogen     0.0000       Methane     95.5018     90.7897       Ethane     3.0123     5.3675       Ethylene     0.0000     0.0000       Propane     0.4638     1.2119       Propylene     0.0000     0.0000       Butalene     0.1190     0.4099       Butylene     0.0000     0.0000       Butadiene     0.0000     0.0000       Heptane     0.0000     0.0000       Carbon Monoxide     0.0000     0.0000       Carbon Monoxide     0.0000     0.0000       Carbon Dioxide     0.6458     1.6843 <td></td> <td>0.0020</td> <td></td>		0.0020	
N2     73.6490       O2     13.5476       CO2     3.1849       H20     8.7317       SO2     0.0000       CO     0.0023       HC     0.014       NOX     0.0023       Aero Energy Fuel Number     900-3029 (Black Hills Wyoming) Volume % Weight %       Hydrogen     0.0000       Methane     95.5018       90.7897     Ethane       Ethane     3.0123       S.3675     Ethylene       Propane     0.4638       Propylene     0.0000       Butylene     0.0000       Butylene     0.0000       Butylene     0.0000       Butylene     0.0000       Hexane     0.0126       Cyclopentane     0.0000       Hexane     0.0135       Mitrogen     0.2200       Oloxide     0.6458       Vater Vapor     0.0000       Cyclopentane     0.0000       Mitrogen     0.2200       Oxide     0.6458       Nitrogen	Exh Mole % Wet (NOT FOR USE	IN ENVIRONI	MENTAL PERMITS)
12.     73.5476       O2     13.5476       CO2     3.1849       H20     8.7317       SO2     0.0000       CO     0.0023       HC     0.0014       NOX     0.0023       HC     0.0000       Weight %       Hydrogen     0.0000       Methane     95.5018       90.7897       Ethane     3.0123       S.3675       Ethylene     0.0000       Propylene     0.0000       0.0000     0.0000       Butylene     0.0000       Butylene     0.0000       O220     0.0000       Butane     0.1190       Pentane     0.0240       Cyclopentane     0.0000       Heptane     0.0000       Cyclopentane     0.0000       Heptane     0.0000       Outod     0.0000       Cyclopentane     0.0000       Nitrogen     0.2200       Oxodo     0.0000       Cyclopentane	N2	73 6490	
CO2     3.1849       H20     8.7317       SO2     0.0000       CO     0.0023       HC     0.0014       NOX     0.0023       Aero Energy Fuel Number     900-3029 (Black Hills Wyoming)       Volume % Weight %       Hydrogen     0.0000       Mydrogen     0.0000       Methane     95.5018       90.7897     Ethane       3.0123     5.3675       Ethylene     0.0000       Propane     0.4638       0.1190     0.4099       Butylene     0.0000       Butylene     0.0000       Stoppentane     0.0135       Ootool     0.0000       Petane     0.0000       Cyclopentane     0.0000       Heytane     0.0000       Carbon Monoxide     0.0000       Carbon Dioxide     0.6458       Heytane     0.0000       Ox000     0.0000       Carbon Dioxide     0.0000       Ox000     0.0000       Auter Vapor	02	13 5476	
OO2     5.7317       SO2     0.0000       CO     0.0023       HC     0.0014       NOX     0.0023       Aero Energy Fuel Number     900-3029 (Black Hills Wyoming)       Volume % Weight %       Hydrogen     0.0000       Methane     95.5018       90.7897       Ethane     3.0123       S.3675       Ethylene     0.0000       Propane     0.4638       Propylene     0.0000       Butalene     0.1190       Butylene     0.0000       Butadiene     0.0000       Popane     0.4638       Heptane     0.0000       Potopol     0.0000       Butadiene     0.1190       Outod     0.0000       Pentane     0.0240       Volupentane     0.0000       Outod     0.0000       Carbon Monoxide     0.0000       Carbon Dioxide     0.6458       Nitrogen     0.2200       Vater Vapor     0.0000 <td< td=""><td>CO2</td><td>3 1849</td><td></td></td<>	CO2	3 1849	
Los     0.1011       SO2     0.0000       CO     0.0023       HC     0.0014       NOX     0.0023       Aero Energy Fuel Number     900-3029 (Black Hills Wyoming) Volume % Weight %       Hydrogen     0.0000       Methane     95.5018       90.7897     Ethane       S023     5.3675       Ethylene     0.0000       Propane     0.4638       Propylene     0.0000       Butylene     0.0000       Butylene     0.0000       Butylene     0.0000       Butylene     0.0000       Butadiene     0.0000       Pentane     0.0240       Cyclopentane     0.0000       Heptane     0.0000       Carbon Monoxide     0.0000       Carbon Monoxide     0.0000       Carbon Dioxide     0.6458       Nitrogen     0.2200       Oxygen     0.0000       Mydrogen Sulfide     0.0000       Mydrogen Sulfide     0.0000       Murogen Sulfide	H20	8 7317	
CO2     0.0023       HC     0.0014       NOX     0.0023       Aero Energy Fuel Number     900-3029 (Black Hills Wyoming)       Volume % Weight %       Hydrogen     0.0000       Methane     95.5018       90.7897       Ethane     3.0123       5.3675       Ethylene     0.0000       Propylene     0.0000       Butane     0.1190       904099     Butylene       0.0000     0.0000       Butane     0.1190       900400     0.0000       Pentane     0.0240       0.0023     0.0000       Pentane     0.0000       Carbon Monoxide     0.0000       Carbon Monoxide     0.0000       Outoon     0.0000       Carbon Dioxide     0.6458       Nitrogen     0.2200       Vater Vapor     0.0000       Outoo     0.0000       Arbono     0.0000       Vater Vapor     0.0000       Outoo     0.0000	SO2	0.0000	
OC     0.0014       NOX     0.0023       Aero Energy Fuel Number     900-3029 (Black Hills Wyoming)       Volume % Weight %       Hydrogen     0.0000       Methane     95.5018       90.7897       Ethane     3.0123       Ethane     3.0123       S.3675       Ethylene     0.0000       Propane     0.4638       0.1190     0.4099       Butylene     0.0000       Butylene     0.0000       Butylene     0.0000       Outodo     0.0000       Pertane     0.0240       Cyclopentane     0.0000       Heytane     0.0000       Carbon Monoxide     0.0000       Carbon Dioxide     0.6458       Heytane     0.0000       Carbon Dioxide     0.0000       Outodo     0.0000       Vater Vapor     0.0000       Outodo     0.0000       Mytogen Sulfide     0.0000       Outodo     0.0000       Heytane     0.0000 <td>0</td> <td>0.0000</td> <td></td>	0	0.0000	
NOX     0.0013       Aero Energy Fuel Number     900-3029 (Black Hills Wyoming) Volume % Weight %       Hydrogen     0.0000     0.0000       Methane     95.5018     90.7897       Ethane     3.0123     5.3675       Ethylene     0.0000     0.0000       Propane     0.4638     1.2119       Propylene     0.0000     0.0000       Butalene     0.1190     0.4039       Butylene     0.0000     0.0000       Butalene     0.0000     0.0000       Pentane     0.0240     0.1026       Cyclopentane     0.0000     0.0000       Heytane     0.0000     0.0000       Carbon Monoxide     0.0000     0.0000       Carbon Dioxide     0.6458     1.6843       Nitrogen     0.2200     0.3652       Water Vapor     0.0000     0.0000       Oxygen     0.0000     0.0000       Auge     0.0000     0.0000       Mitrogen Sulfide     0.0000     0.0000       Btu/ls, LHV     21000	HC	0.0020	
Aero Energy Fuel Number     900-3029 (Black Hills Wyoming) Volume % Weight %       Hydrogen     0.0000     0.0000       Methane     95.5018     90.7897       Ethane     3.0123     5.3675       Ethylene     0.0000     0.0000       Propane     0.4638     1.2119       Propylene     0.0000     0.0000       Butalene     0.1190     0.4099       Butylene     0.0000     0.0000       Pentane     0.0240     0.1026       Cyclopentane     0.0000     0.0000       Heytane     0.0000     0.0000       Carbon Monoxide     0.0000     0.0000       Carbon Dioxide     0.6458     1.6843       Nitrogen     0.2200     0.3652       Water Vapor     0.0000     0.0000       Chydogen Sulfide     0.0000     0.0000       Murogen     2200     0.3652       Water Vapor     0.0000     0.0000       Ammonia     0.0000     0.0000       Btu/ls, LHV     21000     21000       Btu/scf, LHV	NOX	0.0023	
Volume %     Weight %       Hydrogen     0.0000     0.0000       Methane     95.5018     90.7897       Ethane     3.0123     5.3675       Ethylene     0.0000     0.0000       Propane     0.4638     1.2119       Propylene     0.0000     0.0000       Butylene     0.0000     0.0000       Butylene     0.0000     0.0000       Butylene     0.0000     0.0000       Butylene     0.0000     0.0000       Pentane     0.0220     0.3682       Heptane     0.0000     0.0000       Carbon Dioxide     0.0000     0.0000       Carbon Dioxide     0.6458     1.6843       Nitrogen     0.2200     0.3652       Water Vapor     0.0000     0.0000       Armonia     0.0000     0.0000       Hydrogen Sulfide     0.0000     0.0000       Btu/scf, LHV     23274     Etu/scf, HHV       Btu/scf, LHV     23274     Fuel Temp, °F       FG.9     NOx Scalar     1.01	Aero Energy Fuel Number	900-3029 (BI	ack Hills Wyoming)
Hydrogen     0.0000     0.0000       Methane     95.5018     90.7897       Ethane     3.0123     5.3675       Ethylene     0.0000     0.0000       Propane     0.4638     1.2119       Propylene     0.0000     0.0000       Butalene     0.1190     0.4039       Butylene     0.0000     0.0000       Butalene     0.0000     0.0000       Propylene     0.0000     0.0000       Butalene     0.0000     0.0000       Pentane     0.0240     0.1026       Cyclopentane     0.0000     0.0000       Heytane     0.0000     0.0000       Carbon Monoxide     0.0000     0.0000       Carbon Dioxide     0.6458     1.6843       Nitrogen     0.2200     0.3652       Water Vapor     0.0000     0.0000       Ammonia     0.0000     0.0000       Btu/scf, LHV     21000     1.026       Btu/scf, HHV     1037.6     1.011       Specific Gravity     0.58	Acro Energy Fuer Humber	Volume %	Weight %
National     95.5018     90.7897       Ethane     3.0123     5.3675       Ethylene     0.0000     0.0000       Propane     0.4638     1.2119       Propylene     0.0000     0.0000       Butale     0.1190     0.4099       Butylene     0.0000     0.0000       Pentane     0.0240     0.1026       Cyclopentane     0.0000     0.0000       Heptane     0.0000     0.0000       Carbon Monoxide     0.0000     0.0000       Carbon Dioxide     0.6458     1.6843       Nitrogen     0.2200     0.3652       Water Vapor     0.0000     0.0000       Oxygen     0.0000     0.0000       Ammonia     0.0000     0.0000       Btu/scf, LHV     21000     1037.6       Btu/scf, HHV     1037.6     1011       Specific Gravity     0.58     58	Hydrogen	0 0000	0,0000
Institution     00.001     00.000       Ethane     3.0123     5.3675       Ethylene     0.0000     0.0000       Propylene     0.4638     1.2119       Propylene     0.0000     0.0000       Butane     0.1190     0.4099       Butylene     0.0000     0.0000       Propylene     0.0000     0.0000       Butane     0.1190     0.4099       Butylene     0.0000     0.0000       Pentane     0.0240     0.1026       Cyclopentane     0.0000     0.0000       Heptane     0.0000     0.0000       Carbon Dioxide     0.6458     1.6843       Nitrogen     0.2200     0.3652       Water Vapor     0.0000     0.0000       Ammonia     0.0000     0.0000       Hydrogen Sulfide     0.0000     0.0000       Btu/scf, LHV     21000     Btu/scf, HHV       Btu/scf, HHV     1037.6     Btu/sc, HHV       NOx Scalar     1.011     Specific Gravity	Methane	95 5018	90 7897
Ensitio     0.0100     0.0000       Propane     0.4638     1.2119       Propylene     0.0000     0.0000       Butane     0.1190     0.4099       Butylene     0.0000     0.0000       Butylene     0.0000     0.0000       Propylene     0.0000     0.0000       Butylene     0.0000     0.0000       Pertane     0.0240     0.1026       Cyclopentane     0.0000     0.0000       Heptane     0.0000     0.0000       Carbon Dioxide     0.0000     0.0000       Cyagen     0.2200     0.3652       Water Vapor     0.0000     0.0000       Armonia     0.0000     0.0000       Btu/lsc, LHV     21000     1.026       Btu/lsc, LHV     23274     1.011       Specific Gravity     0.58     5.8	Ethane	3 0123	5 3675
Entypicity     0.0000     0.0000       Propane     0.4638     1.2119       Propylene     0.0000     0.0000       Butane     0.1190     0.4099       Butylene     0.0000     0.0000       Butalene     0.0000     0.0000       Pentane     0.0240     0.1026       Cyclopentane     0.0000     0.0000       Heptane     0.0000     0.0000       Carbon Monoxide     0.0000     0.0000       Carbon Dioxide     0.6458     1.6843       Nitrogen     0.2200     0.3652       Water Vapor     0.0000     0.0000       Oxygen     0.0000     0.0000       Ammonia     0.0000     0.0000       Btu/ls, LHV     21000     1037.6       Btu/ls, LHV     23274     1041       Specific Gravity     0.58     58	Ethylene	0.0000	0.0000
Inspiration     0.1000     0.1000       Propylene     0.0000     0.0000       Butane     0.1190     0.4099       Butylene     0.0000     0.0000       Butane     0.0000     0.0000       Butane     0.0000     0.0000       Pentane     0.0240     0.1026       Cyclopentane     0.0000     0.0000       Hexane     0.0135     0.0689       Heptane     0.0000     0.0000       Carbon Monoxide     0.0000     0.0000       Carbon Dioxide     0.6458     1.6843       Nitrogen     0.2200     0.3652       Water Vapor     0.0000     0.0000       Oxygen     0.0000     0.0000       Ammonia     0.0000     0.0000       Btu/lscf, LHV     21000     1037.6       Btu/lscf, HHV     1037.6     10411       But/lscf, HHV     23274     1041       Fuel Temp, °F     76.9     NOx Scalar       NOx Scalar     1.011     Specific Gravity	Propane	0.4638	1 2119
Butane     0.1190     0.4099       Butylene     0.0000     0.0000       Butadiene     0.0000     0.0000       Pentane     0.0240     0.1026       Cyclopentane     0.0000     0.0000       Heptane     0.0135     0.0689       Heptane     0.0000     0.0000       Carbon Monoxide     0.6458     1.6843       Nitrogen     0.2200     0.3652       Water Vapor     0.0000     0.0000       Oxygen     0.0000     0.0000       Hydrogen Sulfide     0.0000     0.0000       Hydrogen Sulfide     0.0000     0.0000       Btu/ls, LHV     21000     1037.6       Btu/ls, HHV     1037.6     10411       Specific Gravity     0.58     1.011	Propylene	0.0000	0.0000
Butylene     0.0000     0.0000       Butylene     0.0000     0.0000       Butylene     0.0000     0.0000       Pentane     0.0240     0.1026       Cyclopentane     0.0000     0.0000       Hexane     0.0135     0.0689       Heptane     0.0000     0.0000       Carbon Dioxide     0.0000     0.0000       Carbon Dioxide     0.6458     1.6843       Nitrogen     0.2200     0.3652       Water Vapor     0.0000     0.0000       Cxygen     0.0000     0.0000       Hydrogen Sulfide     0.0000     0.0000       Ammonia     0.0000     0.0000       Btu/lscf, LHV     21000     Btu/scf, LHV       Btu/lscf, LHV     1037.6     Btu/lsch, HHV       Btu/lsch, HHV     23274     Fuel Temp, °F       For Temp, °F     76.9     NOx Scalar       NOx Scalar     1.011     Specific Gravity	Butane	0.1190	0.4099
Butadiene     0.0000     0.0000       Pentane     0.0240     0.1026       Cyclopentane     0.0000     0.0000       Hexane     0.0135     0.0689       Heptane     0.0000     0.0000       Carbon Monoxide     0.0000     0.0000       Carbon Dioxide     0.6458     1.6843       Nitrogen     0.2200     0.3652       Water Vapor     0.0000     0.0000       Oxygen     0.0000     0.0000       Ammonia     0.0000     0.0000       Btu/ls, LHV     21000     1.011       Stur/ls, HHV     1037.6     1.011       Specific Gravity     0.58     1.011	Butylene	0.0000	0.0000
Pentane     0.0240     0.1026       Cyclopentane     0.0000     0.0000       Hexane     0.0135     0.0689       Heptane     0.0000     0.0000       Carbon Monoxide     0.0000     0.0000       Carbon Dioxide     0.6458     1.6843       Nitrogen     0.2000     0.0000       Oxygen     0.0000     0.0000       Murogen Sulfide     0.0000     0.0000       Ammonia     0.0000     0.0000       Btu/lb, LHV     21000     1037.6       Btu/lscf, LHV     1037.6     1047.6       Btu/lscf, LHV     23274     Fuel Temp, °F       Fuel Temp, °F     76.9     NOx Scalar       NOx Scalar     1.011     Specific Gravity	Butadiene	0.0000	0.0000
Cyclopentane     0.0000     0.0000       Hexane     0.0135     0.0689       Heptane     0.0000     0.0000       Carbon Monoxide     0.0000     0.0000       Carbon Dioxide     0.6458     1.6843       Nitrogen     0.2200     0.3652       Water Vapor     0.0000     0.0000       Oxygen     0.0000     0.0000       Hydrogen Sulfide     0.0000     0.0000       Ammonia     0.0000     0.0000       Btu/scf, LHV     21000     Btu/scf, LHV       Btu/scf, LHV     1037.6     Btu/lb, HHV       Stu/lb, HHV     23274     Fuel Temp, °F       NOx Scalar     1.011     Specific Gravity	Pentane	0 0240	0 1026
b) solution     b) solution       Hexane     0.0135     0.0689       Heptane     0.0000     0.0000       Carbon Monoxide     0.0000     0.0000       Carbon Dioxide     0.6458     1.6843       Nitrogen     0.2200     0.3652       Water Vapor     0.0000     0.0000       Oxygen     0.0000     0.0000       Hydrogen Sulfide     0.0000     0.0000       Ammonia     0.0000     0.0000       Btu/lsc, LHV     21000     Btu/scf, LHV       Btu/lsc, HHV     1037.6     Btu/lsc, HHV       Btu/lsb, HHV     23274     Fuel Temp, °F       Yeal Temp, °F     76.9     NOx Scalar       NOx Scalar     1.011     Specific Gravity	Cyclopentane	0.0000	0.0000
Heptane     0.0000     0.0000       Carbon Monoxide     0.0000     0.0000       Carbon Dioxide     0.6458     1.6843       Nitrogen     0.2200     0.3652       Water Vapor     0.0000     0.0000       Oxygen     0.0000     0.0000       Hydrogen Sulfide     0.0000     0.0000       Ammonia     0.0000     0.0000       Btu/lb, LHV     21000     1037.6       Btu/lscf, LHV     1037.6     1047.6       Btu/lb, HHV     23274     Fuel Temp, °F       Yeel Temp, °F     76.9     NOx Scalar       1.011     Specific Gravity     0.58	Hexane	0.0135	0.0689
Nitrogen     0.0000     0.0000       Carbon Monoxide     0.0000     0.0000       Carbon Dioxide     0.6458     1.6843       Nitrogen     0.2200     0.3652       Water Vapor     0.0000     0.0000       Oxygen     0.0000     0.0000       Hydrogen Sulfide     0.0000     0.0000       Ammonia     0.0000     0.0000       Btu/lscf, LHV     21000     Btu/scf, LHV       Btu/lscf, HHV     1037.6     Btu/lsc, HHV       Dtu/lsc, HHV     23274     Fuel Temp, °F       NOx Scalar     1.011     Specific Gravity	Hentane	0.0000	0.0000
Carbon Dioxide     0.6458     1.6843       Nitrogen     0.2200     0.3652       Water Vapor     0.0000     0.0000       Oxygen     0.0000     0.0000       Hydrogen Sulfide     0.0000     0.0000       Ammonia     0.0000     0.0000       Btu/ls, LHV     21000     Btu/scf, LHV       Btu/ls, HV     1037.6     Btu/ls, HHV       Btu/ls, HHV     23274     Fuel Temp, °F       Fuel Temp, °F     76.9     NOx Scalar       NOx Scalar     1.011     Specific Gravity	Carbon Monovide	0.0000	0.0000
Suito Bound State     0.000     1.000       Nitrogen     0.2200     0.3652       Water Vapor     0.0000     0.0000       Oxygen     0.0000     0.0000       Hydrogen Sulfide     0.0000     0.0000       Ammonia     0.0000     0.0000       Btu/ls, LHV     21000     Btu/scf, LHV       Btu/ls, HHV     1037.6     Btu/ls, HHV       Btu/ls, HHV     23274     Fuel Temp, °F       Fuel Temp, °F     76.9     NOx Scalar       NOx Scalar     1.011     Specific Gravity	Carbon Dioxide	0.6458	1 6843
Water Vapor     0.0000     0.0000       Oxygen     0.0000     0.0000       Hydrogen Sulfide     0.0000     0.0000       Ammonia     0.0000     0.0000       Btu/lo, LHV     21000     Btu/scf, LHV       Btu/lo, LHV     23274       Fuel Temp, °F     76.9       NOx Scalar     1.011       Specific Gravity     0.58	Nitrogen	0 2200	0.3652
Nation Vopen     0.0000     0.0000       Oxygen     0.0000     0.0000       Hydrogen Sulfide     0.0000     0.0000       Ammonia     0.0000     0.0000       Btu/lb, LHV     21000     0.0000       Btu/scf, LHV     936.2     0.0000       Btu/lb, HHV     1037.6     0.0000       Btu/lb, HHV     23274     0.0000       Fuel Temp, °F     76.9     0.000       NOx Scalar     1.011     Specific Gravity     0.58	Water Vapor	0.0000	0.0000
Hydrogen Sulfide     0.0000     0.0000       Ammonia     0.0000     0.0000       Btu/lsc, LHV     21000     Btu/scf, LHV       Btu/scf, LHV     936.2     Btu/scf, LHV       Btu/lsc, HHV     1037.6     Btu/lsc, HHV       NOx Scalar     1.011     Specific Gravity	Oxygen	0.0000	0.0000
Ammonia     0.0000     0.0000       Btu/ls, LHV     21000       Btu/scf, LHV     936.2       Btu/ls, HHV     1037.6       Btu/ls, HHV     23274       Fuel Temp, °F     76.9       NOx Scalar     1.011       Specific Gravity     0.58	Hydrogen Sulfide	0.0000	0.0000
Btu/lb, LHV     21000       Btu/scf, LHV     936.2       Btu/scf, HHV     1037.6       Btu/lb, HHV     23274       Fuel Temp, °F     76.9       NOx Scalar     1.011       Specific Gravity     0.58	Ammonia	0.0000	0.0000
Btu/scf, LHV     936.2       Btu/scf, HHV     1037.6       Btu/lb, HHV     23274       Fuel Temp, °F     76.9       NOx Scalar     1.011       Specific Gravity     0.58	Btu/lb_I_HV	21000	
Btu/sci, HHV     1037.6       Btu/sci, HHV     23274       Fuel Temp, °F     76.9       NOx Scalar     1.011       Specific Gravity     0.58	Btu/scf I HV	936.2	
Btu/lb, HHV     23274       Fuel Temp, °F     76.9       NOx Scalar     1.011       Specific Gravity     0.58	Btu/scf_HHV	1037 6	
Fuel Temp, °F     76.9       NOx Scalar     1.011       Specific Gravity     0.58	Btu/lb_HHV	2227/	
NOx Scalar 1.011 Specific Gravity 0.58	Fuel Temp °F	76 9	
Specific Gravity 0.58	NOx Scalar	1 011	
		0.59	

Estimated Average Engine Performance NOT FOR GUARANTEE, REFER TO PROJECT F&ID FOR DESIGN



GE Energy

Performance By: Adesoji Dairo Project Info: Black Hills Wyoming

Engine: LM6000 PF-SPRINT-25 Deck Info: G0125P - 8i6.scp Generator: BDAX 7-290ERJT 60Hz, 13.8kV, 1PF (35405) Fuel: Site Gas Fuel#900-3029, 21000 Btu/lb,LHV

Date: 06/30/2011 Time: 1:05:44 PM Version: 3.9.0

Case #	100
Ambient Conditions Dry Bulb, °C Wet Bulb, °C RH, % Altitude, m Ambient Pressure, kPa	35.0 17.7 20.0 1813.6 81.353
Engine Inlet Comp Inlet Temp, °C RH, % Conditioning Tons or kBtu/hr	8.3 95.0 CHILL 885
Pressure Losses Inlet Loss, mmH2O Volute Loss, mmH2O Exhaust Loss, mmH2O Partload % KW, Gen Terms Est. kJ/kWh, LHV Guar. kJ/kWh, LHV	127.00 101.60 304.80 <b>100</b> <b>38820</b> <b>8738</b> <b>8916</b>
<b>Fuel Flow</b> GJ/hr, LHV kg/hr	339.2 6944
NOx Control	DLE
SPRINT kg/hr	LPC 3206
Control Parameters HP Speed, RPM LP Speed, RPM PS3 - CDP, kPa T25 - HPC Inlet Temp, °C T3CRF - CDT, °C T48IN, °K T48IN, °C	10354 3600 2547.7 89.4 507 1137 864
Exhaust Parameters Temperature, °C kg/sec kg/hr Energy, KJ/s- Ref 0 °K Energy, KJ/s- Ref T2 °C Kj/kg-R	457.9 106.7 384063 83469 52243 1.1440
Emissions (ESTIMATED, NOT FOF NOx mg/Nm3 Ref 15% O2 NOx as NO2, kg/hr CO mg/Nm3 Ref 15% O2 CO, kg/hr CO2, kg/hr HC mg/Nm3 Ref 15% O2 HC, kg/hr SOX as SO2, kg/hr	R GUARANTEE) 51 15 31 8.90 19025.34 11 3.05 0.00


#### GE Energy

#### Performance By: Adesoji Dairo Project Info: Black Hills Wyoming

Engine: LM6000 PF-SPRINT-25 Deck Info: G0125P - 8i6.scp Generator: BDAX 7-290ERJT 60Hz, 13.8kV, 1PF (35405) Fuel: Site Gas Fuel#900-3029, 21000 Btu/lb,LHV

Date: 06/30/2011 Time: 1:05:44 PM Version: 3.9.0

Case #	100	
Exh Wght % Wet (NOT FOR USE		MENTAL PERMITS)
AR	1.2435	
N2	72.9173	
02	15.3205	
02	4.9537	
H20	5.5593	
SU2	0.0000	
	0.0023	
NOX	0.0008	
Exh Mole % Dry (NOT FOR USE I		IENTAL PERMITS)
AR	0.9650	
N2	80 6950	
02	14.8437	
CO2	3 4896	
H20	0.0000	
SO2	0,0000	
CO	0.0026	
HC	0.0015	
NOX	0.0026	
Exh Mole % Wet (NOT FOR USE		MENTAL PERMITS)
AR	0.8808	
N2	73.6490	
02	13.5476	
CO2	3.1849	
H20	8.7317	
SO2	0.0000	
CO	0.0023	
110	0.0044	
HC	0.0014	
NOX	0.0014	
Aero Energy Fuel Number	0.0014 0.0023 900-3029 (Bl	ack Hills Wyoming)
NOX Aero Energy Fuel Number	0.0014 0.0023 900-3029 (Bl Volume %	ack Hills Wyoming) Weight %
NOX Aero Energy Fuel Number Hydrogen	0.0014 0.0023 900-3029 (Bl Volume % 0.0000	ack Hills Wyoming) Weight % 0.0000
NOX Aero Energy Fuel Number Hydrogen Methane	0.0014 0.0023 900-3029 (Bl Volume % 0.0000 95.5018	ack Hills Wyoming) Weight % 0.0000 90.7897
HC NOX Aero Energy Fuel Number Hydrogen Methane Ethane	0.0014 0.0023 900-3029 (Bi Volume % 0.0000 95.5018 3.0123	ack Hills Wyoming) Weight % 0.0000 90.7897 5.3675
HC NOX Aero Energy Fuel Number Hydrogen Methane Ethane Ethane	0.0014 0.0023 900-3029 (Bl Volume % 0.0000 95.5018 3.0123 0.0000	ack Hills Wyoming) Weight % 0.0000 90.7897 5.3675 0.0000
HC NOX Aero Energy Fuel Number Hydrogen Methane Ethane Ethylene Propane	0.0014 0.0023 900-3029 (Bl Volume % 0.0000 95.5018 3.0123 0.0000 0.4638	ack Hills Wyoming) Weight % 0.0000 90.7897 5.3675 0.0000 1.2119
HC NOX Aero Energy Fuel Number Hydrogen Methane Ethane Ethylene Propane Propylene	0.0014 0.0023 900-3029 (Bi Volume % 0.0000 95.5018 3.0123 0.0000 0.4638 0.0000	ack Hills Wyoming) Weight % 0.0000 90.7897 5.3675 0.0000 1.2119 0.0000
HC NOX Aero Energy Fuel Number Hydrogen Methane Ethane Ethylene Propylene Butane	0.0014 0.0023 900-3029 (Bl Volume % 0.0000 95.5018 3.0123 0.0000 0.4638 0.0000 0.1190	ack Hills Wyoming) Weight % 0.0000 90.7897 5.3675 0.0000 1.2119 0.0000 0.4099
HC NOX Aero Energy Fuel Number Hydrogen Methane Ethane Ethylene Propylene Butane Butylene	0.0014 0.0023 900-3029 (Bi Volume % 0.0000 95.5018 3.0123 0.0000 0.4638 0.0000 0.1190 0.0000	ack Hills Wyoming) Weight % 0.0000 90.7897 5.3675 0.0000 1.2119 0.0000 0.4099 0.0000
HC NOX Aero Energy Fuel Number Hydrogen Methane Ethane Ethylene Propane Propylene Butane Butane Butane Butalene	0.0014 0.0023 900-3029 (Bi Volume % 0.0000 95.5018 3.0123 0.0000 0.4638 0.0000 0.1190 0.0000 0.0000	ack Hills Wyoming) Weight % 0.0000 90.7897 5.3675 0.0000 1.2119 0.0000 0.4099 0.0000 0.0000
HC NOX Aero Energy Fuel Number Hydrogen Methane Ethane Ethylene Propane Propylene Butane Butylene Butadiene Pentane	0.0014 0.0023 900-3029 (B) Volume % 0.0000 95.5018 3.0123 0.0000 0.4638 0.0000 0.4638 0.0000 0.1190 0.0000 0.0000 0.0000	ack Hills Wyoming) Weight % 0.0000 90.7897 5.3675 0.0000 1.2119 0.0000 0.4099 0.0000 0.0000 0.0000 0.1026
HC NOX Aero Energy Fuel Number Hydrogen Methane Ethane Ethylene Propylene Butane Butylene Butane Butylene Butadiene Pentane Cyclopentane	0.0014 0.0023 900-3029 (Bi Volume % 0.0000 95.5018 3.0123 0.0000 0.4638 0.0000 0.1190 0.0000 0.0000 0.0240 0.0000	ack Hills Wyoming) Weight % 0.0000 90.7897 5.3675 0.0000 1.2119 0.0000 0.4099 0.0000 0.0000 0.1026 0.0000
HC NOX Aero Energy Fuel Number Hydrogen Methane Ethane Ethylene Propylene Butane Butylene Butaliene Pentane Cyclopentane Hexane	0.0014 0.0023 900-3029 (Bi Volume % 0.0000 95.5018 3.0123 0.0000 0.4638 0.0000 0.1190 0.0000 0.0240 0.0240 0.0000 0.0135	ack Hills Wyoming) Weight % 0.0000 90.7897 5.3675 0.0000 1.2119 0.0000 0.4099 0.0000 0.0000 0.0000 0.1026 0.0000 0.00689 0.0000
HC NOX Aero Energy Fuel Number Hydrogen Methane Ethane Ethylene Propylene Butane Butane Butane Butylene Butylene Butylene Butylene Prentane Cyclopentane Hexane Heptane	0.0014 0.0023 900-3029 (Bi Volume % 0.0000 95.5018 3.0123 0.0000 0.4638 0.0000 0.1190 0.0000 0.0240 0.0000 0.0135 0.0000	ack Hills Wyoming) Weight % 0.0000 90.7897 5.3675 0.0000 1.2119 0.0000 0.4099 0.0000 0.0000 0.1026 0.0000 0.0000 0.00689 0.0000
HC NOX Aero Energy Fuel Number Hydrogen Methane Ethane Ethylene Propane Propylene Butane Butylene Butadiene Pentane Cyclopentane Hexane Heptane Carbon Monoxide	0.0014 0.0023 900-3029 (B) Volume % 0.0000 95.5018 3.0123 0.0000 0.4638 0.0000 0.1190 0.0000 0.0000 0.0000 0.0240 0.0000 0.0135 0.0000 0.0135	ack Hills Wyoming) Weight % 0.0000 90.7897 5.3675 0.0000 1.2119 0.0000 0.4099 0.0000 0.0000 0.1026 0.0000 0.0000 0.0689 0.0000 0.0689 0.0000
HC NOX Aero Energy Fuel Number Hydrogen Methane Ethane Ethylene Propane Propylene Butane Butylene Butadiene Pentane Cyclopentane Hexane Heptane Carbon Monoxide Carbon Dioxide	0.0014 0.0023 900-3029 (Bi Volume % 0.0000 95.5018 3.0123 0.0000 0.4638 0.0000 0.1190 0.0000 0.0000 0.0240 0.0000 0.0135 0.0000 0.0015 0.0000 0.0000	ack Hills Wyoming) Weight % 0.0000 90.7897 5.3675 0.0000 1.2119 0.0000 0.4099 0.0000 0.4099 0.0000 0.0000 0.0000 0.0000 0.0689 0.0000 0.0689 0.0000 0.0689 0.0000 0.6689
HC NOX Aero Energy Fuel Number Hydrogen Methane Ethane Ethylene Propylene Butane Butylene Butadiene Pentane Cyclopentane Hexane Heptane Carbon Monoxide Carbon Monoxide Nitrogen Nitrogen	0.0014 0.0023 900-3029 (Bi Volume % 0.0000 95.5018 3.0123 0.0000 0.4638 0.0000 0.1190 0.0000 0.0240 0.0000 0.0240 0.0000 0.0135 0.0000 0.0135 0.0000 0.0135 0.0000 0.0135 0.0000	ack Hills Wyoming) Weight % 0.0000 90.7897 5.3675 0.0000 1.2119 0.0000 0.4099 0.0000 0.0000 0.1026 0.0000 0.0689 0.0000 0.0689 0.0000 1.6843 0.3652
HC NOX Aero Energy Fuel Number Hydrogen Methane Ethane Ethylene Propylene Butane Butylene Butylene Butylene Pentane Cyclopentane Hexane Heptane Carbon Monoxide Carbon Dioxide Nitrogen Water Vapor	0.0014 0.0023 900-3029 (Bi Volume % 0.0000 95.5018 3.0123 0.0000 0.4638 0.0000 0.4638 0.0000 0.0240 0.0000 0.0135 0.0000 0.0135 0.0000 0.0135 0.0000 0.6458 0.2200 0.0000	ack Hills Wyoming) Weight % 0.0000 90.7897 5.3675 0.0000 1.2119 0.0000 0.4099 0.0000 0.1026 0.0000 0.1026 0.0000 0.0689 0.0000 0.0689 0.0000 0.0689 0.0000 1.6843 0.3652 0.0000
HC NOX Aero Energy Fuel Number Hydrogen Methane Ethane Ethylene Propane Propylene Butane Butylene Butadiene Pentane Cyclopentane Hexane Heptane Carbon Monoxide Carbon Dioxide Nitrogen Water Vapor Oxygen	0.0014 0.0023 900-3029 (B) Volume % 0.0000 95.5018 3.0123 0.0000 0.4638 0.0000 0.4638 0.0000 0.0115 0.0000 0.0135 0.0000 0.0135 0.0000 0.0000 0.6458 0.2200 0.0000 0.0000 0.0000	ack Hills Wyoming) Weight % 0.0000 90.7897 5.3675 0.0000 1.2119 0.0000 0.4099 0.0000 0.1026 0.0000 0.1026 0.0000 0.0689 0.0000 0.0689 0.0000 0.6843 0.3652 0.0000 0.0000 0.0000
HC NOX Aero Energy Fuel Number Hydrogen Methane Ethane Ethylene Propane Propylene Butane Butylene Butadiene Pentane Cyclopentane Hexane Heptane Carbon Monoxide Carbon Dioxide Nitrogen Water Vapor Oxygen Hydrogen Sulfide Ammonia	0.0014 0.0023 900-3029 (B) Volume % 0.0000 95.5018 3.0123 0.0000 0.4638 0.0000 0.1190 0.0000 0.0240 0.0000 0.0240 0.0000 0.0135 0.0000 0.0000 0.6458 0.2200 0.0000 0.0000 0.0000 0.0000 0.0000	ack Hills Wyoming) Weight % 0.0000 90.7897 5.3675 0.0000 1.2119 0.0000 0.4099 0.0000 0.4099 0.0000 0.0000 0.1026 0.0000 0.0689 0.0000 0.0689 0.0000 0.6843 0.3652 0.0000 0.0000 0.0000 0.0000 0.0000
HC NOX Aero Energy Fuel Number Hydrogen Methane Ethane Ethylene Propylene Butane Butylene Butalene Pentane Cyclopentane Heptane Carbon Monoxide Carbon Dioxide Nitrogen Water Vapor Oxygen Hydrogen Sulfide Ammonia	0.0014 0.0023 900-3029 (Bi Volume % 0.0000 95.5018 3.0123 0.0000 0.4638 0.0000 0.1190 0.0000 0.0240 0.0000 0.0240 0.0000 0.0135 0.0000 0.0000 0.6458 0.2200 0.0000 0.0000 0.0000	ack Hills Wyoming) Weight % 0.0000 90.7897 5.3675 0.0000 1.2119 0.0000 0.4099 0.0000 0.1026 0.0000 0.1026 0.0000 0.0689 0.0000 0.0689 0.0000 0.0000 1.6843 0.3652 0.0000 0.0000 0.0000 0.0000 0.0000
HC NOX Aero Energy Fuel Number Hydrogen Methane Ethane Ethylene Propane Propylene Butane Butylene Butadiene Pentane Cyclopentane Hexane Heptane Carbon Monoxide Carbon Monoxide Carbon Dioxide Nitrogen Water Vapor Oxygen Hydrogen Sulfide Ammonia	0.0014 0.0023 900-3029 (B) Volume % 0.0000 95.5018 3.0123 0.0000 0.4638 0.0000 0.1190 0.0000 0.0240 0.0000 0.0240 0.0000 0.0135 0.0000 0.0000 0.6458 0.2200 0.0000 0.0000 0.0000 0.0000 0.0000	ack Hills Wyoming) Weight % 0.0000 90.7897 5.3675 0.0000 1.2119 0.0000 0.4099 0.0000 0.4099 0.0000 0.1026 0.0000 0.0000 0.0689 0.0000 0.0000 0.6843 0.3652 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
HC NOX Aero Energy Fuel Number Hydrogen Methane Ethane Ethylene Propane Propylene Butane Butylene Butadiene Pentane Cyclopentane Hestane Heptane Carbon Monoxide Carbon Monoxide Carbon Dioxide Nitrogen Water Vapor Oxygen Hydrogen Sulfide Ammonia kJ/kg, LHV kJ/Nm3, LHV	0.0014 0.0023 900-3029 (Bi Volume % 0.0000 95.5018 3.0123 0.0000 0.4638 0.0000 0.4638 0.0000 0.0240 0.0000 0.0240 0.0000 0.0240 0.0000 0.0240 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	ack Hills Wyoming) Weight % 0.0000 90.7897 5.3675 0.0000 1.2119 0.0000 0.4099 0.0000 0.4099 0.0000 0.0000 0.0000 0.0000 0.0689 0.0000 0.0000 1.6843 0.3652 0.0000 0.0000 0.0000 0.0000 0.0000
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HC NOX Aero Energy Fuel Number Hydrogen Methane Ethane Ethylene Propane Propylene Butane Butylene Butatiene Pentane Cyclopentane Hexane Heptane Carbon Monoxide Carbon Dioxide Nitrogen Water Vapor Oxygen Hydrogen Sulfide Ammonia kJ/kg, LHV kJ/Nm3, LHV kJ/km3, HHV	0.0014 0.0023 900-3029 (B) Volume % 0.0000 95.5018 3.0123 0.0000 0.4638 0.0000 0.1190 0.0000 0.0240 0.0000 0.0240 0.0000 0.0240 0.0000 0.0135 0.0000 0.0135 0.0000 0.0000 0.6458 0.2200 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	ack Hills Wyoming) Weight % 0.0000 90.7897 5.3675 0.0000 1.2119 0.0000 0.4099 0.0000 0.1026 0.0000 0.0000 0.0689 0.0000 0.0689 0.0000 0.0689 0.0000 0.0000 1.6843 0.3652 0.0000 0.0000 0.0000 0.0000 0.0000
HC NOX Aero Energy Fuel Number Hydrogen Methane Ethane Ethylene Propane Propylene Butane Butylene Butadiene Pentane Cyclopentane Hexane Heptane Carbon Monoxide Carbon Monoxide Carbon Dioxide Nitrogen Water Vapor Oxygen Hydrogen Sulfide Ammonia kJ/kg, LHV kJ/Nm3, LHV kJ/km3, HHV KJ/kg, HHV Fuel Temp, °C	0.0014 0.0023 900-3029 (Bl Volume % 0.0000 95.5018 3.0123 0.0000 0.4638 0.0000 0.1190 0.0000 0.0240 0.0000 0.0240 0.0000 0.0135 0.0000 0.0135 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.000000	ack Hills Wyoming) Weight % 0.0000 90.7897 5.3675 0.0000 1.2119 0.0000 0.4099 0.0000 0.4099 0.0000 0.1026 0.0000 0.0689 0.0000 0.0689 0.0000 0.6843 0.3652 0.0000 0.0000 0.0000 0.0000 0.0000
HC NOX Aero Energy Fuel Number Hydrogen Methane Ethane Ethylene Propylene Butane Butylene Butadiene Pentane Cyclopentane Hexane Heptane Carbon Monoxide Carbon Monoxide Carbon Dioxide Nitrogen Water Vapor Oxygen Hydrogen Sulfide Ammonia kJ/kg, LHV kJ/Nm3, LHV kJ/km3, HHV kJ/kg, HHV	0.0014 0.0023 900-3029 (Bi Volume % 0.0000 95.5018 3.0123 0.0000 0.4638 0.0000 0.4638 0.0000 0.0240 0.0000 0.0240 0.0000 0.0240 0.0000 0.0240 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00240 0.00240 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.000000	ack Hills Wyoming) Weight % 0.0000 90.7897 5.3675 0.0000 1.2119 0.0000 0.4099 0.0000 0.4099 0.0000 0.0000 0.0000 0.0000 1.6843 0.3652 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000

GE LM6000 PF Sprint Technology Attributes





Balachandar Naidu PhD Senior Product Marketing Manager One Neumann Way, MD S155 T 513-552-6863 varathar@ge.com

### LM6 PF SPRINT<sup>®</sup> – State of the Art Gas turbine

The LM6000PF is a gas turbine engine derived from GE's proven CF6-80C2 aircraft engine. Aeroderivative engines such as the LM6000 have several distinguishing features. The LM6000 has a dual shaft architecture. The low-speed shaft rotates at 3600 rpm to permit direct connection to a 2-pole electric generator while the air-flow and the high-speed shaft speed modulate with power. This engine also has a high operating pressure ratio (OPR 32), which in a simple-cycle configuration leads to high thermal efficiencies and low CO2 emissions.

The gas turbine was first introduced in the early 1990's. Since then, GE has sold about a 1000 LM6 gas turbines with fleet hours exceeding 20 million hours. The LM6 gas turbine has achieved best-in-class reliability and availability with fleet averages approaching 99% and 98% respectively.

Since the introduction, GE has continuously invested in improving the gas turbine with state-of-the-art aviation technologies. Some of the critical technologies that make the LM6 a state-of-the art gas turbine are listed below.

#### **Compressor Technologies**

- LPC and HPC SPRINT<sup>®</sup> system (Spray Intercooling system) to improve compressor efficiency
- VIGV and 5-stage VSV to achieve better compressor operability
- Electrostatic suppression bushings

#### **Combustor Technologies**

- High temperature Thermal Barrier Coatings
- Full range premixed combustion for low NOx at startup
- Best in class aeroderivative Dry Low Emissions technology
- Single crystal heat shields in combustor with proven life
- Adaptive flame temperature trim to avoid exposure to high combustion dynamics
- Flame temperature control which accounts for fuel property variations

#### **Turbine Technologies**

- Single Crystal alloys for HPT
- High Temperature TBC coatings
- State-of-the art cooling

#### Package Technologies

- SPRINT<sup>®</sup> system to enable efficient operation at high ambient temperatures
- State of the art fuel system and NOx mitigation system.
- Control system modulation of Sprint<sup>®</sup> flow to maximize part power efficiency

Brush Turbine Generator Cross Section



# **TYPICAL DAX GENERATOR CROSS-SECTION**



- 1. Stator (armature) winding
- 2. Stator core
- 3. Permanent magnet pilot exciter (PMG)
- 4. Exciter field
- 5. Exciter armature
- 6. Exciter fan
- 7. Rotating rectifier (diode wheel)
- 8. Rotor
- 9. Endcap (retaining ring)
- 10. Non drive (exciter) end
- 11. Oil seals
- 12. Main bearing (one at each end)
- 13. Endframe
- 14. Winding supports
- 15. Fan shroud
- 16. Mounting feet
- 17. Shaft mounted cooling fan (one at each end)
- 18. Stator frame
- 19. Drive (coupling) end
- 20. Cooling air inlets
- 21. Cooling air exhausts
- 22. Access to holding down bolts
- 23. Access to anti-condensation heaters
- 24. Soleplates

Contact:

BRUSH Turbogenerators Inc. 15110 Northwest Freeway - #150 Houston TX 77040

T: 281-580-1314 e: serviceus@brush.eu Web site: www.brush.eu

Brush Turbine Generator Data Curves



# ELECTRICAL DATA SHEET

#### P O Box 18, Falcon Works, Loughborough, Leics. LE11 1HJ, England Telephone: +44 (0) 1509 611511 Fax: +44 (0) 1509 612345 E-mail: Sales@bem.fki-et.com

#### 1. RATING DETAILS

	1.1	Frame size		BDAX 7-290ERJT
	1.2	Terminal voltage		13.80 kV
	1.3	Frequency		60 Hz
	1.4	Speed		3600 rev/min
	1.5	Power factor		0.850
	1.6	Applicable national standard		IEEE C50.13
	1.7	Rated air inlet temperature		15.0 °C
	1.8	Rated output	65.400	) MW, 76.941 MVA
2.	PERFO	RMANCE CURVES		
	2.1	Output vs air inlet temperature		H.E.P. 24155
	2.2	Generator capability diagram		H.E.P. 24156
	2.3	Efficiency vs output		H.E.P. 24157
	2.4	Open and short circuit curves		H.E.P. 24158
	2.5	V-curves		H.E.P. 24159
	2.6	Permitted duration of negative sequence current		H.E.P. 1216
3.	REACT	ANCES		
	3.1 3.2 3.3	Direct axis synchronous reactance, X $_{d(i)}$ Direct axis saturated transient reactance, X' $_{d(v)}$ Direct axis saturated sub transient reactance, X" $_{d(v)}$		254% 21.6 % ±15 % 15.6 % ± 15 %
	3.4 3.5	Unsaturated negative sequence reactance, $X_{2(i)}$ Unsaturated zero sequence reactance, X $_{\text{o}(i)}$		19.1 % 10.3 %
	3.6 3.7 3.8	Quadrature axis synchronous reactance, X $_{q(i)}$ Quadrature axis saturated transient reactance, X' $_{q(v)}$ Quadrature axis saturated sub transient reactance, X" $_{q(v)}$	()	233% 26% 19%
	3.9	Short circuit ratio		0.44
<u>Notes:</u>			Date:	04-Dec-2007
1.	The electronic values.	trical details provided are calculated Unless otherwise stated, all values are	Ref:	120404/16/296S/120R
	subject t national	o tolerances as given in the relevant standards.	Page:	1 of 2



# **ELECTRICAL DATA SHEET - CONTINUATION**

#### BDAX 7-290ERJT, 65.400 MW, 0.850 pf, 13.80 kV, 60 Hz

#### 4. RESISTANCES AT 20°C

4.1	Rotor resistance	0.138 ohms
4.2	Stator resistance per phase	0.0033 ohms
TIME	CONSTANTS AT 20°C	
5.1	Transient O.C. time constant, T' <sub>do</sub>	9.7 seconds
5.2	Transient S.C. time constant, T' $_{\rm d}$	0.66 seconds
5.3	Sub transient O.C. time constant T" do	0.05 seconds
5.4	Sub transient S.C. time constant, T <sup>"</sup> d	0.04 seconds

#### 6. INERTIA

5.

6.1	Moment of inertia, WR <sup>2</sup> (See note 2)	990 Kg.m <sup>2</sup>
6.2	Inertia constant, H	0.91 kW.secs/kVA

#### 7. <u>CAPACITANCE</u>

7.1	Capacitance per phase of stator winding to earth	0.19 microfarad
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#### 8. EXCITATION

8.1	Excitation current at no load, rated voltage	325 amps
8.2	Excitation voltage at no load, rated voltage	45 volts
8.3	Excitation current at rated load and P.F.	1013 amps
8.4	Excitation voltage at rated load and P.F.	185 volts
8.5	Inherent voltage regulation, F.L. to N.L.	37 %

#### Notes:

1.	The electrical details provided are calculated values.		
	Unless otherwise stated, all values are subject to	Date:	04-Dec-2007
	tolerances as given in the relevant national standards.		
		Ref:	120404/16/296S/120R
2.	The rotor inertia value may vary slightly with		
	generator / turbine interface. In the event of conflict, the figure quoted on the rotor geometry drawing takes precedence.	Page	: 2 of 2







**Brush Turbine Generator Efficiency Information** 



Generators convert the mechanical driver power to electrical output.

Robust original Brush design and modern manufacturing techniques provide our customers with one of the higher efficient mechanical to electrical conversions in the industry. The input power is defined in units of horsepower (HP) or shaft kilowatt (SKW) and the generator output as KW or MW (where MW is a 1000Kw).

Taking the popular General Electric LM6000PF Gas Turbine Package as our example for this explanation, the BDAX7-290 generator is nominally rated at 65MW at an ambient air inlet temperature of 15 deg C at sea level. This open air cooled generator selection has been fine tuned by Brush design to be the most effective technical solution for a variety of project conditions. Investment in modeling and development programs which are physically verified by test measurement have enabled continuous improvement and improved utilization of the construction materials.

TEWAC coolers and alternate utility conditions are all available as options to the same physical build without compromising the expected life and performance.

As the generator converts the mechanical energy shaft energy to electrical voltage and current (KW) the internal materials create heat due to the physical properties of the materials used in construction. These losses occur in the following principal components:

- Bearing friction lubricating oil is heated.
- Windage losses ambient cooling air is forced through the internal components. Shaft mounted fans push air around restricted spaces inside the generator, to carry heat away and out of the generator casing.
- The main rotating body (rotor) in the center of the generator contains a winding which creates a very strong magnetic field. The continuous copper strip is fed with a power supply from a brushless exciter which is also rotor mounted. The copper windings get hot as a result of the circulating electrical current.
- The stationary component of the generator is the magnetic stator core which captures the rotating magnetic energy and an electrical winding that converts it to volts and amperes(KW) which is connected to the power utility. Energy is lost in both the magnetic material and the winding copper all creating heat.
- All these active electrical conductors are wrapped in electrical insulation which must transfer the heat to a place where the cooling air can move the heat into the cooling air circuit.
- The heat exits the generator mostly as an increase in the cooling air temperature. A small amount of heat enters the lubricating oil, and a very small amount is radiated from the generator casing surface.

All these losses add up to approximately 1½ % of the output of the machine – so most Brush generators are around 98.5% efficient. The losses comprise fixed portions which relate to the rotating speed of the generator (in this case 3600rpm) and the terminal output voltage – and a variable portion which relate to the output power, so at half capacity the variable losses are halved.



In general, Brush find that in this class of generator (rated from 25 to 150MW capacity), our efficient conversion of the driver horsepower (HP) mechanical energy to electrical KW power output leads many competitors. Brush have modeled and validated numerous design improvements over the product design life, to ensure that the most effective design is provided for the broadest range of operating conditions. Alternate components and material selections are available to provide the customer with the best efficiencies for their many different applications.

Data is provided in the attachment for this BDAX7-290 example. Observe that the efficiency remains above 98% from 30 to 65MW which is a very broad operating range. Even when the driver and electrical load are only used at half capacity the generator losses are only 2%.

In addition to best in class efficiency, Brush generators are renown for their reliability in operations, durability in service and at world competitive first cost.

Derek E. King

#### **General Sales Manager**

BRUSH Turbogenerators Inc. Houston - Texas - USA

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AQT Watertube Heater Brochure (Inlet Heater)



# Solution builder in energy management

# **AQT** Watertube Heater Glycol/Water, Thermal Fluid

The Simoneau AQT Watertube Heater is an O-type construction with gas-tight, welded steel intercasing, water cooled rear wall, staggered bent tube convection section, ceramic wool front wall. Simoneau's AQT Watertube Heater applications glycol/water mixture and thermal fluid heating.

Typical industries include manufacturing & processing facilities, pulp & paper, petrochemical, pharmaceuticals, hospitals, universities and many others.

### Simoneau's AQT Watertube Heater Design Features:

- Capacities: up to 75 MMBTU/HR.
- Design pressures: up to 500 psig.
- Temperature up to 550 °F.
- Two pass flue gas contact with staggered tube arrangement for maximum heat transfer.
- Balanced heat transfer prevents thermal shock.
- Operates with natural gas, #2 oil and alternative gases.
- Meets or exceeds NOx Emission Standards while providing high turndown ratio.

### AQT Watertube Heater | Glycol/Water, Thermal Fluid

#### Benefits of Simoneau's AQT Watertube Heater Design:

- High efficiency provides significant fuel savings.
- Minimizes installation and maintenance costs.
- Extensive capacity range and excellent long-term reliability to meet commercial, industrial and institutional applications.
- Provides quick load response, low operating and reduced maintenance costs.
- Heater system components (burner, controls and emissions options) designed specifically to provide ease of operation.





#### Why Simoneau:

As a Solution Builder in Energy Management, Simoneau utilizes its technical expertise (most qualified engineering team in the industry) and quality manufacturing to provide custom solutions for your specific boiler applications. Reliability, efficiency and the safety of its boiler systems are key results of the Simoneau designs. Our integration of technical expertise, quality manufacturing, on-time delivery and field support makes Simoneau your partner of choice.

#### To learn more about Simoneau and its products, please contact:



#### LE GROUPE SIMONEAU INC.

1541 De Coulomb Street Boucherville (Québec) J4B 8C5 P. 450 641.9140 • 1 800 748.3783 • F. 450 641.9141 info@groupesimoneau.com Represented by:

AQT Watertube Heater Data Sheet (Inlet Heater)

# Physical data sheet

# **AQT Type** Heater Glycol / Thermal Fluid

AQT Heaters are registred under ASME Code Section I.



D'

Boiler	Capacity	A B C D		D Gas Outlat	WEIGHTS (in Pounds)		
Model Number	MMBTU / hr	Lengui	Width	neight	uas oullet	Dry	Flooded
A1-100	2,678	82 5/8"	54"	97 11/16"	12" dia.	7,200	8,250
A1-125	3,347	88 3/4"	54"	97 11/16"	16" dia.	7,750	9,000
A1-150	4,017	100 7/8"	54	97 11/16"	16" dia.	8,750	10,000
A1-175	4,686	110"	54"	97 11/16"	18" dia.	9,250	10,750
A1-200	5,356	121 1/4"	54"	97 11/16"	18" dia.	10,250	12,000
A1-250	6,695	118"	64"	109 3/16"	20" dia.	12,250	14,500
A1-300	8,034	127 1/4"	64"	109 3/16"	20" dia.	13,250	15,500
A1-350	9,373	139"	64"	109 3/16"	20" dia.	14,250	16,750
A1-400	10,712	171 5/16"	78"	120 15/16"	24" dia.	17,250	20,500
A1-450	12,051	177 3/8"	78"	120 15/16"	24" dia.	18,000	21,250
A1-500	13,390	189 1/2"	78"	120 15/16"	24" dia.	19,250	23,000
A1-600	16,068	196 1/4"	90"	131 3/8"	30" dia.	23,500	28,250
A1-700	18,746	214 1/2"	90"	131 3/8"	32" dia.	25,750	31,250
A1-800	21,424	241 1/2"	90"	131 3/8"	32" dia.	28,040	29,750
A1-900	24,102	253 5/8"	90"	131 3/8"	32" dia.	29,750	36,000
A1-1000	26,780	202 1/2"	108"	144 1/4"	36" dia.	35,000	43,250
A1-1100	29,458	211 1/2"	108"	144 1/4"	36" dia.	36,500	45,000
A1-1200	41,400	220 5/8"	108"	144 1/4"	36" dia.	37,500	46,850

Capacities up to 2000 HP available upon request. All dimensions are imperial.

Sizing and dimension may vary depending on temperature and pressure design and are available upon request.

-ACCESS DOOR

# Physical data sheet

# **AQT Type** Heater Glycol / Thermal Fluid

Typical AQT Heater Glycol / Thermal Fluid









### DESIGNED BY OUR ENGINEERING TEAM:



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# Solution builder in energy management

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APPENDIX B-10 Fuel Gas Heater Brochure



# **"ENGINEERED SOLUTIONS"**

# **Indirect Fired Water Bath Heaters**

#### **OVERVIEW**

Indirect fired water bath heaters are used successfully in hundreds of utility, processing, and upstream oil and gas industry applications.

Water bath heaters are commonly used applications where process in temperatures do not exceed 170°F.

#### Typical uses include:

- Heating natural gas prior to pressure reduction to eliminate frost formation downstream of expansion valving.
- Preventing hydrate formation in well stream fluids.
- Heating well stream fluids prior to phase separation.
- Heating process streams to maintain fluid viscosity at a minimum to reduce HP pumping requirements.
- Heating critical feed stocks that require tightly controlled film to bulk temperature differentials.
- Heating turbine fuel gases to maintain a given dew point temperature.

#### **HEATER COMPONENTS**

The indirect fired water bath heater consists of the following components each designed to meet specific design criteria:

The heater shell is an atmospheric vessel designed in accordance with The flue gas stack is designed to API 12 K requirements. The shell contains the process coil, firetube (combustion chamber), and heat media.

The firetube is commonly of the U-tube configuration. The tube is removable & designed to efficiently transfer heat into the surrounding heat media and to minimize flue gas friction losses.



#### HEATER OPERATION

The process to be heated flows through a serpentine configured coil that is mounted in the upper reaches of the heater shell. A controlled amount of heat is liberated into the firetube (combustion chamber) which is located in the lower reaches of the heater shell where heat is efficiently transferred form the firetube in the bath media. The heat contained in the bath media is then transferred by natural convection into the process stream which flows through the process coil.

The process coil is a pressure The expansion tank is designed to Section VIII Division 1 requirements.

provide positive flue gas flow (draft) by overcoming the friction losses in the complete combustion system.

of inhibited ethylene or propylene glycol specified mechanical & operation and water which is blended to a requirements. Including simple pneuconsistency to provide the proper freeze protection for a given application.

containing part commonly designed in reduce internal corrosion within the accordance with API-12K or ASME heater shell by keeping the heater shell code liquid packed & moving the wet dry interface of the expanding bath media from the heater shell into the expansion tank. The expansion tank is designed to contain 100% of the expanded bath media from a temperature of 40° to the maximum operating temperature.

Accessories Items: TERI designs & manufactures heaters with a wide The heat media is commonly a mixture variety of accessories to meet customer matic controls to sophisticated remotely controlled & monitored equipment.

# "ENGINEERED SOLUTIONS"



#### STANDARD FEATURES INCLUDE

- · Laser cut shop fabricated components
- Individually removable firetubes
- 304 SS Flue gas stack or stacks
- Stack clean out tee
- Flue gas stack anti reverse-draft diverters w/rain cap & bird screens
- "Pilot In A Drawer" assemblies for easy maintenance & inspection
- Basic electric & pneumatic in addition to
   PLC control systems
- Multi mitered firetube bends (no single miter cut to greater than 22.5°)
- Positive seal flange designs
- Bath media expansion reservoir designed to hold 6% of the total bath media
- Heat media level gauge
- Heat media temperature Indicator
- Shell designed in accordance with API 12K
- Coil designed and stamped in accordance with ASME-8-1
- 100% Radiography on process coil welds
- Process coil, National Board Stamped

#### Optional Control Enhanced Designs

- Pneumatic controlled equipment operation
- Electrical controlled equipment operation
- Combination pneumatic & electrical controlled equipment operation
- Flame-Safeguard assemblies including, Pneumatic, 120VAC & 12VDC or Solar Power
- Manual OR Automatic pilot ignition designs

#### Optional Fabricated Enhanced Components

- Cushioned (Electrically Insulated) process coil supports & Tube Sheets
- Shell internally grit or sandblasting w/water soluble rust preventive coating
- Customized heater supports to meet existing pier locations
- Hot dipped galvanized heater skids, ladders & platforms

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	/LI= A	Р	<u> </u>	D	-	-	<u> </u>
	u/⊓i A 20"	р с'	6.62"	10'0"	E 5'0"	Г 1'0"	4'7"
0.10	20	0	0.03	100	0 C	12	17
0.25	24	7.5	8.63	10.0.	7.2.	1.2.	17
0.50	30″	10'0"	10.75″	12'0"	7'0"	1′8″	2'3"
0.75	36"	12'0"	10.75"	12'0"	9'0"	2'0"	2'8"
1.00	42"	15'0"	12.75"	14'0"	10'0"	2'2"	3'1"
1.25	42"	15'0"	12.75"	14'0"	10'0"	2'2"	3'1"
1.50	48"	17'5"	14"	15'0"	12'6"	2'10"	3'7"
1.75	48"	20'0"	16"	15'0"	16'0"	2'10"	3'7"
2.00	54"	20'0"	18"	15'0"	15'0"	3'0"	3'11"
2.50	54"	22'5"	18"	16'0"	17'6"	3'0"	3'11"
3.00	60"	22'5"	20"	16'0"	18'6"	3'0"	4'4"
3.50	72"	27'7"	22"	17'5"	22'6"	4'0"	5'3"
4.00	72"	30'0"	24"	17'5"	25'0"	4'0"	5'3"
4.50	84"	32'0"	24"	17'5"	27'0"	4'6"	6'2"
5.00	84"	32'0"	26"	17'5"	27'0"	4'6"	6'2"
6.00	84"	32'0"	28"	17'5"	27'0"	4'6"	6'2"
7.00	96"	30'0"	2@22"	17'5"	25'0"	5'6"	6'11"
8.00	96"	32'0"	2@22"	17'5"	27'0"	5'6"	6'11"
10.00	102"	32'0"	2@26"	20'0"	27'0"	6'0"	7'6"
	(OTHER SI	ZES ARE A	VAILABLE .	"ENG	INEERED SOLUT	FIONS")	. 0

	Units	Ethylene	Propylene
Freezing Point	Temp (°F)	-32	-24
Boiling Point (1 Atm)	Temp (°F)	225	222
Specific Gravity	60 / 60	1.064	1.043
Viscosity @ 200°F	Centipoises	0.75	0.75
Specific Heat @ 200°F	Btu / Lb / °F	0.83	0.91
Thermal Conductivity	Btu / Hr, Sq Ft, °F / Ft	0.28	0.022

\*Properties are representative of 50% Glycol / 50% Water

<u>Heater Type</u>	Process Temp (F)
Water/Glycol LP Steam (<15 Psig) Heat Transfer Oil Eutectic Salt Flue Gas Recirculation	160° 220° 400° 600° 625°

.....

Fuel Gas Heater Data Sheet



#### INDIRECT FIRED HEATER SPECIFICATION SHEET

Link Since         Engreen on TBD         Constraints Handing Note:         Constraints         Constraints <thconstraints< th="">         Constraints         Constra</thconstraints<>	Customer Address	CH2M Hill 9189 South Jamai	ca Street	Date: Customer Reference	22-Aug-11
Buring agent         Devid Chamberian           During agent         Devid Chamberian           During agent         Bath Meda Voum (Ga) Head Mig (MB Burkhy)         EASA HEATER DATA         REMARKS           During Agent         Bath Meda Voum (Ga) Head Mig (MB Burkhy)         1.114 Bath Meda Voum (Ga) Head Mig (MB Burkhy)         Soso Englere Gyoci Soso Englere Gyoci Bath Meda Voum (Ga) Head Mig (MB Burkhy)         REMARKS           Type of Fuld Total fuld Entering Same Bath Meda Voum (Ga) Head Mig (MB Burkhy)         Num (Ga) Bath Meda Voum (Ga) Head Mig (MB Burkhy)         Num (Ga) Bath Meda Voum (Ga) Head Mig (MB Burkhy)         Num (Ga) Bath Mig (Ga	City/State/Zip Location Station	Englewood, CO 80 TBD TBD David Chamberlair	1112	Customer Project No Quotation Item Number: Operating Data	Q00322 BE Data: 800Psig/27°F To 795Psig/77°F
Details United Bank Maid Volume (Ba) Hand Mark Hand Mark (Ba) Hand Mark Volume (Ba) Hand Mark Vol	Purchasing Agent	David Chamberlair	1		
Outside Dunneter (Inches)         49.00 (1000         Bah Media Volume (Gai) (1000         1.11 (1000         0.000         Description         Second (1000         0.000           Type of Fluid Tools functioning (1000         FROCESS CONDITIONS         REMARKS         REMARKS           Type of Fluid Tools functioning Status         CCH         NULLET         OUTLET         Nuture Gai           Vigor         BhY         Notation (1000         Action (1000         Action (1000         Action (1000           Upped Fluid Status         EXP         Notation (1000         Action (1000         Action (1000         Action (1000           Upped Fluid Upped (1000)         Exp         Nature Gai         Action (1000         Action (1000)         Action (1000         Action (1000)         Action (1			BASIC HEATER DATA		REMARKS
Leage IPI III         Total Pressure (MBruch)         REMARKS           Type of Fuid Transferred         NLET         OUTLET         REMARKS         REMARKS           Type of Fuid Transferred         SCPL         NuET         OUTLET         REMARKS           Type of Fuid Transferred         SCPL         NA         NA         NA           Lipud Societ Corol         Ibhr         46.000         NA         NA           Lipud Societ Corol         Ibhr         NA         NA         NA           Lipud Societ Corol         Ibhr <t< td=""><td>Outside Diamotor (Inchos)</td><td>48.00</td><td>Bath Modia Volume (Gal)</td><td>1 1 1 4</td><td>50/50 Ethylopo Glycol</td></t<>	Outside Diamotor (Inchos)	48.00	Bath Modia Volume (Gal)	1 1 1 4	50/50 Ethylopo Glycol
Nominal Raining (MM BluvHr)         1.000         Heater Weight (Wei Lbs)         17.80           Process CONSTICMS         REMARKS           Type of Fluid Tash fund Entering Liquid Density (fr-Cur) Liquid D	Length (Ft)	18.00	Heater Weight (Dry Lbs)	8,400	30/30 Ethylene Glycol
PROCESS CONDITIONS         REMARKS           Total field Entoring         SCFH         INLET         OUTLET           Vapor         Buhr         1,000,000         4	Nominal Rating (MM Btu/Hr)	1.600	Heater Weight (Wet Lbs)	17,680	
Incode Output         Inclusion         Inclusion           Type of Fluid         SecFH         Natural Gas         Natural Gas           Vacat         Ibb/r         45.002         45.002           Vacat         Ibb/r         NA         NA           Liquid Specific Gravity         Ibb/r         NA         NA           Vacat Specific Heat         Blub/rs-F         0.883         0.642           Vapor Viscoréy         Cp         0.011         0.012           Vapor Specific Heat         Blub/rs-F         0.823         0.642           Vapor Specific Heat         Blub/rs         0.22         77.60           Vapor Specific Heat         Blub/rs         1.32         77.60           Vapor Specific Heat         Blub/rs         1.521.417         64.52           Vapor Thema					DEMADKS
Type of Puid Tadi fuid Entring         Netwal Gas         Netwal Gas           Vapor Liguid         Ibhr         1.000,000         45,692         45,692           Vapor Liguid         Ibhr         45,692         45,692         45,692           Netwal Contaction         Ibhr         NA         NA         NA           File Monocated to Cond         Ibhr         NA         NA         NA           Liquid Specific Heat         Buhr H-F         NA         NA         NA           Liquid Specific Heat         Buhr H-F         NA         NA         NA           Vapor Molecular W         Babra Mol         17.340         Puid Specific Gravity         0.600           Vapor Molecular W         Babra Mol         17.340         Puid Specific Gravity         0.600           Vapor Molecular W         Babra Mol         17.340         Puid Specific Gravity         0.600           Vapor Molecular W         Babra Mol         17.340         Puid Specific Gravity         0.600           Vapor Molecular W         Babra Mol         17.340         Puid Specific Gravity         0.600           Vapor Molecular W         File         2.7         7.760         After Regulation: 75         75           Pressure Toro (AllowCalc)			INI FT		
Total function         SCPH         1.000,000	Type of Fluid		Natural Gas	Natural Gas	
Vapor         Ib/r         45.692           Liquid         Buhr         45.692           Steam         Buhr         Buhr           Plad Vaported of Cond         Buhr         NA.           Plad Vaported of Cond         Buhr         NA.           Liquid Sporter Main         Buhr         NA.           Vapor Sporter Main         Buhr         0.680           Vapor Sporter Main         Buhr         1.21,411           Postance Cond         McOreratan         1.71 </td <td>Total fluid Entering</td> <td>SCFH</td> <td>1,000,000</td> <td></td> <td></td>	Total fluid Entering	SCFH	1,000,000		
Lauid         Ibhr           Sixam         Bohr           Puid Vaccinde Cond         Bhr           Liquid Density (INCun)         Bhr           Vapor Moccular W         Burbs Mol           Japati Density         BarBa           Vapor Moccular W         BarBa           Vapor Moccular W         BarBa           Japati Density         BarBa           Vapor Moccular W         BarBa           Japati Density         BarBa           Vapor Themac Cond.         Burb-F           Operating Pressure         Paid           Pressure Torp (Allow/Calc)         File           Pressure Torp (Allow/Calc)         Burb-F           Pressure Torp (Allow/Calc)         Burb-F           Paid Specific Cond         Statistic Cond           Heat Transfer Red (FoulerCalcenn)         Burb-F           Transfer Red (FoulerCalcenn)         Burb-F           Transfer Red (FoulerCalcenn)         Burb-F           Transfer Red (FoulerCalcenn)	Vapor	lb/hr	45,692	45,692	
Steam         Ibor           Deal apportand to Cond         Ibbr           Flux apportand to Cond         Ibbr           Plux apportand to Cond         Ibbr           Liquid Specific Heat         Burbe-F           Uquid Specific Heat         Burbe-F           Vapor Density         Ibbr           Vapor Obecidar Wi         Ibbr Mol           Vapor Viscosity         Cp           Vapor Specific Heat         Burbe-F           Steam         Cond           Vapor Specific Heat         Burbe-F           Pouling Resistance         Fig           Fouling Resistance         Fig           Fouling Resistance         Fig           Fouling Resistance         Fig           Freasure Cond (LINTD)         T17           Transferred         Burbe-F           State Reside (Social Action Code         ASME Sec 8 Div 1           Temperature (LINTD)         T17           Temperature (LINTD)         T18 <t< td=""><td>Liquid</td><td>lb/hr</td><td></td><td></td><td></td></t<>	Liquid	lb/hr			
Non-Contentation         IDM           Lipid Viportion Corbin         IbM           Lipid Viportion Corbin         IbM           Lipid Viportion Corbin         IbM           Lipid Specific Fleat         Bufb-F           Lipid Specific Fleat         Bufb-FF           Lipid Specific Fleat         Bufb-FF           Vapor Miccular Wi         IbS/TS           Vapor Obensity         IbS/TS           Vapor Specific Heat         Bufb-FF           Vapor Themad Cond         Bufb-FF           Pressure Drop (Allow/Calc)         Feig           Paradig Pressure         Feig           Paradig Pressure         Feig           Paradig Pressure         Feig           Paradig Pressure	Steam	lb/hr			
Tuber Application Work         Builting         NA         NA           Liquid Specific Heat         Builth-FF         NA         NA           Liquid Specific Heat         Builth-FF         NA         NA           Liquid Specific Heat         Builth-FF         NA         NA           Vapor Molecular Wi         Builth-FF         NA         NA           Vapor Vescelly         Betrin         3:175         2:775           Vapor Specific Heat         Builth-FF         0.002         0.002           Vapor Specific Heat         Builth-FF         0.022         0.022           Vapor Specific Heat         Builth-FF         0.022         0.022           Vapor Specific Heat         Builth-FF         0.028         0.022           Vapor Specific Heat         Builth-FF         0.028         0.022           Vapor Specific Heat         Builth-FF         7.70         After Regulation:         75           Velocity         Field         -         52.88         After Regulation:         75           Pressure Drop (AllowCalc)         Peid         -         11.13         -         171 F           Transfer Heat Ground Clean)         Builth-FI2:F         7.23         Radograph (Percent)         100	Fluid Veperized or Cond	ID/III lb/br			
Lugid Specify         Op         NA         NA           Lugid Specify         Cp         NA         NA           Lugid Specify         Bubh-F         NA         NA           Lugid Thermal Cond         Bubh-F         NA         NA           Vapor MicroliaW M         Ibs/Bis Mol         17.340         Fluid Specific Gravity         0.600           Vapor MicroliaW M         Ibs/Bis Mol         17.340         Fluid Specific Gravity         0.600           Vapor Specific Heat         Bubh-F         0.063         0.042	Liquid Density (In/Out)	ID/TII Ib/ft3	ΝA	NA	
Ligid Specific Heat         Bulb-F         N.A.         N.A.           Updd Themal Cond         Bulb-fri-Fr         N.A.         N.A.         N.A.           Vapor Denily         Ibs/fb Mol         17.340         Fluid Specific Gravity         0.660           Vapor Viscosity         Cp         0.011         0.012         0.012           Vapor Specific Heat         Bulb-F         0.683         0.642         0.022           Vapor Thermal Cond.         Btulh-F.F         0.020         7.70         After Regulation:         77           Operating Pressure         Psig         800         769         After Regulation:         75           Velocity         Hride: FBu         -         52.88         -         -         11.3           Foung Resistance         Intrd: FBu         -         11.13         -         -         171         F           Tarnsferred         Btu/h-f2-F         79.39         116.88         -         171         F           Tarnsferred         Btu/h-f2-F         79.39         116.88         -         171         F           Tarnsferred         Btu/h-f2-F         79.39         166.00         ASME Sec 9 Div 1         765           Trest Pressure	Liquid Viscosity	Cn	N.A.	N.A.	
Liquid Thermal Cond         Bu/hr-FF         N.A.         N.A.           Vapor Miceolar Wt         Bu/hr M3         3.175         2.715           Vapor Miceolar Wt         Bu/hr M3         3.175         2.715           Vapor Obensity         Bu/hr H-F         0.031         0.012           Vapor Specific Heat         Bt/hr H-F         0.020         0.022           Vapor Thermal Cond.         Bt/hr H-F         0.020         0.022           Temperature (IN/OUT)         F         2.7         77.00           Operating Pressure         Psig         600         769           Velocity         trise         -         11.13           Foung Resistance         trice         -         11.13           Fransered         Bu/h-f-2.F         71.20         Operating Bath Temperature         171           Transformed         Bu/h-f2.F         71.20         Operating Bath Temperature         171           Transformed         Bu/h-f2.F         71.20         Operating Bath Temperature         171         F           Tender State Could Clean)         Bu/h-f1.2.F         71.20         Operating Bath Temperature         171         F           Tender State Coll Contar         F         State Contant Stamped	Liquid Specific Heat	Btu/lb-F	N.A.	N.A.	
Vapor Molecular Wi         Ibs/bits Mol         17.340 (Mapor Density)         Ipuid Specific Gravity         0.600           Vapor Viscosity         Cp         0.011         0.012         0.022           Vapor Viscosity         Cp         0.011         0.013         0.014           Vapor Specific Heat         Bu/hr-Hr-F         0.020         0.022         0.022           Vapor Specific Heat         Freesure         Psig         0.020         75           Prostrating Pressure         Psid         Transfer Red Fould-Otean         11.13         1           Freesure         Psig         72.0         72.0         75           Pressure         Psig         2010 2020         Norminal         100         ASME Sec 8 Div 1           Teransfer Red Fould	Liquid Thermal Cond	Btu/hr-ft-F	N.A.	N.A.	
Vapor Density         Ibe/t3         3.175         2.715           Vapor Viscosity         Cp         0.011         0.012           Vapor Specific Heat         Bu/h-F/F         0.683         0.642           Vapor Specific Heat         Bu/h-F/F         0.020         0.022           Temperature (In/Out)         F         27         77.00         After Regulation:         75           Operating Pressure         Peig         800         789         After Regulation:         75           Velocity         Wisc	Vapor Molecular Wt	lbs/lbs Mol	17.340		Fluid Specific Gravity 0.600
Vapor Specific Heat         Buthr-FF         0.011         0.012           Vapor Specific Heat         Buthr-FF         0.020         0.022           Temporature (Ir/Out)         F         2.27         77.00           Operating Pressure         Peig         800         789           Velocity         Maec	Vapor Density	lbs/ft3	3.175	2.715	
Vapor Specific Heat         Blufb-Fr         0.063         0.642           Vapor Thermal Cond.         Blufb-Hr-Fr         0.020         0.022           Temperature (In/Out)         F         2.7         77.00         After Regulation:         77           Operating Pressure         Psig         800         789         After Regulation:         75           Velocity         tr/sec	Vapor Viscosity	Ср	0.011	0.012	
Vale         But/Inferrial Colo.         But/Inferrial Colo.         But/Inferrial Colo.         But/Inferrial Colo.         Coloration Coloraticon Coloraticon Coloration Coloraticon Coloration Coloration Co	Vapor Specific Heat	Btu/lb-F	0.683	0.642	
Ampendation (Incluit)         Feig         22         7.00         After Regulation:         7.5           Velocity         fuse	Vapor Thermal Cond.	Btu/hr-tt-F	0.020	0.022	After Pequilation 77
Valuation         res         occ         52.8           Pressure Drop (AllowCalc)         Paid	Operating Pressure	F Psia	27	77.00	After Regulation: 77
Pressure Drop (AllowCalc) Fouling Resistance         Psid hrtf2-F/Btu	Velocity	ft/sec		52.88	Alter Regulation. 755
Fouling Resistance         hr-ft2-F/Bu         REMARKS           Heat Transferred         Btuhr         1,521,417         Operating Bath Temperature         171         F           Transfer Rate (Fouled/Clean)         Btuhr         1,521,417         Operating Bath Temperature         171         F           Transfer Rate (Fouled/Clean)         Btuhr         1,521,417         Operating Bath Temperature         171         F           Design Fressure         Psig         90         Fabrication Code         ASME Sec 8 Div 1         00           Design Frenperature         F         -20 to 250°F         National Board Stamped         Yes         Nominal           Number of Pass/Path         Units         8         Connections (Size/Rating)         Nominal         0.237 in           Total Number of Tubes         Units         1         16,5         Outlet         4in ANSI 600# RFWN           Number of Paths         Units         1         0.237 in         Outlet         4in ANSI 600# RFWN           Tube Size         Inches         0.237 in         0.237 in         0.237 in         0.237 in           Tube Size         Inches         0.237         Surface Area Actual         164 Fiz         0.237 in           Corrosion Allowance         Inches <td>Pressure Drop (Allow/Calc)</td> <td>Psid</td> <td></td> <td>11.13</td> <td></td>	Pressure Drop (Allow/Calc)	Psid		11.13	
THERMAL DATA         REMARKS           Heat Transfered         Btu/hr         1,521,417         Operating Bath Temperature         171         F           Tampler Rate (FouldClCam)         Btu/hr./ft2-F         116.88         P         1171         F           Design Pressure         Psig         116.88         Fabrication Code         ASME Sec 8 Div 1         F           Design Temperature         F         -20 to 250°F         National Board Stamped         Yes         Naminal           Number of Paths         Units         8         Connections (Size/Rating)         Nominal           Total Number of Tubes         Units         8         Connections (Size/Rating)         Nominal           Straight Tube Length         Ft         16.5         Outlet         4in ANSI 600# RFWN           Straight Tube Length         Ft         16.5         Outlet         4in ANSI 600# RFWN           Tube Size         Inches         02.337         Surface/Rate Actual         164         Fr2           Corrosion Allowance         Inches         0.237         Surface Area Actual         164         Fr2           Shell Diameter         Inches         114         164         Fr2         0.145         114         164         164         16	Fouling Resistance	hr-ft2-F/Btu			
Heat Transformed         Btu/hr Transfer Rate (Fouled(Clean)         Btu/hr-ft2-F         T22/ 7 22/ 7 22/ 7 16.88         (Dervating Bath Temperature         171 F           Temperature Diff (LMTD)         Btu/hr-ft2-F         7 22/ 7 22/ 7 16.88         0         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         <		THERMAL DATA		REMARKS	
Transfer Rate (Fouled/Clean)         Buthr-ft2-F         79.29 116.88           Temperature Diff (LMTD)         116.88         116.88           Design Pressure         Psig         900         Fabrication Code         ASME Sec 8 Div 1           Design Pressure         Psig         1350         Radiography (Percent)         100           Design Temperature         F         -20 to 250 <sup>+</sup> F         National Board Stamped         Yes           Number of Paths         Units         8         Connections (Size/Rating)         Nominal           Total Number of Tubes         Units         8         Outlet         4in ANSI 600# RFWN           Heat Flux         Btuhr-ft2         9.269         Inlet and Outlet header Thk         0.237 In           Yob Size         Inches         0.237         Surface Area Actual         164 Ft2           Corrosion Allowance         Inches         0.237         Surface Area Actual         164 Ft2           Corrosion Allowance         Inches         0.145         Set         Set           HEATER DATA         Return Bend Type         SR         Set           Design Code         API 12K         Treq per ASME         0.145           Shell Congh         1         1         Treq per ASME         0.14	Heat Transferred	Btu/hr	1,521,417	Operating Bath Temperature	171 F
PROCESS COIL DATA           Design Pressure         Psig         900         Fabrication Code         ASME Sec 8 Div 1           Test Pressure         Psig         1350         Radiography (Percent)         100           Design Temperature         F         -20 to 250°F         National Board Stamped         Yes           Number of Pass/Path         Units         1         Connections (Size/Rating)         Nominal           Total Number of Tubes         Units         8         Connections (Size/Rating)         Nominal           Straight Tube Length         Ft         16.5         Outlet         4in ANSI 600# RFWN           Heat Flux         Blu/hr-ft2         9.269         Inlet and Outlet header Velocity         52.88         ft/sec           Tube Size         Inches         0.237         Surface Area Actual         164         Ft/2           Tube Wall Thickness         Inches         0.237         Surface Area Actual         164         Ft/2           Design Code         API 12K         Treq per 49 CFR, Part 192         0.145         Shell Diameter         0.145         Shell Charde Meetand/Thk         0.111         in           Shell Diameter         Inches         1/4         8         Treq per 49 CFR, Part 192         0.145         She	Transfer Rate (Fouled/Clean) Temperature Diff (LMTD)	Btu/hr-ft2-F	79.29 116.88		
Design     Pressure     Psig     900     Fabrication Code     ASME Sec 8 Div 1       Test Pressure     Psig     1350     Radiography (Percent)     100       Design Temperature     F     -20 to 250°F     National Board Stamped     Yes       Number of Pass/Path     Units     1     Connections (Size/Rating)     Nominal       Total Number of Tubes     Units     1     Connections (Size/Rating)     Nominal       Total Number of Tubes     Units     1     Connections (Size/Rating)     Nominal       Tube Size     Inches     0D     4.500     Header Thk     0.237 In       Tube Size     Inches     0D     4.500     Header Velocity     52.88 ft/sec       Corrosion Allowance     Inches     0.237     Surface Area Actual     164 Ft2       Corrosion Allowance     Inches     0.237     Surface Area Actual     164 Ft2       Shell Diameter     Inches     48     Treq per 49 CFR, Part 192     0.145       Shell Diameter     Inches     14     Tube Size     0.145       Shell Chik)     Inches     14     Treq per 49 CFR, Part 192     0.145       Shell Chik)     Inches     14     Treq per 49 CFR, Part 192     0.145       Shell Chik)     Inches     14     Treq per 49 CFR, Par			PROCESS COIL DATA	•	
Test PressurePsig1350Radiography (Percent)100Design TemperatureF-20 to 250°FNational Board StampedYesNumber of PashSUnits8Connections (Size/Rating)NominalTotal Number of TubesUnits8Inlet4in ANSI 600# RFWNStraight Tube LengthFt9,269Inlet and Outlet header Thk0.237 InTube SizeInches04.500Header Velocity52.88 ft/secTube Wall ThicknessInches0.237Surface Area Actual164 Ft2Corrosion AllowanceInchesAPI 12KSec0.145Design CodeAPI 12K164Treq per 49 CFR, Part 1920.145Shell Lengthft11417.75Selected Pipe Tmin (12.5% mill Tol)0.207 inFiretube Iongthft17.75Selected Pipe Tmin (12.5% mill Tol)0.207 inFiretube Head DensityBtu/hr-rh29,302Firetube Head Density0.237 inFiretube Head DensityBtu/hr-rh29,302Firetube Head Density0.237 inFiretube Head DensityBtu/hr-rh29,302Firetube Head Density0.207 inFiretube Head DensityBtu/hr-rh29,440Ft16Stack DiameterIn18Ft16Firetube Head DensityBtu/hr-rh29,302Firetube Head Density0.207 inFiretube Head DensityBtu/hr-rh29,440Ft16Stack HeightFt16FtFtStack Height<	Design Pressure	Psig	900	Fabrication Code	ASME Sec 8 Div 1
Design Temperature     F     -20 to 250°F     National Board Stamped     Yes       Number of Pass/Path     Units     8     Connections (Size/Rating)     Nominal       Total Number of Tubes     Units     8     Inlet     4in ANSI 600# RFWN       Straight Tube Length     Ft     16.5     Outlet     4in ANSI 600# RFWN       Heat Flux     Bitu/hr-ft2     9,269     Inlet and Outlet header Thk     0.237     In       Tube Size     Inches     0.237     Surface Area Actual     164     Ft2       Corrosion Allowance     Inches     0.237     Surface Area Actual     164     Ft2       Corrosion Allowance     Inches     None     Return Bend Type     St       Design Code     API 12K     Treq per 49 CFR, Part 192     0.145       Shell Diameter     Inches     14     Treq per ASME     0.111     in       Shell Chtk)     Inches     1/4     Treq per ASME     0.237     in       Firetube Diameter     Inches     1/4     Treq per ASME     0.145     1/45       Shell Chtk)     Inches     1/4     Treq per ASME     0.237     in       Firetube Diameter     Inches     1/4*     Selected Pipe Tmin (12.5% mill Tol)     0.207     in       Firetube Enapth     ft <td>Test Pressure</td> <td>Psig</td> <td>1350</td> <td>Radiography (Percent)</td> <td>100</td>	Test Pressure	Psig	1350	Radiography (Percent)	100
Number of Pask/Path         Units         8           Number of Paths         Units         1         Connections (Size/Rating)         Nominal           Total Number of Tubes         Units         8         Inlet         4in ANSI 600# RFWN           Straight Tube Length         Ft         16.5         Outlet         4in ANSI 600# RFWN           Heat Flux         Btu/hr-ft2         9,269         Inlet and Outlet header Thk         0.237         Inlet         0.237         Inlet         4in ANSI 600# RFWN           Tube Size         Inches         0.237         Surface Area Actual         164         Ft2           Corrosion Allowance         Inches         0.237         Surface Area Actual         164         Ft2           Corrosion Allowance         Inches         0.237         Surface Area Actual         164         Ft2           Corrosion Allowance         Inches         0.237         Surface Area Actual         164         Ft2           Corrosion Allowance         Inches         Nominel         Return Bend Type         SR         State         52.88         ft/sec         144         State         53.53         53.53         53.53         53.53         53.53         53.53         53.53         53.53         53.53	Design Temperature	F	-20 to 250°F	National Board Stamped	Yes
Number of PathsUnits1Connections (Size/Rating)NorminalTotal Number of TubesUnits8Inlet4in ANSI 600# RFWNStraight Tube LengthFt16.5Outlet4in ANSI 600# RFWNHeat FluxBtu/hr-ft29,269Inlet and Outlet header Thk0.237 InTube SizeInches04.500Header Velocity52.88 fr/secTube Wall ThicknessInches0.237Surface Area Actual164 Ft2Corrosion AllowanceInches0.237Surface Area Actual164 Ft2Design CodeNoneReturn Bend TypeSRShell DiameterInchesAPI 12KShell DiameterInches48Treq per 49 CFR, Part 1920.145Shell ChrkyInches1/418Treq per ASME0.111 inShell ChrkyInches1/4175Selected Pipe Tmin (12.5% mill Tol)0.207 inFiretube Lengthft17.75Selected Pipe Tmin (12.5% mill Tol)0.207 in1Firetube Hat DensityBtu/hr-ft29,3029,302Firetube Hat Density0.207 inFiretube Flux RateBtu/hr-ft29,4401855Stack HeightFt165555Stack LeightFt165555Stack LeightFt165555Percent of Net Shell Vol.%6.57.3%55	Number of Pass/Path	Units	8		
Total Number of TubesUnitsaaInit4in ANSI 600# RFVNNStraight Tube LengthFt16.5Outlet and Outlet header Thk0.237 InTube SizeInches0D4.500Header Velocity52.88 ft/secTube Wall ThicknessInches0.237Surface Area Actual164 Ft2Corrosion AllowanceInchesNoneReturn Bend TypeSRRemarks and/or Other DataDesign CodeAPI 12KShell DiameterInches48Treq per 49 CFR, Part 1920.145Shell Lengthtt18Shell Cift14Treq per 49 CFR, Part 1920.145Shell Lengthtt17.75Selected Pipe Tmin (12.5% mill Tol)0.207 inFiretube DiameterInches1/4" - SA53-B1Tube Wall Thickness0.237 inFiretube Lengthft17.75Selected Pipe Tmin (12.5% mill Tol)0.207 inFiretube Heat DensityBtu/hr-in29,3029,302Firetube Heat Density5Firetube Heat DensityBtu/hr-if29,4401655Stack DiameterIn18155Stack DiameterIn18555Firetube Heat DensityBtu/hr-if29,440555Stack DiameterIn16555Firetube Heat DensityFt16555Stack LeightFt16 <td< td=""><td>Number of Paths</td><td>Units</td><td>1</td><td>Connections (Size/Rating)</td><td></td></td<>	Number of Paths	Units	1	Connections (Size/Rating)	
Index EnglinIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndexIndex </td <td>Straight Tube Length</td> <td>Units Et</td> <td>8</td> <td>Inlet</td> <td>4III ANOI 600# REWN Ain ANSI 600# REWN</td>	Straight Tube Length	Units Et	8	Inlet	4III ANOI 600# REWN Ain ANSI 600# REWN
Tube SizeInchesInchesInchesInchesTube Wall ThicknessInches0.237Surface Area Actual164Ft2Corrosion AllowanceInches0.237Surface Area Actual164Ft2Corrosion AllowanceInches0.237Surface Area Actual164Ft2The Marker	Heat Flux	Btu/hr-ft2	9 269	Inlet and Outlet header Thk	0.237 In
Tube Wall Thickness Corrosion AllowanceInches0.237 InchesSurface Area Actual164F12Corrosion AllowanceInchesNoneReturn Bend TypeSRHEATER DATARemarks and/or Other DataDesign CodeDesign CodeAPI 12K 48Treq per 49 CFR, Part 1920.145Shell DiameterInches48Treq per 49 CFR, Part 1920.145Shell Lengthft18Treq per ASME0.111inShell ChikInches11/417.75Selected Pipe Tmin (12.5% mill Tol)0.207 inFiretube Lengthft11/4* - SA53-BTube Wall Thickness0.237 inFiretube Heat DensityBtu/hr-in29,3029,3029,302Firetube Flux RateBtu/hr-ft29,440185tack HeightFtStack HeightFt1618.0018.0018.00Expansion Tank Lengthft18.0018.0018.00Expansion Tank Lengthft6.57.3%	Tube Size	Inches OD	4.500	Header Velocity	52.88 ft/sec
Corrosion AllowanceInchesNoneReturn Bend TypeSRHEATER DATADesign CodeRemarks and/or Other DataDesign CodeAPI 12KTreq per 49 CFR, Part 1920.145Shell DiameterInches48Treq per 49 CFR, Part 1920.145Shell Lengthft18Treq per ASME0.111 inShell (Thk)Inches1/417.650.111 inFiretube DiameterInches OD18Tube Wall Thickness0.237 inNumber of Firetubes1Tube Wall Thickness0.207 inFiretube Lengthft17.75Selected Pipe Tmin (12.5% mill Tol)0.207 inFiretube Heat DensityBtu/hr-fn29,3029,302145Stack DiameterIn181814Stack DiameterIn1818Stack HeightFt1618Expansion Tank Diameterin18.00Expansion Tank Lengthft6.5Percent of Net Shell Vol.%7.3%	Tube Wall Thickness	Inches	0.237	Surface Area Actual	164 Ft2
HEATER DATARemarks and/or Other DataDesign CodeAPI 12KShell DiameterInchesShell Lengthftft18Shell (Thk)InchesFiretube DiameterInches ODNumber of Firetubes1Firetube Lengthftft17.75Selected Pipe Tmin (12.5% mill Tol)O.207 inFiretube Flux RateBtu/hr-fn2Stack DiameterInIn18Stack HeightFtft6.5Expansion Tank Lengthftft6.5Percent of Net Shell Vol.%%7.3%	Corrosion Allowance	Inches	None	Return Bend Type	SR
Design Code         API 12K           Shell Diameter         Inches         48         Treq per 49 CFR, Part 192         0.145           Shell Length         ft         18         Treq per ASME         0.111 in           Shell (Thk)         Inches         114         Treq per ASME         0.111 in           Shell (Thk)         Inches         114         Treq per ASME         0.111 in           Shell (Thk)         Inches OD         18         Treq per ASME         0.237 in           Number of Firetubes         1         Tube Wall Thickness         0.237 in           Firetube Length         ft         17.75         Selected Pipe Tmin (12.5% mill Tol)         0.207 in           Firetube (Material/Thk)         Inches         1/4" - SA53-B         Fretube Heat Density         Btu/hr-fit2         9,302           Firetube Flux Rate         Btu/hr-fit2         9,440         Fretube Flux Rate         In         18           Stack Diameter         In         18         Fretube Height         Ft         16           Expansion Tank Diameter         in         18.00         Ft         5.5           Percent of Net Shell Vol.         %         7.3%         Ft         5.5	HEATER DATA			Remarks and/or Other Da	ata
Shell Diameter     Inches     48     Treq per 49 CFR, Part 192     0.145       Shell Length     ft     18     Treq per 49 CFR, Part 192     0.145       Shell Ungth     ft     18     Treq per ASME     0.111 in       Shell (Thk)     Inches     1/4     Inches     0.114       Firetube Diameter     Inches     00     18     Inches     0.237 in       Number of Firetubes     1     Tube Wall Thickness     0.237 in       Firetube Length     ft     17.75     Selected Pipe Tmin (12.5% mill Tol)     0.207 in       Firetube (Material/Thk)     Inches     1/4" - SA53-B     Inches     1       Firetube Heat Density     Btu/hr-fi12     9,302     Inches     Inches       Stack Diameter     In     18     Inches     Inches       Stack Diameter     In     18     Inches     Inches       Stack Height     Ft     16     Inches     Inches       Expansion Tank Diameter     in     18.00     Inches     Inches       Expansion Tank Length     ft     6.5     Inches     Inches       Percent of Net Shell Vol.     %     7.3%     Inches     Inches	Design Code		API 12K		
Shell Length     ft     18     Treq per ASME     0.111 in       Shell (Thk)     Inches     1/4     1/4     1/4       Firetube Diameter     Inches     0D     18       Number of Firetubes     1     Tube Wall Thickness     0.237 in       Firetube Length     ft     17.75     Selected Pipe Tmin (12.5% mill Tol)     0.207 in       Firetube (Material/Thk)     Inches     1/4" - SA53-B     1/4" - SA53-B     1/4" - SA53-B       Firetube Heat Density     Btu/hr-in2     9,302     1/4" - SA53-B     1/4" - SA53-B       Firetube Heat Density     Btu/hr-ft2     9,302     1/4" - SA53-B     1/4" - SA53-B       Stack Diameter     In     18     1/4" - SA53-B     1/4" - SA53-B     1/4" - SA53-B       Stack Diameter     In     18     1/4" - SA53-B     1/4" - SA53-B     1/4" - SA53-B       Stack Diameter     In     18     1/4" - SA53-B     1/4" - SA53-B     1/4" - SA53-B       Stack Diameter     In     18     1/4" - SA53-B     1/4" - SA53-B     1/4" - SA53-B       Stack Height     Ft     16     1/4" - SA53-B     1/4" - SA53-B     1/4" - SA53-B       Stack Height     ft     6.5     1/4" - SA53-B     1/4" - SA53-B     1/4" - SA53-B       Stack Height     ft     6.5	Shell Diameter	Inches	48	Treq per 49 CFR, Part 192	0.145
Site (Tilk)     Incluses     1/4       Firetube Diameter     Inches OD     18       Number of Firetubes     1     Tube Wall Thickness     0.237 in       Firetube Length     ft     17.75     Selected Pipe Tmin (12.5% mill Tol)     0.207 in       Firetube (Material/Thk)     Inches     1/4" - SA53-B     1     1     1       Firetube Heat Density     Btu/hr-in2     9,302     9,302     1     1       Stack Diameter     In     18     1     1     1       Stack Leight     Ft     16     1     1     1       Expansion Tank Diameter     in     18.00     1     1     1       Expansion Tank Length     ft     6.5     1     1     1       Percent of Net Shell Vol.     %     7.3%     1     1	Shell Length	ft Inchoo	18	Treq per ASME	0.111 in
Number of Firetubes1Tube Wall Thickness0.237 inFiretube Lengthft17.75Selected Pipe Tmin (12.5% mill Tol)0.207 inFiretube (Material/Thk)Inches1/4" - SA53-B0.2370.207 inFiretube Heat DensityBtu/hr-in29,3020.2070.2070.207Firetube Flux RateBtu/hr-ft29,4400.2070.2070.207Stack DiameterIn180.2070.2070.207Stack HeightFt160.2070.207Expansion Tank Lengthft6.50.2070.207Percent of Net Shell Vol.%7.3%0.2070.207	Firetube Diameter		1/4		
Firetube Length     ft     17.75     Selected Pipe Tmin (12.5% mill Tol)     0.207 in       Firetube (Material/Thk)     Inches     1/4" - SA53-B     0.207     0.207 in       Firetube Heat Density     Btu/hr-in2     9,302     0.207     0.207     0.207       Firetube Flux Rate     Btu/hr-in2     9,302     0.207     0.207     0.207       Stack Diameter     In     18     0.207     0.207     0.207       Stack Height     Ft     16     0.207     0.207     0.207       Expansion Tank Diameter     in     18.00     0.207     0.207       Expansion Tank Length     ft     6.5     0.207     0.207       Percent of Net Shell Vol.     %     7.3%     0.207     0.207	Number of Firetubes		1	Tube Wall Thickness	0.237 in
Firetube (Material/Thk)Inches1/4" - SA53-BFiretube Heat DensityBtu/hr-in29,302Firetube Flux RateBtu/hr-ft29,440Stack DiameterIn18Stack HeightFt16Expansion Tank Lengthft6.5Percent of Net Shell Vol.%7.3%	Firetube Length	ft	17.75	Selected Pipe Tmin (12.5% mill Tol)	0.207 in
Firetube Heat DensityBtu/hr-in29,302Firetube Flux RateBtu/hr-ft29,440Stack DiameterIn18Stack HeightFt16Expansion Tank Lengthft6.5Percent of Net Shell Vol.%7.3%	Firetube (Material/Thk)	Inches	1/4" - SA53-B	· · · · · · · · · · · · · · · · · · ·	
Firetube Flux RateBtu/hr-ft29,440Stack DiameterIn18Stack HeightFt16Expansion Tank Lengthft8.00Expansion Tank Lengthft6.5Percent of Net Shell Vol.%7.3%	Firetube Heat Density	Btu/hr-in2	9,302		
Stack DiameterIn18Stack HeightFt16Expansion Tank Diameterin18.00Expansion Tank Lengthft6.5Percent of Net Shell Vol.%7.3%	Firetube Flux Rate	Btu/hr-ft2	9,440		
Stack Height     Ft     16       Expansion Tank Length     in     18.00       Expansion Tank Length     ft     6.5       Percent of Net Shell Vol.     %     7.3%	Stack Diameter	In	18		
Expansion Tank Length ft 6.5 Percent of Net Shell Vol. % 7.3%	Stack Height	Ft in	16		
Percent for thet Shell Vol. % 7.3%	Expansion Tank Length	iri ft	18.00		
	Percent of Net Shell Vol.	%	7.3%		

Diesel Emergency Generator Data Sheet

# **DIESEL GENERATOR SET**





Image shown may not reflect actual package.

#### **FEATURES**

#### **FUEL/EMISSIONS STRATEGY**

• EPA Certified for Stationary Emergency Application (EPA Tier 2 emissions levels)

#### **DESIGN CRITERIA**

• The generator set accepts 100% rated load in one step per NFPA 110 and meets ISO 8528-5 transient response.

#### UL 2200

• UL 2200 listed packages available. Certain restrictions may apply. Consult with your Cat® Dealer.

#### FULL RANGE OF ATTACHMENTS

- Wide range of bolt-on system expansion attachments, factory designed and tested
- Flexible packaging options for easy and cost effective installation

#### SINGLE-SOURCE SUPPLIER

• Fully prototype tested with certified torsional vibration analysis available

#### WORLDWIDE PRODUCT SUPPORT

- Cat dealers provide extensive post sale support including maintenance and repair agreements
- Cat dealers have over 1,800 dealer branch stores operating in 200 countries
- The Cat® S•O•S<sup>™</sup> program cost effectively detects internal engine component condition, even the presence of unwanted fluids and combustion by-products

# STANDBY 600 ekW 750 kVA 60 Hz 1800 rpm 480 Volts

Caterpillar is leading the power generation marketplace with Power Solutions engineered to deliver unmatched flexibility, expandability, reliability, and cost-effectiveness.

#### CAT ® C18 ATAAC DIESEL ENGINE

- Utilizes ACERT™ Technology
- Reliable, rugged, durable design
- Field-proven in thousands of applications worldwide
- Four-stroke-cycle diesel engine combines consistent performance and excellent fuel economy with minimum weight
- · Electronic controlled governor

#### **CAT GENERATOR**

- Matched to the performance and output characteristics of Cat engines
- Load adjustment module provides engine relief upon load impact and improves load acceptance and recovery time
- UL 1446 Recognized Class H insulation

#### **CAT EMCP 4 CONTROL PANELS**

- Simple user friendly interface and navigation
- Scalable system to meet a wide range of customer needs
- Integrated Control System and Communications Gateway

## FACTORY INSTALLED STANDARD & OPTIONAL EQUIPMENT

System	Standard	Optional
Air Inlet	Light Duty Air Filter	[] Single element air filter
	Service indicator	[] Dual element air filter
		[] Heavy-duty dual element air filter with precleaner
		[] Air inlet shut-off
Cooling	Radiator package mounted	[] Radiator duct flange
Ŭ	Coolant level sight gauge	[] Low coolant level sensor
	Coolant drain line with valve	
	Fan and belt guards	
	Cat® Extended Life Coolant*	
Exhaust	Dry exhaust manifold	[] Industrial [] Residential [] Critical Mufflers
	Stainless steel exhaust flex fittings with split-cuff	[] Manifold and turbocharger guards
	Exhaust flange outlets	[] Elbows and through-wall kits
Fuel	Primary fuel filter with integral water separator	[] Integral single wall fuel tank base
	Secondary fuel filters	[] Integral dual wall UL fuel tankbase
	Fuel priming pump	[] Sub-base dual wall UL listed fuel tank base
	Flexible fuel lines	[] Manual transfer pump
	Fuel cooler*	[] Fuel level switch
	*Not inlcuded with packages without radiators	
Generator	Class H insulation	[] Oversize generators
	Class H temperature rise	[] Internal excited (IE)
	VR6 voltage regulator with 3-phase sensing with load	[] Permanent magnet excitation(PMG)
	adjustment	[] Cat digital voltage regulator (CDVR) with kVAR/PF
	IP23 Protection	control
		[] Anti-condensation space heaters
		[] Coastal Insulation Protection (CIP)
		[] Reactive droop
Power Termination	<ul> <li>Power Center houses EMCP controller and</li> </ul>	[] Power Center mounting option (right side)
	power/control terminations (rear mounted)	[] Circuit breakers, UL listed, 3 pole (80% & 100%
	Power terminal strips (NEMA or IEC mechanical lug	Rated)
	holes)	[] Circuit breakers, IEC compliant, 3-4 pole(100%
	Segregated low voltage wiring termination panel	Rated)
	IP22 protection	[] Multiple circuit breaker options
	• Bottom cable entry	[] C.B. Shunt trips
Governor	• ADEIVI ····· A4	[] Load Share Module
Control Panels	EMCP 4.1 (mounted in Power Center)	[ ] EMCP 4.2
	Speed adjustment	[] Local annunciator module (NFPA 99/110)
	Voltage adjustment	[] Remote annunciator module (NFPA 99/110)
	Emergency stop pushbutton	[] Digital I/O module
Lube	Lubricating oil	[] Oil temperature sensor
	Oil drain line with valves	[] Manual sump pump
	<ul> <li>Oil filter and dipstick</li> </ul>	
	• Fumes disposal	
	Lube oil level indicator	
	Oil cooler	
Mounting	<ul> <li>Formed steel narrow base frame</li> </ul>	[] Oil skid base
	Linear vibration isolation-seismic zone 4	[] Formed steel wide base frame
Starting/Charging	• 24 volt starting motor	[] Jacket water heater with shut-off valves
	<ul> <li>24 volt, 45 amp charging alternator</li> </ul>	[] Engine block heater
		[] Ether starting aid
		] Battery disconnect switch
		[] Battery chargers (5 or 10 amp)
		[] Oversize batteries
-		[] Batteries with rack and cables
General	Paint - Caterpillar Yellow except rails and radiators	UL 2200 package
	gloss black	
	• Flywneel housing - SAE No. 0	I JEU or CE Certificate of Conformance
		[] veather protective enclosure
		[] Sound attenuated protective enclosure

60 Hz 1800 rpm 480 Volts

## **SPECIFICATIONS**

#### **CAT GENERATOR**

#### CAT DIESEL ENGINE

C18 ATAAC, I-6, 4-Stroke Water-cooled Diesel

Bore	
Stroke	183.00 mm (7.2 in)
Displacement	18.13 L (1106.36 in <sup>3</sup> )
Compression Ratio	
Aspiration	Air-to-Air Aftercooled
Fuel System	MEUI
Governor Type	. Caterpillar ADEM control system

#### **CAT EMCP 4 SERIES CONTROLS**

EMCP 4 controls including:

- Run / Auto / Stop Control
- Speed and Voltage Adjust
- Engine Cycle Crank
- 24-volt DC operation
- Environmental sealed front face
- Text alarm/event descriptions
- Digital indication for:
- RPM
- DC volts
- Operating hours
- Oil pressure (psi, kPa or bar)
- Coolant temperature
- Volts (L-L & L-N), frequency (Hz)
- Amps (per phase & average)
- ekW, kVA, kVAR, kW-hr, %kW, PF (4.2 only)
- Warning/shutdown with common LED indication of:
- Low oil pressure
- High coolant temperature
- Overspeed
- Emergency stop
- Failure to start (overcrank)
- Low coolant temperature
- Low coolant level

Programmable protective relaying functions:

- Generator phase sequence
- Over/Under voltage (27/59)
- Over/Under Frequency (81 o/u)
- Reverse Power (kW) (32) (4.2 only)
- Reverse reactive power (kVAr) (32RV)
- Overcurrent (50/51)

Communications:

- Four digital inputs (4.1)
- Six digital inputs (4.2 only)
- Four relay outputs (Form A)
- Two relay outputs (Form C)
- Two digital outputs
- Customer data link (Modbus RTU) (4.2 only)
- Accessory module data link (4.2 only)
- Serial annunciator module data link (4.2 only)
- Emergency stop pushbutton

Compatible with the following:

- Digital I/O module
- Local Annunciator
- Remote CAN annunciator
- Remote serial annunciator

## STANDBY 600 ekW 750 kVA

60 Hz 1800 rpm 480 Volts

# FAT

## **TECHNICAL DATA**

Open Generator Set 1800 rpm/60 Hz/480 Volts	DM8518			
Generator Set Package Performance				
Genset Power rating @ 0.8 pf	750 kVA			
Genset Power rating with fan	600 ekW			
Coolant to aftercooler				
Coolant to aftercooler temp max	49 ° C	120 ° F		
Fuel Consumption				
100% load with fan	161.6 L/hr	42.7 Gal/hr		
75% load with fan	129.8 L/hr	34.3 Gal/hr		
50% load with fan	91.7 L/hr	24.2 Gal/hr		
Cooling System <sup>1</sup>				
Air flow restriction (system)	0.12 kPa	0.48 in. water		
Air flow (max @ rated speed for radiator arrangement)	804 m³/min	28393 cfm		
Engine Coolant capacity with radiator/exp. tank	81.8 L	21.6 gal		
Engine coolant capacity	20.8 L	5.5 gal		
Radiator coolant capacity	61.0 L	16.1 gal		
Inlet Air				
Combustion air inlet flow rate	47.8 m³/min	1688.0 cfm		
Exhaust System				
Exhaust stack gas temperature	534.6 ° C	994.3 ° F		
Exhaust gas flow rate	135.5 m³/min	4785.1 cfm		
Exhaust flange size (internal diameter)	203 mm	8 in		
Exhaust system backpressure (maximum allowable)	10.0 kPa	40.2 in. water		
Heat Rejection				
Heat rejection to coolant (total)	189 kW	10748 Btu/min		
Heat rejection to exhaust (total)	634 kW	36056 Btu/min		
Heat rejection to aftercooler	153 kW	8701 Btu/min		
Heat rejection to atmosphere from engine	86 kW	4891 Btu/min		
Heat rejection to atmosphere from generator	41.0 kW	2331.7 Btu/min		
Alternator <sup>2</sup>				
Motor starting capability @ 30% voltage dip	1633 skVA			
Frame	LC7024F			
Temperature Rise	150 ° C	270 ° F		
Lube System				
Sump refill with filter	64.0 L	16.9 gal		
Emissions (Nominal) <sup>3</sup>				
NOx g/hp-hr	5.84 g/hp-hr			
CO g/hp-hr	.48 g/hp-hr			
HC g/hp-hr	.01 g/hp-hr			
PM g/hp-hr	.035 g/hp-hr			

<sup>1</sup> For ambient and altitude capabilities consult your Cat dealer. Air flow restriction (system) is added to existing restriction from factory. <sup>2</sup> Generator temperature rise is based on a 40° C (104° F) ambient per NEMA MG1-32. Some packages may have oversized generators with a different temperature rise and motor starting characteristics.

<sup>3</sup> Emissions data measurement procedures are consistent with those described in EPA CFR 40 Part 89, Subpart D & E and ISO8178-1 for measuring HC, CO, PM, NOx. Data shown is based on steady state operating conditions of 77°F, 28.42 in HG and number 2 diesel fuel with 35° API and LHV of 18,390 btu/lb. The nominal emissions data shown is subject to instrumentation, measurement, facility and engine to engine variations. Emissions data is based on 100% load and thus cannot be used to compare to EPA regulations which use values based on a weighted cycle.

## STANDBY 600 ekW 750 kVA

60 Hz 1800 rpm 480 Volts



## **RATING DEFINITIONS AND CONDITIONS**

Meets or Exceeds International Specifications: AS1359, CSA, IEC60034-1, ISO3046, ISO8528, NEMA MG 1-22, NEMA MG 1-33, UL508A, 72/23/EEC, 98/37/EC, 2004/108/EC

**Standby** - Output available with varying load for the duration of the interruption of the normal source power. Average power output is 70% of the standby power rating. Typical operation is 200 hours per year, with maximum expected usage of 500 hours per year. Standby power in accordance with ISO8528. Fuel stop power in accordance with ISO3046. Standby ambients shown indicate ambient temperature at 100% load which results in a coolant top tank temperature just below the shutdown temperature.

**Ratings** are based on SAE J1349 standard conditions. These ratings also apply at ISO3046 standard conditions. **Fuel rates** are based on fuel oil of 35° API [16° C (60° F)] gravity having an LHV of 42 780 kJ/kg (18,390 Btu/lb) when used at 29° C (85° F) and weighing 838.9 g/liter (7.001 lbs/U.S. gal.). Additional ratings may be available for specific customer requirements, contact your Cat representative for details. For information regarding Low Sulfur fuel and Biodiesel capability, please consult your Cat dealer. 60 Hz 1800 rpm 480 Volts



DIMENSIONS

Package Dimensions							
Length	3933.4 mm	154.86 in					
Width	1536.0 mm	60.47 in					
Height	2165.8 mm	85.27 in					
Weight	4306 kg	9,493 lb					

NOTE: For reference only - do not use for installation design. Please contact your local dealer for exact weight and dimensions. (General Dimension Drawing #2859356).

Performance No.: DM8518

Feature Code: C18DE97

Gen. Arr. Number: 2476127

Source: U.S. Sourced

June 14 2011

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Materials and specifications are subject to change without notice. The International System of Units (SI) is used in this publication.

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Diesel Fire Pump Data Sheet



JU6H-UFAD58 JU6H-UFADM8 JU6H-UFADNG JU6H-UFADMG JU6H-UFADN0

D58 JU6H-UFADP0 . NG JU6H-UFADP8 J DN0 JU6H-UFADQ0 J

0 JU6H-UFAD88 8 JU6H-UFADR0 0 JU6H-UFADR8

JU6H-UFADS8 JU6H-UFADW8 JU6H-UFADS0 JU6H-UFADX8

JU6H-UFADT0

**MODELS** 

JU6H-UFAD98

# USA Purchased - EPA Tier 3 Emissions Certified<sup>1</sup>

# FM-UL-cUL APPROVED RATINGS BHP/KW

JU6H	RATED SPEED									
MODEL	(1760)		2100		23	50	2400			
UFADM8	175	131								
UFADMG			175	131	175	131				
UFAD58	183	137								
UFADNG	190	142	181	135	183	137	183	137		
UFADN0	197	147	197	147	200	149	200	149		
UFADP0	220	164	209	156	211	157	211	157		
UFADP8	220	164								
UFADQ0			224	167	226	169	226	169		
UFAD88	237	177								
UFADR0			238	177.5	240	179	240	179		
UFADR8	250	187								
UFADS8	260	194								
UFADS0			260	194	268	200	268	200		
UFADT0	229	171	274	204	275	205	275	205		
UFADW8	282	211								
UFADX8	305	227.5								
UFAD98	315	235								



Engines are:

EPA Tier 3 Emissions Certified Off-Road (40 CFR Part 89) and NSPS Stationary (40 CFR Part 60 Sub Part IIII); CARB Approved Off-Road (Title 13 CCR Section 2423) and ATCM Stationary (Title 17 CCR Section 93115.6 (a) (4)) for 2010 engines manufactured by John Deere Power Systems.

## SPECIFICATIONS

	JU6H-UFAD MODELS																
ITEM	M8	MG	58	NG	NO	P8	88	P0	Q0	R0	R8	S8	S0	Т0	W8	X8	98
Number of Cylinders		6															
Aspiration		TRWA															
Rotation*		Clockwise (CW)															
Weight – Ib (kg)		1747 (791)															
Compression Ratio		19.0:1 17.0:1															
Displacement - cu. in. (I)		415 (6.8)															
Engine Type		4 Stroke Cycle – Inline Construction															
Bore & Stroke – in. (mm)		4.19 x 5.00 (106 x 127)															
Installation Drawing		D628															
Wiring Diagram AC		C07591															
Wiring Diagram DC		C071367, C071360, C071361 C071368, C071360, C071761															
Engine Series		John Deere 6068 Series Power Tech E John Deere 6068 Series Power Tech Plus															
Speed Interpolation		N/A Opt. N/A Opt. N/A															

Abbreviations: CW – Clockwise TRWA – Turbocharged with Raw Water Aftercooling N/A – Not Available

\*Rotation viewed from Heat Exchanger / Front of engine

#### **CERTIFIED POWER RATING**

- Each engine is factory tested to verify power and performance.
- FM-UL power ratings are shown at specific speeds, Clarke engines can be applied at a single rated RPM setting ± 50 RPM.



- Engines are to be used for stationary emergency standby fire pump service only. Engines are to be tested in accordance with NFPA 25.
- Engines are rated at standard SAE conditions of 29.61 in. (752.1 mm) Hg barometer and 77°F (25°C) inlet air temperature [approximates 300 ft. (91.4 m) above sea level] by the testing laboratory (see SAE Standard J 1349).
- A deduction of 3 percent from engine horsepower rating at standard SAE conditions shall be made for diesel engines for each 1000 ft. (305 m) altitude above 300 ft. (91.4 m)
- A deduction of 1 percent from engine horsepower rating as corrected to standard SAE conditions shall be made for diesel engines for every 10°F (5.6°C) above 77°F (25°C) ambient temperature.







#### Page 1 of 9



JU6H-UFADM8 JU6H-UFAD JU6H-UFADMG JU6H-UFAD

 JU6H-UFAD58
 JU6H-UFADP0
 JU6H-UFAD88
 JU6H-UFADS8

 JU6H-UFADNG
 JU6H-UFADP8
 JU6H-UFADR0
 JU6H-UFADS0

 JU6H-UFADN0
 JU6H-UFADQ0
 JU6H-UFADR8
 JU6H-UFADT0

JU6H-UFADS8 JU6H-UFADW8 JU6H-UFADS0 JU6H-UFADX8 JU6H-UFADT0 JU6H-UFAD98

**MODELS** 

## ENGINE EQUIPMENT

EQUIPMENT	STANDARD	OPTIONAL
Air Cleaner	Direct Mounted, Washable, Indoor Service with Drip Shield	Disposable, Drip Proof, Indoor Service Outdoor Type
Alternator	12V-DC, 42 Amps with Poly-Vee Belt and Guard	24V-DC, 40 Amps with Poly-Vee Belt and Guard
Exhaust Protection	Metal Guards on Manifolds and Turbocharger	
Coupling	Bare Flywheel	UL Listed Driveshaft and Guard, JU6H-UFADMG/58/NG/N0/Q0/R0- CDS30-S1; JU6H-UFADM8/P8/P0/T0/88/R8/S8/S0/W8/X8/98- CDS50-SC at 1760/2100 RPM only
Electronic Control Module	12V-DC, Energized to Stop, Primary ECM always Powered on	24V-DC, Energized to Stop, Primary ECM always Powered on
Exhaust Flex Connection*	Stainless Steel Flex, 150# ANSI Flanged Connection, 5" for JU6H- UFADM8/MG/58/NG/N0/P8/88;	Stainless Steel Flex, 150# ANSI Flanged Connection, 6" for JU6H- UFADM8/MG/58/NG/N0/P8/88;
	Stainless Steel Flex, 150# ANSI Flanged Connection, 6" for JU6H- UFADP0/Q0/R0/R8/S8/S0/T0/W8/X8/98	Stainless Steel Flex, 150# ANSI Flanged Connection, 8" for JU6H- UFADP0/Q0/R0/R8/S8/S0/T0/W8/X8/98
Flywheel Housing	SAE #3	
Flywheel Power Take Off	11.5" SAE Industrial Flywheel Connection	
Fuel Connections	Fire Resistant, Flexible, USA Coast Guard Approved, Supply and Return Lines	Stainless Steel, Braided, cUL Listed, Supply and Return Lines
Fuel Filter	Primary Filter with Priming Pump	
Fuel Injection System	High Pressure Common Rail	
Engine Heater	120V-AC, 1500 Watt	240V-AC, 1500 Watt
Governor, Speed	Dual Electronic Control Modules	
Heat Exchanger	Tube and Shell Type, 60 PSI (4 BAR), NPT(F) Connections	
Instrument Panel	Multimeter to Display English and Metric, Tachometer, Hourmeter, Water Temperature, Oil Pressure and One (1) Voltmeter with Toggle Switch, Front Opening	
Junction Box	Integral with Instrument Panel; For DC Wiring Interconnection to Engine Controller	
Lube Oil Cooler	Engine Water Cooled, Plate Type	
Lube Oil Filter	Full Flow with By-Pass Valve	
Lube Oil Pump	Gear Driven, Gear Type	
Manual Start Control	On Instrument Panel with Control Position Warning Light	
Overspeed Control	Electronic, Factory Set, Not Field Adjustable	
Raw Water Solenoid Operation	Automatic from Fire Pump Controller and from Engine Instrument Panel	
Run – Stop Control	On Instrument Panel with Control Position Warning Light	
Starters	Two (2) 12V-DC	Two (2) 24V-DC
Throttle Control	Adjustable Speed Control by Increase/Decrease Button, Tamper Proof in Instrument Panel	
Water Pump	Centrifugal Type, Poly-Vee Belt Drive with Guard	

Abbreviations : DC – Direct Current, AC – Alternating Current, SAE – Society of Automotive Engineers, NPT(F) – National Pipe Tapered Thread (Female), NPT(M) – National Pipe Tapered Thread (Male), ANSI – American National Standards Institute

\*JU6H-UFADP8/R8/S8/W8/X8/98 – All provided with orifice plate mounted in flex exhaust. Note: Engine Controller needs 2 additional signals: Injector Failure, Alternate ECM Selected



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C132702 revJ 28DEC10 Specifications and information contained in this brochure subject to change without notice.



Fire Protection Products, Inc. JU6H-UFADM8 INSTALLATION & OPERATION DATA (I&O Data)

#### USA Produced

#### Basic Engine Description

Engine Manufacturer	John Deere C	0.				
	Compression (Diesel)					
Number of Cylinders	6	· · · ·				
Bore and Stroke - in (mm)	4.19 (106) X 5 (127)					
Displacement - in <sup>3</sup> (L)	415 (6.8)					
Compression Ratio	_ 19.0:1					
Valves per cylinder						
Intake	_ 1					
Exhaust	_ 1					
Combustion System	Direct Injection	n				
Engine Type	_ In-Line, 4 Stro	ke Cycle				
Fuel Management Control	_ Electronic, Hig	gh Pressure Common Ra	ail			
Firing Order (CW Rotation)	_ 1-5-3-6-2-4					
Aspiration	_ Turbocharged					
Charge Air Cooling Type	_ Raw Water					
Rotation, viewed from front of engine, Clockwise (CW)	_ Standard					
Engine Crankcase Vent System	_ Open					
Installation Drawing	_ D628					
Weight - Ib (kg)	_ 1747 (792)					
	4=00					
Power Rating	<u>1760</u>					
	_ 175 (131)					
Cooling System - [C051386]	1760					
Engine Coolant Heat - Btu/sec (kW)	90 (95)					
Engine Radiated Heat - Btu/sec (kW)	40 (42 2)					
Heat Exchanger Minimum Flow	_ +0 (+2.2)					
$60^{\circ}$ F (15°C) Raw H <sub>2</sub> 0 - gal/min (L/min)	13 (49.2)					
$95^{\circ}$ F (35°C) Raw H <sub>2</sub> O - gal/min (L/min)	20 (75.7)					
Heat Exchanger Maximum Cooling Raw Water	/					
Inlet Pressure - psi (bar)	_ 60 (4.1)					
Flow - gal/min (L/min)	_ 40 (151)					
Typical Engine H <sub>2</sub> 0 Operating Temp - °F (°C) <sup>[1]</sup>	_ 180 (82.2) - 19	95 (90.6)				
Thermostat						
Start to Open - °F (°C)	_ 180 (82.2)					
Fully Opened - °F (°C)	_ 203 (95)					
Engine Coolant Capacity - qt (L)	_ 20.5 (19.4)					
Coolant Pressure Cap - lb/in² (kPa)	_ 15 (103)					
Maximum Engine Coolant Temperature - °F (°C)	_ 230 (110)					
Minimum Engine Coolant Temperature - °F (°C)	_ 160 (71.1)					
High Coolant Temp Alarm Switch - °F (°C)	_ 235 (113)					
Flactric System - DC	Standard		Ontional			
System Voltage (Nominal)	12		24			
Battery Canacity for Ambients Above 32°F (0°C)	12		24			
Voltage (Nominal)	12	[C07633]	24	[C07634]		
Qty. Per Battery Bank	_ 1		2			
SAE size per J537	_ 8D		4D			
CCA @ 0°F (-18°C)	_ 1400		1050			
Reserve Capacity - Minutes	_ 430		290			
Battery Cable Circuit, Max Resistance - ohm	_ 0.0012		0.0012			
Battery Cable Minimum Size						
0-120 in. Circuit Length <sup>[2]</sup>	_ 00		00			
121-160 in. Circuit Length <sup>[2]</sup>	_ 000		000			
161-200 in. Circuit Length <sup>[2]</sup>	0000		0000			
Charging Alternator Maximum Output - Amp,	_ 40	[C071363]	55	[C071365]		
Starter Cranking Amps, Rolling - @60°F (15°C)	_ 440	[RE69704/RE70404]	250	[C07819/C07820]		

NOTE: This engine is intended for indoor installation or in a weatherproof enclosure. <sup>1</sup>Engine H<sub>2</sub>O temperature is dependent on raw water temperature and flow. <sup>2</sup>Positive and Negative Cables Combined Length.


Fire Protection Products, Inc.	JU6H-UFADM8
INSTALLATION	& OPERATION DATA (I&O Data)
	USA Produced

Exhaust System	<u>1760</u>	
Exhaust Flow - ft. <sup>3</sup> /min (m <sup>3</sup> /min)	1100 (31.1)	
Exhaust Temperature - °F (°C)	1000 (538)	
Maximum Allowable Back Pressure - in H <sub>2</sub> 0 (kPa)	30 (7.5)	
Minimum Exhaust Pipe Dia in (mm) <sup>[3]</sup>	5 (127)	
Fuel System	1760	
Fuel Consumption - gal/hr (L/hr)	10.4 (39.4)	
Fuel Return - gal/hr (L/hr)	15.4 (58.3)	
Fuel Supply - gal/hr (L/hr)	25.8 (97.7)	
Fuel Pressure - Ib/in <sup>2</sup> (kPa)	3 (20.7) - 6 (41.4)	
Minimum Line Size - Supply - in.	.50 Schedule 40 Steel Pipe	
Pipe Outer Diameter - in (mm)	0.848 (21.5)	
Minimum Line Size - Return - in.	.375 Schedule 40 Steel Pipe	
Pipe Outer Diameter - in (mm)	0.675 (17.1)	
Maximum Allowable Fuel Pump Suction Lift with clean Filter - in H <sub>2</sub> 0 (mH <sub>2</sub> 0)	_ 80 (2)	
Maximum Allowable Fuel Head above Fuel pump, Supply or Return - ft (m)	6.6 (2)	
Fuel Filter Micron Size	_ 2	
Heater System	Standard	<u>Optional</u>
Engine Coolant Heater		
Wattage (Nominal)	1500	1500
Voltage - AC. 1 Phase	120 (+5%, -10%)	240 (+5%, -10%)
Part Number	[C124948]	[C124949]
		[0.2.0]
Air System	<u>1760</u>	
Combustion Air Flow - ft. <sup>3</sup> /min (m <sup>3</sup> /min)	360 (10.2)	
Air Cleaner	<u>Standard</u>	<u>Optional</u>
Part Number	[C03396]	[C03327]
Туре	Indoor Service Only, with Shield	Canister, Single-Stage
Cleaning method	Washable	Disposable
Air Intake Restriction Maximum Limit		
Dirty Air Cleaner - in H <sub>2</sub> 0 (kPa)	12 (3)	10 (2.5)
Clean Air Cleaner - in $H_20$ (kPa) (Air T = (Air T =))))))))))))))))))))))))))))))	- 6 (1.5)	5 (1.2)
Maximum Allowable Temperature (Air To Engine Inlet) - "F ("C)"	_ 130 (54.4)	
Lubrication System		
	40 (276) - 60 (414)	
Low Oil Pressure Alarm Switch - Ib/in <sup>2</sup> (kPa)	30 (207)	
In Pan Oil Temperature - °F (°C)	_ 220 (104) - 245 (118)	
Total Oil Capacity with Filter - qt (L)	_ 21.1 (20)	
Lube Oil Heater	Optional	Optional
Wattage (Nominal)	150	150
Voltage	_120V (+5%, -10%)	240V (+5%, -10%)
Part Number	C04430	C04431
Performance	<u>1760</u>	
BMEP - lb/in² (kPa)	_ 190 (1310)	
Piston Speed - ft/min (m/min)	1467 (447)	
Mechanical Noise - dB(A) @ 1m	_ C133847	
Power Curve	_ C133746	

<sup>3</sup>Based on Nominal System. Back pressure flow analysis must be done to assure maximum allowable back pressure is not exceeded. (Note: minimum exhaust Pipe diameter is based on: 15 feet of pipe, on 90° elbow, and a silencer pressure drop no greater than one half of the maximum allowable back pressure.) <sup>4</sup>Review for horsepower derate if ambient air entering engine exceeds 77°F (25°C). [] indicates component reference part number.

## JU4H & JU6H ENGINE MODELS ENGINE MATERIALS AND CONSTRUCTION

#### Air Cleaner

Туре	Indoor Usage Only
	<b>Oiled Fabric Pleats</b>
Material	Surgical Cotton
	Aluminum Mesh

### Air Cleaner - Optional

Туре	Canister
Material	Pleated Paper
Housing	Enclosed

#### Camshaft

Material	Cast Iron
	Chill Hardened
Location	In Block
Drive	Gear, Spur
Type of Cam	Ground

#### Charge Air Cooler (JU6H-60,62,68,74,84, ADK0, AD58, ADNG, ADN0, ADQ0, ADR0, AAQ8, AARG, ADP8, ADP0, ADT0, AD88, ADR8, AD98, ADS0, ADW8, ADX8, AD98 only)

Type.....Raw Water Cooled

Materials (	in contact with ra	w wate	er)
Tubes		90/10	CU/NI
Headers		36500	Muntz
Covers		83600	Red Brass
Plumbing		316 St	ainless Steel/ Brass
		90/10	Silicone
-			

### Coolant Pump

Type.....Centrifugal Drive.....Poly Vee Belt

#### **Coolant Thermostat**

Туре	Non Blocking
Qty	1

#### **Connecting Rod**

Туре	I-Beam Taper
Material	Forged Steel Alloy

#### Crank Pin Bearings

Туре	Precision Half Shell
Number	1 Pair Per Cylinder
Material	Wear-Guard

#### **Crankshaft**

Material	Forged Steel
Type of Balance	Dynamic

#### Cylinder Block

Туре	One Piece with
	Non-Siamese Cylinders
Material	Annealed Gray Iron

#### Cylinder Head

Type..... Slab 2 Valve Material.... Annealed Gray Iron

#### Cylinder Liners

Туре	Centrifugal Cast, Wet Liner
Material	Alloy Iron Plateau, Honed

#### <u>Valves</u>

Туре	Poppet
Arrangement	Overhead Valve
Number/Cylinder	1 intake
	1 exhaust
Operating Mechanism	Mechanical Rocker Arm
Type of Lifter	Large Head
Valve Seat Insert	Replaceable

### Fuel Pump

Туре	Diaphragm
Drive	Cam Lobe

#### Heat Exchanger (USA)

Туре	Tube & Shell
<u>Materials</u>	
Tube& Headers	Copper
Shell	Copper
Electrode	Zinc

#### Heat Exchanger (UK)

Tube & Bundle
Copper
Aluminum

#### Injection Pump

Туре	Rotary
Drive	Gear

#### Lubrication Cooler

Type.....Plate

#### Lubrication Pump

Туре	Gear
Drive	Gear

#### Main Bearings

Туре	Precision Half Shells
Material	Steel Backed-Aluminum Lined

#### <u>Piston</u>

Type and Material	Aluminum Alloy with Reinforced
	Top Ring Groove
Cooling	Oil Jet Spray

#### Piston Pin

Type.....Full Floating - Offset

#### Piston Rings

Number/Piston	3
Тор	Keystone Barrel Faced -
	Plasma Coated
Second	Tapered Cast Iron
Third	Double Rail Type
	w/Expander Spring

Wet Cooling Tower Data Sheet



JL Hermon & Associates, Inc. 7342 South Alton Way, Ste. H, Centennial CO 80112 P: 303-771-4045 F: 303-771-6657 E: jmick@jlhermon.com

# MARLEY FIELD ERECTED COOLING TOWER

TO:	Zachry Engineering	DATE:	June 30, 2011
ATTN:	Thomas Freeman – 303-928-4575	FROM:	Jim Mick
PROJECT:	Cheyenne 2 x 1 CC Project	JLH No.	Z01-11-5217

## **BUDGETARY SELECTION**

<b>DESIGN CONDITIONS:</b>	Flow	28,000 gpm
	Hot Water	91 °F
	Cold Water	71 °F
	Wet Bulb	63 °F
	Plume Abatement	None
TOWER DESCRIPTION:	Model	F448A53C4.003A
	Number of Cells	3
	Pump Head	18.41 ft
	Fan Diameter	30 ft
	Motor Size	3 @ 150 Hp
	Brake Horsepower	3 @ 147.5 Hp
	Evaporation	608 gpm
	Drift Rate	0.0005 %
TOWER DIMENSION:	Tower Width	54 ft
	Tower Length	158.2 ft
	Tower Height	39.84 ft
	Fan Deck Height	26.09 ft
BASIN DIMENSION:	Basin Width	54 ft
	Basin Length	158.5 ft
<b>BUDGET PRICE:</b>	\$1,546,000 USD	

This budget price is based upon a scope that includes engineering, prefabrication of materials, freight to jobsite and supervision and labor to field assemble the above field erected cooling tower. The following are not included, and should be provided by the purchaser: Sales and/or use taxes, concrete cold water basin, anchor bolts, fire protection sprinkler system (if required by Owner's insurance underwriter), pumps, piping, valves, water make-up, motor starter, disconnects, and controls.

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# **Greenhouse Gas PSD Permit Application**

Cheyenne Generating Station Cheyenne, Wyoming

Submitted by Black Hills Corporation 1515 Wynkoop Street, Suite 500 Denver, CO 80202

Submitted to U.S. Environmental Protection Agency, Region VIII Denver, CO

Prepared by CH2MHILL。

August 2011



Fred Carl Director Environmental Services 409 Deadwood Avenue • PO Box 1400 Rapid City, South Dakota 57709-1400 P (605) 721-2219, F (605) 721-1338 fred.carl@blackhillscorp.com

August 5, 2011

Mr. Carl Daly Director of Air Programs EPA Region 8 1595 Wynkoop Street Denver, CO 80202-1129

RE: Black Hills Corporation Cheyenne Generating Station Submittal of Greenhouse Gas PSD Construction Air Permit Application

Dear Mr. Daly,

Black Hills Corporation is submitting a Greenhouse Gas PSD Construction Permit Application for the Cheyenne Generating Station in the City of Cheyenne in Laramie County, Wyoming. Included in this submittal are five (5) copies of the permit application in 3-ring binders. As we discussed in the pre-application meeting for this project held in your offices on July 8, 2011, the application for the PSD permit for the criteria pollutant emissions will be submitted to the Wyoming Department of Environmental Quality.

The Cheyenne Generating Station (CGS) will be a nominal 220 MW gross electric generating facility that includes five (5) 40 MW combustion turbines. Two of the turbines will operate in combined cycle mode and three will operate in simple cycle mode. The planned start of construction is summer 2012.

Please contact Tim Rogers, Black Hills Corporation at (605) 721-2286 or Joe Hammond, CH2M HILL at (720) 286-5919 on any questions that EPA may have during the application review. We appreciate your assistance on this important project.

Sincerely, Fred Carl

Director, Environmental Services Black Hills Corporation

Cc Mark Lux, Tim Rogers; BHC Chad Schlichtemeier,;Wyoming DEQ Robert Pearson; CH2M HILL

> Improving life with energy www.blackhillscorp.com

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Black Hills Corporation (Black Hills) plans to construct a new nominal 220-megawatt (MW) gross simple- and combined-cycle natural gas-fired combustion turbine power plant in Laramie County, Wyoming. The project, named the Cheyenne Generating Station (CGS), will be located within the city limits of the City of Cheyenne, Wyoming, approximately 5 miles southeast of the downtown area.

Cheyenne Light, Fuel and Power Company (Cheyenne Light) is a wholly owned subsidiary of Black Hills. It was acquired from Xcel Energy on January 1, 2005, and provides electric utility service to Laramie County, Wyoming, including the City of Cheyenne.

Presently, electricity sold by Cheyenne Light is generated elsewhere (primarily the Gillette, Wyoming, area) and is transmitted to Cheyenne for retail delivery. There is currently no local generation capability in the Cheyenne area. The CGS will provide a local source of electricity to increase the amount of available electricity and to improve reliability of power delivery in the Cheyenne area.

The CGS project will include the following:

- Five 40-MW combustion turbine generators (CTGs) fired by clean-burning natural gas. Two of the turbines will be operated in combined-cycle mode and three will be operated in simple-cycle mode.
- One wet cooling tower for the combined-cycle steam turbine
- Three electric chiller units, each with cooling towers, for inlet air cooling for all of the CTGs
- Six natural gas inlet air heaters for inlet air heating for all of the CTGs
- Two fuel gas heaters, natural gas-fired
- One diesel emergency generator
- One diesel fire pump

In accordance with the terms of federal regulations, Black Hills is applying to U.S. Environmental Protection Agency (EPA) Region 8 for a permit to construct the CGS. The application is limited to requesting a permit for the emissions of greenhouse gases (GHGs) from the CGS and contains a description of the project, a review of applicable federal regulations, a listing of the emissions, and a best available control technology analysis.

The CGS will have potential emissions of 963,874 tons per year (tpy) of GHGs expressed as carbon dioxide equivalent (CO<sub>2</sub>e). This is comprised of 962,929 tpy of carbon dioxide (CO<sub>2</sub>), 1.8 tpy of nitrous oxide (N<sub>2</sub>O), and 18.2 tpy of methane (CH<sub>4</sub>). Because the emissions of CO<sub>2</sub>e exceed 100,000 tpy, this plant will be a major new source and will be subject to the Prevention of Significant Deterioration (PSD) rules.

Because the emission rate of GHG exceeds the 100,000-tpy limit specified in the Final Prevention of Significant Deterioration and Title V Greenhouse Gas Tailoring Rule (Tailoring Rule), a best available control technology (BACT) analysis was performed. The BACT analysis concludes that the CGS project operating at its design energy conversion efficiency is BACT for GHGs.

# Acronyms and Abbreviations

BACT	best available control technology
Black Hills	Black Hills Corporation
CAA	Clean Air Act
CatOx	Catalytic Oxidation
CEM	continuous emissions monitor
CFR	Code of Federal Regulations
CGS	Cheyenne Generating Station
CH <sub>4</sub>	methane
Cheyenne Light	Cheyenne Light, Fuel and Power Company
СО	carbon monoxide
$CO_2$	carbon dioxide
CO <sub>2</sub> e	carbon dioxide equivalent
CTG	combustion turbine generator
°F	degrees Fahrenheit
EPA	U.S. Environmental Protection Agency
FIP	Federal Implementation Plan
FR	Federal Register
GHG	greenhouse gas
GWP	global warming potential
HFC	hydrofluorocarbon
HHV	higher heating value
HRSG	heat recovery steam generator
IPCC	Intergovernmental Panel on Climate Change
IRP	Integrated Resource Plan
kW	kilowatt
kWh	kilowatt-hour

LAER	Lowest Achievable Emission Rate
lb	pound
lb/hr	pound per hour
LHV	lower heating value
MACT	maximum achievable control technology
MRR	Final Mandatory Reporting of Greenhouse Gases Rule, or Mandatory Reporting Rule
MMBtu	million British thermal units per hour
MW	megawatt
N <sub>2</sub> O	nitrous oxide
NAAQS	National Ambient Air Quality Standards
NO <sub>X</sub>	nitrogen oxide
NSR	New Source Review
N <sub>2</sub> O	nitrous oxide
O <sub>2</sub>	oxygen
PFC	perfluorocarbon
PM <sub>10</sub>	particulate matter less than 10 microns in diameter
ppm	parts per million
PTE	potential to emit
PSD	Prevention of Significant Deterioration
RACT	Reasonably Available Control Technology
RBLC	RACT/BACT/LAER Clearinghouse
SCR	Selective Catalytic Reduction
$SF_6$	sulfur hexafluoride
SIP	State Implementation Plan
SO <sub>2</sub>	sulfur dioxide
STG	steam turbine generator
tpy	tons per year
WDEQ	Wyoming Department of Environmental Quality
VOC	volatile organic compound

# SECTION 1.0

Black Hills Corporation (Black Hills) plans to construct a new nominal 220-megawatt (MW) gross simple and combined-cycle combustion turbine power plant located in Laramie County, Wyoming. The project, named the Cheyenne Generating Station (CGS), will be located in the City of Cheyenne approximately 5 miles southeast of the downtown area.

The facility will produce electrical power for Cheyenne Light, Fuel and Power Company (Cheyenne Light), a wholly owned subsidiary of Black Hills. Cheyenne Light provides electric service to Laramie County, Wyoming, and the City of Cheyenne, with more than 38,000 customers.

Presently, electricity sold by Cheyenne Light is generated elsewhere (primarily the Gillette, Wyoming, area) and is transmitted to Cheyenne for retail delivery. There is presently no local generation capability in the Cheyenne area. The CGS will provide a local source of electricity to increase the amount of available electricity and to improve reliability of power delivery in the Cheyenne area.

The power plant will include the following:

- Five 40-MW combustion turbine generators (CTGs) fired by clean-burning natural gas. Two of the turbines will be operated in combined-cycle mode and three will be operated in simple-cycle mode. Operating in combined-cycle will provide approximately 20-MW.
- One wet cooling tower for the combined-cycle steam turbine
- Three electric chiller units, each with cooling towers, for inlet air cooling for all of the CTGs
- Six natural gas inlet air heaters for inlet air heating for all of the CTGs
- Two fuel gas heaters, natural gas-fired
- One diesel emergency generator
- One diesel fire pump

In accordance with the terms of federal regulations, Black Hills is applying to U.S. Environmental Protection Agency (EPA) Region 8 for a permit to construct the CGS. The application is limited to requesting a permit for the emissions of greenhouse gases (GHGs) and contains a description of the project, a review of applicable regulations, a listing of the emissions, and a best available control technology (BACT) analysis.

Section 1.1 provides project contacts and an overview of the documentation being submitted with the application for a permit to construct the CGS.

# 1.1 Project Contacts

The following individuals may be contacted for additional information on this project:

Applicant	Tim Rogers Environmental Manager Black Hills Corporation 625 Ninth Street Rapid City, SD 57709 (605) 721-2286 TRogers@bh-corp.com
Permitting Consultant	Joe Hammond Senior Project Manager CH2M HILL, Inc. 9193 South Jamaica Street Englewood, CO 80112 (720) 286-5919 joe.hammond@ch2m.com

# 1.2 Document Overview

The following is an overview of the information included in this permit application.

- **Section 1.0 Introduction.** This section provides an overview of the project and describes the application organization.
- Section 2.0 Project Description. This section includes a general description of the proposed project including equipment and operations of the project. Information regarding non-emitting processes and equipment is provided for a general understanding of plant operations.
- Section 3.0 Greenhouse Gas Emissions Summary. This section provides a summary of emissions-related information.
- Section 4.0 Greenhouse Gas Regulatory Review. This section contains a detailed regulatory review of federal GHG air regulations that may impact the permitting, construction, or operation of the proposed project.
- Section 5.0 BACT Analysis. This section includes a BACT analysis for GHG pollutants. This analysis follows the EPA-prescribed five-step top-down approach. Requested permit limits are also included in this section.
- **Appendix A Location Map and Plot Plan.** This appendix includes a location map, plot plan, and general equipment arrangement drawing for the proposed project.
- **Appendix B Greenhouse Gas Supporting Documentation.** This appendix contains the calculations used to determine the GHG emissions for this permit application.

# Project Description

Black Hills proposes to construct and operate the CGS in Cheyenne, Wyoming. A plot plan of the facility and a map detailing the location of the proposed facility can be found in Appendix A. The facility will be a nominal 220-MW gross output power plant that will produce electrical power for the Black Hills-owned Cheyenne Light, Fuel and Power (CLFP) electric retail service territory in Laramie County, Wyoming, including the City of Cheyenne and Black Hills Power (BHP) service territory in Wyoming and South Dakota. Facility output varies with ambient temperature, with higher output at lower ambient temperatures. A general arrangement of the turbine layout and associated equipment can be found in Appendix A.

The CGS facility configuration was selected based upon the needs identified in the CLFP *Integrated Resource Plan* (IRP).<sup>1</sup> The CLFP Certificate of Public Convenience and Necessity (CPCN) was filed with the Wyoming Public Service Commission (August 1, 2011 – Docket Number 20003-112-EA11) and was based upon CLFP IRP that identified three simple-cycle combustion turbines (nominally 120 MW gross output). The CLFP CPCN further identifies the potential build-out of the site to accommodate future generation needs. Black Hills plans to submit a BHP CPCN in fall 2011 and will be based upon the BHP IRP that tentatively (plan has not been finalized) identifies the need for two simple-cycle combustion turbines configured in combined cycle mode (nominally 100 MW gross output). The Black Hills' Integrated Resource Plans will show the public need for increased capacity requirements in the CLFP and BHP service areas, reserve generation requirements, and generation within the service area of Cheyenne for reliability reasons. The necessary generation will be primarily peaking with base-load capability and further enable renewable generation (wind, solar, and other renewable resources).

The proposed CGS facility will consist of five combustion turbines. Combustion turbines CT01A and CT01B will operate in a 2 X 1 combined-cycle design consisting of two 40-MW CTGs with one heat recovery steam generator (HRSG) for each CTG with no duct burners. Steam from the HRSGs will be combined to flow to a steam turbine that will produce additional electricity. The total generating capacity of the combined-cycle configuration will be approximately 100 MW. Combustion turbines CT02A, CT02B, and CT03A, will each be high-efficiency 40-MW CTGs, operating in simple-cycle mode.

Inlet air chillers with wet cooling towers will be provided for each CTG to cool the combustion air, which will enhance overall plant output during times of higher ambient temperature. Inlet air heaters will also be provided for each CTG to heat the combustion air, which will prevent icing during times of lower ambient temperature.

The proposed CGS facility will also have fuel gas pre-heaters, an emergency generator, and a fire pump.

<sup>&</sup>lt;sup>1</sup> The IRP determines the capacity expansion, which takes into consideration the size of the electrical systems' demand, and further defines the size of combustion turbines selected.

# 2.1 Power Generation

Power will be produced in the plant by a total of six generators, one for each of the five 40-MW CTGs plus one steam turbine generator (STG). All other facility operations ancillary to the primary generation function are described below.

# 2.2 Emission Sources

# 2.2.1 Combined-Cycle Combustion Turbine Generators

The CGS will use two 40-MW combustion turbines CT01A and CT01B will be operated in a 2 X 1 combined-cycle design with two CTGs and one steam turbine. The combustion turbines will be fired exclusively with pipeline-quality natural gas and are very similar to large aircraft jet engines in function and design. The combustion turbines will be equipped with unfired (no duct burner) HRSGs to extract heat from each combustion turbine exhaust to make steam. The steam will be used in an STG to produce more electricity. The combined-cycle configuration will consist of two CTGs, two HRSGs (one for each CTG), and one STG.

# 2.2.2 Simple-Cycle Combustion Turbine Generators

The CGS will use three 40-MW combustion turbines operated in simple-cycle mode, without heat recovery from the turbine exhaust. These combustion turbines, designated as CT02A, CT02B, and CT03A, will be fired exclusively with pipeline-quality natural gas and are very similar to large aircraft jet engines in function and design. The combustion turbines have the capability to reach full-load operation quickly after initiation of startup, thereby reducing overall startup emissions.

Each combustion turbine consists of a compressor, combustor, and expansion turbine. After filtration, air passes through the compressor before combining with the fuel and entering the low nitrogen oxide (NO<sub>X</sub>) combustor. The combustion products and compressed air pass through the expansion turbine, which drives both the compressor and the generator. Up to approximately 40 MW of gross electrical power are produced by each CTG over and above the work required by the compressor. The exhaust gas from each combustion turbine enters the Selective Catalytic Reduction (SCR) and Catalytic Oxidation (CatOx) catalysts at high temperature (approximately 850 degrees Fahrenheit [°F] at full load).

# 2.2.3 Wet Cooling Towers

## 2.2.3.1 Inlet Chiller Cooling Towers

An inlet air chilling system will be installed at the compressor inlet of each CTG, downstream of the inlet air filter. The inlet air chilling system serves to enhance the overall output of the plant by lowering the temperature of the ambient air entering the CTGs during periods of high air temperature. The cooling process takes place at the cooling coils where air is cooled before entering the compressor section of the turbine. At low temperatures, the air becomes denser and, therefore, more air flows though the CTGs. The net increase in airflow results in higher power output for each of the CTGs at high ambient temperatures. Three inlet chiller cooling towers will be used to serve the inlet chilling system at CGS.

## 2.2.3.2 Unit 1 Cooling Tower

One wet cooling tower will be installed to provide cooling to condense the steam that is exhausted from the steam turbine on the combined cycle configuration. The steam condensers will have circulating cooling water flow through tubes that will absorb the heat from the condensing steam that is exhausted from the steam turbines. The warmed circulating water is then pumped to the cooling tower where it flows down through the tower and is cooled through evaporation, in a manner similar to other cooling towers. The cooled circulating water then flows back to the steam condensers to pick up more heat.

# 2.2.4 Inlet Air Heaters

An inlet air heating system will be installed at the compressor inlet of each CTG, upstream of the inlet air filter. The inlet air heating system **raises** the temperature of the ambient air entering the CTGs during periods of low air temperature to prevent icing.

## 2.2.5 Fuel Gas Heaters

A fuel gas pre-heat system will be utilized on each CTG to raise the temperature of the natural gas above the saturation temperature. Natural gas fired fuel gas heaters will be used on the five combustion turbines.

# 2.2.6 Diesel Fire Pump

One diesel fire pump will be used to provide fire protection water for the plant. This engine will fire only ultra-low-sulfur diesel fuel, and will operate only during testing that is anticipated to occur once per week. Total operating hours for the fire pump are 250 hours per year or less.

# 2.2.7 Emergency Generator

One diesel emergency generator will be used to provide emergency power for the plant. This engine will fire only ultra-low-sulfur diesel fuel, and will operate only during testing that is anticipated to occur once per week. Total operating hours for the emergency generator are 250 hours per year or less.

# 2.2.8 Storage Tanks

Storage tanks at the site will include diesel tanks for the fire water pump and emergency generator, aqueous ammonia storage tanks for the SCR NO<sub>x</sub> emissions control unit, and several water storage tanks.

# 2.3 Non-Emitting Major Facility Components

# 2.3.1 Ancillary Facilities

Other facilities used to support power generation at the CGS will include the following:

- Water treatment system to remove solids and hardness from plant makeup water
- Wastewater treatment system to allow recycle of cooling tower blowdown and other plant wastewater
- Plant and instrument air compressors (electric-driven) and auxiliary equipment

- Plant sumps, sump pumps, and oily water separator
- Miscellaneous fire protection equipment
- Septic system for sanitary waste
- Steam and water sampling systems
- Administration and warehouse/maintenance buildings

# 2.4 Emission Controls

The CGS will include the following emission controls:

- Dry low NO<sub>X</sub> burners on the CTGs, and a SCR system to reduce NO<sub>X</sub> emissions on all CTGs
- An oxidation catalyst to reduce carbon monoxide (CO) and volatile organic compound (VOC) emissions from the CTGs
- Good combustion design and operation to reduce particulate matter of 10 microns in diameter (PM<sub>10</sub>) emissions from the CTGs
- Use of pipeline-quality natural gas to minimize sulfur dioxide (SO<sub>2</sub>) emissions from the CTGs
- High-efficiency drift eliminators on the steam condenser cooling towers to reduce PM<sub>10</sub> emissions in the cooling tower drift

# 2.5 Emissions Monitoring

As required by Title 40 of the Code of Federal Regulations (CFR) Parts 60 and 75, the CGS will use continuous emissions monitors (CEMs) for NO<sub>X</sub>, CO, and oxygen (O<sub>2</sub>) for all five CTGs. These CEMs will average and record data on frequencies consistent with state and federal acid rain rules. The plant will also monitor and record the natural gas flow rate and will analyze natural gas fuel quality as required by the acid rain rules.

# 2.6 Operating Schedule

The exact annual operating schedule of the CGS will be dependent on the demand for electric power within Cheyenne Light's electric system. Thus, the exact operating schedule cannot be accurately predicted at this time.

For this reason, the permit limits requested in this application, and the resulting assumptions used in the ambient impact analysis and BACT analysis, are as follows:

- Up to 8,760 hours per turbine per year of CTG operation (both simple and combined cycle) at 100 percent load or at any lesser load rate
- Up to 600 startups for each simple-cycle combustion turbine per year
- Up to 600 startups for each combined-cycle combustion turbine per year

- Up to 5,330 hours per tower per year of inlet chiller cooling tower operation
- Up to 8,760 hours per year of combined-cycle cooling tower operation

These hours could be based on continuous short-term or long-term operation. In other words, the plant could operate up to 8,760 hours per year (counting startup episodes) and could operate 24 hours per day, 7 days per week, and 365 days per year.

# 2.7 Permitting and Construction Schedule

The planned permitting and construction timeline is shown in Table 2-1.

TABLE 2-1

Permitting and Construction Schedule

Event	Date	
Air Permit Application Filed with EPA	August 5, 2011	
Air Permit Application Filed with WDEQ	September 1, 2011	
Air Permits Issued by EPA and WDEQ	Summer 2012	
Begin Purchase Major Pieces of Equipment	Summer 2012	
Start of Construction	Summer 2013	
Commercial Operation	Summer 2014	

GHG emission estimates were prepared for all point emissions sources from the CGS, including the combustion turbines and auxiliary equipment. The annual carbon dioxide  $(CO_2)$  equivalent  $(CO_2e)$  emissions were estimated based on 100 percent capacity factor (full-load operation for 8,760 hours per year) for each of the combustion turbines. More detailed GHG emission calculations are provided in Appendix B.

# 3.1 Combustion Turbines

The CGS project consists of two nominal 40-MW combustion turbines operating in a 2 X 1 combined-cycle configuration, designated as CT01A and CT01B. There will also be three nominal 40-MW combustion turbines operating in simple cycle identified as CT02A, CT02B, and CT03A. Each combustion turbine has a separate stack, which will be a separate emission point.

# 3.2 Auxiliary Equipment

In addition to the five combustion turbines planned for the CGS project, there are several other small GHG combustion sources associated with auxiliary equipment that will operate at the CGS:

- (6) Natural gas-fired inlet air heaters (nominal 16-million-British-thermal-units-per hour [MMBtu/hr] air heater with estimated emissions of 4,117 CO<sub>2</sub>e tons/year each)
- (2) Natural gas-fired fuel gas heaters (nominal 4.5-MMBtu/hr gas heater with estimated emissions of 1,153 CO<sub>2</sub>e tons/year each)
- (1) Diesel-fired emergency generator (nominal 839-BHP engine with estimated emissions of 226 CO<sub>2</sub>e tons/year each)
- (1) Diesel-fired fire pumps (nominal 327-BHP engine with estimated 51 CO<sub>2</sub>e tons/year each)

# 3.3 GHG Emission Summary

The GHG emission sources for the project are shown in Table 3-1, along with estimated annual  $CO_2e$  emissions.

TABLE 3-1

GHG	Emission	Source	Summary	
				_

Source Number	Emission Point	Estimated Annual CO <sub>2</sub> e Emissions
EP01 and EP02	(2) Nominal 40-MW Combined-Cycle Combustion Turbines CT01A and CT01B	374,635
EP03, EP04, and EP05	(3) Nominal 40-MW Combined-Cycle Combustion TurbinesCT02A, CT02B, and CT03A	561,953
EP06 through EP11	Six (6) Inlet Air Heaters	24,703
EP18 and EP19	Two (2) Fuel Gas Heaters	2,306
EP16	One (1) Diesel Fire Pump	51
EP15	One (1) Diesel Standby Generator	226

# Regulatory Review

This section provides a regulatory review of the applicability of federal air quality permitting requirements for GHGs and GHG air pollution control regulations for the CGS project proposed by Black Hills. The purpose of this section is to provide appropriate explanation and rationale regarding the applicability of these regulations to the CGS project. The review is limited to federal regulations for GHG because there are no State of Wyoming regulations for GHG that apply to the permitting of CGS. Because the Wyoming Department of Environmental Quality (WDEQ) has a SIP-approved PSD program for all criteria pollutants but has not adopted regulations under the Tailoring Rule, WDEQ is the permitting authority for the CGS non-GHG pollutants (other regulated NSR pollutants), while EPA Region 8 is the permitting authority for the CGS GHG pollutants. Both agencies have agreed to work together to process these two air permits for CGS.

# 4.1 Federal Regulations

The proposed project was evaluated to determine compliance with applicable federal GHG air quality regulations. Potentially applicable federal GHG regulations include the following:

- Final Prevention of Significant Deterioration and Title V Greenhouse Gas Tailoring Rule (Tailoring Rule) 40 CFR 51.166, 52.21, as published in the *Federal Register* (FR) June 3, 2010 (75 FR 31514)
- Federal Implementation Plan (FIP) for State of Wyoming GHG 40 CFR 52.37, as published in the *Federal Register* December 30, 2010 (75 FR 82246)
- New Source Review (NSR) 40 CFR 51 and 52

On April 2, 2007, the U.S. Supreme Court found that GHGs are air pollutants under Clean Air Act (CAA) section 302(g) (*Massachusetts* v. *EPA*, 549 U.S. 497 [2007]). GHG includes the six gases of CO<sub>2</sub>, nitrous oxide (N<sub>2</sub>O), methane (CH<sub>4</sub>), hydrofluorocarbons (HFCs), perfluorocarbons (PFCs), and sulfur hexafluoride (SF<sub>6</sub>). Of these, the first three will be emitted from the CGS. These gases have different potential to affect global warming, termed the global warming potential (GWP). The GWP of the three emitted gases are CO<sub>2</sub> (1), N<sub>2</sub>O (310), and CH<sub>4</sub> (21).

Based on the series of legal and regulatory actions that culminated in the Tailoring Rule, regulation of major increases of GHG emissions through the Prevention of Significant Deterioration (PSD) permit program was required. EPA recognized that the major source threshold levels for the criteria pollutants for PSD pollutants of 100 or 250 tons per year (tpy) would make virtually every new project a major source. Accordingly, in June, 2010, EPA adopted the Tailoring Rule to raise the major source thresholds for GHG to 75,000 or 100,000 tons of GHG per year.

The State of Wyoming has an approved State Implementation Plan (SIP) based program for the criteria pollutants for the PSD permitting of new major sources. However, Wyoming has decided to not include GHG in the state PSD permitting program. Accordingly, the GHG PSD program is being implemented by the EPA for major sources of GHG within the State of Wyoming through the federally approved FIP.

## 4.1.1 Greenhouse Gas Tailoring Rule

On June 3, 2010, EPA issued the final Tailoring Rule (75 FR 31514), which allowed the phasing in of the PSD permitting process for new major sources of GHGs such as the CGS project. Step 2 of the Tailoring Rule requires that beginning July 1, 2011, all new sources with the potential to emit (PTE) greater than 100,000 tpy of CO<sub>2</sub>e (including the statutory threshold of 100 or 250 tons on a mass basis) comply with PSD and Title V requirements. All references to "tons" are provided in terms of short tons (2,000 pounds/ton) instead of metric tonnes, in accordance with EPA GHG PSD permitting guidance.

As shown in Table 4-1, under the Tailoring Rule, the CGS will be a major source subject to PSD permitting because the total emissions of CO<sub>2</sub>e exceed 100,000 tpy. The CGS project will result in an increase in CO<sub>2</sub>e emissions of 963,874 tpy, and more than 100 tpy in certain criteria pollutants. Therefore, the project is classified as a major source for PSD applicability determination.

### TABLE 4-1

GHG Pollutants Expected to be Emitted, Annual Emission Rates, Global Warming Potential, and Annual Emissions Rates Adjusted for Global Warming Potential

Pollutant	Proposed Facility GHG Emissions (TPY)	Global Warming Potential (GWP)	GHG Emissions Adjusted for GWP (TPY)
Carbon Dioxide (CO <sub>2</sub> )	962,929	1	962,929
Nitrous Oxide (N <sub>2</sub> O)	1.82	310	564
Methane (CH <sub>4</sub> )	18.17	21	381
Total GHG as CO <sub>2</sub> e			963,874

## 4.1.2 Federal Implementation Plan for Wyoming

EPA has determined that the Wyoming SIP is deficient for purposes of the PSD permitting of GHG. Accordingly, EPA adopted a FIP in which it retains the authority to issue a PSD permit for GHG. Thus, this application is being filed with EPA Region 8 for the sole purpose of obtaining a PSD permit for the emissions of GHG from the CGS. The permit for the emissions of the criteria and hazardous pollutants from CGS will be obtained from the State of Wyoming.

EPA has not adopted ambient air quality standards or new source performance standards for GHG. Accordingly, this application only contains a BACT analysis for GHG.

## 4.1.3 New Source Review

PSD is the portion of NSR that applies to pollutants that are in attainment of National Ambient Air Quality Standards (NAAQS). Because there are no ambient air quality standards for GHG, all portions of the United States are in attainment for GHG. Major new or modified air emission sources locating in Laramie County are, therefore, potentially subject to PSD review for these GHG pollutants.

The first step in PSD review is determining whether the proposed facility is a major PSD source. As noted above, the CGS will be a major source. Therefore, CGS is subject to PSD review for GHG. The primary elements of PSD requirements are as follows:

• Application of BACT to emissions of GHG

# 5.1 Background

Black Hills plans to build a natural gas-fired combustion turbine generating facility in the southeast section of the City of Cheyenne in Laramie County, Wyoming, pursuant to its approved *Integrated Resource Plan* filed before the Wyoming Public Service Commission (described in Section 2.0, Project Description). The proposed site is immediately west of the Dry Creek Water Reclamation Facility, which is located approximately 5 miles southeast of the downtown area.

The CGS will consist of a total of five natural gas-fired CTGs sized at a nominal 40-MW capacity each. Two CTGs will be configured for combined-cycle operation and will each be equipped with dry-low NO<sub>x</sub> combustors and a HRSG without duct burners, with steam flowing from the two HRSGs to one condensing STG with condenser in a "2x1" configuration. The combined-cycle generation capacity is nominally 100 MW. All of the CTGs will be equipped with SCR for NO<sub>x</sub> control and Catalytic Oxidation for CO and VOC control. Three CTGs will operate in simple cycle. CGS auxiliary equipment includes one mechanical draft cooling towers, six natural gas-fired inlet air chiller units with mechanical draft cooling towers, six natural gas-fired inlet air heaters, two natural gas-fired fuel heaters, one diesel-fired fire pump, and one diesel-fired emergency generator.

# 5.1.1 CGS Business Plan and Combustion Turbine Selection

The Cheyenne Light CPCN and associated IRP (Docket Number 20003-112-EA11), were filed August 1, 2011, with the Wyoming Public Service Commission, and present the business plan in detail. The Black Hills Power CPCN and associated IRP will be submitted to the Commission in fall 2011. Generally, Black Hills' CPCN and associated IRP show the public need for increased capacity requirements, reserve generation requirements, and generation within the service area of Cheyenne for reliability reasons. The necessary generation will be primarily peaking with baseload capability and further enable renewable generation (wind, solar, and other renewable resources). Black Hills identified natural gas simple-combined-cycle gas turbines to be the best-suited generation source to meet this CGS business plan<del>.</del>

While Black Hills has determined the nominal output of each combustion turbine to be 40 MW, the combustion turbine manufacturer has not been selected. Table 5-1 lists potential combustion turbine manufacturers and a comparison of estimated performance efficiency at the CGS site conditions.

#### TABLE 5-1

Combustion Turbine Comparison

Turbine <sup>1</sup>	Production (kW)	Gross Heat Rate (Btu/kWh) HHV	Efficiency	
Dresser-Rand				
DR-63G PC	35,150	9,095	37.5%	
GE Energy Aeorderivative		· · · ·		
LM6000PC	39,253	9,487	36.0%	
LM6000PC Sprint	40,605	9,419	36.2%	
LM6000PD	34,612	9,103	37.5%	
LM6000PD Sprint	38,079	9,091	37.5%	
LM6000PF	34,612	9,103	37.5%	
LM6000PF Sprint	38,649	9,079	37.6%	
LM6000PG	42,995	9,556	35.7%	
GE Energy Oil & Gas				
LM6000PD	33,964	9,283	36.8%	
IHI Power Systems				
LM6000PC	34,306	9,198	37.1%	
LM6000PC Sprint	37,129	9,228	37.0%	
LM6000PD	33,800	9,231	37.0%	
LM6000PD Sprint	37,236	9,213	37.0%	
LM6000PG	40,084	9,157	37.3%	
Pratt & Whitney Power System	S			
FT8 TwinPac	41,267	9,898	34.5%	
SwiftPac 50 DLN	41,175	9,914	34.4%	
Rolls-Royce				
Trent 60 DLE	41,537	9,064	37.7%	
Trent 60 DLE ISI	46,612	8,913	38.3%	
Siemens Energy				
SGT-800	37,772	10,126	33.7%	
SGT-900	39,781	11,626	29.4%	

<sup>1</sup> Specifications for production output at 59°F, 5,950-Foot Altitude, Gross Output, HHV.

Black Hills will select a combustion turbine that best meets its business plan, its system, and operational criteria, with possible selection of any combustion turbine from Table 5.1. A key consideration is that installation of combustion turbines from only one manufacturer is desired, and both simple-cycle and combined-cycle operational considerations must be evaluated. Due to differences in exhaust temperatures and other factors, turbines with lower efficiency than others in simple-cycle operation. As will be demonstrated below, Black Hills proposes to establish annual GHG mass and output-based limits assuming use of a turbine from the top of the possible efficiency range, and will agree to comply with those limits regardless of actual turbine selection. Black Hills will perform a complete competitive bidding process to select the combustion turbine for the CGS project, and the selected combustion turbine will be subject to the GHG BACT permit limits established by EPA as part of this permitting process.

Therefore, Table 5-2 below lists the assumed combustion turbine attributes to be used within the GHG BACT analysis, and represents high-efficiency operation in both simpleand combined-cycle operation.

Combustion Turbine Criteria	Assumed Value <sup>1</sup>
Simple-Cycle Combustion Turbine Gross Output (MW)	37
2x1 Combined-Cycle Combustion Gross Turbine Output (MW)	97
Simple-Cycle Gross Heat Rate (Btu/KWh) HHV	9,300
Combined-Cycle Gross Heat Rate (Btu/KWh) HHV	7,200
Heat Input (Btu/hr) HHV	366

TABLE 5-2

Efficient Combustion Turbine Definition

<sup>1</sup> 60<sup>0</sup> F at site elevation.

# 5.2 Regulatory Basis

GHGs have become subject to emission permitting through PSD and Title V programs. On June 3, 2010, EPA issued the final Tailoring Rule (75 FR 31514), which allowed phasing in the PSD permitting process for new sources of GHGs such as the CGS project. Step 2 of the Tailoring Rule requires that beginning July 1, 2011, all new sources with PTE greater than 100,000 tpy of GHGs on a CO<sub>2</sub>e basis, and with a GHG PTE of 100 or 250 tpy, depending on source type, on a mass basis will become subject to PSD and Title V requirements. All references to tons within the table and in this BACT analysis are provided in terms of short tons (2,000 pounds/ton) instead of metric tonnes, in accordance with EPA GHG PSD permitting guidance.

The CGS project will be a new source with a GHG PTE of greater than 100,000 tpy CO<sub>2</sub>e and greater than the 100-tpy mass basis for listed sources, and will also have a PTE of greater than 100 tpy for certain criteria pollutants. Because the Wyoming Department of Environmental Quality (WDEQ) has a SIP-approved PSD program for all criteria pollutants but has not adopted regulations under the Tailoring Rule, WDEQ is the permitting authority

for the CGS non-GHG pollutants (other regulated NSR pollutants), while EPA Region 8 is the permitting authority for the CGS GHG pollutants. Therefore, this GHG BACT analysis was prepared for presentation to EPA Region 8 as part of the CGS permit application process.

# 5.3 Emissions Summary

Per EPA Tailoring Rule definitions, GHGs consist of the following gases:

- Carbon Dioxide (CO<sub>2</sub>)
- Methane (CH<sub>4</sub>)
- Nitrous oxide (N<sub>2</sub>O)
- Hydrofluorocarbons (HFCs)
- Perfluorocarbons (PFCs)
- Sulfur hexafluoride (SF<sub>6</sub>)

To determine CO<sub>2</sub>e emissions, mass flows of each individual gas are multiplied by the appropriate GWP as referenced to the Intergovernmental Panel on Climate Change (IPCC) Second Assessment Report, and the results are summed.

The combustion turbines, inlet air heaters, and fuel gas heaters will be fired with pipelinequality natural gas, and complete combustion will result in water and  $CO_2$  byproducts. However, incomplete combustion will result in some unburned natural gas or CH<sub>4</sub> emissions. Additionally, due to the presence of nitrogen in the combustion air, some small quantities of N<sub>2</sub>O will also be emitted. The standby generator and fire pump engines will be fired with diesel fuel, again resulting in  $CO_2$  emissions from oxidation of the fuel and with minor quantities of CH<sub>4</sub> emissions resulting from incomplete combustion and N<sub>2</sub>O emissions from conversion of nitrogen from the atmosphere and fuel.

Table 5-3 represents potential sources and estimated quantities of GHG emissions from CGS project equipment.

TABLE 5-3

Equipment	Description	Total CO <sub>2</sub> e Emissions (t/yr)	
Two (2) Combustion Turbines in Combined-Cycle Operation with no HRSG Duct Burner	vo (2) Combustion Turbines Combined-Cycle Operation th no HRSG Duct Burner		
Three (3) Simple-Cycle Combustion Turbines	Maximum Heat Input Each 366 MMBtu/hr Higher Heating Value (HHV)	561,953	
Two (2) Fuel Gas Heaters	Maximum Heat Input 4.5 MMBtu/hr each	2,306	
One (1) Diesel Fire Pump	Maximum Heat Input 2.5 MMBtu/hr	51	
One (1) Diesel Standby Generator	Maximum Heat Input 5.52 MMBtu/hr	226	
Six (6) Inlet Air Heaters	Maximum Heat Input 16.07 MMBtu/hr each	24,703	
Total		963,874	

CGS Estimated GHG Emissions by Equipment Category

## 5.3.1 GHG BACT Analysis Assumptions

During the completion of GHG BACT analysis, the following assumptions were made:

- 1. Table 5-3 above presents estimated CGS GHG emissions in terms of CO<sub>2</sub>e emissions, and only includes emissions of CO<sub>2</sub>, CH<sub>4</sub>, and N<sub>2</sub>O. The CGS is not expected to emit HFCs or PFCs because these man-made gases are primarily used as cooling, cleaning, or propellant agents. SF<sub>6</sub> is also a man-made gas that may be used as an insulating gas for high-voltage equipment and circuit breakers; however, Black Hills does not plan to install electrical equipment containing SF<sub>6</sub> at the CGS. Therefore, only CO<sub>2</sub>, CH<sub>4</sub>, and N<sub>2</sub>O will be included in CO<sub>2</sub>e totals.
- 2. From the GHG emissions inventory presented in Appendix A, the relative quantities of  $CH_4$  and  $N_2O$  total only approximately 20 tpy, or less than 0.002 percent of total  $CO_2e$  emissions. Due to the extremely small contribution of  $CH_4$  and  $N_2O$  emissions to the total, the CGS GHG BACT analysis only included the five-step process for  $CO_2$  emissions.
- 3. Completion of the BACT analysis for criteria pollutants will result in the installation of an SCR system for NO<sub>x</sub> emissions reduction, and an oxidation catalyst for control of CO and VOCs for each turbine.
- 4. During actual combustion turbine operation, the oxidation catalyst may result in minimal increases in CO<sub>2</sub> from the oxidation of any CO and CH<sub>4</sub> in the flue gas. However, the EPA Final Mandatory Reporting of Greenhouse Gases Rule (Mandatory Reporting Rule or MRR) (40 CFR 98) factors for estimating CO<sub>2</sub>e emissions from the combustion of natural gas assume complete combustion of the fuel. While the oxidation catalyst has the potential of incrementally increasing CO<sub>2</sub> emissions, these emissions are already accounted for in the MRR factors and included in the CO<sub>2</sub>e totals.
- 5. Similarly, the SCR catalyst may result in an increase in N<sub>2</sub>O emissions. Although quantifying the increase is difficult, it is generally estimated to be very small or negligible. From the GHG emissions inventory, the estimated N<sub>2</sub>O emissions from all combustion turbines total only 1.5 tpy. Therefore, even if there were an order-of-magnitude increase in N<sub>2</sub>O as a result of the SCR, the impact to CO<sub>2</sub>e emissions would be insignificant.

Use of the SCR and oxidation catalyst slightly decreases the project thermal efficiency due to backpressure on the turbines (these impacts are already included in the emission inventory) and, as noted above, may create a marginal but unquantifiable increase to N<sub>2</sub>O emissions. The combustion turbine SCR systems will be designed to reduce NO<sub>x</sub> from the combustion turbine low-NO<sub>x</sub> burners (LNBs) from 25 parts per million (ppm) to 3 ppm. Similarly, the oxidation catalyst systems have the benefits of reducing both CO and VOCs. The oxidation catalyst reduces CO and VOC emissions from 70 ppm to 6 ppm, and from 8.4 ppm to 3 ppm, respectively.

While elimination of the NO<sub>x</sub> and CO/VOC controls could conceivably be considered as an option within the GHG BACT, the environmental benefits of the NO<sub>x</sub>, CO, and VOC control are assumed to outweigh the marginal increase to GHG emissions. Thus, even if carried forward through the GHG BACT analysis, they would be eliminated in Step 4 due to other

environmental impacts. Therefore, we have not considered omission of these controls within the BACT analysis.

# 5.4 Top-Down BACT Process

The EPA has developed a recommended process for conducting BACT analyses, referred to as the "top-down" method. The following steps to conducting a top-down analysis are listed in the EPA's *New Source Review Workshop Manual* (EPA, 1990):

- Step 1: Identify all control technologies
- Step 2: Eliminate technically infeasible options
- Step 3: Rank remaining control technologies by control effectiveness
- Step 4: Evaluate most effective controls and document results
- Step 5: Select BACT

Each of these steps, described in the following sections, has been conducted for GHG emissions for the CGS project. The following top-down BACT analysis for CO<sub>2</sub>e has been prepared in accordance with the EPA's *New Source Review Workshop Manual* (EPA, 1990). A top-down BACT analysis takes into account energy, environmental, economic, and other costs associated with each alternative technology.

# 5.5 Combustion Turbine BACT for GHGs

## Step 1: Identify All Control Technologies

The combustion turbines will be nominal 40 MW machines that utilize the latest emissions control technology. There are two basic alternatives identified to limit the GHG emissions of this project. These options include

- Carbon Capture and Storage (CCS)
- Electrical Generation Efficiency

Black Hills' CGS Business Plan and IRP have determined that the proposed mix of natural gas combined-cycle and simple-cycle power generation is the only alternative that meets all of the CGS requirements for economic and reliable power 24 hours per day and in all weather conditions. As such, other generation technologies such as coal, wind, and solar were not evaluated in this BACT analysis. This is consistent with EPA's March 2011 *PSD and Title V Permitting Guidance for Greenhouse Gases*, which states, "EPA has recognized that a Step 1 list of options need not necessarily include inherently lower polluting processes that would fundamentally redefine the nature of the source proposed by the permit applicant...", and "...the permitting authority should keep in mind that BACT, in most cases, should not regulate the applicant's purpose or objective for the proposed facility..." (p. 26) Nonetheless, it should be noted that the CGS is intended to provide supplemental and backup generation for solar and wind projects, and renewable generation is not an adequate supplement and backup for other renewable generation; a fuel-based alternative is required.

The only identified alternatives are post-combustion CCS and energy efficiency of the proposed generation facility.

## Step 2: Eliminate Technically Infeasible Options Effectiveness Carbon Capture and Storage Systems

CCS systems involve use of adsorption or absorption processes to remove  $CO_2$  from flue gas, with subsequent desorption to produce a concentrated  $CO_2$  stream. The concentrated  $CO_2$  is then compressed to "supercritical" temperature and pressure, a state in which  $CO_2$ exists neither as a liquid nor a gas, but instead has physical properties of both liquids and gases. The supercritical  $CO_2$  would then be transported to an appropriate location for underground injection into a suitable geological storage reservoir, such as a deep saline aquifer or depleted coal seam, or used in crude oil production for enhanced oil recovery.

The concentration of CO<sub>2</sub> is required because injection of exhaust streams containing high levels of nitrogen, oxygen and dilute CO<sub>2</sub> is not technically feasible. Research into technically and economically feasible capture systems is ongoing and is the focus of many large-scale grants from the U.S. Department of Energy (DOE). Adequate techniques for compression of CO<sub>2</sub> exist, but such compression systems require large amounts of energy. Furthermore, the capture process is energy intensive. It is estimated that a significant portion of power plant output would be required for CO<sub>2</sub> capture and subsequent compression. As stated in the August 2010 *Report of the Interagency Task Force on Carbon Capture and Storage*, "For a [550 MWe net output] natural gas combined cycle (NGCC) plant, the capital cost would increase by \$340 million and an energy penalty of 15 percent would result from the inclusion of CO<sub>2</sub> capture."

Research into geologic storage requirements is also ongoing. DOE research programs are investigating the reliability, permanence, risks, required monitoring, verification, and other issues to be addressed before geologic storage can proceed on a large commercial scale. Many regulatory issues remain to be resolved, such as pore space ownership, financial responsibility requirements, long-term risk following closure of the sequestration site, and issues regarding CO<sub>2</sub> purity and potential contamination of aquifers.

CCS systems are not currently available on a commercial basis. Large-scale demonstration projects are currently being planned or are in early stages of development, but no company or vendor currently offers a commercially available turn-key, integrated CCS system.

The Interagency Task Force on Carbon Capture and Storage consists of 14 executive departments and federal agencies, co-chaired by the DOE and EPA. As detailed in its August 2010 report, one goal of the task force is to bring five to 10 commercial demonstration projects online by 2016. With demonstration projects still years away, clearly the technology is not currently commercially available.

In the EPA PSD GHG permitting guidance, it is acknowledged that, "A number of ongoing research, development, and demonstration projects may make CCS technologies more widely applicable *in the future*" (italics added). "While CCS is a promising technology, EPA does not believe that at this time CCS will be a technically feasible BACT option in certain cases." As noted above, to establish that an option is technically infeasible, the permitting record should show that an available control option has neither been demonstrated in practice nor is available and applicable to the source type under review. EPA recognizes the significant logistical hurdles that the installation and operation of a CCS system presents and that sets it apart from other add-on controls that are typically used to reduce emissions

of other regulated pollutants and already have an existing reasonably accessible infrastructure in place to address waste disposal and other offsite needs. Logistical hurdles for CCS may include obtaining contracts for offsite land acquisition (including the availability of land), the need for funding (including, for example, government subsidies), timing of available transportation infrastructure, and developing a site for secure long-term storage. Not every source has the resources to overcome the offsite logistical barriers necessary to apply CCS technology to its operations, and smaller sources will likely be more constrained in this regard.

The Interagency Task Force report notes the lack of demonstration in practice: "Current technologies could be used to capture CO<sub>2</sub> from new and existing fossil energy power plants; however, they are not ready for widespread implementation primarily because they have not been demonstrated at the scale necessary to establish confidence for power plant application. Since the CO<sub>2</sub> capture capacities used in current industrial processes are generally much smaller than the capacity required for the purposes of GHG emissions mitigation at a typical power plant, there is considerable uncertainty associated with capacities at volumes necessary for commercial deployment."

Therefore, the CCS alternative is not considered technically feasible for the CGS project, and is eliminated from further consideration. While it is being eliminated based on technical feasibility in Step 2, it should be acknowledged that even if carried forward for further analysis, it would undoubtedly be eliminated in Step 4 based on cost effectiveness. The technical risks associated with the technologies would make the project un-financeable. The energy requirements for the capture and compression systems alone would dramatically increase the overall cost of generation for the project, and the cost of capture and compression systems, pipelines, development of storage reservoirs, and monitoring systems is very high as well.

## **Electrical Generation Efficiency**

EPA's *PSD and Title V Permitting Guidance for Greenhouse Gases* (EPA, 2011) identifies three categories of control technologies (p. 25):

- 1. Inherently lower-emitting processes/practices/designs
- 2. Add-on controls, and
- 3. Combinations of lower-emitting process/practices/designs and add-on controls

Because there are no demonstrated add-on controls, only those processes, practices, and designs that result in lower GHG emissions are applicable for this BACT analysis. As noted above, the project includes both simple-cycle and combined-cycle generation in this phase of the project, and possible but unplanned future expansion of the facility could include build-out of the simple-cycle combustion turbines into combined-cycle systems. The CGS project as proposed will utilize a high-efficiency, state-of-the-art, combustion turbine and HRSG design. Operation will use good combustion practices and result in energy efficient operation to provide steam to a new steam turbine generator.

In addition, installation of two combustion turbines in a combined-cycle configuration results in a lower resultant plant heat rate as compared to only simple-cycle combustion turbines. In some cases, the turbine which is most efficient in simple-cycle mode will result in a less efficient turbine for combined-cycle operations.

Furthermore, inlet air chillers will be used to prevent loss of turbine efficiency that results during hot weather. The following analysis will demonstrate that the overall generation efficiency meets or exceeds that of other recently implemented projects.

The permit limits proposed in this application are based on assumed use of a combustion turbine of 37 MW gross output and a gross heat rate of 9,300 Btu/kWh (HHV) for simple-cycle operation. This results in an estimated net output of approximately 97 MW at a net heat rate of 7,200 Btu/kWh (HHV) for the 2x1 combined-cycle system. The combined-cycle system will not have duct firing. All noted performance information is based upon CGS site conditions at 60°F; the high altitude of the area results in marginal decreases to turbine efficiency compared to other locations. The CGS project will utilize all new equipment.

## **Combustion Turbine Generator Comparable Permitted Emissions**

A search of the EPA's RACT/BACT/LAER Clearinghouse (RBLC) was performed for simple- and combined-cycle projects with combustion turbines similar to those proposed for the CGS project. No GHG permit information was found in searching the RBLC for comparable units. Information from other recent combustion turbine projects was researched for this BACT analysis, even though this information has not yet been posted to the RBLC.

## **Efficiency Review**

An efficiency review of the proposed CGS project was completed with two metrics: 1) RBLC comparable unit heat rates and 2) comparison of CO<sub>2</sub>e emission rates.

## **RBLC Efficiency Comparison**

The RBLC information presented in Table 5-4 below provides a comparison of efficiencies for projects with combustion turbines in the same nominal 40-MW size range as the CGS project. The information presented is for combustion turbines operating in simple cycle. No information was found for comparable 40-MW combined-cycle units without duct burning.

Facility	State	Description	Heat Capacity MMBtu/hr (HHV)	Net MW	Heat Rate Btu/kWh (HHV)
Arvah B. Hopkins Generating Station	Florida	GE LM6000PC Simple Cycle	489.5	50	9,790
Lambie Energy Center	California	GE LM6000PC Simple Cycle	500	49.9	10,020
Creole Trail LNG	Louisiana	Combustion Turbine Simple Cycle	290	30	9,667
Western Farmers Electric	Oklahoma	Combustion Turbine Simple Cycle	462.7	50	9,254
El Colton, LLC	California	LM6000 (Enhanced Sprint)	456.5	48.7	9,374
Indigo Energy Facility	California	LM6000 (Enhanced Sprint)	450	45	10,000
Bayonne Energy Center	New Jersey	Rolls Royce Trent 60WLE	603	64	9,422

### TABLE 5-4

RBLC Efficiency Information – Simple Cycle

Notes: Used 1.108 for HHV/LHV conversion factor.

The combustion turbines compared above are similar in size to those planned for the CGS project. As noted above, this analysis and resulting CGS proposed permit limits are based on use of a turbine with simple-cycle gross heat rate of 9,300 Btu/kWh (HHV). An exact comparison cannot be made between the CGS combustion turbines and those listed in Table 5-1 above because each project has unique equipment and site conditions, primarily elevation and temperature. However, the CGS heat rate compares very favorably with all of the reviewed comparable projects listed above, which demonstrates the high-efficiency attributes of the CGS project.

## CO<sub>2</sub>e Emission Rate Comparison

In simple-cycle operation, the CGS turbines are estimated to produce 1,102 pounds of  $CO_2e/MWh$  at average ambient conditions and full-load operation. Considering the range of normal operating loads (50 to 100 percent generator output), and ambient temperature (0°F to 108°F), GHG output for the CGS simple-cycle combustion turbines range from 1,072 to 1,603 pounds of  $CO_2e$  for new and clean combustion turbine prior to any degradation.

Table 5-5 below presents operating information from the EPA Acid Rain database, and was developed using actual comparable operating unit information from 2010.

State	Facility Name	Unit ID	Operating Time (Hr)	Net Load (MWh)	CO₂ Tons	lb CO₂/MWh
CA	El Cajon Energy Center	1	242	9450	5652	1196
ОК	Horseshoe Lake	10	710	29293	18142	1239
ОК	Horseshoe Lake	9	174	6851	4248	1240
CA	Orange Grove Project	CTG1	632	25017	15734	1258
CA	Orange Grove Project	CTG2	654	24954	15847	1270
FL	Arvah B Hopkins	HC4	903	27627	17623	1276
FL	Polk	**2	249	27652	18500	1338
FL	Arvah B Hopkins	HC3	662	18283	12529	1371
FL	Polk	**5	476	51662	36111	1398
FL	Polk	**4	563	60221	42443	1410
FL	Polk	**3	204	23176	16600	1432
NJ	Bayonne Plant Holding, LLC	2001	1055	35582	28385	1595
NJ	Bayonne Plant Holding, LLC	1001	1208	39061	32004	1639
NJ	Bayonne Plant Holding, LLC	4001	1134	36629	30200	1649
NE	C W Burdick	GT-3	24	426	399	1871
NE	C W Burdick	GT-2	33	606	579	1912
CA	Escondido Energy Center, LLC	CT1A	28	345	466	2702
CA	Escondido Energy Center, LLC	CT1B	28	345	468	2718

TABLE	5-5
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CGS Comparable Unit GHG Emissions

Notes:

Net load 5% lower than gross load.

Data as per EPA Clean Air Markets – Data and Maps. Based on 2010 data.

The CGS combustion turbine GHG output compares favorably with the facilities shown Table 5-5 above. It is recognized that in establishing any permit limit, allowance must be given for load variances, impact of ambient conditions, startup and shutdown, and equipment degradation over time. This is exemplified by reviewing the information from Table 5-5, because all of these units can be considered as "peaking" due to the low number of annual operating hours. The resultant wide variance in pounds of CO<sub>2</sub>e/MWh may likely be attributed to the significant proportion of time in startup and shutdown and/or reduced load operation, as well as lower thermal efficiency for older units.

Note that, based on the combustion turbine defined above, and considering the range of normal operating loads (50 to 100 percent output), and ambient temperature (0°F to 108°F), GHG output for the CGS 2x1 combined-cycle system ranges from 833 to 985 pounds of CO<sub>2</sub>e for a new or clean combustion turbine prior to any degradation.

## Step 3: Rank Remaining Control Technologies by Control Effectiveness

The only remaining technically feasible GHG control technology for the CGS project is the electrical generation efficiency. This option is presented in Table 5-6 based on their energy efficiencies expressed in terms of heat rate.

TABLE 5-	6
CGS Pro	ect GHG Control Technology Ranking

Configuration	Gross Plant Heat Rate (HHV) (Btu/kWh) <sup>1</sup>
Electrical Generation Combined-Cycle Efficiency (without duct firing)	7,200
Electrical Generation Simple-Cycle Efficiency	9,300

Note: <sup>1</sup>At CGS site conditions.

## Step 4: Evaluate Most Effective Controls and Document Results

The proposed CGS electrical generation efficiency is determined to be the most effective GHG control technology. From a review of the three evaluation metrics presented above, the CGS combustion turbine net heat rate was found to favorably compare with other combustion turbines and projects.

## Step 5: Select BACT

The only remaining option is the "Electrical Generation Efficiency" option, which, therefore, is selected as BACT. This option determined to consist of the CGS project as proposed with new state-of-the-art combustion turbines. Consistent with the review criteria presented above, the CGS project evaluated combustion turbine exhibits comparable efficiency with most of the evaluated alternative combustion turbines, and superior efficiency over the Pratt & Whitney and Siemens machines. Therefore, Black Hills proposes that CGS GHG BACT consist of installation of combustion turbines from any manufacturer with a rating of nominal 40 MW. However, the annual CO<sub>2</sub> emissions limit for the five new combustion turbines will be based upon the BACT emission limits proposed below, which are based upon a combustion turbine from the top of the efficiency range shown. The proposed permit

limit of annual total tons of  $CO_2e$  and lb/MWh would remain fixed regardless of the combustion turbine selected.

The estimated total annual CO<sub>2</sub>e emissions from the combustion turbines are 936,588 tpy, and this value is proposed to be the annual CO<sub>2</sub>e permit limit for the five combustion turbines.

EPA's PSD permitting guidance for GHGs suggests use of output-based BACT emission limits and longer-term averaging periods for GHGs. Based on Black Hills' analysis of conservative scenarios for number of turbine startups and shutdowns, partial load operation, and ambient temperature during operations, and considering the range of normalized GHG emissions noted above and eventual turbine degradation, proposed BACT permit limits are 1,100 lb/MWh for each combined-cycle combustion turbine and 1,600 lb/MWh for each simple-cycle combustion turbine on an annual average basis. If the averaging time is less than 1 year, these permit limits should be increased accordingly.

# 5.6 Small Combustion Sources BACT for GHGs

In addition to the five combustion turbines planned for the CGS project, there are several other small combustion sources associated with auxiliary equipment which will operate at the plant. The GHG calculations for these small combustion sources are located in Appendix B.

- (6) Natural gas-fired inlet air heaters (nominal 16-MMBtu/hr air heater with estimated emissions of 4,117 CO<sub>2</sub>e tons/year each)
- (2) Natural gas-fired fuel gas heaters (nominal 4.5-MMBtu/hr gas heater with estimated emissions of 1,153 CO<sub>2</sub>e tons/year each)
- (1) Diesel-fired emergency generator (nominal 839-BHP engine with estimated emissions of 226 CO<sub>2</sub>e tons/year each)
- (1) Diesel-fired fire pumps (nominal 327-BHP engine with estimated 51 CO<sub>2</sub>e tons/year each)

The total GHG emissions from the above small combustion sources are very minor as compared to the emissions from the combustion turbines. However, for completeness, these minor GHG emission sources were evaluated in aggregate below.

# Step 1: Identify All Control Technologies

The available control technologies for the CGS minor GHG sources are identical to those identified for the combustion turbines. These options include

- Carbon Capture and Storage Systems (CCS
- Small Combustion Source Efficiency
- Efficient Use of Energy

## Step 2: Eliminate Technically Infeasible Options Effectiveness

## Carbon Capture and Storage Systems

As discussed above, CCS for GHG control is not considered a technically feasible control option. Therefore, CCS is eliminated from further consideration for auxiliary boiler GHG reduction.

## Small Combustion Source Efficiency

This small combustion sources for the CGS project will incorporate a high-efficiency design.

## Efficient Use of Energy

The small combustion sources will not be operated continuously, but only during conditions when they are needed. For example, the inlet air heaters and fuel gas heaters will be operated only when required for safety reasons to protect against icing of the turbines or fuel lines. Therefore, energy will be utilized in an efficient manner.

## Step 3: Rank Remaining Control Technologies by Control Effectiveness

The remaining technically feasible GHG control technologies for the CGS project are "Small Combustion Source Efficiency "and "Efficient Use of Energy." Both technologies are equally important toward minimizing GHG emissions.

## Step 4: Evaluate most effective controls and document results

The remaining technically feasible GHG control technologies for the CGS project are "Small Combustion Source Efficiency "and "Efficient Use of Energy." Both technologies will be implemented for the CGS project.

## Step 5: Select BACT

GHG BACT for the CGS small equipment are "Small Combustion Source Efficiency "and "Efficient Use of Energy." All auxiliary equipment will be selected with consideration for high design efficiency, and will be operated in an efficient manner. Due to the estimated minor CO<sub>2</sub>e emissions contribution from these small combustion sources, no GHG permit limit is recommended for the CGS auxiliary equipment.
## APPENDIX A Location Map and Plot Plans

CGS Site Location and Fenceline Map



Cheyenne Generating Station Fenceline and Power Block

CH2MHILL

APPENDIX A-2 CGS Structures and Emission Points





APPENDIX A-3 Zachry CGS Site General Arrangement



APPENDIX B GHG Support Documentation

## APPENDIX B-1 CGS GHG Emission Calculations

## Black Hills Corporation Cheyenne Generating Station Potential to Emit Facility Wide Greenhouse Gas Revision 07-28-11

Emission	Description	Consumption	Emission Factors (kg/MMBtu)			Emissions (tons/year)			
Point		(MMBtu/hr)	CO2	CH₄	N <sub>2</sub> O	CO <sub>2</sub>	CH₄	N <sub>2</sub> O	CO <sub>2</sub> -equivalent
EP01	Combined Cycle Combustion Turbine CT01A	366	53.02	0.001	0.0001	187,134.03	3.53	0.35	187,317.56
EP02	Combined Cycle Combustion Turbine CT01B	366	53.02	0.001	0.0001	187,134.03	3.53	0.35	187,317.56
EP03	Simple Cycle Combustion Turbine CT02A	366	53.02	0.001	0.0001	187,134.03	3.53	0.35	187,317.56
EP04	Simple Cycle Combustion Turbine CT02B	366	53.02	0.001	0.0001	187,134.03	3.53	0.35	187,317.56
EP05	Simple Cycle Combustion Turbine CT03A	366	53.02	0.001	0.0001	187,134.03	3.53	0.35	187,317.56
EP06	Inlet Air Heater 01	16.0680	53.02	0.001	0.0001	4,113.13	0.08	0.01	4,117.17
EP07	Inlet Air Heater 02	16.0680	53.02	0.001	0.0001	4,113.13	0.08	0.01	4,117.17
EP08	Inlet Air Heater 03	16.0680	53.02	0.001	0.0001	4,113.13	0.08	0.01	4,117.17
EP09	Inlet Air Heater 04	16.0680	53.02	0.001	0.0001	4,113.13	0.08	0.01	4,117.17
EP10	Inlet Air Heater 05	16.0680	53.02	0.001	0.0001	4,113.13	0.08	0.01	4,117.17
EP11	Inlet Air Heater 06	16.0680	53.02	0.001	0.0001	4,113.13	0.08	0.01	4,117.17
EP15	Diesel Generator	5.52	73.96	0.003	0.0006	225.01	0.01	0.00	225.77
EP16	Diesel Fire Pump	2.5	73.96	0.003	0.0006	50.95	0.00	0.00	51.13
EP18	Fuel Gas Heater 01	4.5	53.02	0.001	0.0001	1,151.92	0.02	0.00	1,153.05
EP19	Fuel Gas Heater 02	4.5	53.02	0.001	0.0001	1,151.92	0.02	0.00	1,153.05
	Total PTE for Facility					962,928.74	18.17	1.82	963,873.80
Notes:   (1) CO2 Emission Factors from Table C-1 of the EPA's Mandatory Reporting Rule.   (2) CH4 and N2O Emission Factors from Table C-2 of the EPA's Mandatory Reporting Rule.   (3) Global Warming Potentials are:									
( )	CO <sub>2</sub>	1							
	CH <sub>4</sub>	21							
	N <sub>2</sub> O	310							
(4) Combustion Turbines (hr/yr operation per turbine)		8760							
(5) Inlet Air Heaters (hr/yr operation per turbine)		4380							
(6) Diesel Emergency Generator (hr/yr operation per turbine)		500							
(7) Diesel Fire Pump (hr/yr operation per turbine)		250							
(8) Fuel Gas Heaters (hr/yr operation per turbine)		4380							