



INDIANA DEPARTMENT OF ENVIRONMENTAL MANAGEMENT

We Protect Hoosiers and Our Environment.

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Eric J. Holcomb
Governor

Bruno Pigott
Commissioner

January 13, 2017

Mr. Robert A. Kaplan
Acting Regional Administrator
U.S. Environmental Protection Agency
Region 5
77 West Jackson Boulevard
Chicago, IL 60604-3950

Re: Preliminary Recommendations Concerning
Round 3 Air Quality Designations for the
2010 Primary 1-Hour Sulfur Dioxide National
Ambient Air Quality Standard

Dear Mr. Kaplan:

This letter is in response to United States Environmental Protection Agency's (U.S. EPA's) July 22, 2016, memorandum *Area Designations for the 2010 Primary Sulfur Dioxide National Ambient Air Quality Standard-Round 3* and prior guidance on area designations issued by U.S. EPA on March 20, 2015. The letter's primary purpose is to provide information for U.S. EPA's evaluation prior to Round 3 designations. As required, the Indiana Department of Environmental Management (IDEM) is providing new modeling analyses for areas where modeling is being used to characterize air quality around certain sulfur dioxide (SO₂) sources, as well as preliminary recommendations for Round 3 designations. IDEM is also including information about newly installed air monitors where air monitoring is being used to characterize air quality around certain SO₂ sources for Round 4 designations.

Implementation of the 2010 primary 1-hour SO₂ standard began in 2013 when U.S. EPA established nonattainment areas based on 2010-2012 monitoring data. Subsequently, on March 2, 2015, U.S. EPA entered into a consent decree with the Sierra Club and Natural Resources Defense Council (NRDC) establishing a timeline for the completion of air quality characterizations and designations in all remaining areas of the country. The court order directed U.S. EPA to complete the designations in three additional rounds: Round 2 by July 2, 2016, Round 3 by December 31, 2017, and Round 4 by December 31, 2020.

On June 30, 2016, U.S. EPA completed designations for all Round 2 sources. U.S. EPA has designated all of Indiana's Round 2 sources as unclassifiable/attainment. The final rule was published in the Federal Register on July 12, 2016 (81 FR 45039).

On August 10, 2015, U.S. EPA announced the Data Requirements Rule (DRR), which requires the characterization of air quality near sources with SO₂ emissions at or greater than 2,000 tons per year (tpy) or have been identified by IDEM or U.S. EPA “as requiring further air quality characterization.” Under the DRR, states must submit air quality information to U.S. EPA according to timeframes that coincide with the court-ordered dates for designations in all remaining areas under Rounds 3 and 4.

IDEM has been working with U.S. EPA to identify all sources in Indiana that are subject to the DRR and provide data for the characterization of nearby air quality. As required, on January 7, 2016, IDEM submitted a list of 11 stationary sources identified for air quality characterization under the DRR, thus beginning the Round 3 designation process. On March 26, 2016, U.S. EPA added six sources to the list, including: five Round 2 sources that U.S. EPA identified as also meeting DRR characterization requirements; and one source, U.S. Mineral Products (Isolatek), for which U.S. EPA believed further study was necessary. IDEM disagrees with U.S. EPA’s addition of U.S. Mineral Products to the list of Indiana sources subject to the DRR, as further explained in Attachment 3. Table 1 contains an up-to-date list of DRR sources identified by U.S. EPA and IDEM, along with the selected approaches for air quality characterization for each source area.

Table 1: Indiana SO₂ Sources Subject to the Data Requirements Rule

| Facility | County | 2014 SO ₂ Emissions (Tons) | Selected Approach for Characterization |
|--|------------|---------------------------------------|--|
| Duke – Gallagher | Floyd | 3,524 | Modeling |
| Duke – Gibson | Gibson | 22,055 | Round 2 Source ^a |
| U.S. Mineral Products (Isolatek) ^b | Huntington | < 2,000 | See Attachment 3 |
| NIPSCO – R.M. Schahfer | Jasper | 8,412 | Modeling |
| Indiana-Kentucky Electric Corporation - Clifty Creek | Jefferson | 3,731 | Round 2 Source ^a |
| ArcelorMittal USA | Lake | 2,163 | Modeling |
| Coke Energy | Lake | 4,952 | Modeling |
| U.S. Steel – Gary Works | Lake | 3,285 | Modeling |
| NIPSCO – Michigan City | LaPorte | 15,991 | Round 2 Source ^a |
| ArcelorMittal – Burns Harbor | Porter | 12,189 | Monitoring See Attachment 5 |
| SABIC Innovative Plastics | Posey | 4,030 | Modeling |
| Vectren – A.B. Brown | Posey | 8,080 | Round 2 Source ^a |
| AEP – Rockport | Spencer | 54,979 | Round 2 Source ^a |
| Hoosier Energy – Merom | Sullivan | 3,318 | Modeling |
| Duke – Cayuga | Vermillion | 3,448 | Modeling |
| Alcoa Warrick Power Plant | Warrick | 4,993 | See Attachment 4 |
| Alcoa Warrick Operations | Warrick | 3,500 | See Attachment 4 |

^a IDEM completed a characterization for this source under Round 2 designation requirements. U.S. EPA issued final Round 2 designations on June 30, 2016 (81 FR 45039).

^b Added by U.S. EPA.

By January 1, 2017, each state air agency must ensure that new ambient air monitors are operational where air monitoring is selected to inform Round 4 designations. Only one DRR source, ArcelorMittal – Burns Harbor, opted for ambient monitoring of SO₂ to characterize air quality. See Attachment 5 for information regarding the operation of SO₂ monitors at the ArcelorMittal – Burns Harbor facility. U.S. EPA will evaluate three complete years of air monitoring data from these monitors for the completion of Round 4 designations by the court-ordered date of December 31, 2020.

By January 13, 2017, each state air agency must provide to U.S. EPA its modeling analysis for source-areas where modeling is used to determine Round 3 designations. Table 2 contains IDEM’s Round 3 designation recommendations, based on new air quality modeling analyses for the source areas.

Table 2: Indiana’s Round 3 Designation Recommendations

| Source | County | Boundary/Area | Recommendation |
|---|----------------|--|--------------------------------|
| Duke Energy Gallagher | Floyd | County | Attainment |
| U.S. Mineral Products (Isolatek) | Huntington | See Attachment 3 | See Attachment 3 |
| NIPSCO R.M. Schahfer | Jasper (P) | Kankakee Township | Attainment |
| ArcelorMittal USA, Coke Energy, U.S. Steel Gary Works | Lake (P) | Calumet Township North Township | Attainment |
| SABIC Innovative Plastics | Posey (P) | Black Township | Attainment |
| Hoosier Energy Merom | Sullivan (P) | Gill Township | Attainment |
| Duke Energy Cayuga | Vermillion (P) | Eugene Township Vermillion Township | Attainment |
| Alcoa Warrick Power Plant, Alcoa Warrick Operations Plant | Warrick (P) | Anderson Township | Attainment See Attachment 4 |

(P) denotes partial county recommendation

IDEM is attaching new modeling analyses, as required, and several additional documents listed here, to provide U.S. EPA with detailed information for review prior to completing Round 3 designations.

Attachment 1: Indiana’s Preliminary Recommendations Concerning Round 3 Designations for the 2010 Primary 1-Hour Sulfur Dioxide (SO₂) National Ambient Air Quality Standards (NAAQS)

Attachment 2: Indiana’s Air Quality Modeling Technical Support Document Preliminary Designation Recommendations Data Requirements Rule (Round 3) for the 2010 Primary 1-Hour Sulfur Dioxide (SO₂) National Ambient Air Quality Standards (NAAQS)

Attachment 3: U.S. Mineral Products (Isolatek) Discussion

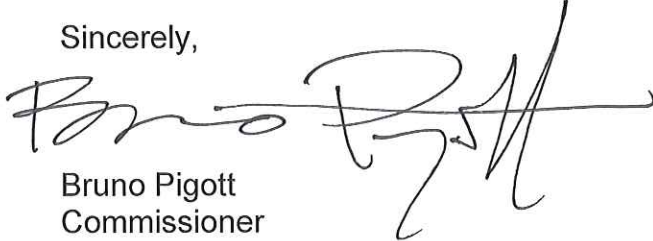
Attachment 4: Alcoa Warrick Attainment Discussion

Attachment 5: ArcelorMittal - Burns Harbor SO₂ Air Quality Monitor System
Documentation

This submittal consists of one (1) hard copy of the required documentation. An electronic version of the submittal in PDF format that is identical to the hard copy has been sent to Doug Aburano, Chief of U.S. EPA Region 5's Attainment Planning and Maintenance Section and Chris Panos of U.S. EPA Region 5.

Thank you for this opportunity to submit information, including Indiana's new modeling analyses and preliminary recommendations, for Round 3 designations under the 2010 primary 1-hour SO₂ NAAQS. If you have any questions or need additional information, please contact Keith Baugues, Assistant Commissioner, Office of Air Quality, at (317) 232-8222 or kbaugues@idem.IN.gov.

Sincerely,



Bruno Pigott
Commissioner

BP/kb/sd/bc/gf/as
Attachments

cc: Chris Panos, U.S. EPA Region 5 (no enclosures)
John Summerhays, U.S. EPA Region 5 (no enclosures)
Doug Aburano, U.S. EPA Region 5 (no enclosures)
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Attachment 1

Indiana's Preliminary Recommendations
Concerning Round 3 Designations for the 2010 Primary
1-Hour Sulfur Dioxide (SO₂) National Ambient Air
Quality Standards (NAAQS)

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| Source | County | Boundary/Area | Recommendation |
|---|----------------|--|--------------------------------|
| Duke Energy Gallagher | Floyd | County | Attainment |
| U.S. Mineral Products (Isolatek) | Huntington | See Attachment 3 | See Attachment 3 |
| NIPSCO R.M. Schahfer | Jasper (P) | Kankakee Township | Attainment |
| ArcelorMittal USA, Coke Energy, U.S. Steel Gary Works | Lake (P) | Calumet Township and North Township | Attainment |
| SABIC Innovative Plastics | Posey (P) | Black Township | Attainment |
| Hoosier Energy Merom | Sullivan (P) | Gill Township | Attainment |
| Duke Energy Cayuga | Vermillion (P) | Eugene Township Vermillion Township | Attainment |
| Alcoa Warrick Power Plant, Alcoa Warrick Operations Plant | Warrick (P) | Anderson Township | Attainment See Attachment 4 |

(P) denotes partial county recommendation

The following sources, though identified by U.S. EPA as being subject to the Data Requirements Rule, were addressed under Round 2 designations and designated by U.S. EPA on June 30, 2016 (81 FR 45039).

| Area Name | Source Area | County Name | Designation |
|----------------------|----------------------|---------------|---------------------------|
| Gibson County, IN | Duke Gibson | Gibson | Unclassifiable/Attainment |
| Jefferson County, IN | IKEC Clifty Creek | Jefferson (P) | Unclassifiable/Attainment |
| LaPorte County, IN | NIPSCO Michigan City | LaPorte | Unclassifiable/Attainment |
| Posey County, IN | Vectren A.B. Brown | Posey (P) | Unclassifiable/Attainment |
| Spencer County, IN | AEP Rockport | Spencer (P) | Unclassifiable/Attainment |

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Attachment 2

Indiana's Air Quality Modeling Technical Support Document

Preliminary Designation Recommendations

Data Requirements Rule (Round 3)

2010 Primary 1-Hour Sulfur Dioxide (SO₂) National Ambient Air Quality Standard (NAAQS)

January 2017

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- Enclosure 2: Lake County DRR Source Modeling Inventory
- Enclosure 3: Carmeuse Commissioner’s Order #2016-04
- Enclosure 4: SABIC Commissioner’s Order #2016-03

MODELING TECHNICAL SUPPORT DOCUMENT FOR PRELIMINARY DESIGNATION RECOMMENDATIONS

DATA REQUIREMENTS RULE (ROUND 3) FOR THE 2010 PRIMARY 1-HOUR SULFUR DIOXIDE (SO₂) NATIONAL AMBIENT AIR QUALITY STANDARD

1.0 1-Hour SO₂ NAAQS and Designation Process

The United States Environmental Protection Agency (U.S. EPA) established the 1-hour primary sulfur dioxide (SO₂) National Ambient Air Quality Standard (NAAQS) of 75 parts per billion (ppb) as published in the Federal Register (FR) on June 22, 2010 (75 FR 35519). This standard is based on the 3-year average of the annual 99th percentile of the 1-hour daily maximum concentrations. For air quality modeling purposes, the Indiana Department of Environmental Management (IDEM), Office of Air Quality (OAQ) uses an equivalent 1-hour SO₂ NAAQS of 196.2 micrograms per cubic meter (µg/m³) as stated in 76 FR 69051. This is based on the 3-year average of the annual 99th percentile of the 1-hour daily maximum modeled SO₂ concentrations, representing the fourth high of the 1-hour daily maximum SO₂ modeled concentrations.

Implementation of the standard began in 2013, when U.S. EPA made initial designations based on 2010-2012 monitoring data (78 FR 47191). Subsequently, on March 2, 2015, U.S. EPA entered into a consent decree with the Sierra Club and the Natural Resources Defense Council establishing a timeline for the completion of air quality characterizations designations in all remaining areas of the country. The court order directed U.S. EPA to complete the designations in three additional rounds: Round 2 by July 2, 2016 (81 FR 45039), Round 3 by December 31, 2017, and Round 4 by December 31, 2020.

Round 3 and 4 designations are implemented through U.S. EPA's SO₂ Data Requirements Rule (DRR) (80 FR 51051). Round 3 designations apply to source areas that opt to characterize SO₂ through modeling and have *not* implemented ambient air monitoring by January 1, 2017. Round 4 designations apply to source areas that opt to characterize SO₂ by having implemented new ambient air monitoring by January 1, 2017. In addition, sources may opt to take permanent federally enforceable emission limits in order to reduce SO₂ emissions to below the DRR threshold of 2,000 tons per year.

2.0 Data Requirements Rule

As stated above, Round 3 designations are implemented through U.S. EPA’s SO₂ DRR. Under this rule, SO₂ should be characterized in the vicinity of sources that had actual emissions in 2014 of 2,000 tons or more, or have been identified by IDEM or U.S. EPA “as requiring further air quality characterization.”

Requirements specific to the DRR were followed in order to implement the 1-hour SO₂ NAAQS. Indiana identified 11 sources within the state that met the criteria established in the DRR. This list of sources was submitted to U.S. EPA – Region V on January 7, 2016. On March 25, 2016, U.S. EPA subsequently identified six additional sources meeting the criteria for air quality characterizations under the DRR. Five of these sources were “consent decree” sources and were designated unclassifiable/attainment under Round 2 (81 FR 45039). The sixth source, U.S. Mineral Products (U.S. Minerals) was listed by U.S. EPA as subject to the DRR due to concern for air quality in the area. All DRR sources, the counties they reside and their 2014 SO₂ emissions are listed in Table 2.1.

Table 2.1 - Indiana Sources Subject to the Data Requirements Rule

| Facility | County | 2014 SO ₂ Emissions (tons) |
|---------------------------------------|------------|---------------------------------------|
| Duke – Gallagher | Floyd | 3,524 |
| Duke – Gibson | Gibson | Round 2 Source ^a |
| U.S. Mineral Products (Isolatek) | Huntington | < 2,000 ^b |
| NIPSCO – R.M. Schahfer | Jasper | 8,412 |
| IKEC–Clifty Creek Generating Station | Jefferson | Round 2 Source ^a |
| ArcelorMittal – USA | Lake | 2,163 |
| Coke Energy | Lake | 4,952 |
| U.S. Steel – Gary Works | Lake | 3,285 |
| NIPSCO - Michigan City | LaPorte | Round 2 Source ^a |
| ArcelorMittal - Burns Harbor | Porter | 12,189 |
| SABIC Innovative Plastics | Posey | 4,030 |
| Vectren—A.B. Brown Generating Station | Posey | Round 2 Source ^a |
| AEP - Rockport | Spencer | Round 2 Source ^a |
| Hoosier Energy – Merom | Sullivan | 3,318 |
| Duke – Cayuga | Vermillion | 3,448 |
| Alcoa Warrick Power Plant | Warrick | 4,993 |
| Alcoa Warrick Operations Plant | Warrick | 3,500 ^c |

^a IDEM completed characterization for this source under Round 2 designation requirements. U.S. EPA issued final Round 2 designations on June 30, 2016 (81 FR 45039).

^b Added by U.S. EPA.

^c Alcoa Warrick Operations shut down its smelter operations on March 31, 2016, reducing SO₂ emissions to < 1 ton source-wide.

As per the requirements of the DRR, air agencies were required to indicate whether they will rely on 1) air quality modeling, 2) ambient monitoring or 3) establishing a limit of a source's total SO₂ emissions to below 2,000 tons per year, to characterize air quality in the area surrounding the DRR sources. Indiana reviewed each source and determined that eight sources will conduct air dispersion modeling to characterize air quality including, where appropriate, modeling non-DRR sources. One source, ArcelorMittal – Burns Harbor, opted to rely on ambient monitoring to characterize air quality (see Section 10.0 and transmittal Attachment 5). For U.S. Mineral Products (Isolatek), Indiana disagrees with U.S. EPA on its inclusion as being subject to the DRR (see transmittal Attachment 3). Lastly, for Alcoa Warrick Operations and Alcoa Warrick Power Indiana feels that these two facilities and the surrounding area should be designated attainment based on historical SO₂ ambient monitoring showing attainment of the SO₂ standard and the fact that the Operations Plant shut down their aluminum smelting operations on March 31, 2016 and has negligible SO₂ emissions as a result of the shutdown (see transmittal Attachment 4).

U.S. EPA has established deadlines for each step of the 1-hour SO₂ designation process in the DRR. Indiana met the first deadline by submitting its list of DRR sources on January 7, 2016.

- **January 15, 2016** - States were required to submit their list of SO₂ sources for characterizing air quality under the DRR to U.S. EPA.
- **July 1, 2016** – States were required to submit modeling protocols for sources characterizing air quality in the area with air dispersion modeling.
- **July 1, 2016** – States were required to submit Annual Monitoring Network Plans that detailed modifications to SO₂ monitors intended to satisfy the DRR.
- **January 1, 2017** – SO₂ monitors intended to satisfy the DRR are required to be operational.
- **January 13, 2017** – States electing to characterize air quality by air dispersion modeling are required to provide modeling analyses to U.S. EPA.
- **January 13, 2017** – Federally enforceable and permanent emission limits to keep source emissions below 2,000 tons of SO₂ must be adopted and effective.
- **August 2017** – Expected date by which U.S. EPA will notify states of intended designations.
- **December 2017** – Date by which U.S. EPA will complete final designations for the majority of the country.
- **August 2019** – Approximate due date for state attainment plans for areas designated nonattainment in 2017.
- **May 2020** – Required certification of 2019 monitoring data; states have the opportunity to provide updated state recommendations to U.S. EPA.
- **August 2020** – Expected date by which U.S. EPA would notify states of intended designations for remainder of the country not yet designated.

- **December 2020** – Date by which the U.S. EPA would complete final designations for the remainder of the country.
- **August 2022** – Approximate due date for state attainment plans for areas designated nonattainment in 2020.

3.0 Methodology for DRR Air Quality Modeling

The modeling methodology resembles modeling used to evaluate New Source Review (NSR) and Prevention of Significant Deterioration (PSD) sources. However, U.S. EPA provided further guidance in order to conduct an appropriate air dispersion modeling analysis to support 1-hour SO₂ designation recommendations. U.S. EPA's SO₂ NAAQS Designations Modeling Technical Assistance Document (TAD) guidance has several recommendations for modeling methodology for determining attainment designations, including:

- 1) Use of actual emissions to assess modeled concentrations to reflect current air quality.
- 2) Use of three years of modeling results to calculate a simulated 1-hour SO₂ design value consistent with the 3-year monitoring period to develop 1-hour SO₂ design values.
- 3) Placement of receptors only in locations where an air quality monitor could be placed.
 - Based on the SO₂ NAAQS Designations Modeling TAD, Section 4.2; Indiana placed modeling receptors only where feasible to place a monitor. Therefore, in bodies of water or an area where monitor siting criteria would not be reasonably met, Indiana did not place receptors.
 - Indiana matched up the modeling domain with Google map projections to ensure the proximity of the receptors to shorelines and have provided receptor/mapping details for each modeling analysis.
- 4) Use of actual stack heights rather than relying on Good Engineering Practice (GEP) stack heights when modeling actual emissions.

Indiana followed U.S. EPA's designation modeling recommendations to conduct 1-hour SO₂ modeling to determine whether there are modeled violations of the 1-hour SO₂ NAAQS. Modeling results looked at the 4th high maximum daily 1-hour SO₂ concentrations averaged over the 3-year modeled period with representative temporally varying seasonal SO₂ background concentrations included within the AERMOD modeling run to determine the attainment status of the area in the vicinity of the DRR source.

4.0 Model Selection for DRR Modeling

4.1 AERMOD Dispersion Model

In accordance with Appendix A of Appendix W to 40 Code of Federal Regulations (CFR) Part 51, Indiana used the American Meteorological Society/Environmental Protection Agency Regulatory Model (AERMOD) version 15181 for all dispersion modeling. U.S. EPA's SO₂ NAAQS Designations Modeling TAD, specific to attainment designation modeling, recommended using actual stack heights when modeling actual emissions instead of following the GEP stack height requirement. BPIPPRIME was used to account for any building downwash concerns.

4.2 AERMAP

The AERMOD terrain preprocessor mapping program, AERMAP, was used to determine all the terrain elevation heights for each receptor, building, and source locations using the Universal Transverse Mercator (UTM) coordinate system. The most recent AERMAP version 11103 assigned the elevations from the National Elevation Dataset (NED) using the North American Datum (NAD) 1983 as recommended in 40 CFR Part 51, Appendix W, Revision to the Guideline on Air Quality Models and later revised in the "AERMOD Implementation Guide."

4.3 Land Use Determination

The Auer Land Use Classification Scheme was used to determine land use in the area of each source, pursuant to 40 CFR Part 51, Appendix W section 7.2.3(c). Land use types were classified within a 3 kilometer radius about the source. If land use types I1 (heavy industrial), I2 (light moderate industrial), C1 (commercial), R2-R3 (compact residential) account for over 50 percent of the total land area, urban dispersion coefficients were used. If not, the rural dispersion coefficients were used.

5.0 Receptor Grid and Modeling Domain

The receptor grid and modeling domain was based on guidance provided in the memorandum "Updated Guidance for Area Designations for the 2010 Primary Sulfur Dioxide National Ambient Air Quality Standards", dated March 20, 2015 and the SO₂ NAAQS Designations Modeling TAD. Indiana used a multi-nested rectangular receptor grid with appropriate spacing of receptors based on the distance from the modeled emission points to detect significant concentration gradients. Indiana has conducted exploratory modeling on each of the DRR sources and did not find maximum modeled 1-hour SO₂ impacts or DRR source-culpable modeled violations that extended out beyond 10 kilometers. In situations where multiple sources covered by the DRR were evaluated in the same area, the modeling domain extended to include

all sources and the appropriate distances to model maximum 1-hour SO₂ impacts to determine attainment designations for the area. Indiana generally used the following multi-nested rectangular receptor grid in all cases, with additional receptors added as needed:

- Receptor spacing at the fence line for each facility placed every 50 meters.
- Receptor spacing at 100 meters out to a distance of 3,000 meters (3 kilometers) beyond each facility (grid was extended if modeling results warranted).
- Receptor spacing at 250 meters out to a distance of 5,000 meters (5 kilometers) beyond each facility (grid was extended if modeling results warranted).
- Receptor spacing at 500 meters out to a distance of 10,000 meters (10 kilometers) beyond each facility (grid was extended if modeling results warranted).

6.0 Meteorology

6.1 AERMET

As stated in 40 CFR Part 51, Appendix W, section 8.3.1.2 and the SO₂ NAAQS Designations Modeling TAD, Indiana used three years (2012-2014 or 2013-2015) of National Weather Service (NWS) and on-site surface data and upper air meteorological data processed with the latest version of the AERMOD meteorological data preprocessor program AERMET (version 15181). Table 6.1 below lists the modeled facilities as mentioned in the DRR and the corresponding surface and upper air meteorological stations used to conduct modeling.

Table 6.1 - National Weather Service Stations/Onsite Meteorological Stations

| DRR Facility | Surface Meteorology | Upper Air Meteorology |
|---|--|-----------------------|
| SABIC Innovative Plastics Hoosier Energy - Merom | Evansville, IN NWS | Lincoln, IL NWS |
| Duke – Gallagher | Louisville, KY NWS | Wilmington, OH NWS |
| Arcelormittal – USA Coke Energy U.S. Steel – Gary Works ArcelorMittal Burns Harbor | Gary-IITRI onsite meteorological data processed with South Bend, IN NWS | Lincoln, IL NWS |
| NIPSCO – R.M. Schahfer | South Bend, IN NWS | Lincoln, IL NWS |
| Duke –Cayuga | Indianapolis, IN NWS | Lincoln, IL NWS |

Indiana requested on November 9, 2016 for concurrence by U.S. EPA for the use of the adjusted surface friction velocity (ADJ_U*) Beta option in order to more accurately model 1-hour SO₂ concentrations from DRR sources located in Lake County. On December 20, 2016, U.S. EPA finalized “Revisions to the Guidelines on Air Quality Models, Enhancements to the AERMOD Dispersion Modeling System and Incorporation of Approaches to Address Ozone and Fine

Particulate Matter”. This rule approved ADJ_U* as a regulatory option and was used in the DRR modeling for Lake County.

6.2 AERMINUTE/AERSURFACE

The 1-minute wind speeds and wind directions, taken from the Automated Surface Observing System (ASOS) NWS stations and onsite meteorological stations, were processed with the U.S. EPA’s 1-minute data processor AERMINUTE (version 15272) program.

The U.S. EPA’s AERSURFACE (version 13016) program was used to determine the surface characteristics; albedo, Bowen ratio, and surface roughness for the Indianapolis, Evansville, South Bend, Indiana and Louisville, Kentucky NWS meteorological tower locations. Surface characteristics were determined at each NWS location for each of 12 wind direction sectors with a recommended default radius of one kilometer.

The albedo and the Bowen ratio surface characteristics were adjusted during the three winter months of January, February, and December in accordance with the U.S. EPA Region V document, “Regional Meteorological Data Processing Protocol,” dated May 6, 2011. Additionally, a dry or wet Bowen ratio value was used during months when soil moisture conditions were abnormally dry or wet; otherwise the Bowen ratio value for average soil moisture conditions was used. The surface roughness value for snow cover was used if more than half of the month had days with at least one inch of snow on the ground. Otherwise, the no snow cover surface roughness value was used.

7.0 SO₂ Background Concentrations

The modeling of all DRR sources used adjusted temporally varying seasonal background concentrations or concentrations without upwind major source SO₂ impacts. Each source used 1-hour SO₂ monitoring data, taken from nearby monitors, considered representative of background concentrations for the area. Since most SO₂ monitoring sites located in the state are downwind of large SO₂ sources, impacts from the upwind direction of the large SO₂ source were removed from the monitoring data since those sources were included in the modeling inventory. The 99th percentile SO₂ concentrations by season (winter, spring, summer and fall) for each hour of the day were calculated to determine the temporally varying seasonal SO₂ background, which were directly input into the model and were part of the final modeled results. This procedure was used to prevent double counting of SO₂ sources within the background concentration values used for this attainment designation modeling.

Temporally varying seasonal SO₂ background concentrations were developed in accordance with the recommended U.S. EPA guidance for establishment of such background concentrations in

Section 8.2 of 40 CFR Part 51, Appendix W and considered appropriate and representative of the area. The latest three years of SO₂ air quality monitoring data (2012-2014 or 2013-2015) were used to develop background concentrations for each of the areas mentioned in the DRR. The procedures used to develop the SO₂ background concentrations are included as Enclosure 1. Table 7.1 shows the DRR facility and corresponding 1-hour SO₂ monitoring sites used for representative background concentrations in the air quality characterization.

Table 7.1 - Indiana DRR Sources and Nearby Background Monitoring Sites

| Facility | County | Monitoring Sites |
|---|------------|--|
| SABIC Innovative Plastics | Posey | Evansville – Buena Vista |
| Duke – Gallagher | Floyd | New Albany – Green Valley |
| NIPSCO – R.M. Schahfer | Jasper | Wheatfield – Center St. |
| Hoosier Energy – Merom | Sullivan | Terre Haute – North Lafayette Road |
| Duke – Cayuga | Vermillion | Fountain County -North of State Road 234 |
| ArcelorMittal – USA Coke Energy U.S. Steel – Gary Works | Lake | Gary-IITRI and Hammond |
| ArcelorMittal - Burns Harbor | Porter | Dunes Acres Substation |

8.0 SO₂ Emissions Sources to be Modeled

8.1 DRR Sources

Indiana modeled the hourly continuous emissions monitoring (CEM) data from sources subject to the DRR, where available. Along with the hourly SO₂ emission data, hourly variable stack gas flow rate and temperature of the exhaust stream were modeled, if available. This variation in parameters may influence dispersion characteristics of the exhaust stream and impact modeled 1-hour SO₂ concentrations.

For those emission sources without continuous emissions data, actual short-term emissions taken from the source’s latest available emissions reporting were used. The SO₂ NAAQS Designations Modeling TAD, Section 5 was referenced to best characterize any temporal and/or seasonal variability of emissions. This would include any seasonal, monthly, or daily variations that can be quantified. Specific emissions characterizations that were modeled will be addressed for each DRR source later in this document.

There are instances where sources emitted less than 2,000 tons of SO₂ in 2014 and are not listed as a DRR source, but are located in the vicinity of a DRR source within the modeling receptor grid. This was considered a cluster source and the source was evaluated along with the DRR

source in the air quality modeling analysis to determine the air quality characterization in the area.

8.2 Inventory Sources

Based on the U.S. EPA memo “Additional Clarification Regarding Application of Appendix W Modeling Guidance for the 1-hour NO₂ National Ambient Air Quality Standard”, dated March 1, 2011, page 16, Indiana is focused on the characterization of air quality within 10 kilometers for each of the DRR sources. U.S. EPA’s SO₂ NAAQS Designations Modeling TAD Section 4.1, page 7, mentions the number of sources to be explicitly modeled should cause a significant concentration gradient and the number of those sources to be modeled would generally be small. Indiana developed a list of SO₂ emission sources in the county of the DRR source, as well as larger SO₂ emission sources in adjacent counties and states, as requested by U.S. EPA – Region 5, that were explicitly modeled.

Emission sources near the DRR source were evaluated to determine if those sources could cause or contribute to a 1-hour SO₂ NAAQS violation. Indiana used the following threshold as a screening method to narrow the focus of sources that could potentially have an impact on designations: sources with SO₂ emissions greater than 250 tons per year and located within 30 kilometers of the DRR source. While this method was applied on an area-by-area basis, Indiana felt this was an accurate representation of air quality in the area, especially since the hourly seasonal background concentrations adequately captures SO₂ impacts from surrounding sources. IDEM also identified sources with emissions less than 250 tons that were included in DRR modeling due to their proximity within the DRR source receptor grid used in the dispersion modeling. Actual emissions taken from the latest available emissions inventories were modeled for sources identified by these threshold levels to determine air quality characteristics in the area.

8.3 Intermittent Sources

Emergency generators, fire pumps, and startup/shutdown emissions were handled consistent to the March 1, 2011 guidance “Additional Clarification Regarding Application of Appendix W Modeling Guidance for the 1-hour NO₂ NAAQS”, dated March 1, 2011. U.S. EPA recommended using appropriate data based on emissions scenarios that are continuous enough or frequent enough to contribute significantly to the annual distribution of maximum daily 1-hour concentrations. Review of the hours of operations for combustion turbines, emergency generators, startup/shutdown, fire pumps, and other auxiliary operations associated with the sources addressed by the DRR have been determined to operate much less than 500 hours per year and have random and infrequent schedules that cannot be controlled. Indiana feels that the intent of the DRR is to determine the attainment status of the area surrounding large SO₂ emission sources based on actual emissions coming from the large units. As such, this is

Indiana's main focus of the designation determinations. This approach is consistent with previous 1-hour SO₂ nonattainment and designation modeling submitted by IDEM to U.S. EPA.

9.0 Analysis of Modeling Results

The purpose of this modeling demonstration is to characterize air quality and determine area designations as it relates to attainment of the 1-hour SO₂ NAAQS in accordance with the DRR. The 99th percentile of the 1-hour daily maximum modeled concentrations represents the fourth high of the 1-hour daily maximum SO₂ modeled concentrations and are averaged across three years to compare resulting concentrations to the 1-hour SO₂ NAAQS of 75 ppb (196.2 µg/m³).

Modeled concentrations include representative temporally varying seasonal 1-hour SO₂ background values to determine the overall impact from the DRR sources. This resulting concentration is compared to the 1-hour SO₂ standard to indicate whether a modeled violation of the SO₂ NAAQS has occurred. All concentrations that fall at or below the 1-hour SO₂ NAAQS are determined to attain the standard and the area surrounding the DRR source is recommended as attainment.

10.0 ArcelorMittal – Burns Harbor (Source ID 18-127-00001)

10.1 Source Description

ArcelorMittal - Burns Harbor, LLC (Burns Harbor) is a stationary steel works plant for the production of coke, limited coal chemical, molten iron, molten steel, steel slabs, hot rolled steel, steel coils, steel plates, cold rolled and/or coated steel sheet and plate. Specific emission units associated with Burns Harbor include a coke oven process plant, coke by-products recovery plant, blast furnace granulated coal injection system, continuous sintering process plant, two blast furnaces, basic oxygen furnaces shop, slab/plate mill complex, hot strip mill, cold sheet mill operations, power station, service shop and technical maintenance operations and fugitive dust emission operations including sinter plant and blast furnace operations.

10.2 Characterization of Modeled Area

Burns Harbor opted to select the monitoring option for air quality characterization in the vicinity of its facility. Therefore, a modeling analysis was conducted to determine the location of maximum modeled 1-hour SO₂ impacts near the facility. Once the location of maximum impacts was determined, Burns Harbor located an ambient air monitor near that location in order to accurately measure the SO₂ impacts from Burns Harbor and nearby SO₂ sources to compare with the 1-hour SO₂ NAAQS.

10.3 Summary of DRR Monitoring Approach

Burns Harbor and IDEM completed a modeling analysis and SO₂ Monitor Quality Assurance and Project Plan (QAPP) to site an SO₂ monitor and submitted both to U.S. EPA- Region 5 on June 10, 2016. On August 5, 2016, U. S. EPA approved the analysis and general monitor site location based on “hot spot” modeling to determine the maximum modeled 1-hour SO₂ concentration. Burns Harbor procured monitoring equipment and obtained, from the Port of Indiana, a lease for land. U.S. EPA approved IDEM’s monitoring network for 2017 on October 31, 2016, which included the Burns Harbor SO₂ monitor. Burns Harbor was able to construct a concrete pad and shelter, set up and calibrate the equipment in early December 2016 and began operation of the monitor in mid-December, well ahead of the January 1, 2017 deadline. Clean Air Engineering completed testing of the communications system and verified calibration of all monitoring equipment. This monitor has been assigned AQS Identification number: 18-127-0028 and was operational on or before January 1, 2017. The monitoring network, consisting of the ArcelorMittal – Burns Harbor and the Dunes Acres Substation (AQS ID #18-127-0011) monitors meets the DRR requirement.

11.0 SABIC Innovative Plastics (Source ID 18-129-00002)

11.1 Source Description

SABIC Innovative Plastics Mt. Vernon, LLC (SABIC) is a plastics manufacturing facility. SABIC produces plastics for industries such as automotive, consumer electronics and medical devices.

SABIC is retrofitting their facility with a cogeneration (CoGen) plant that will use natural gas to create a majority of the steam for the site. Currently, SABIC’s coal-fired boilers provide approximately 40 percent of the facility’s steam. The U.S. EPA recently issued a new Maximum Achievable Control Technology (MACT) standard for industrial, commercial, and institutional boilers. SABIC is building their CoGen plant to address those standards. Significant SO₂ emission reductions are a byproduct of this project as several coal-fired boilers at SABIC were shut down once the project became fully operational by the end of December of 2016.

SABIC was identified as a Data Requirements Rule (DRR) source based on their actual 2014 SO₂ emissions of 4,030 tons exceeding the DRR threshold of 2,000 tons of SO₂. While the CoGen project helped SABIC realize significant SO₂ emission reductions, potential SO₂ emissions from the facility were still above 2,000 tons. The modeling option was chosen to address the DRR.

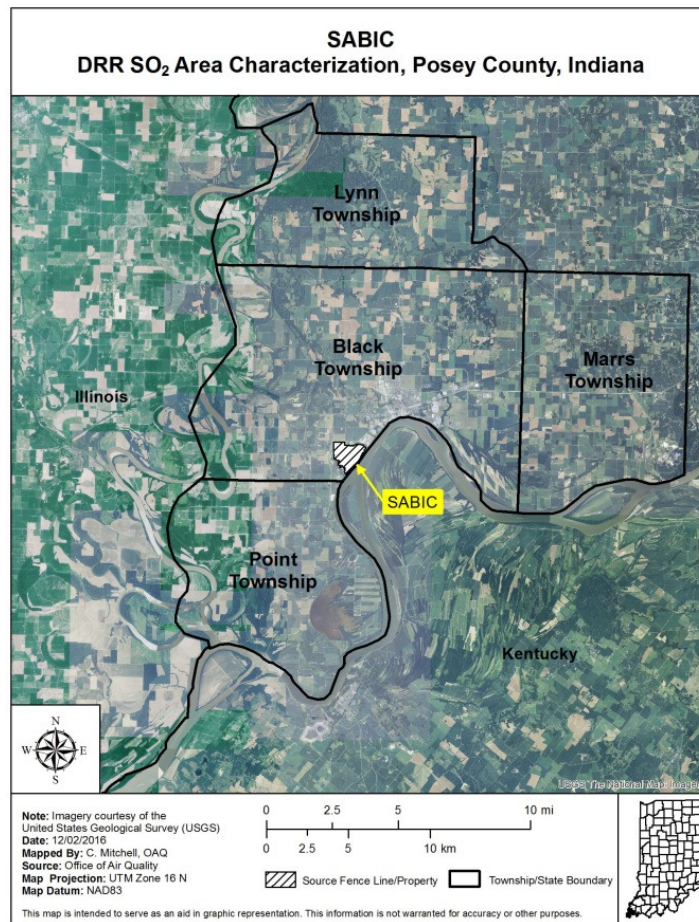
Initial modeling, using actual emissions data from 2014, showed higher modeled 1-hour SO₂ concentrations. However, after discussions with SABIC, it was decided they would request a

Commissioner's Order to establish plant-wide SO₂ emission limits that would be federally enforceable and permanent and would model attainment of the 1-hour SO₂ standard.

11.2 Characterization of Modeled Area

SABIC is located at 1 Lexan Lane, Mt. Vernon, Indiana, less than a mile from the Ohio River in Black Township, Posey County, Indiana. A map of the area surrounding the SABIC facility and the township in which SABIC is located is shown below in Figure 11.1.

Figure 11.1 - SABIC Innovative Plastics and Surrounding Area



11.3 Background Concentrations

The nearest 1-hour SO₂ monitored concentrations were taken from the Evansville – Buena Vista monitor (AQS #18-163-0021). The 99th percentile values from 2013 through 2015 and the 3-year design value are listed below in Table 11.1. Concentrations are well below the 1-hour SO₂ standard.

Table 11.1 – SABIC 99th Percentile 1-hour SO₂ Background Values and 3-year Design Value (ppb)

| Monitoring Site | 2013 | 2014 | 2015 | 2013-2015 |
|--------------------------|------|------|------|-----------|
| Evansville – Buena Vista | 18.6 | 32.3 | 18 | 23 |

11.4 Modeling Methodology

The SABIC DRR modeling methodology resembles modeling used to evaluate New Source Review (NSR) and Prevention of Significant Deterioration (PSD) sources. However, Indiana has relied on U.S. EPA guidance “EPA’s SO₂ NAAQS Designations Modeling Technical Assistance Document” in order to conduct an appropriate air dispersion modeling analysis for SABIC to support 1-hour SO₂ designation recommendations.

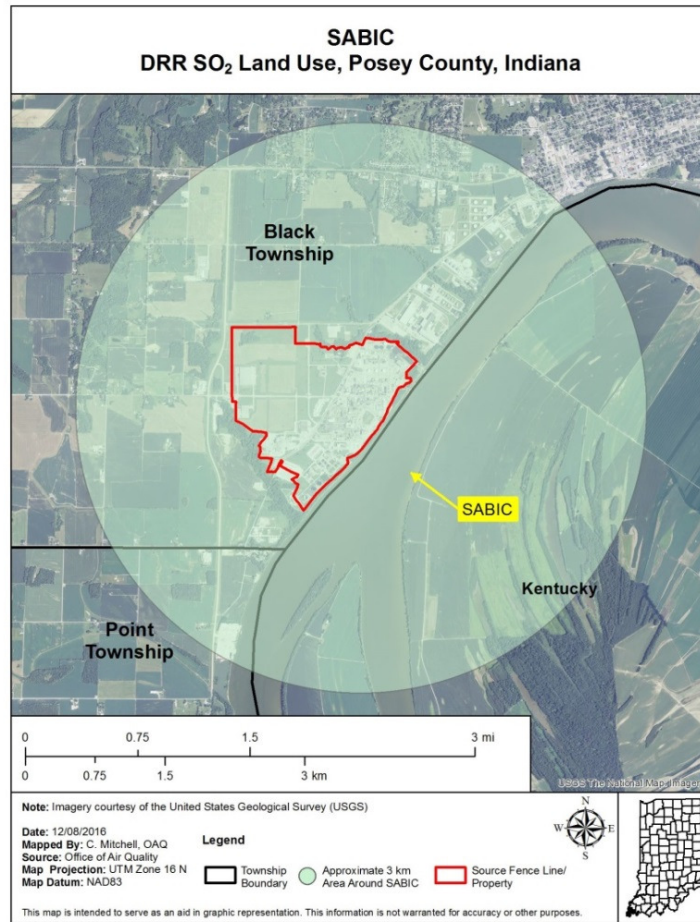
11.4.1 Model Selection

In accordance with Appendix A of Appendix W to 40 Code of Federal Regulations (CFR) Part 51, Indiana used the American Meteorological Society/Environmental Protection Agency Regulatory Model (AERMOD) version 15181. BPIPPRIME was used to account for any building downwash concerns.

11.4.2 Model Options

All regulatory default options within AERMOD were used to determine the air quality characteristics surrounding SABIC. The area is considered primarily rural, based on the Auer’s Classification Land Use methodology with a vast majority of the land use types within 3 kilometers of SABIC, classified as metropolitan natural (A1), agricultural rural (A2), water surfaces (A5) and estate residential (R4). Therefore, a rural classification was used, as provided for in the Guideline on Air Quality Models, Section 7.2.3 (EPA, 2005b). No variation of the population selection was necessary. Figure 11.2 shows the 3-kilometer radius area surrounding SABIC that was analyzed to determine the land use classification.

Figure 11.2 – SABIC 3-km Radius to Determine Auer Land Use



11.4.3 AERMAP

The AERMOD terrain preprocessor mapping program, AERMAP, was used to determine all the terrain elevation heights for each receptor, building, and source locations using the Universal Transverse Mercator (UTM) coordinate system. The most recent AERMAP version 11103 assigned the elevations from the National Elevation Dataset (NED) using the North American Datum (NAD) 1983 as recommended in the, “40 CFR Part 51, Revision to the Guideline on Air Quality Models” Appendix W and later revised in the “AERMOD Implementation Guide.”

11.5 Meteorological Data

11.5.1 AERMET

As stated in 40 CFR Part 51, Appendix W, section 8.3.1.2 and the SO₂ NAAQS Designations Modeling TAD, Indiana used 2013-2015 National Weather Service (NWS) surface and upper air meteorological data processed with the latest version of the AERMOD meteorological data

preprocessor program AERMET (version 15181). Table 11.2 below lists surface and upper air meteorological stations used to conduct modeling.

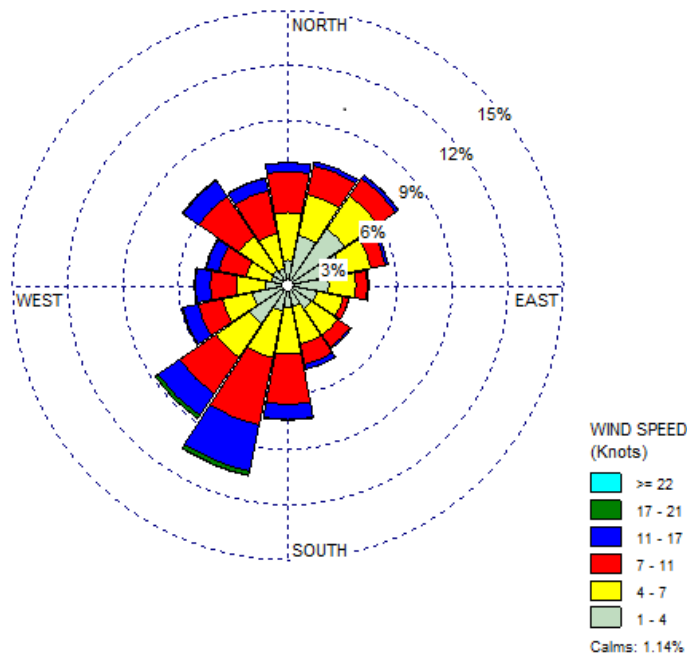
Table 11.2 – SABIC NWS Stations/Onsite Meteorological Stations

| Facility | Surface Meteorology | Upper Air Meteorology |
|---------------------------|---------------------|-----------------------|
| SABIC Innovative Plastics | Evansville, IN NWS | Lincoln, IL NWS |

11.5.2 Wind Rose

The Evansville National Weather Service (NWS) surface meteorological data and the Lincoln, Illinois upper air meteorological data taken from 2013 through 2015 was used to determine the meteorological conditions for the area surrounding SABIC in AERMOD. The Evansville NWS wind rose for the 3-year modeled period 2013-2015 is shown as Figure 11.3 below. The Evansville NWS wind rose depicts the predominant wind direction as from the southwest for the 3-year modeled period of 2013-2015.

Figure 11.3 - Evansville 3-year Cumulative Wind Rose (2013 – 2015)



11.5.3 AERMINUTE/AERSURFACE

The 1-minute wind speeds and wind directions, taken from the Automated Surface Observing System (ASOS) NWS stations and onsite meteorological stations, were processed with the U.S. EPA 1-minute data processor program AERMINUTE version 15272.

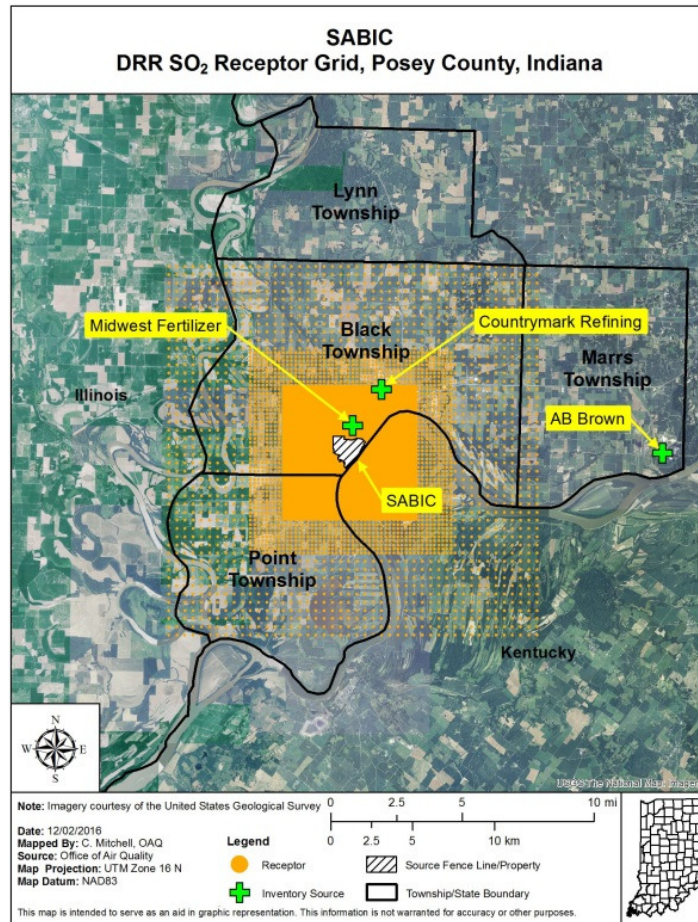
The U.S. EPA program AERSURFACE version 13016 was used to determine the surface characteristics; albedo, Bowen ratio, and surface roughness for the Evansville, Indiana NWS meteorological tower location. Surface characteristics were determined at the NWS location for each of 12 wind direction sectors with a recommended default radius of one kilometer. The albedo and the Bowen ratio surface characteristics were adjusted during the three winter months of January, February, and December in accordance with the U.S. EPA Region V document, “Regional Meteorological Data Processing Protocol,” dated May 6, 2011. Additionally, a dry or wet Bowen ratio value was used during months when soil moisture conditions were abnormally dry or wet; otherwise the Bowen ratio value for average soil moisture conditions was used. The surface roughness value for snow cover was used if more than half of the month had days with at least one inch of snow on the ground. Otherwise, the no snow cover surface roughness value was used.

11.6 Receptor Grid and Modeling Domain

The receptor grid and modeling domain was based on guidance provided in the memorandum “Updated Guidance for Area Designations for the 2010 Primary Sulfur Dioxide National Ambient Air Quality Standards”, dated March 20, 2015 and the SO₂ NAAQS Designations Modeling TAD. Indiana used a multi-nested rectangular receptor grid with appropriate spacing of receptors based on the distance from the modeled emission points to detect significant concentration gradients. The modeling domain extended out to include all sources and the appropriate distances to model maximum 1-hour SO₂ impacts to determine attainment designations for the area. Indiana used the following multi-nested rectangular receptor grid which are listed below and depicted in Figure 11.4:

- Receptor spacing at the fence line for the DRR facility was placed every 50 meters.
- Receptor spacing at 100 meters was placed out to a distance of 3,000 meters (3 kilometers) beyond the DRR facility.
- Receptor spacing at 250 meters was placed out to a distance of 5,000 meters (5 kilometers) beyond the DRR facility.
- Receptor spacing at 500 meters was placed out to a distance of 10,000 meters (10 kilometers) beyond the DRR facility.

Figure 11.4 – SABIC Receptor Grid



The SABIC property is fully fenced and has regular security patrols to keep unauthorized people off the property. Since this is the case, receptors were placed along the property lines.

11.7 Stack Heights

The use of actual stack heights rather than relying on Good Engineering Practice (GEP) stack heights when modeling actual emissions was utilized in the analysis per the SO₂ NAAQS Designations Modeling TAD.

11.8 Temporally Varying Seasonal 1-Hour SO₂ Background

Temporally varying seasonal SO₂ background concentrations were developed in accordance with the recommended U.S. EPA guidance for establishment of such background concentrations in Section 8.2 of 40 CFR Part 51, Appendix W and considered appropriate and representative of the area. The latest three years of SO₂ air quality monitoring data (2013-2015) was used.

The 99th percentile SO₂ concentrations by season (winter, spring, summer and fall) for each hour of the day were calculated to determine the temporally varying seasonal SO₂ background, which were directly input into the model and were part of the final modeled results.

Temporally varying seasonal 1-hour SO₂ background concentrations were taken from the Evansville – Buena Vista Road monitor for 2013 - 2015. The hourly seasonal SO₂ values used for representative background concentrations for the area surrounding SABIC are listed below in Table 11.3.

Table 11.3 – SABIC 99th Percentile Temporally Varying Seasonal SO₂ Background Values (ppb)

| | Hr 1 | Hr 2 | Hr 3 | Hr 4 | Hr 5 | Hr 6 | Hr 7 | Hr 8 |
|--------|------|------|------|------|------|------|------|------|
| Winter | 6.30 | 4.83 | 4.63 | 4.36 | 5.77 | 4.84 | 4.70 | 7.39 |
| Spring | 5.12 | 3.89 | 4.09 | 3.98 | 3.40 | 4.20 | 6.83 | 7.59 |
| Summer | 2.70 | 2.48 | 1.00 | 1.00 | 1.96 | 2.65 | 2.80 | 5.55 |
| Fall | 4.44 | 4.52 | 4.50 | 4.50 | 4.80 | 4.60 | 4.97 | 5.70 |

| | Hr 9 | Hr 10 | Hr 11 | Hr 12 | Hr 13 | Hr 14 | Hr 15 | Hr 16 |
|--------|------|-------|-------|-------|-------|-------|-------|-------|
| Winter | 9.29 | 10.42 | 9.20 | 10.67 | 11.55 | 17.57 | 8.71 | 16.01 |
| Spring | 9.99 | 9.84 | 11.89 | 11.65 | 7.94 | 9.89 | 8.39 | 8.55 |
| Summer | 9.93 | 11.05 | 8.50 | 9.02 | 7.34 | 5.65 | 5.49 | 5.16 |
| Fall | 7.55 | 10.68 | 11.37 | 11.21 | 10.39 | 12.92 | 9.11 | 7.56 |

| | Hr 17 | Hr 18 | Hr 19 | Hr 20 | Hr 21 | Hr 22 | Hr 23 | Hr 24 |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|
| Winter | 9.94 | 16.85 | 8.28 | 6.67 | 5.74 | 6.58 | 6.79 | 7.98 |
| Spring | 11.04 | 12.53 | 9.99 | 8.40 | 5.81 | 3.92 | 7.04 | 6.65 |
| Summer | 4.11 | 6.99 | 5.88 | 4.05 | 3.36 | 2.45 | 3.58 | 2.19 |
| Fall | 8.20 | 6.95 | 5.23 | 8.60 | 5.70 | 4.68 | 4.46 | 4.40 |

11.9 SO₂ Emissions Included in the Modeling Analysis

11.9.1 DRR Source: SABIC Emissions

As a result of the CoGen project, a number of SO₂ emission units will shut down. The unit that will still have significant SO₂ emissions is the COS Vent Oxidizer. SABIC has 16 carbon monoxide (CO) reactors, or generators, that are used to manufacture carbon monoxide. The CO generators are located in the phosgene process area. CO is generated by combusting coke (a petroleum-based material that consists mostly of carbon, with minor amounts of sulfur as an impurity) in the CO generators under low-oxygen conditions. Because the coke contains low levels of sulfur, the raw CO from the CO generators contains sulfur-containing impurities

(carbonyl sulfide, carbon disulfide, and hydrogen sulfide). These impurities need to be removed prior to the next step in the manufacturing process, where CO is combined with chlorine to make phosgene.

The raw CO is purified by passing it through one of several carbon adsorbers. At the outlet of the adsorber, a gas chromatograph measures the concentrations of the sulfur-containing compounds in the purified CO. Once a certain level of sulfur-containing compounds is detected, the flow of raw CO is switched to another adsorber and the spent adsorber is regenerated by desorbing the sulfur-containing compounds with heated nitrogen.

The adsorbed regeneration gas (primarily nitrogen, with low levels of sulfur-containing compounds) is then vented to either the COS Vent Oxidizer or the COS Flare. The regeneration gas passes through a valve that directs the flow to either the COS Vent Oxidizer or the COS Flare, but cannot direct the flow to both simultaneously. The COS Vent Oxidizer is the primary control device; the COS Flare serves as a back-up to the COS Vent Oxidizer or during safety interlock of the system. Both the COS Vent Oxidizer and COS Flare eliminate the sulfur-containing compounds in the regeneration gas by thermal combustion.

Since SO₂ emissions can be routed to either the COS Vent Oxidizer or COS Flare, modeling was performed for both scenarios to determine the worst-case dispersion. Other ancillary sources such as the liquid waste boilers were included in the inventory. Most of the other ancillary sources have small SO₂ emissions (i.e. generators and fire pumps) but were included in the modeling. All SABIC emission limits were based on fuel usage and emissions calculations taken from U.S. EPA's AP-42 emission factors. All the emission limits that are in the Commissioner's Order #2016-03 have been represented in the modeling analysis. The Commissioner's Order can be found in Enclosure 4.

11.9.2 Inventoried SO₂ Sources Included in the Modeling

SO₂ sources from the surrounding area were evaluated to determine if their SO₂ emissions had a potential impact on the air quality surrounding SABIC, beyond what is captured through background monitoring data. The latest available actual emissions were input for some of the inventory sources.

CountryMark had a reduction in SO₂ emissions as a result of installing equipment to recover the vacuum off-gas (a refinery fuel gas) rather than combusting it in the crude heater. The recovered vacuum off-gas is routed to the refinery amine unit and sulfur recovery unit where a high percentage of the sulfur compounds are converted to molten sulfur. Since this was the case, the 2015 emissions were used in the modeling analysis. A.B. Brown was modeled with the SO₂ emission limits listed in their Commissioner's Order #2016-01. Midwest Fertilizer is still under

construction and is not in full operation so an SO₂ emission rate taken from their permit was modeled. Table 11.4 lists the sources that were included in the AERMOD run to determine overall air quality characteristics.

Table 11.4 – SABIC Modeling Source Inventory

| Source | Source ID | Location | SO ₂ Emissions (tpy) |
|--------------------|-----------|--------------|---------------------------------|
| CountryMark | 129-00037 | Posey County | 65.7 |
| A.B. Brown | 129-00010 | Posey County | Emission Limits ^a |
| Midwest Fertilizer | 129-00059 | Posey County | 1.3 |

^a A.B. Brown established SO₂ emission limits in response to Round 2 designation requirements

11.10 Modeling Results

The 99th percentile of the 1-hour daily maximum modeled concentrations represents the fourth high of the 1-hour daily maximum SO₂ modeled concentrations and were averaged across three years to compare resulting concentrations to the 1-hour SO₂ NAAQS of 75 ppb (196.2 µg/m³). Modeled concentrations include representative temporally varying seasonal 1-hour SO₂ background values to determine the overall impact. The resulting concentrations were compared to the 1-hour SO₂ standard to indicate whether a modeled violation of the SO₂ NAAQS occurred. All concentrations fell below the 1-hour SO₂ NAAQS and were determined to attain the standard and the area surrounding SABIC is recommended as attainment.

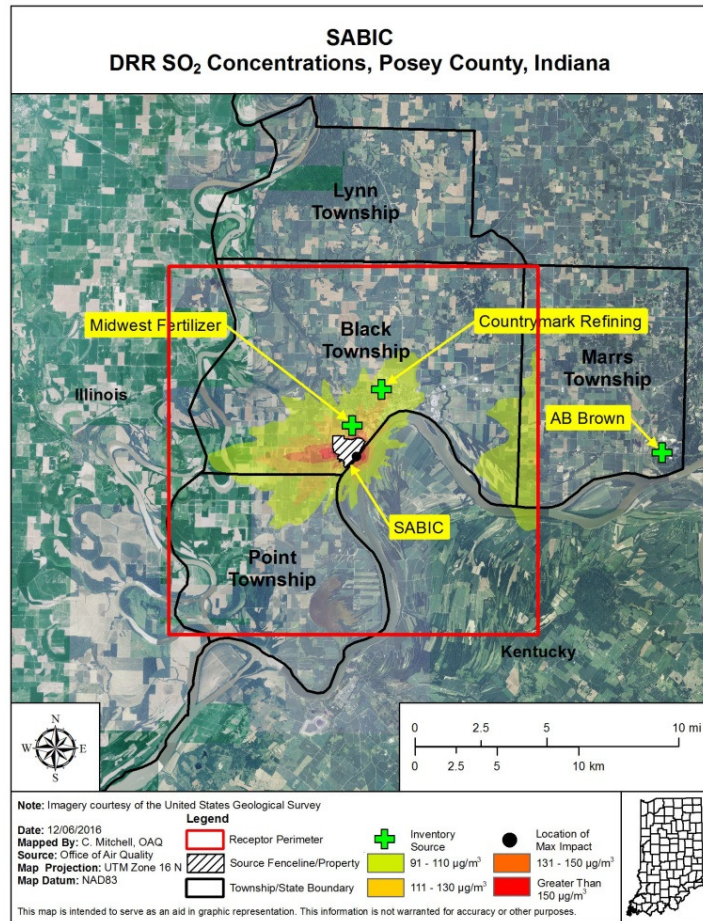
The COS Vent Oxidizer was the worst-case modeling scenario and was limited to 415 lbs of SO₂/hr which equates to a 269.21 lbs of SO₂/hr over a 24-hour averaging period. The COS Vent Oxidizer represented 93 percent of SABIC's total SO₂ modeled contributions. The other 7 percent of the modeled contributions were from SABIC's ancillary units, which also have SO₂ limits, as well as impacts from all other modeled inventory sources. Table 11.5 shows the modeled results used to establish SABIC's SO₂ emission limits. The overall maximum concentration was 191.9 µg/m³; occurring at UTM coordinates: 418467.1 East, 4195409.8 North.

Table 11.5 – SABIC Modeling Results

| Emission Scenarios | Maximum Modeled Concentration Including Seasonal Hourly Background ($\mu\text{g}/\text{m}^3$) | 1-Hour SO_2 NAAQS ($\mu\text{g}/\text{m}^3$) | Facility Models Attainment |
|-------------------------|---|---|----------------------------|
| SABIC COS Flare | 135.4 | 196.2 | Yes |
| SABIC COS Vent Oxidizer | 191.9 | 196.2 | Yes |

The concentration isopleths showing the maximum predicted 99th percentile daily 1-hour SO_2 concentration gradients can be found in Figure 11.5. The modeling demonstrated attainment of the 1-hour SO_2 standard with the emission limits listed in SABIC’s Commissioner’s Order.

Figure 11.5 – SABIC Modeling Results



12.0 Lake County: Source IDs ArcelorMittal – USA (18-089-00316)/Cokenergy (18-089-00383)/U.S. Steel (18-089-00121)

12.1 Source Description

ArcelorMittal - USA is an integrated steel mill consisting of two blast furnaces, one sinter plant, one basic oxygen furnace (BOF) complex, one hot metal Reladle/Desulf complex, an 84 inch hot strip mill with three reheat furnaces, mill finishing and sheet finishing operations, plate mill furnaces, two coke batteries, and five power station boilers. Some processes such as the BOF steel making processes have roof monitor emissions in addition to stack emissions. The blast furnaces also have non-point slag pit loadout fugitive emissions which are modeled as volume sources.

Cokenergy is an integrated steel mill consisting of one lime spray dryer Flue Gas Desulfurization unit and baghouse for the heat recovery coal carbonization facility (HRCC) waste gas stream operated by Indiana Harbor Coke Company (IHCC).

U.S. Steel is an integrated steel mill consisting of three coke batteries, a coke plant by-product recovery plant, one coke oven gas desulfurization facility, a coke plant boiler house, a sinter plant, four blast furnaces, two Basic Oxygen Process (BOP) shops with hot metal transfer and desulfurization stations, an 84 inch hot strip mill, a boiler house, and a TurboBlower boiler house. Some processes such as the BOF steel making processes have roof monitor emissions in addition to stack emissions. The blast furnaces also have non-point slag pit fugitive emissions which are modeled as volume sources.

The modeling option was chosen to address the DRR for each of the three DRR sources in Lake County.

12.2 Characterization of Modeled Area

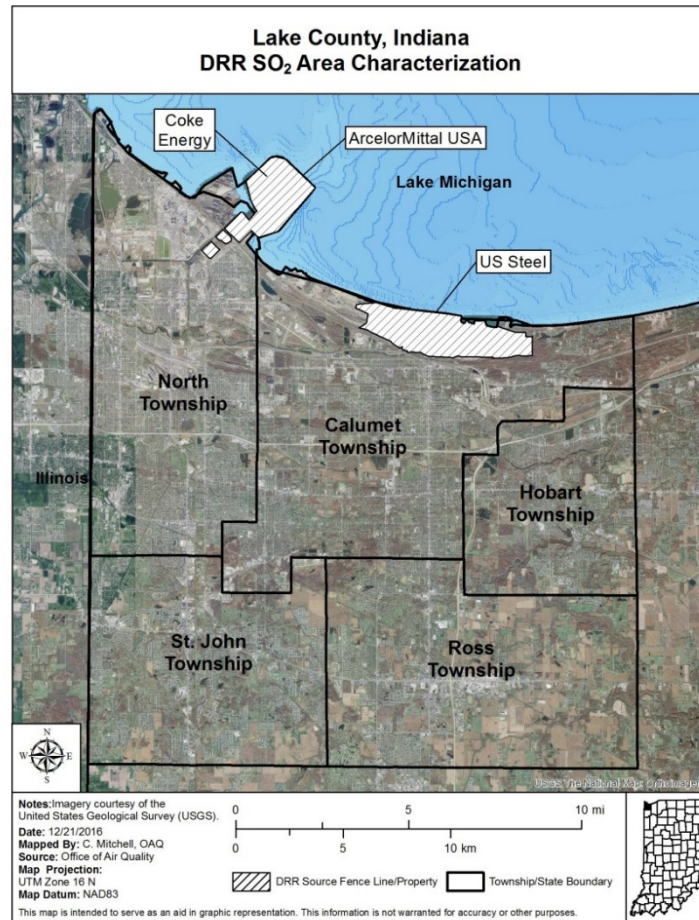
ArcelorMittal - USA is located at 3001 Dickey Road, East Chicago, in North Township, Lake County, Indiana. The northern end of the ArcelorMittal plant borders the southern shoreline of Lake Michigan.

Cokenergy is located at 3210 Watling Street, East Chicago, in North Township, Lake County, Indiana. CokeEnergy is located on the same property as ArcelorMittal – USA.

U.S. Steel is located at 1 North Broadway, Gary, in Calumet Township, Lake County, Indiana. The northern end of the U.S. Steel plant borders the southern shoreline of Lake Michigan.

A map of the area surrounding the three DRR facilities in Lake County and the townships in which each DRR facility is located is shown in Figure 12.1

Figure 12.1 - Lake County DRR Sources and Surrounding Area



12.3 Background Concentrations

The nearest 1-hour SO₂ monitored concentrations were taken from the Hammond 141st Street (AQ#18-089-2008) and Gary-IITRI (AQ#18-089-0022) monitors. The Hammond monitor was used for the western half of the receptor grid and Gary-IITRI for the eastern half. The 99th percentile values from 2013 through 2015 and the 3-year design value are listed below in Table 12.1

Table 12.1 – Lake County 99th Percentile 1-hour SO₂ Background Values and 3-year Design Value (ppb)

| Monitoring Site | 2013 | 2014 | 2015 | 2013-2015 |
|------------------------------|------|------|-------------------|-----------|
| Hammond 141 st St | 23.7 | 20.2 | 26.0 ^a | 23 |
| Gary-IITRI | 43.2 | 53.1 | 35.0 | 44 |

^a Incomplete data.

12.4 Modeling Methodology

The Lake County DRR modeling methodology resembles modeling used to evaluate New Source Review (NSR) and Prevention of Significant Deterioration (PSD) sources. However, Indiana has relied on U.S. EPA guidance “SO₂ NAAQS Designations Modeling Technical Assistance Document” in order to conduct an appropriate air dispersion modeling analysis for Lake County to support 1-hour SO₂ designation recommendations.

12.4.1 Model Selection

In accordance with Appendix A of Appendix W to 40 Code of Federal Regulations (CFR) Part 51, Indiana used the American Meteorological Society/Environmental Protection Agency Regulatory Model (AERMOD) version 15181. BPIPPRIME was used to account for any building downwash concerns.

12.4.2 Model Options

ArcelorMittal - USA/Cokenergy/U.S. Steel used the adjustment to the surface friction velocity, (ADJ_U*), AERMET option in their modeling analysis. This option was recently accepted as a regulatory option in the final rule “Revisions to the Guidelines on Air Quality Models, Enhancements to the AERMOD Dispersion Modeling System and Incorporation of Approaches to Address Ozone and Fine Particulate Matter”, signed on December 20, 2016. The ADJ_U* regulatory option provides for better model performance.

Non-regulatory options within AERMOD were used to determine the air quality characteristics for Lake County. This is due to the use of site-specific meteorology. The area is considered primarily urban, based on population density. The population value used was equal to the sum of population of cities where sources exist and any adjacent cities which meet the population density criteria. Technically, Gary, Indiana did not meet the strict definition of population density for urban classification. However, at least one-quarter of the area of Gary consists of U.S. Steel. By definition an integrated steel mill is considered urban with light-moderate to heavy industrial use. The entire population lives in the remainder of Gary. After factoring out 25% of the Gary’s land area, Gary meets the 750 people/sq km population density threshold for using an urban dispersion coefficient. Therefore, an urban classification with an area population

of 243,149 was used in the model input, as provided for in the Guideline on Air Quality Models, Section 7.2.3 (EPA, 2005b). Table 12.2 details the surrounding sizes and population densities of towns in the area to determine the overall population density for the appropriate urban land use characterization. All other regulatory default options were selected to perform the air quality analysis for the three Lake County DRR facilities.

Table 12.2 - Lake County Urban Population

| City | Population | Area sq mi | Population Density per sq mi | Population Density per sq km | Adjusted Density per sq km |
|--------------|------------|---------------|------------------------------------|------------------------------------|----------------------------------|
| Gary | 80,294 | 49.87 | 1,610 | 613 | 818 |
| Hammond | 80,830 | 22.78 | 3,548 | 1,344 | N/A |
| East Chicago | 29,698 | 14.09 | 2,108 | 950 | N/A |
| Whiting | 4,997 | 1.8 | 2,776 | 1,081 | N/A |
| Munster | 23,603 | 7.57 | 3,118 | 1,198 | N/A |
| Highland, IN | 23,727 | 6.94 | 3,419 | 1,318 | N/A |
| Total | 243,149 | | | | |

12.4.3 AERMAP

The AERMOD terrain preprocessor mapping program, AERMAP, was used to determine all the terrain elevation heights for each receptor, building, and source locations using the Universal Transverse Mercator (UTM) coordinate system. The most recent AERMAP version 11103 assigned the elevations from the National Elevation Dataset (NED) using the North American Datum (NAD) 1983 as recommended in the, “40 CFR Part 51, Revision to the Guideline on Air Quality Models” Appendix W and later revised in the “AERMOD Implementation Guide.”

12.5 Meteorological Data

12.5.1 AERMET

The Gary-IITRI surface meteorological data and the Lincoln, Illinois upper air meteorological data taken from 2013 through 2015 were used to determine the meteorological conditions surrounding the three Lake County DRR sources. The Gary-IITRI surface meteorological data was used to more accurately include the influence of Lake Michigan on the meteorological conditions in the area immediately surrounding the three Lake County DRR facilities. The Gary-IITRI surface data was processed without turbulence parameters in order to use the ADJ_U* option. This was processed with the latest version of the AERMOD meteorological data

preprocessor program AERMET (version 15181). Table 12.3 below lists the surface and upper air meteorological stations used to conduct modeling.

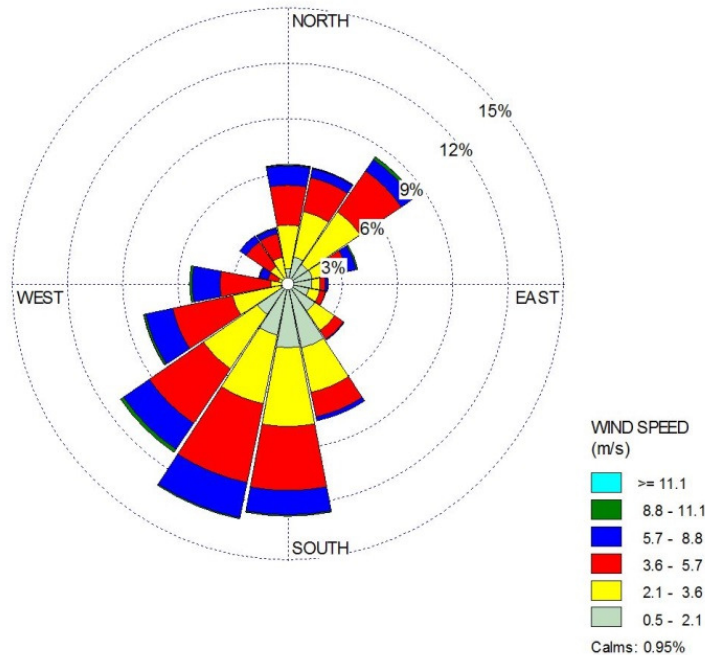
Table 12.3 – Lake County NWS Stations/Onsite Meteorological Stations

| Facility | Surface Meteorology | Upper Air Meteorology |
|--|---------------------------------------|-----------------------|
| ArcelorMittal-USA/U.S. Steel/ Cokenergy | Gary-IITRI Monitor/ South Bend NWS | Lincoln, IL NWS |

12.5.2 Wind Rose

The Gary-IITRI surface meteorological data and the Lincoln, Illinois upper air meteorological data taken from 2013 through 2015 were used to determine the meteorological conditions for the Lake County area. The Gary-IITRI wind rose for the 3-year modeled period 2013-2015 is shown as Figure 12.2 below. The Gary wind rose depicts the predominant wind direction as from the southwest for the 3-year modeled period.

Figure 12.2 – Gary-IITRI 3-year Cumulative Wind Rose (2013 – 2015)



12.5.3 AERMINUTE/AERSURFACE

The 1-minute wind speeds and wind directions, taken from the Automated Surface Observing System (ASOS) NWS stations and onsite meteorological stations, were processed with the U.S. EPA 1-minute data processor program AERMINUTE version 15272. All regulatory default options were selected with the exception of the use of the adjustment to the surface friction

velocity, (ADJ_U*) option. The ADJ_U* option has been demonstrated to provide better model performance for determining 1-hour SO₂ concentrations. The ADJ_U* option has been accepted by U.S. EPA in a final rulemaking signed on December 20, 2016.

The U.S. EPA program AERSURFACE version 13016 was used to determine the surface characteristics; albedo, Bowen ratio, and surface roughness for the Gary-IITRI, Indiana meteorological tower location. Surface characteristics were determined at the NWS location for each of 12 wind direction sectors with a recommended default radius of one kilometer.

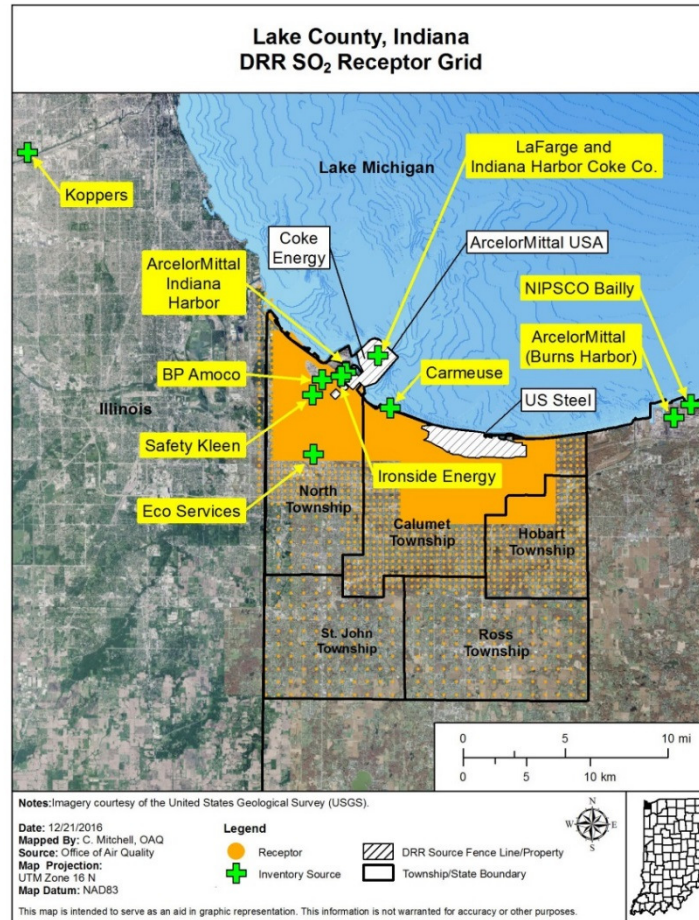
The albedo and the Bowen ratio surface characteristics were adjusted during the three winter months of January, February, and December in accordance with the U.S. EPA Region V document, “Regional Meteorological Data Processing Protocol,” dated May 6, 2011. Additionally, a dry or wet Bowen ratio value was used during months when soil moisture conditions were abnormally dry or wet; otherwise the Bowen ratio value for average soil moisture conditions was used. The surface roughness value for snow cover was used if more than half of the month had days with at least one inch of snow on the ground. Otherwise, the no snow cover surface roughness value was used.

12.6 Receptor Grid and Modeling Domain

The receptor grid and modeling domain was based on guidance provided in the memorandum “Updated Guidance for Area Designations for the 2010 Primary Sulfur Dioxide National Ambient Air Quality Standards”, dated March 20, 2015 and the SO₂ NAAQS Designations Modeling TAD. Indiana used a multi-nested rectangular receptor grid with appropriate spacing of receptors based on the distance from the modeled emission points to detect significant concentration gradients. The modeling domain extended out to include all sources and the appropriate distances to model maximum 1-hour SO₂ impacts to determine attainment designations for the area. Indiana used the following multi-nested rectangular receptor grids listed below and depicted in Figure 12.3. Focus was emphasized on receptor placement near each of the Lake County DRR sources; expected 1-hour SO₂ impacts would be anticipated to be very near each source.

- Receptor spacing at the fence line for each facility was placed every 50 meters.
- Receptor spacing at 100 meters was placed out to a distance of 5,000 meters (5 kilometers) beyond each facility.
- Receptor spacing at 500 meters was placed out to a distance of 10,000 meters (10 kilometers) beyond each facility and east to the Porter County line.
- Receptor spacing at 1000 meters was placed beyond 10,000 meters (10 kilometers) from each facility to the south to cover the southern extent of St. John, Ross and North townships.

Figure 12.3 – Lake County Receptor Grid



ArcelorMittal - USA, Cokenergy and U.S. Steel have fenced areas, natural boundaries and gated areas with regular security patrols to keep unauthorized people off the property. Since this is the case, receptors were placed along the property lines as appropriate.

12.7 Stack Heights

The use of actual stack heights rather than relying on Good Engineering Practice (GEP) stack heights when modeling actual emissions was utilized in the analysis per the SO₂ NAAQS Designations Modeling TAD.

12.8 Temporally Varying Seasonal 1-Hour SO₂ Background

Temporally varying seasonal SO₂ background concentrations were developed in accordance with the recommended U.S. EPA guidance for establishment of such background concentrations in Section 8.2 of 40 CFR Part 51, Appendix W and considered appropriate and representative of the

area. The latest three years of SO₂ air quality monitoring data (2013-2015) was used from both the Hammond and Gary sites.

The 99th percentile SO₂ concentrations by season (winter, spring, summer and fall) for each hour of the day were calculated to determine the temporally varying seasonal SO₂ background, which were directly input into the model and were part of the final modeled results.

Temporally varying seasonal 1-hour SO₂ background concentrations were taken from the Hammond (west) and Gary (east) monitors for 2013 - 2015. Two sets of 1-hour SO₂ background were used to best represent the Lake County DRR sources, ArcelorMittal – USA and Cokenergy are located in the western portion of the county and U.S. Steel is located in the eastern portion of the county. Hammond monitor will also measure the SO₂ impacts from Illinois. The hourly seasonal SO₂ values used for representative background concentrations for the Lake County DRR sources are listed below in Table 12.4 for the Hammond monitor and in Table 12.5 for the Gary-IITRI monitor.

Table 12.4 – Lake County Hammond Monitor 99th Percentile Temporally Varying Seasonal SO₂ Background Values (ppb)

| | Hr 1 | Hr 2 | Hr 3 | Hr 4 | Hr 5 | Hr 6 | Hr 7 | Hr 8 |
|--------|------|------|------|------|------|------|------|------|
| Winter | 5.4 | 5.7 | 5.94 | 6.08 | 6.12 | 6.18 | 5.8 | 6.14 |
| Spring | 5.74 | 5.53 | 5.44 | 5.34 | 5.6 | 6.07 | 6.4 | 7.03 |
| Summer | 4.87 | 4.63 | 4.6 | 4.8 | 5.57 | 5.28 | 6.01 | 6.57 |
| Fall | 5.03 | 4.13 | 5.34 | 3.84 | 4.61 | 6.35 | 6.1 | 6.28 |

| | Hr 9 | Hr 10 | Hr 11 | Hr 12 | Hr 13 | Hr 14 | Hr 15 | Hr 16 |
|--------|------|-------|-------|-------|-------|-------|-------|-------|
| Winter | 6.73 | 7.03 | 8.76 | 7.72 | 7.89 | 7.18 | 8.78 | 7.84 |
| Spring | 8.27 | 8.43 | 9.19 | 7.68 | 8.2 | 8.09 | 8.14 | 8.86 |
| Summer | 8.97 | 7.54 | 8.77 | 8.31 | 9 | 7.96 | 8.95 | 6.51 |
| Fall | 8.1 | 8.04 | 8.11 | 6.84 | 8.08 | 7.52 | 8.16 | 7.74 |

| | Hr 17 | Hr 18 | Hr 19 | Hr 20 | Hr 21 | Hr 22 | Hr 23 | Hr 24 |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|
| Winter | 6.9 | 6.18 | 6.44 | 5.74 | 5.58 | 5.74 | 5.68 | 5.58 |
| Spring | 8.85 | 9.4 | 9.24 | 7.76 | 7.9 | 6.84 | 7 | 7.84 |
| Summer | 7.76 | 7.87 | 7.97 | 6.31 | 6.04 | 8.07 | 5.69 | 5.14 |
| Fall | 8.91 | 6.81 | 7.12 | 7.31 | 6.75 | 5.37 | 4.9 | 3.8 |

Table 12.5 – Lake County Gary - IITRI 99th Percentiles Temporally Varying Seasonal SO₂ Background Values (ppb)

| | Hr 1 | Hr 2 | Hr 3 | Hr 4 | Hr 5 | Hr 6 | Hr 7 | Hr 8 |
|--------|------|------|------|------|------|------|------|------|
| Winter | 9.69 | 7.35 | 7.1 | 6.74 | 6.87 | 7.03 | 6.32 | 7.42 |
| Spring | 7.31 | 4.59 | 7.82 | 4.88 | 6.88 | 7.84 | 8.58 | 6.96 |
| Summer | 1.37 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Fall | 6.98 | 5.64 | 5.44 | 5.56 | 7.57 | 4.64 | 5.24 | 8.02 |

| | Hr 9 | Hr 10 | Hr 11 | Hr 12 | Hr 13 | Hr 14 | Hr 15 | Hr 16 |
|--------|------|-------|-------|-------|-------|-------|-------|-------|
| Winter | 8.35 | 9.35 | 9.52 | 9.35 | 8.66 | 8.5 | 12.29 | 10.44 |
| Spring | 8.22 | 8.17 | 10.34 | 15.5 | 9.62 | 9.02 | 9.54 | 9.05 |
| Summer | 5.83 | 9.03 | 7.29 | 7.47 | 5.47 | 4.47 | 3.93 | 3.77 |
| Fall | 6.9 | 6.81 | 8.5 | 8.82 | 8.84 | 8.96 | 7 | 6.45 |

| | Hr 17 | Hr 18 | Hr 19 | Hr 20 | Hr 21 | Hr 22 | Hr 23 | Hr 24 |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|
| Winter | 9.33 | 6.84 | 7.22 | 8.35 | 6.4 | 6.81 | 8.64 | 9.04 |
| Spring | 8.24 | 7.84 | 7.38 | 6.34 | 7.32 | 6.44 | 8.73 | 7.58 |
| Summer | 3.72 | 3.97 | 2.53 | 2.41 | 2.4 | 1 | 2.24 | 2.83 |
| Fall | 6.46 | 4.62 | 4.71 | 7.14 | 4.64 | 4.94 | 7.01 | 7.19 |

12.9 SO₂ Emissions Included in the Modeling Analysis

12.9.1 DRR Source Emissions

ArcelorMittal - USA and U.S. Steel were modeled using different emission methodologies. Continuous emission monitoring data (CEM) data was available for several emission units while others had seasonal or weekly varying emission rates that were modeled. Cokenergy has emission data collected by a continuous emission monitor; therefore, CEM data was modeled. ArcelorMittal – USA and U.S. Steel have processes with varying hourly emissions rates that were based on a daily maximum emission rate. Emissions were allocated for each hour of the day. Emission units without CEM data or daily emission records were averaged across the three modeled years (2013-2015). Enclosure 2 contains a listing of all of the AERMOD inputs of all the DRR and inventory sources for Lake County.

12.9.2 Carmeuse Lime’s Commissioner’s Order – SO₂ Emission Limits

Carmeuse Lime, Inc. (Carmeuse) is a stationary lime manufacturing plant (Source I.D. 089-00112) located at 1 North Carmeuse Drive in Gary in Lake County. Carmeuse is not a DRR source but was identified as potentially impacting SO₂ air quality near the Lake County DRR sources. SO₂ sources from the surrounding area in Lake County were evaluated to determine if their emissions would impact the air quality surrounding the DRR sources, beyond what is

captured through background SO₂ ambient air monitoring data. Initial modeling, using actual emissions data from Carmeuse showed potential 1-hour SO₂ concentrations higher than the 1-hour SO₂ NAAQS. Therefore, Carmeuse submitted a request on November 15, 2016 for a Commissioner's Order to establish SO₂ emission limits that would be federally enforceable and permanent which demonstrate attainment of the 1-hour SO₂ standard. The Commissioner's Order #2016-04 was signed on November 16, 2016 and is included in Enclosure 3.

Carmeuse's SO₂ emissions are distributed amongst their five kilns. In order to establish hourly emissions limits for Carmeuse through the Commissioner's Order, modeling was conducted to determine limits that demonstrated compliance with the 1-hour SO₂ standard. Each kiln has six stacks so modeling determined each kiln would be limited to 12.0 pounds of SO₂/hour or 2.0 pounds of SO₂/hour for each stack of each kiln. The three DRR sources, surrounding SO₂ source inventories, and temporally varying seasonal SO₂ background concentrations were included in the modeling to establish Carmeuse's emission limits through a Commissioner's Order.

The 720 operating hour rolling average emission limit listed in the Commissioner's Order was based on the 12.0 pound/hour limit modeled for each kiln. U.S. EPA recommended using a flat averaging ratio for emission units with no emission controls, as referenced in Table 1 of U.S. EPA's "Guidance for 1-hour SO₂ Nonattainment Area SIP Submissions". Based on the average ratio of 99th percentile 30-day average SO₂ emission values to the 99th percentile of hourly SO₂ emission values of 0.79, the corresponding 720 operating hour average for each kiln was calculated to be 9.48 lb/hr.

12.9.3 Inventoried SO₂ Sources Included in the Modeling

Inclusion of sources in the DRR modeling was based upon their actual emissions from 2013-2015. The only exception was BP Products (BP), which modeled 2015 SO₂ emissions. BP completed its Whiting Refinery Modernization Project (WRMP) on May 10, 2014. This project was permitted with a significant source modification (Permit #089-25484-00453 issued May 1, 2008) and significant permit modification (Permit #089-25488-00453 issued June 16, 2008), authorizing the construction of new emission units, modifications to existing emission units and operational changes as necessary. A Consent Decree (Civil No. 2:12-cv-00207) was issued to address revisions to BP's WRMP. SO₂ emissions as a result of the WRMP were modeled for the Lake County DRR analysis.

All facilities greater than one-half of the PSD significance threshold of 40 tpy were included. The sources which were explicitly modeled had overall SO₂ emissions of 16,233 tpy. This accounts for 99.8% of the Lake County SO₂ inventory. Continuous emissions monitoring data, seasonal or daily varying emissions or an average of 3-year annual SO₂ emissions were modeled for all sources.

The modeled inventory included two Porter County SO₂ sources (ArcelorMittal – Burns Harbor and the NIPSCO – Bailly Generating Station). Koppers Inc. in Chicago, Illinois, was also included in the inventory. Two coal-fired power plants in Cook County, Illinois shut down in 2012 and as a result were not included in the modeling analysis. The following facilities were included in the air quality modeling analysis to determine the overall SO₂ air quality impact in the area and are listed in Table 12.6.

Table 12.6 - Lake County Modeling Inventory

| Source | Source ID | Location | 2013-2015 Average SO ₂ Emissions (tpy) |
|----------------------------------|--------------|-------------------|---|
| BP Products, North America Inc. | 18-089-00003 | Lake County, IN | 400.2 ^a |
| Carmeuse Lime, Inc | 18-089-00112 | Lake County, IN | Emission Limits ^b |
| Eco Services Corp | 18-089-00242 | Lake County, IN | 255.6 |
| Safety-Kleen Systems Inc. | 18-089-00301 | Lake County, IN | 62.6 |
| ArcelorMittal - USA | 18-089-00318 | Lake County, IN | 1,430.8 |
| Indiana Harbor Coke Company | 18-089-00382 | Lake County, IN | 2,441.1 |
| Ironside Energy LLC | 18-089-00448 | Lake County, IN | 204.5 |
| ISPAT Inland LaFarge NA | 18-089-00458 | Lake County, IN | 122.9 |
| ArcelorMittal – Burns Harbor | 18-127-00001 | Porter County, IN | 12,189 |
| NIPSCO Bailly Generating Station | 18-127-00002 | Porter County, IN | 2013-2015 CEMS Data |
| Koppers Inc. | 170000035076 | Cook County, IL | 1,785.7 |

^a IDEM utilized BP Products' 2015 SO₂ emissions due to the Whiting Refinery Modernization Project, completed on May 10, 2014

^b Carmeuse Lime, Inc. established SO₂ emission limits in Commissioner's Order #2016-04

12.10 Modeling Results

The 99th percentile of the 1-hour daily maximum modeled concentrations represents the fourth high of the 1-hour daily maximum SO₂ modeled concentrations and were averaged across three years to compare resulting concentrations to the 1-hour SO₂ NAAQS of 75 ppb (196.2 µg/m³). Modeled concentrations include representative temporally varying seasonal 1-hour SO₂ background values to determine the overall impact. The resulting concentrations were compared to the 1-hour SO₂ standard to indicate whether a modeled violation of the SO₂ NAAQS occurred. All concentrations fell below the 1-hour SO₂ NAAQS and were determined to attain the standard and the area surrounding the DRR sources is recommended as attainment. Table 12.6 shows the modeled localized peaks for all DRR sources in Lake County and including the Carmeuse's SO₂ emission limits established through the Commissioner's Order. The overall maximum concentration was 192.2 µg/m³, occurring at UTM coordinates 466100.0 East, 4609900.0 North,

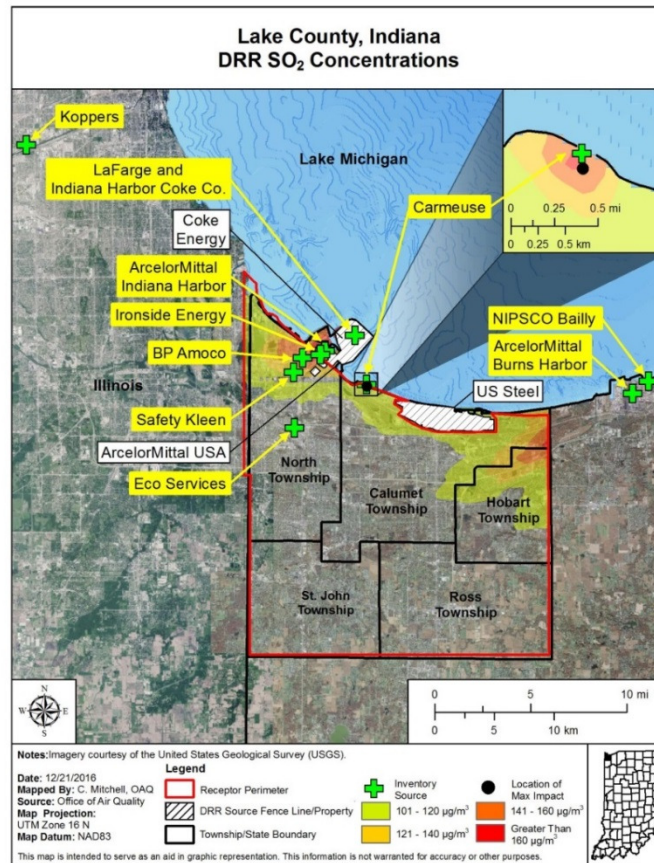
associated with Carmeuse’s maximum impacts. 1-hour SO₂ impacts east of Lake County are being addressed through the air quality characterization of Porter County using the monitoring option for ArcelorMittal – Burns Harbor facility, a DRR source.

Table 12.7 – Lake County Modeling Results

| Source | Maximum Modeled Concentration Including Seasonal Hourly Background (µg/m ³) | 1-Hour SO ₂ NAAQS (µg/m ³) | Models Attainment |
|--------------------|---|---|-------------------|
| Carmeuse Lime | 192.2 | 196.2 | Yes |
| U.S. Steel | 128.1 | 196.2 | Yes |
| Cokenergy | 182.8 | 196.2 | Yes |
| ArcelorMittal USA | 182.8 | 196.2 | Yes |
| Porter County Line | 168.7 | 196.2 | Yes |

The concentration isopleths showing the maximum predicted 99th percentile daily 1-hour SO₂ concentration gradients can be found in Figure 12.5.

Figure 12.4 – Lake County Modeling Results



13.0 Duke-Gallagher (Source ID 153-00005)

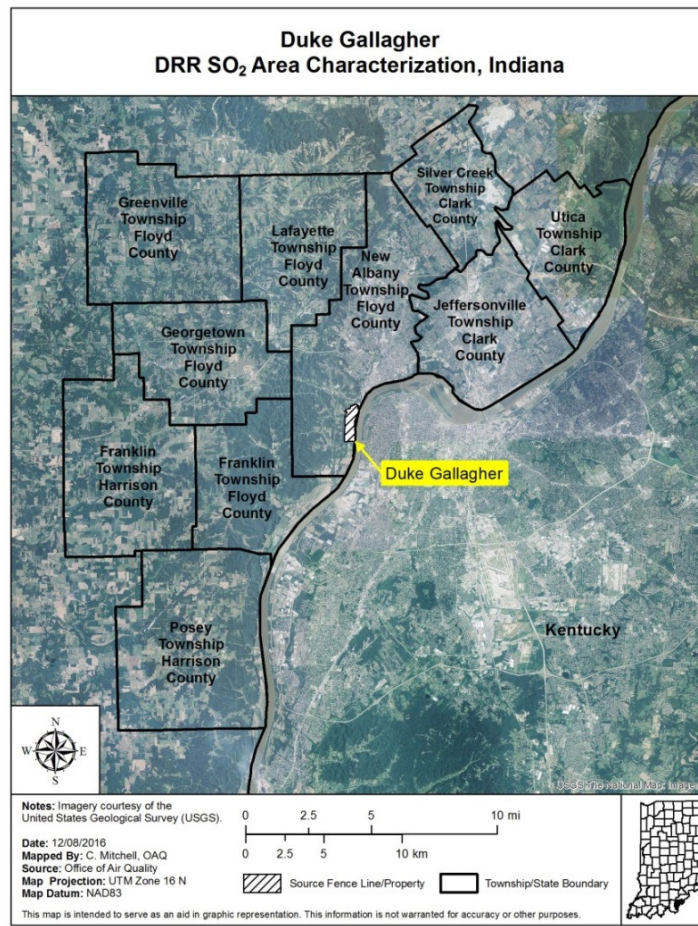
13.1 Source Description

Duke - Gallagher Generating Station (Duke - Gallagher) is a 280 MW coal-fired power plant in Floyd County located in southeast Indiana. Duke - Gallagher has two coal-fired boilers rated at 1,390 MMBtu/hr each. The plant is operated by Duke Energy Indiana, LLC. Duke - Gallagher was identified as a Data Requirements Rule (DRR) source based on their actual 2014 SO₂ emissions of 3,524 tons exceeding the DRR threshold of 2,000 tons of SO₂.

13.2 Characterization of Modeled Area

Duke - Gallagher is located at 30 Jackson St, New Albany, Indiana, on the banks of the Ohio River in New Albany Township, Floyd County, Indiana. A map of the area surrounding Duke - Gallagher is shown below in Figure 13.1.

Figure 13.1 – Duke - Gallagher and Surrounding Area



13.3 Background Concentrations

The nearest 1-hour SO₂ monitored concentrations were taken from the Green Valley monitor (AQS #18-043-1004) located in Floyd County. The 99th percentile values from 2013 through 2015 and the 3-year design value are listed below in Table 13.1.

Table 13.1 – Duke – Gallagher 99th Percentile 1-hour SO₂ Background Values and 3-year Design Value (ppb)

| Monitoring Site | 2013 | 2014 | 2015 | 2013-2015 |
|-------------------------|------|------|------|-----------|
| Floyd Co – Green Valley | 30.0 | 65.0 | 28.0 | 41 |

13.4 Modeling Methodology

The Duke - Gallagher DRR modeling methodology resembles modeling used to evaluate New Source Review (NSR) and Prevention of Significant Deterioration (PSD) sources. However, Indiana has relied on U.S. EPA guidance “SO₂ NAAQS Designations Modeling Technical Assistance Document” in order to conduct an appropriate air dispersion modeling analysis for Duke - Gallagher to support 1-hour SO₂ designation recommendations.

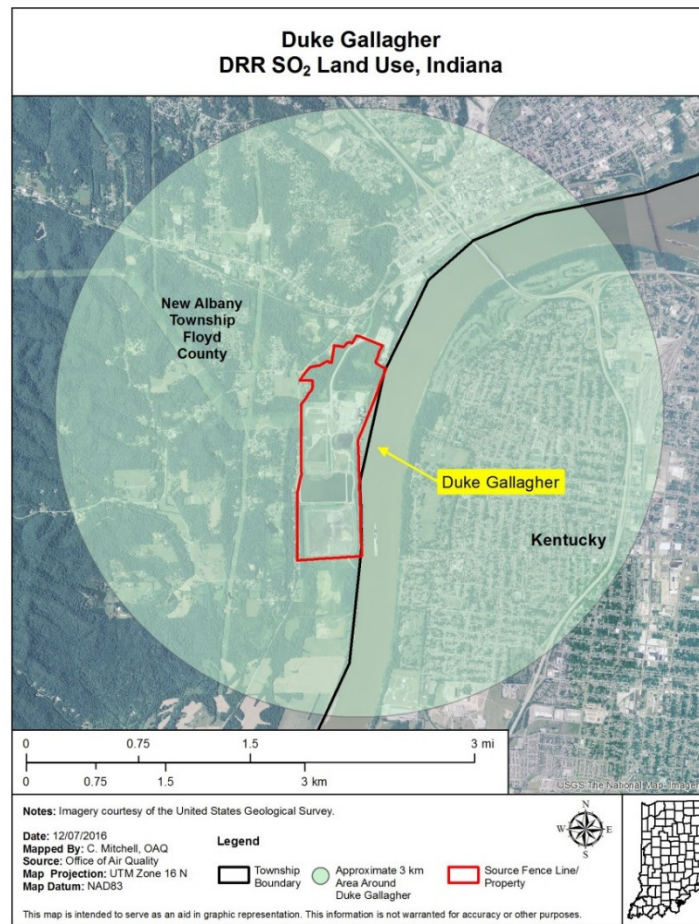
13.4.1 Model Selection

In accordance with Appendix A of Appendix W to 40 Code of Federal Regulations (CFR) Part 51, Indiana used the American Meteorological Society/Environmental Protection Agency Regulatory Model (AERMOD) version 15181. BPIPPRIME was used to account for any building downwash concerns.

13.4.2 Model Options

All regulatory default options within AERMOD were used to determine the air quality characteristics surrounding Duke - Gallagher. The area is considered primarily rural, based on the Auer’s Classification Land Use methodology with a vast majority of the land use types classified as undeveloped rural (A4), water surfaces (A5) and estate residential (R4). Therefore, a rural classification was used, as provided for in the Guideline on Air Quality Models, Section 7.2.3 (EPA, 2005b). No variation of the population selection was necessary. Figure 13.2 shows the 3-kilometer radius area surrounding Duke - Gallagher that was analyzed to determine the land use classification.

Figure 13.2 – Duke – Gallagher 3-kilometer Radius to Determine Auer Land Use



13.4.3 AERMAP

The AERMOD terrain preprocessor mapping program, AERMAP, was used to determine all the terrain elevation heights for each receptor, building, and source locations using the Universal Transverse Mercator (UTM) coordinate system. The most recent AERMAP version 11103 assigned the elevations from the National Elevation Dataset (NED) using the North American Datum (NAD) 1983 as recommended in the, “40 CFR Part 51, Revision to the Guideline on Air Quality Models” Appendix W and later revised in the “AERMOD Implementation Guide.”

13.5 Meteorological Data

13.5.1 AERMET

As stated in 40 CFR Part 51, Appendix W, section 8.3.1.2 and the SO₂ NAAQS Designations Modeling TAD, Indiana used 2013-2015 National Weather Service (NWS) surface and upper air meteorological data processed with the latest version of the AERMOD meteorological data

preprocessor program AERMET (version 15181). Table 13.2 below lists surface and upper air meteorological stations used to conduct modeling.

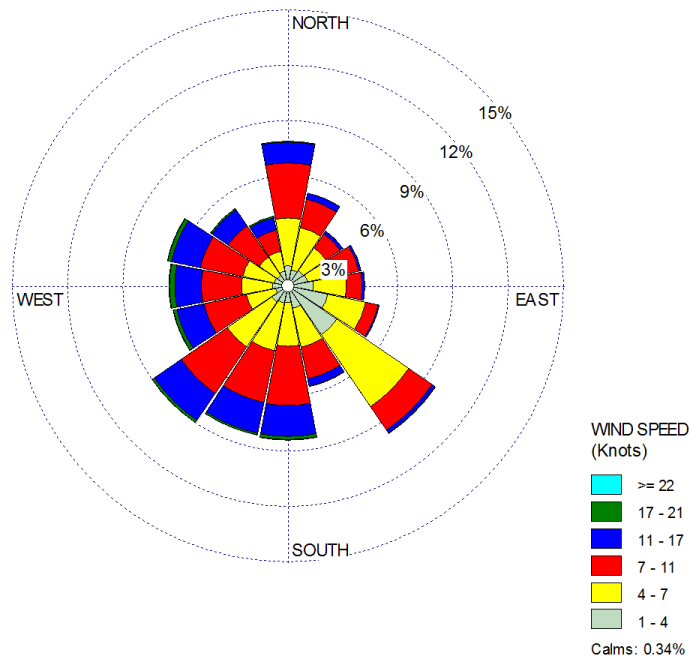
Table 13.2 – Duke - Gallagher NWS Stations/Onsite Meteorological Stations

| Facility | Surface Meteorology | Upper Air Meteorology |
|------------------|---------------------|-----------------------|
| Duke – Gallagher | Louisville, KY NWS | Wilmington, OH NWS |

13.5.2 Wind Rose

The Louisville, Kentucky National Weather Service (NWS) surface meteorological data and Wilmington, Ohio upper air meteorological data taken from 2013 through 2015 were used to determine the meteorological conditions for the area surrounding Duke - Gallagher in AERMOD. The Louisville NWS wind rose for the 3-year modeled period 2013-2015 is shown as Figure 13.3 below. The Louisville NWS wind rose depicts the predominant wind direction as from the southwest for the 3-year modeled period 2013-2015.

Figure 13.3 - Louisville 3-year Cumulative Wind Rose (2013 – 2015)



13.5.3 AERMINUTE/AERSURFACE

The 1-minute wind speeds and wind directions, taken from the Automated Surface Observing System (ASOS) NWS stations and onsite meteorological stations, were processed with the U.S. EPA 1-minute data processor program AERMINUTE version 15272.

The U.S. EPA program AERSURFACE version 13016 was used to determine the surface characteristics; albedo, Bowen ratio, and surface roughness for the Louisville, Indiana NWS meteorological tower location. Surface characteristics were determined at the NWS location for each of 12 wind direction sectors with a recommended default radius of one kilometer.

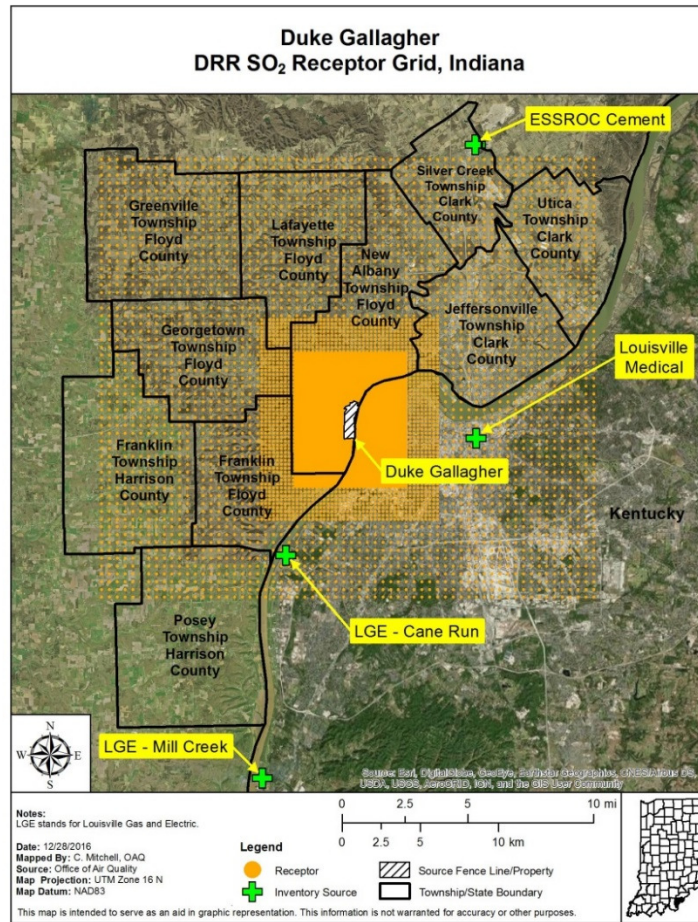
The albedo and the Bowen ratio surface characteristics were adjusted during the three winter months of January, February, and December in accordance with the U.S. EPA Region V document, “Regional Meteorological Data Processing Protocol,” dated May 6, 2011. Additionally, a dry or wet Bowen ratio value was used during months when soil moisture conditions were abnormally dry or wet; otherwise the Bowen ratio value for average soil moisture conditions was used. The surface roughness value for snow cover was used if more than half of the month had days with at least one inch of snow on the ground. Otherwise, the no snow cover surface roughness value was used.

13.6 Receptor Grid and Modeling Domain

The receptor grid and modeling domain was based on guidance provided in the memorandum “Updated Guidance for Area Designations for the 2010 Primary Sulfur Dioxide National Ambient Air Quality Standards”, dated March 20, 2015 and the SO₂ NAAQS Designations Modeling TAD. Indiana used a multi-nested rectangular receptor grid with appropriate spacing of receptors based on the distance from the modeled emission points to detect significant concentration gradients. The modeling domain extended out to include all sources and the appropriate distances to model maximum 1-hour SO₂ impacts to determine attainment designations for the area. Indiana used the following multi-nested rectangular receptor grid which are listed below and depicted in Figure 13.4:

- Receptor spacing at the fence line for each facility was placed every 50 meters.
- Receptor spacing at 100 meters was placed out to a distance of 3,000 meters (3 kilometers) beyond the DRR facility.
- Receptor spacing at 250 meters was placed out to a distance of 5,000 meters (5 kilometers) beyond the DRR facility.
- Receptor spacing at 500 meters was placed out to a distance of 10,000 meters (10 kilometers) beyond the DRR facility.

Figure 13.4 – Duke – Gallagher Receptor Grid



Duke - Gallagher has a fence line, natural features, and security patrols that restrict public access to its property. Receptors were therefore placed along the property boundary where public access is not restricted.

13.7 Stack Heights

The use of actual stack heights rather than relying on Good Engineering Practice (GEP) stack heights when modeling actual emissions was utilized in the analysis per the SO₂ NAAQS Designations Modeling TAD.

13.8 Temporally Varying Seasonal 1-Hour SO₂ Background

Temporally varying seasonal SO₂ background concentrations were developed in accordance with the recommended U.S. EPA guidance for establishment of such background concentrations in Section 8.2 of 40 CFR Part 51, Appendix W and considered appropriate and representative of the area. The latest three years of SO₂ air quality monitoring data (2013-2015) was used.

The 99th percentile SO₂ concentrations by season (winter, spring, summer and fall) for each hour of the day were calculated to determine the temporally varying seasonal SO₂ background, which were directly input into the model and were part of the final modeled results.

Temporally varying seasonal 1-hour SO₂ background concentrations were taken from the Green Valley monitor (AQS #18-043-1004) located in Floyd County for 2013 - 2015. The hourly seasonal SO₂ values used for representative background concentrations for the area surrounding Duke - Gallagher are listed below in Table 13.3.

Table 13.3 – Duke – Gallagher 99th Percentile Temporally Varying Seasonal SO₂ Background Values (ppb)

| | Hr 1 | Hr 2 | Hr 3 | Hr 4 | Hr 5 | Hr 6 | Hr 7 | Hr 8 |
|--------|------|------|------|------|------|------|------|------|
| Winter | 7.27 | 6.90 | 6.40 | 5.80 | 5.82 | 6.69 | 4.36 | 7.85 |
| Spring | 8.01 | 7.38 | 4.23 | 7.32 | 4.86 | 3.90 | 4.28 | 6.25 |
| Summer | 5.60 | 3.46 | 4.10 | 3.47 | 2.57 | 1.89 | 2.30 | 3.70 |
| Fall | 3.70 | 3.76 | 4.23 | 4.06 | 3.13 | 3.30 | 6.33 | 7.51 |

| | Hr 9 | Hr 10 | Hr 11 | Hr 12 | Hr 13 | Hr 14 | Hr 15 | Hr 16 |
|--------|------|-------|-------|-------|-------|-------|-------|-------|
| Winter | 7.24 | 9.10 | 8.98 | 10.66 | 9.42 | 6.60 | 9.96 | 9.70 |
| Spring | 8.39 | 8.87 | 9.50 | 16.88 | 13.04 | 15.89 | 9.10 | 14.09 |
| Summer | 7.70 | 8.10 | 13.52 | 13.08 | 13.15 | 8.94 | 8.57 | 7.78 |
| Fall | 6.96 | 9.52 | 9.46 | 8.82 | 8.87 | 9.06 | 13.28 | 8.62 |

| | Hr 17 | Hr 18 | Hr 19 | Hr 20 | Hr 21 | Hr 22 | Hr 23 | Hr 24 |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|
| Winter | 10.21 | 9.54 | 8.78 | 8.45 | 7.77 | 8.32 | 7.92 | 6.43 |
| Spring | 15.33 | 9.21 | 9.63 | 9.94 | 8.06 | 7.24 | 7.70 | 8.15 |
| Summer | 6.22 | 8.08 | 6.56 | 4.87 | 3.73 | 3.47 | 4.16 | 3.46 |
| Fall | 11.71 | 6.29 | 6.93 | 6.42 | 5.47 | 3.60 | 3.53 | 5.31 |

13.9 SO₂ Emissions Included in the Modeling Analysis

13.9.1 DRR Source: Duke - Gallagher Emissions

Duke - Gallagher has two coal-fired units, Units 2 and 4 that have continuous emission monitoring (CEM) data for SO₂. This hourly CEM data from both units was formatted and used in the 1-hour SO₂ AERMOD model run.

13.9.2 Inventoried SO₂ Sources Included in the Modeling

SO₂ sources from the surrounding area were evaluated to determine if their SO₂ emissions had a potential impact on the air quality surrounding the DRR source, beyond what is captured through background monitoring data. The average actual emissions from 2013-2015 were input for ESSROC and Louisville Medical Center Steam Plant. Louisville Gas & Electric facilities at Cane Run and Mill Creek have reduced their SO₂ emissions with federal regulatory measures including the Mercury and Air Toxics rule, Cross State Air Pollution rule and several other federal rule-makings. SO₂ emission reductions will be achieved through conversion of the coal-fired electric generating units to a natural gas combined cycle unit for Cane Run and additional SO₂ flue-gas desulfurization (FGD) controls and upgrades at the Mill Creek facility. Permitted limits were modeled for each of the Louisville Gas and Electric sources as the emission reductions are federally enforceable and permanent. The following list of sources, found below in Table 13.4, were included in the AERMOD run to determine overall air quality characteristics.

Table 13.4 – Duke – Gallagher Modeling Source Inventory

| Source | Source ID | Location | 2013-2015 SO ₂ Emissions (tpy) |
|---------------------------|--------------|----------------------|---|
| ESSROC Cement Corporation | 18-019-00008 | Clark County, IN | 416 |
| LG & E – Cane Run | 21-111-00126 | Jefferson County, KY | 21 |
| LG & E – Mill Creek | 21-111-00127 | Jefferson County, KY | 13,485 |
| Louisville Medical Center | 21-111-00148 | Jefferson County, KY | 415 |

13.10 Modeling Results

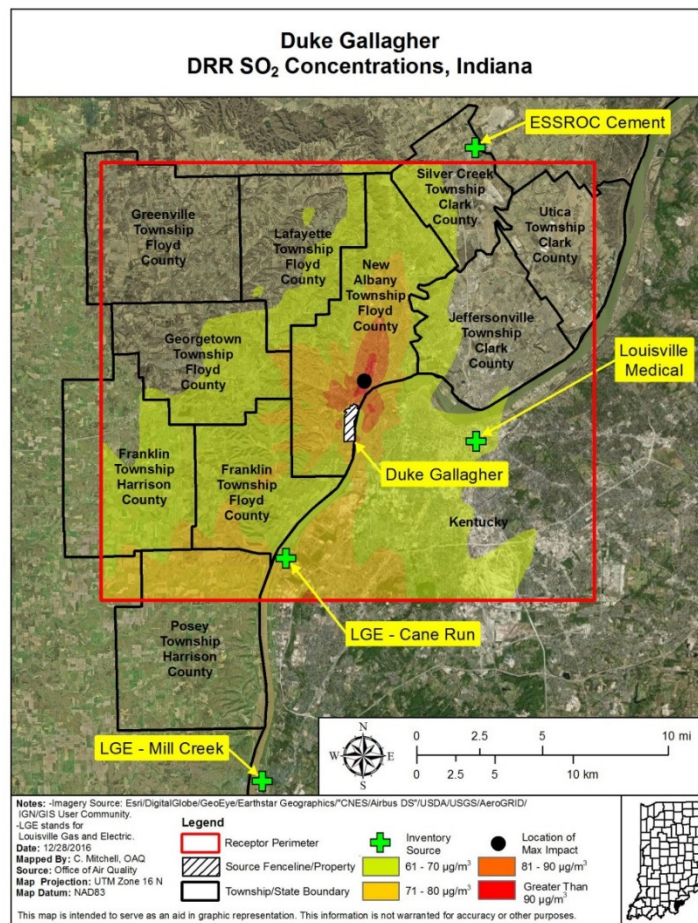
The 99th percentile of the 1-hour daily maximum modeled concentrations represents the fourth high of the 1-hour daily maximum SO₂ modeled concentrations and were averaged across three years to compare resulting concentrations to the 1-hour SO₂ NAAQS of 75 ppb (196.2 µg/m³). Modeled concentrations include representative temporally varying seasonal 1-hour SO₂ background values to determine the overall impact. The resulting concentrations were compared to the 1-hour SO₂ standard to indicate whether a modeled violation of the SO₂ NAAQS occurred. All concentrations fell below the 1-hour SO₂ NAAQS and were determined to attain the standard and the area surrounding Gallagher is recommended as attainment. The maximum predicted 99th percentile daily 1-hour SO₂ concentration is shown in Table 13.5. The overall maximum concentration was 99.5 µg/m³, occurring at UTM coordinates 602300.0 East, 4238000.0 North.

Table 13.5 - Duke – Gallagher Modeling Results

| Emission Scenario | Maximum Modeled Concentration Including Seasonal Hourly Background ($\mu\text{g}/\text{m}^3$) | 1-Hour SO_2 NAAQS ($\mu\text{g}/\text{m}^3$) | Facility Models Attainment |
|-------------------|---|---|----------------------------|
| Gallagher | 99.5 | 196.2 | Yes |

The concentration isopleths showing the maximum predicted 99th percentile daily 1-hour SO_2 concentration gradients can be found in Figure 13.5.

Figure 13.5 – Duke - Gallagher Modeling Results



14.0 NIPSCO – R.M. Schahfer Generating Station (Source ID 18-073-00008)

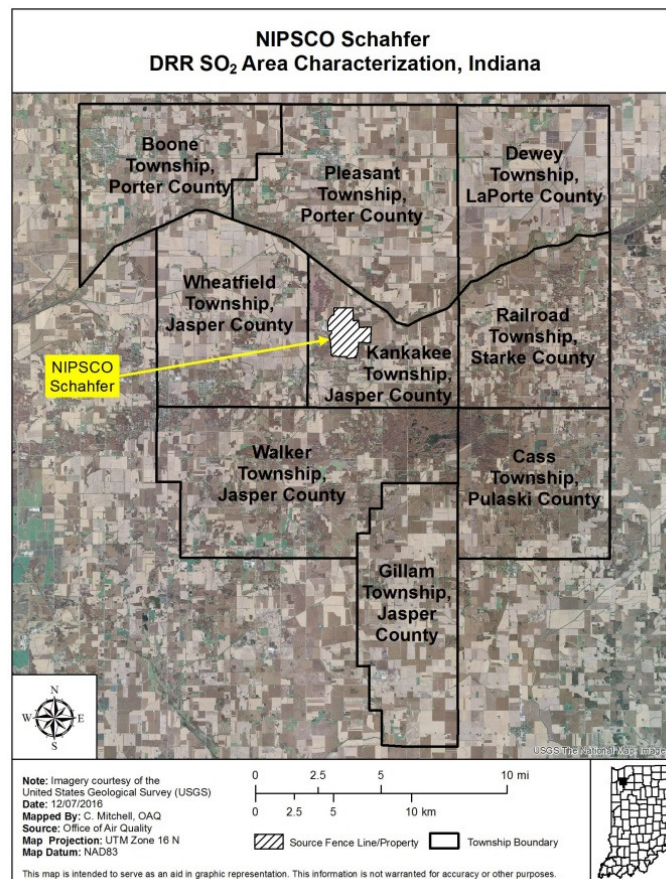
14.1 Source Description

The Northern Indiana Public Service Company (NIPSCO) - R.M. Schahfer Generating Station (NIPSCO - Schahfer) is a stationary electric utility generating station consisting of four units that have a capacity to generate 1,943 megawatts (MW) of electricity combined. NIPSCO - Schahfer has four coal-fired boilers; one boiler is rated at 4,650 MMBtu/hr, one boiler is rated at 5,100 MMBtu/hr, and two boilers are rated at 3,967 MMBtu/hr each. The plant is operated by NiSource.

14.2 Characterization of Modeled Area

The NIPSCO - Schahfer is located at 2723 East 1500 North, Wheatfield, in Kankakee Township, Jasper County, Indiana; approximately 5 miles west of State Road 421. A map of the area surrounding the NIPSCO - Schahfer facility is shown below in Figure 14.1.

Figure 14.1 - NIPSCO - Schahfer and Surrounding Area



14.3 Background Concentrations

The nearest 1-hour SO₂ monitored concentrations were taken from the Wheatfield – Jasper County monitor (AQS #18-073-0002). The 99th percentile values from 2012 through 2014 and the 3-year design value are listed below in Table 14.1.

Table 14.1 – NIPSCO – Schahfer 99th Percentile 1-hour SO₂ Background Values and 3-year Design Value (ppb)

| Monitoring Site | 2012 | 2013 | 2014 | 2012-2014 |
|----------------------------|------|------|------|-----------|
| Wheatfield – Jasper County | 33 | 40 | 18 | 30 |

14.4 Modeling Methodology

The NIPSCO - Schahfer DRR modeling methodology resembles modeling used to evaluate New Source Review (NSR) and Prevention of Significant Deterioration (PSD) sources. However, Indiana has relied on U.S. EPA guidance “SO₂ NAAQS Designations Modeling Technical Assistance Document” in order to conduct an appropriate air dispersion modeling analysis for NIPSCO - Schahfer to support 1-hour SO₂ designation recommendations.

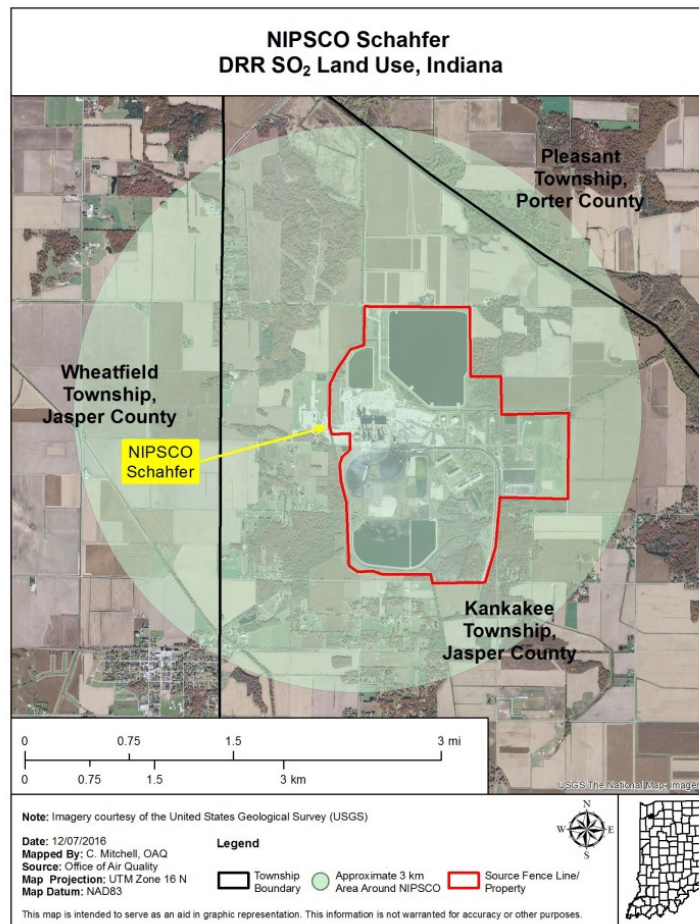
14.4.1 Model Selection

In accordance with Appendix A of Appendix W to 40 Code of Federal Regulations (CFR) Part 51, Indiana used the American Meteorological Society/Environmental Protection Agency Regulatory Model (AERMOD) version 15181. BPIPPRIME was used to account for any building downwash concerns.

14.4.2 Model Options

All regulatory default options within AERMOD were used to determine the air quality characteristics surrounding NIPSCO - Schahfer. The area is considered primarily rural, based on the Auer’s Classification Land Use methodology with a vast majority of the land use types classified as agricultural rural (A2), undeveloped rural (A4), water surfaces (A5) and estate residential (R4). Therefore, a rural classification was used, as provided for in the Guideline on Air Quality Models, Section 7.2.3 (EPA, 2005b). No variation of the population selection was necessary. Figure 14.2 shows the 3-kilometer radius area surrounding NIPSCO - Schahfer that was analyzed to determine the land use classification.

Figure 14.2 – NIPSCO – Schahfer 3-km Radius to Determine Auer Land Use



14.4.3 AERMAP

The AERMOD terrain preprocessor mapping program, AERMAP, was used to determine all the terrain elevation heights for each receptor, building, and source locations using the Universal Transverse Mercator (UTM) coordinate system. The most recent AERMAP version 11103 assigned the elevations from the National Elevation Dataset (NED) using the North American Datum (NAD) 1983 as recommended in the, “40 CFR Part 51, Revision to the Guideline on Air Quality Models” Appendix W and later revised in the “AERMOD Implementation Guide.”

14.5 Meteorological Data

14.5.1 AERMET

As stated in 40 CFR Part 51, Appendix W, section 8.3.1.2 and the SO₂ NAAQS Designations Modeling TAD, Indiana used 2013-2015 National Weather Service (NWS) surface and upper air meteorological data processed with the latest version of the AERMOD meteorological data

preprocessor program AERMET (version 15181). Table 14.2 below lists surface and upper air meteorological stations used to conduct modeling.

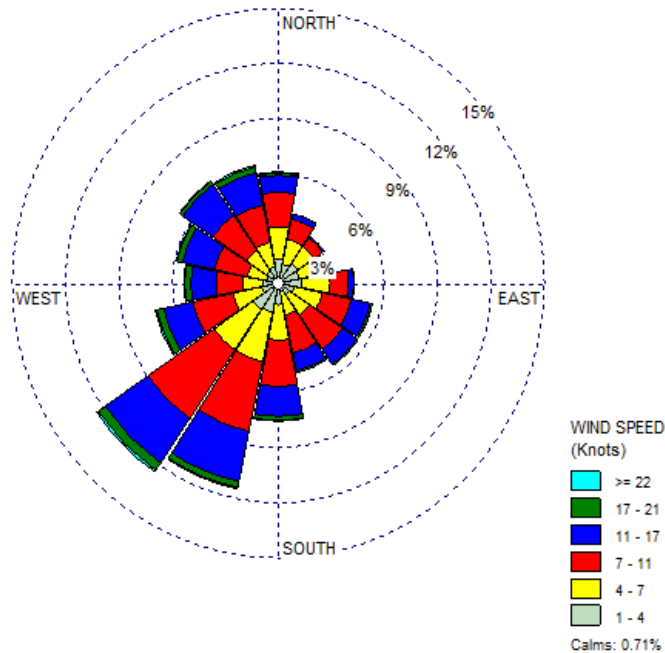
Table 14.2 – NIPSCO – Schahfer NWS Stations/Onsite Meteorological Stations

| Facility | Surface Meteorology | Upper Air Meteorology |
|-------------------|---------------------|-----------------------|
| NIPSCO - Schahfer | South Bend, IN NWS | Lincoln, IL NWS |

14.5.2 Wind Rose

The South Bend National Weather Service (NWS) surface meteorological data and the Lincoln, Illinois upper air meteorological data taken from 2012 through 2014 were used to determine the meteorological conditions for the area surrounding NIPSCO - Schahfer in AERMOD. The South Bend NWS wind rose for the 3-year modeled period 2012-2014 is shown as Figure 14.3 below. The South Bend NWS wind rose depicts the predominant wind direction as from the southwest for the 3-year modeled period 2012-2014.

Figure 14.3 - South Bend 3-year Cumulative Wind Rose (2012 – 2014)



14.5.3 AERMINUTE/AERSURFACE

The 1-minute wind speeds and wind directions, taken from the Automated Surface Observing System (ASOS) NWS stations and onsite meteorological stations, were processed with the U.S. EPA 1-minute data processor program AERMINUTE version 15272.

The U.S. EPA program AERSURFACE version 13016 was used to determine the surface characteristics; albedo, Bowen ratio, and surface roughness for the South Bend, Indiana NWS meteorological tower location. Surface characteristics were determined at the NWS location for each of 12 wind direction sectors with a recommended default radius of one kilometer.

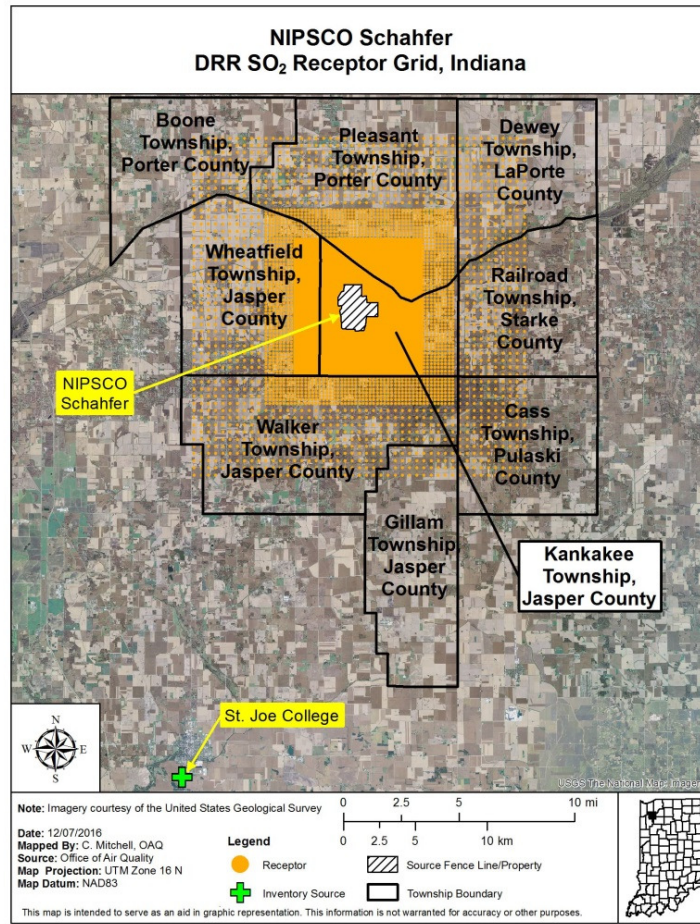
The albedo and the Bowen ratio surface characteristics were adjusted during the three winter months of January, February, and December in accordance with the U.S. EPA Region V document, “Regional Meteorological Data Processing Protocol,” dated May 6, 2011. Additionally, a dry or wet Bowen ratio value was used during months when soil moisture conditions were abnormally dry or wet; otherwise the Bowen ratio value for average soil moisture conditions was used. The surface roughness value for snow cover was used if more than half of the month had days with at least one inch of snow on the ground. Otherwise, the no snow cover surface roughness value was used.

14.6 Receptor Grid and Modeling Domain

The receptor grid and modeling domain was based on guidance provided in the memorandum “Updated Guidance for Area Designations for the 2010 Primary Sulfur Dioxide National Ambient Air Quality Standards”, dated March 20, 2015 and the SO₂ NAAQS Designations Modeling TAD. Indiana used a multi-nested rectangular receptor grid with appropriate spacing of receptors based on the distance from the modeled emission points to detect significant concentration gradients. The modeling domain extended out to include all sources and the appropriate distances to model maximum 1-hour SO₂ impacts to determine attainment designations for the area. Indiana used the following multi-nested rectangular receptor grid, which are listed below and depicted in Figure 14.4:

- Receptor spacing at the fence line for the DRR facility was placed every 50 meters.
- Receptor spacing at 100 meters was placed out to a distance of 3,000 meters (3 kilometers) beyond the DRR facility.
- Receptor spacing at 250 meters was placed out to a distance of 5,000 meters (5 kilometers) beyond the DRR facility.
- Receptor spacing at 500 meters was placed out to a distance of 10,000 meters (10 kilometers) beyond the DRR facility.

Figure 14.4 – NISPCO - Schahfer Receptor Grid



NISPCO - Schahfer's property line is very extensive. Their property is nearly two miles long and is approximately 1.6 miles wide. NISPCO - Schahfer is largely fenced and has regular security patrols to keep unauthorized people off the property. Since this is the case, receptors were placed along the property lines.

14.7 Stack Heights

The use of actual stack heights rather than relying on Good Engineering Practice (GEP) stack heights when modeling actual emissions was utilized in the analysis per the SO₂ NAAQS Designations Modeling TAD.

14.8 Temporally Varying Seasonal 1-Hour SO₂ Background

Temporally varying seasonal SO₂ background concentrations were developed in accordance with the recommended U.S. EPA guidance for establishment of such background concentrations in

Section 8.2 of 40 CFR Part 51, Appendix W and considered appropriate and representative of the area. The latest three years of SO₂ air quality monitoring data (2012-2014) was used.

The 99th percentile SO₂ concentrations by season (winter, spring, summer and fall) for each hour of the day were calculated to determine the temporally varying seasonal SO₂ background, which were directly input into the model and were part of the final modeled results.

Temporally varying seasonal 1-hour SO₂ background concentrations were taken from the Wheatfield monitor for 2012 - 2014. The hourly seasonal SO₂ values used for representative background concentrations for the area surrounding NIPSCO - Schahfer are listed below in Table 14.3.

Table 14.3 – NIPSCO – Schahfer 99th Percentile Temporally Varying Seasonal SO₂ Background Values (ppb)

| | Hr 1 | Hr 2 | Hr 3 | Hr 4 | Hr 5 | Hr 6 | Hr 7 | Hr 8 |
|--------|------|------|------|------|------|------|------|------|
| Winter | 4.75 | 5.00 | 4.71 | 4.68 | 4.00 | 5.00 | 5.40 | 4.00 |
| Spring | 5.54 | 4.57 | 5.60 | 6.16 | 4.55 | 5.00 | 4.47 | 7.00 |
| Summer | 2.44 | 3.43 | 3.00 | 3.45 | 3.00 | 3.00 | 3.49 | 6.53 |
| Fall | 5.26 | 4.00 | 4.00 | 4.00 | 9.00 | 7.41 | 5.29 | 5.49 |

| | Hr 9 | Hr 10 | Hr 11 | Hr 12 | Hr 13 | Hr 14 | Hr 15 | Hr 16 |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|
| Winter | 5.00 | 7.00 | 7.00 | 7.00 | 7.64 | 7.00 | 7.00 | 7.00 |
| Spring | 9.52 | 8.53 | 8.06 | 8.00 | 7.57 | 7.00 | 7.98 | 6.71 |
| Summer | 10.16 | 8.63 | 8.00 | 8.86 | 9.00 | 9.28 | 7.66 | 7.00 |
| Fall | 9.00 | 7.00 | 7.69 | 7.64 | 5.00 | 6.00 | 6.62 | 5.62 |

| | Hr 17 | Hr 18 | Hr 19 | Hr 20 | Hr 21 | Hr 22 | Hr 23 | Hr 24 |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|
| Winter | 7.00 | 7.00 | 6.32 | 5.00 | 5.68 | 6.66 | 6.00 | 6.00 |
| Spring | 5.00 | 4.66 | 7.18 | 7.60 | 6.57 | 5.00 | 4.57 | 4.55 |
| Summer | 4.56 | 4.54 | 6.00 | 7.44 | 5.00 | 3.00 | 3.40 | 2.52 |
| Fall | 5.00 | 6.18 | 6.02 | 5.48 | 4.00 | 5.00 | 4.00 | 7.99 |

14.9 SO₂ Emissions Included in the Modeling Analysis

14.9.1 DRR Source: NIPSCO - Schahfer Generating Station Emissions

NIPSCO - Schahfer has four units, Units BLR4, BLR15, BLR17, and BLR18 that have continuous emission monitoring (CEM) data for SO₂. This hourly CEM data from the four units were formatted and used in the 1-hour SO₂ AERMOD model run. Total annual emissions from NIPSCO – Schahfer from 2015 are approximately one-eighth of the emissions from 2012

through 2014 emissions. Therefore, modeling the 2012-2014 emissions is conservative in nature and will be used for this analysis.

14.9.2 Inventoried SO₂ Sources Included in the Modeling

SO₂ sources from the surrounding area were evaluated to determine if their SO₂ emissions had a potential impact on the air quality surrounding the DRR source, beyond what is captured through background monitoring data. Saint Joseph’s College was found to be within 30 kilometers of NIPSCO - Schahfer. Saint Joseph’s College is no longer a Title V source. The college’s last emission report was in 2012. Those emissions were used in the modeling analysis for NIPSCO - Schahfer as listed in Table 14.4.

Table 14.4 – NIPSCO – Schahfer Modeling Source Inventory

| Source | Source ID | Location | 2012 SO ₂ Emissions (tpy) |
|--------------------|-----------|---------------|--------------------------------------|
| St. Joseph College | 073-00001 | Jasper County | 120.5 |

14.10 Modeling Results

The 99th percentile of the 1-hour daily maximum modeled concentrations represents the fourth high of the 1-hour daily maximum SO₂ modeled concentrations and were averaged across three years to compare resulting concentrations to the 1-hour SO₂ NAAQS of 75 ppb (196.2 µg/m³). Modeled concentrations include representative temporally varying seasonal 1-hour SO₂ background values to determine the overall impact. The resulting concentrations were compared to the 1-hour SO₂ standard to indicate whether a modeled violation of the SO₂ NAAQS occurred. All concentrations fell below the 1-hour SO₂ NAAQS and were determined to attain the standard and the area surrounding NIPSCO - Schahfer is recommended as attainment.

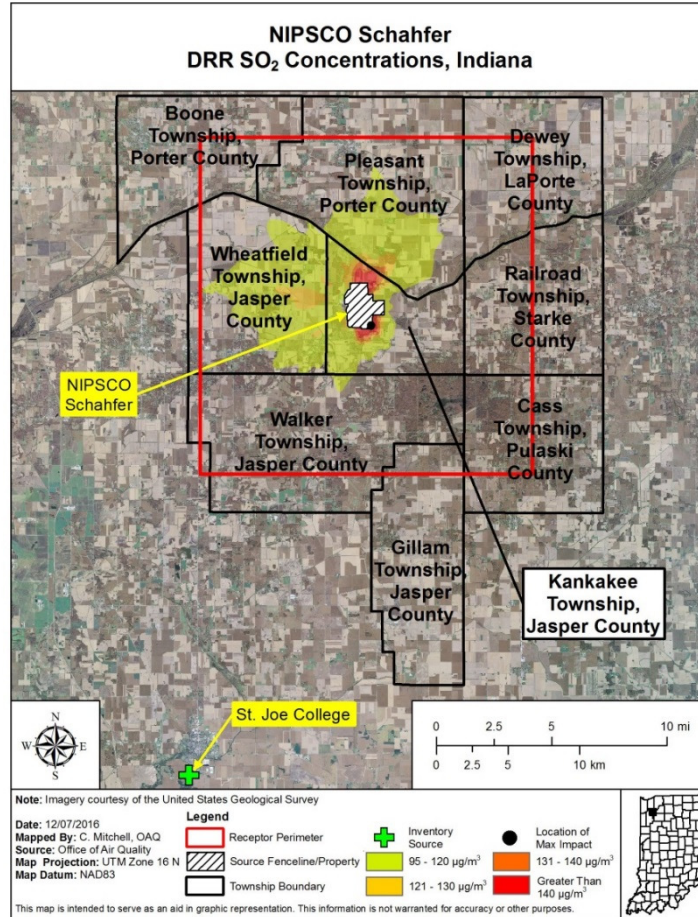
The maximum predicted 99th percentile daily 1-hour SO₂ concentration is shown in Table 14.5. The overall maximum concentration was 162.7 µg/m³, occurring at UTM coordinates 499354.6 East, 4561322.6 North.

Table 14.5 – NIPSCO – Schahfer Modeling Results

| Emission Scenarios | Maximum Modeled Concentration Including Seasonal Hourly Background (µg/m ³) | 1-Hour SO ₂ NAAQS (µg/m ³) | Facility Models Attainment |
|--------------------|---|---|----------------------------|
| NIPSCO - Schahfer | 162.7 | 196.2 | Yes |

The concentration isopleths showing the maximum predicted 99th percentile daily 1-hour SO₂ concentration gradients can be found in Figure 14.5. The modeling showed attainment of the 1-hour SO₂ standard.

Figure 14.5 – NIPSCO Schahfer Modeling Results



15.0 Hoosier Energy - Merom (Source ID 153-00005)

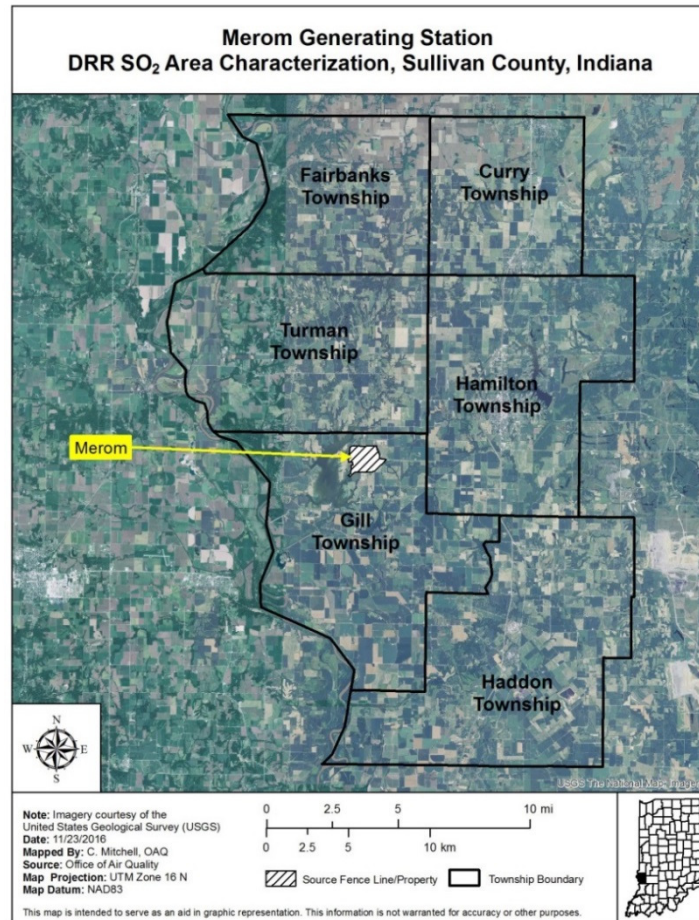
15.1 Source Description

Hoosier Energy - Merom Generating Station (Hoosier Energy - Merom) is a 1070 MW coal fired power plant located in Sullivan County in Southwest Indiana. Hoosier Energy - Merom operates two coal-fired boilers each rated at 5,088 mmBtu/hr. SO₂ emission controls at the facility include a flue gas desulfurization system. Hoosier Energy - Merom was identified as a Data Requirements Rule (DRR) source based on their actual 2014 SO₂ emissions of 3,318 tons exceeding the DRR threshold of 2,000 tons of SO₂.

15.2 Characterization of Modeled Area

Hoosier Energy - Merom is located at 5500 W Old 54, Sullivan, Indiana, approximately 5 miles east of the Wabash River in Gill Township, Sullivan County, Indiana. A map of the area is shown below in Figure 15.1.

Figure 15.1 – Hoosier Energy - Merom and Surrounding Area



15.3 Background Concentrations

The nearest 1-hour SO₂ monitored concentrations were taken from the Terre Haute – Lafayette Road monitor (AQS #18-167-0018). The 99th percentile values from 2013 through 2015 and the 3-year design value are listed below in Table 15.1. The area surrounding the Lafayette Road monitor has been addressed through revisions to the 1-hour SO₂ Nonattainment Area State Implementation Plan.

Table 15.1 – Hoosier Energy – Merom 99th Percentile 1-hour SO₂ Background Values and 3-year Design Value (ppb)

| Monitoring Site | 2013 | 2014 | 2015 | 2013-2015 |
|----------------------------|------|------|------|-----------|
| Terre Haute – Lafayette Rd | 79.1 | 85.0 | 71.0 | 78 |

15.4 Modeling Methodology

The Hoosier Energy - Merom DRR modeling methodology resembles modeling used to evaluate New Source Review (NSR) and Prevention of Significant Deterioration (PSD) sources.

However, Indiana has relied on U.S. EPA guidance “SO₂ NAAQS Designations Modeling Technical Assistance Document” in order to conduct an appropriate air dispersion modeling analysis for Hoosier Energy -Merom to support 1-hour SO₂ designation recommendations.

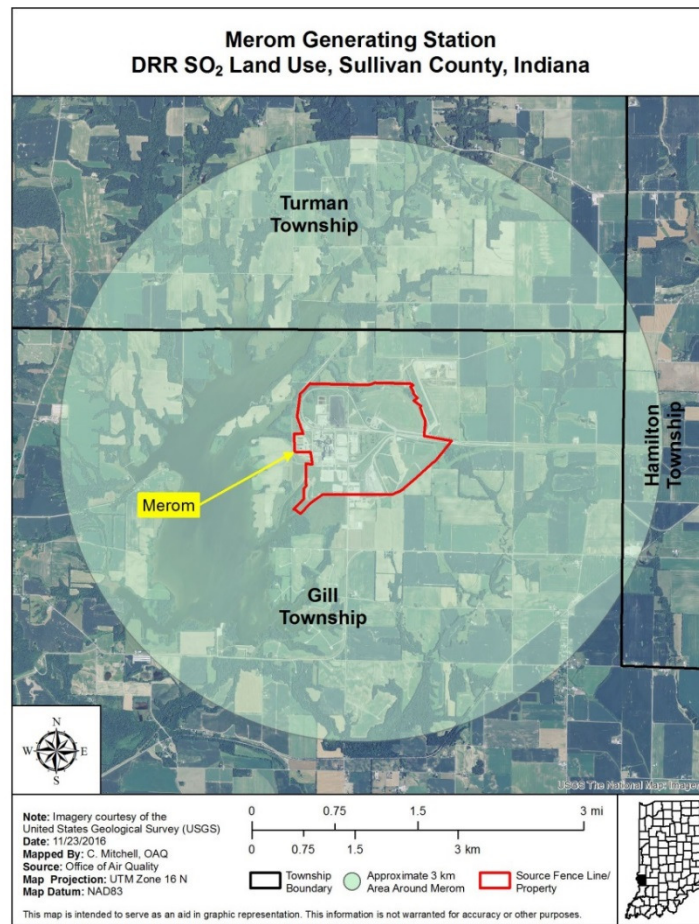
15.4.1 Model Selection

In accordance with Appendix A of Appendix W to 40 Code of Federal Regulations (CFR) Part 51, Indiana used the American Meteorological Society/Environmental Protection Agency Regulatory Model (AERMOD) version 15181. BPIPPRIME was used to account for any building downwash concerns.

15.4.2 Model Options

All regulatory default options within AERMOD were used to determine the air quality characteristics surrounding the Hoosier Energy - Merom. The area is considered primarily rural, based on the Auer’s Classification Land Use methodology with a vast majority of the land use types classified as agricultural rural (A2) and water surfaces (A5). Therefore, a rural classification was used, as provided for in the Guideline on Air Quality Models, Section 7.2.3 (EPA, 2005b). No variation of the population selection was necessary. Figure 15.2 shows the 3-kilometer radius area surrounding Hoosier Energy - Merom that was analyzed to determine the land use classification.

Figure 15.2 – Hoosier Energy – Merom 3-km Radius to Determine Auer Land Use



15.4.3 AERMAP

The AERMOD terrain preprocessor mapping program, AERMAP, was used to determine all the terrain elevation heights for each receptor, building, and source locations using the Universal Transverse Mercator (UTM) coordinate system. The most recent AERMAP version 11103 assigned the elevations from the National Elevation Dataset (NED) using the North American Datum (NAD) 1983 as recommended in the, “40 CFR Part 51, Revision to the Guideline on Air Quality Models” Appendix W and later revised in the “AERMOD Implementation Guide.”

15.5 Meteorological Data

15.5.1 AERMET

As stated in 40 CFR Part 51, Appendix W, section 8.3.1.2 and the SO₂ NAAQS Designations Modeling TAD, Indiana used 2013-2015 National Weather Service (NWS) surface and upper air meteorological data processed with the latest version of the AERMOD meteorological data

preprocessor program AERMET (version 15181). Table 15.2 below lists surface and upper air meteorological stations used to conduct modeling.

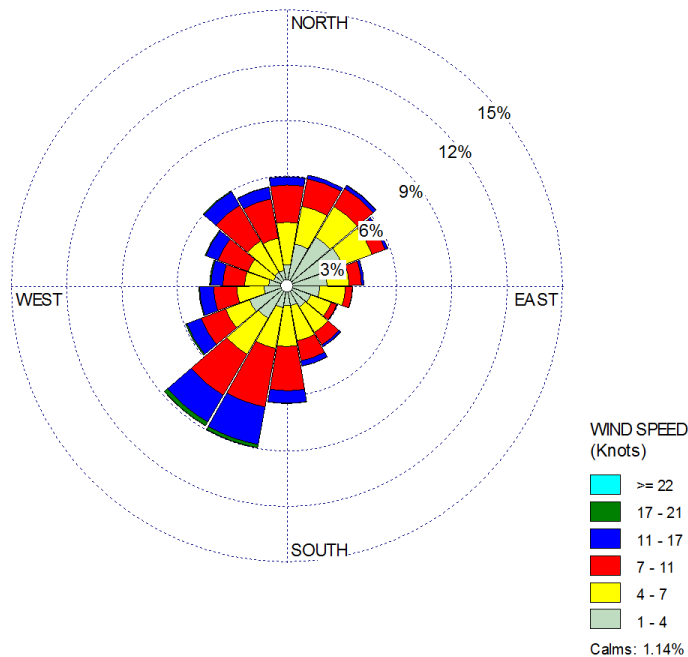
Table 15.2 – Hoosier Energy – Merom NWS Stations/Onsite Meteorological Stations

| Facility | Surface Meteorology | Upper Air Meteorology |
|------------------------|---------------------|-----------------------|
| Hoosier Energy – Merom | Evansville, IN NWS | Lincoln, IL NWS |

15.5.2 Wind Rose

The Evansville, Indiana National Weather Service (NWS) surface meteorological data and the Lincoln, Illinois upper air meteorological data taken from 2013 through 2015 were used to determine the meteorological conditions for the area surrounding Hoosier Energy - Merom in AERMOD. The Evansville NWS wind rose for the 3-year modeled period 2013-2015 is shown as Figure 15.3 below. The Evansville NWS wind rose depicts the predominant wind direction as from the southwest for the 3-year modeled period 2013-2015.

Figure 15.3 - Evansville 3-year Cumulative Wind Rose (2013 – 2015)



15.5.3 AERMINUTE/AERSURFACE

The 1-minute wind speeds and wind directions, taken from the Automated Surface Observing System (ASOS) NWS stations and onsite meteorological stations, were processed with the U.S. EPA 1-minute data processor program AERMINUTE version 15272.

The U.S. EPA program AERSURFACE version 13016 was used to determine the surface characteristics; albedo, Bowen ratio, and surface roughness for the Evansville, Indiana NWS meteorological tower location. Surface characteristics were determined at the NWS location for each of 12 wind direction sectors with a recommended default radius of one kilometer.

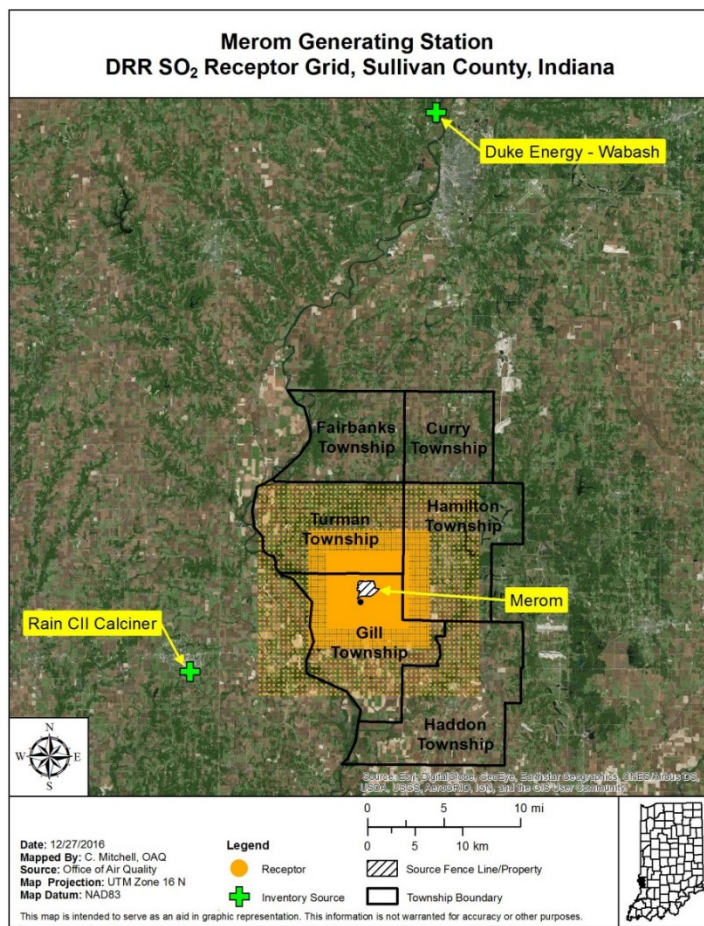
The albedo and the Bowen ratio surface characteristics were adjusted during the three winter months of January, February, and December in accordance with the U.S. EPA Region V document, “Regional Meteorological Data Processing Protocol,” dated May 6, 2011. Additionally, a dry or wet Bowen ratio value was used during months when soil moisture conditions were abnormally dry or wet; otherwise the Bowen ratio value for average soil moisture conditions was used. The surface roughness value for snow cover was used if more than half of the month had days with at least one inch of snow on the ground. Otherwise, the no snow cover surface roughness value was used.

15.6 Receptor Grid and Modeling Domain

The receptor grid and modeling domain was based on guidance provided in the memorandum “Updated Guidance for Area Designations for the 2010 Primary Sulfur Dioxide National Ambient Air Quality Standards”, dated March 20, 2015 and the SO₂ NAAQS Designations Modeling TAD. Indiana used a multi-nested rectangular receptor grid with appropriate spacing of receptors based on the distance from the modeled emission points to detect significant concentration gradients. The modeling domain extended out to include all sources and the appropriate distances to model maximum 1-hour SO₂ impacts to determine attainment designations for the area. Indiana used the following multi-nested rectangular receptor grid which are listed below and depicted in Figure 15.4:

- Receptor spacing at the fence line for each facility was placed every 50 meters.
- Receptor spacing at 100 meters was placed out to a distance of 3,000 meters (3 kilometers) beyond the DRR facility.
- Receptor spacing at 250 meters was placed out to a distance of 5,000 meters (5 kilometers) beyond the DRR facility.
- Receptor spacing at 500 meters was placed out to a distance of 10,000 meters (10 kilometers) beyond the DRR facility.

Figure 15.4 – Hoosier Energy – Merom Receptor Grid



Hoosier Energy - Merom has a fence surrounding the property with security gates restricting public access to all Merom property. Natural barriers immediately surround the property with a reservoir west of the facility and a landfill to the north. Receptors were therefore placed along the property boundary where public access is not restricted.

15.7 Stack Heights

The use of actual stack heights rather than relying on Good Engineering Practice (GEP) stack heights when modeling actual emissions was utilized in the analysis per the SO₂ NAAQS Designations Modeling TAD.

15.8 Temporally Varying Seasonal 1-Hour SO₂ Background

Temporally varying seasonal SO₂ background concentrations were developed in accordance with the recommended U.S. EPA guidance for establishment of such background concentrations in

Section 8.2 of 40 CFR Part 51, Appendix W and considered appropriate and representative of the area. The latest three years of SO₂ air quality monitoring data (2013-2015) was used.

The 99th percentile SO₂ concentrations by season (winter, spring, summer and fall) for each hour of the day were calculated to determine the temporally varying seasonal SO₂ background, which were directly input into the model and were part of the final modeled results.

Temporally varying seasonal 1-hour SO₂ background concentrations were taken from the Terre Haute – Lafayette Road monitor for 2013 - 2015. The hourly seasonal SO₂ values used for representative background concentrations for the area surrounding Hoosier Energy - Merom are listed below in Table 15.3.

Table 15.3 – Hoosier Energy – Merom 99th Percentile Temporally Varying Seasonal SO₂ Background Values (ppb)

| | Hr 1 | Hr 2 | Hr 3 | Hr 4 | Hr 5 | Hr 6 | Hr 7 | Hr 8 |
|--------|------|------|------|------|------|------|------|------|
| Winter | 4.99 | 5.61 | 5.59 | 5.17 | 5.56 | 5.96 | 6.30 | 6.69 |
| Spring | 5.25 | 6.70 | 7.97 | 4.37 | 6.82 | 4.37 | 5.46 | 4.78 |
| Summer | 2.78 | 2.54 | 2.69 | 2.17 | 1.81 | 2.13 | 2.71 | 3.81 |
| Fall | 8.21 | 5.06 | 5.17 | 4.07 | 5.87 | 3.72 | 3.81 | 4.35 |

| | Hr 9 | Hr 10 | Hr 11 | Hr 12 | Hr 13 | Hr 14 | Hr 15 | Hr 16 |
|--------|------|-------|-------|-------|-------|-------|-------|-------|
| Winter | 6.22 | 5.45 | 9.07 | 11.45 | 10.06 | 9.25 | 7.76 | 8.97 |
| Spring | 6.86 | 6.29 | 24.67 | 11.51 | 14.16 | 10.08 | 6.30 | 9.29 |
| Summer | 4.44 | 8.83 | 8.55 | 10.09 | 8.43 | 24.15 | 26.75 | 29.68 |
| Fall | 6.35 | 6.03 | 34.92 | 18.80 | 11.22 | 14.39 | 7.32 | 15.27 |

| | Hr 17 | Hr 18 | Hr 19 | Hr 20 | Hr 21 | Hr 22 | Hr 23 | Hr 24 |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|
| Winter | 10.45 | 16.58 | 8.77 | 8.84 | 7.05 | 6.47 | 8.66 | 6.99 |
| Spring | 8.60 | 16.86 | 5.33 | 4.59 | 8.55 | 4.05 | 5.73 | 6.31 |
| Summer | 12.49 | 6.59 | 5.55 | 3.94 | 6.82 | 4.93 | 4.07 | 2.74 |
| Fall | 5.14 | 5.22 | 5.23 | 5.65 | 9.28 | 7.68 | 9.08 | 8.03 |

15.9 SO₂ Emissions Included in the Modeling Analysis

15.9.1 DRR Source: Hoosier Energy - Merom Emissions

Hoosier Energy - Merom operates two coal-fired units each of which are equipped with Continuous Emission Monitoring (CEM) systems. CEM data from 2013 through 2015 was formatted into an AERMOD ready hourly input file and used in the final modeling.

15.9.2 Inventoried SO₂ Sources Included in the Modeling

SO₂ sources from the surrounding area were evaluated to determine if their SO₂ emissions had a potential impact on the air quality surrounding Hoosier Energy - Merom, beyond what is captured through background monitoring data. The latest available actual emissions were used for inventory sources. Two sources were included in the model in addition to the Hoosier Energy - Merom facility: Rain II Carbon in Illinois and the Duke - Wabash facility in Vigo County, Indiana.

Rain CII Carbon is a green petroleum coke calcining facility that produces aluminum and other raw materials. Rain CII Carbon is located in Crawford County, Illinois, 20 km southwest of Hoosier Energy - Merom and produced 3,132 tpy of SO₂ in 2014. Hourly continuous emission monitoring data from 2013 through 2015 were used in AERMOD for the Rain II facility.

Duke Energy - Wabash was an electric generating facility in located 51 km to the north of Hoosier Energy - Merom in Vigo County, Indiana. The facility retired all of its coal-fired electric generating units (Units 2-6). Units 2-5 were retired on April 16, 2016 and Unit 6 was retired on December 7, 2016. Although this source was outside of the 30 km radius Indiana used to determine background sources, Indiana included this source in the modeling of Hoosier Energy - Merom due to high background concentrations over the 2013-2015 time period. Upwind impacts in the background data from the Wabash facility were adjusted to prevent double counting. Average actual emissions from 2013 through 2015 was used in the modeling and listed in Table 15.4.

Table 15.4 – Hoosier Energy – Merom Modeling Source Inventory

| Source | Source ID | Location | SO ₂ Emissions (tpy) |
|-----------------|-----------|---------------------|---------------------------------|
| Rain CII Carbon | 033025AAJ | Crawford County, IL | 2,750 |
| Duke - Wabash | 167-00021 | Vigo County | 28,154 |

15.10 Modeling Results

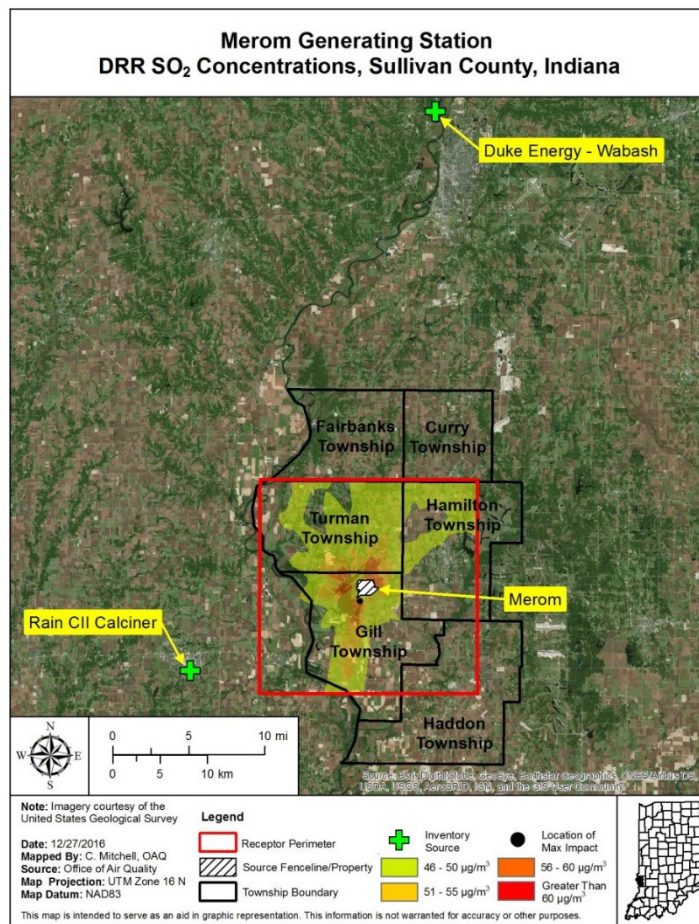
The 99th percentile of the 1-hour daily maximum modeled concentrations represents the fourth high of the 1-hour daily maximum SO₂ modeled concentrations and were averaged across three years to compare resulting concentrations to the 1-hour SO₂ NAAQS of 75 ppb (196.2 µg/m³). Modeled concentrations include representative temporally varying seasonal 1-hour SO₂ background values to determine the overall impact. The resulting concentrations were compared to the 1-hour SO₂ standard to indicate whether a modeled violation of the SO₂ NAAQS occurred. All concentrations fell below the 1-hour SO₂ NAAQS and were determined to attain the standard and the area surrounding Hoosier Energy - Merom is recommended as attainment. The maximum predicted 99th percentile daily 1-hour SO₂ concentration is shown in Table 15.5. The overall maximum concentration was 63.0 µg/m³, occurring at UTM coordinates 455600.0 East, 4323300.0 North.

Table 15.5 – Hoosier Energy – Merom Modeling Results

| Emission Scenarios | Maximum Modeled Concentration Including Seasonal Hourly Background ($\mu\text{g}/\text{m}^3$) | 1-Hour SO_2 NAAQS ($\mu\text{g}/\text{m}^3$) | Facility Models Attainment |
|------------------------|---|---|----------------------------|
| Hoosier Energy – Merom | 63.0 | 196.2 | Yes |

The concentration isopleths showing the maximum predicted 99th percentile daily 1-hour SO_2 concentration gradients can be found in Figure 15.5.

Figure 15.5 – Hoosier Energy - Merom Modeling Results



16.0 - Duke - Cayuga Generating Station (Source ID 18-165-00001)

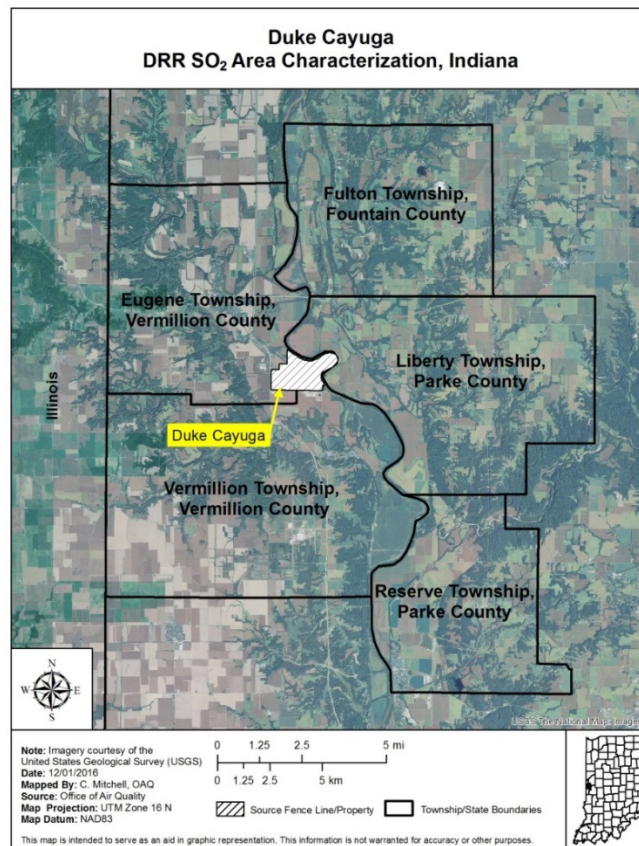
16.1 Source Description

Duke - Cayuga Generating Station (Duke - Cayuga) is an electric generating station owned by Duke Energy Indiana, LLC. Duke - Cayuga is a two-unit generating facility built between 1967 and 1968. Units 1 and 2 are equipped with scrubbers to reduce the stations sulfur dioxide emissions by approximately 95 percent. The two coal-fired boilers are rated at 4,802 MMBtu/hour each and have a generating capacity of 1104 megawatts. Duke - Cayuga was identified as a Data Requirements Rule (DRR) source based on their actual 2014 SO₂ emissions of 3448.4 tons exceeding the DRR threshold of 2,000 tons of SO₂.

16.2 Characterization of Modeled Area

The Duke - Cayuga is located off of State Road 63, Cayuga, Indiana on the banks of the Wabash River, Eugene Township, Vermillion County, Indiana. A map of the area surrounding Duke - Cayuga used for DRR modeling is shown in Figure 16.1.

Figure 16.1 - Duke - Cayuga and Surrounding Area



16.3 Background Concentrations

The nearest 1-hour SO₂ monitored concentrations were taken from the Fountain County monitor (AQS #18-045-0001). The 99th percentile values from 2012 through 2014 and the 3-year design value are listed below in Table 16.1.

Table 16.1 – Duke – Cayuga 99th Percentile 1-hour SO₂ Background Values and 3-year Design Value (ppb)

| Monitoring Site | 2012 | 2013 | 2014 | 2012-2014 |
|-----------------|------|------|------|-----------|
| Fountain County | 30 | 34 | 22 | 29 |

16.4 Modeling Methodology

The Duke - Cayuga DRR modeling methodology resembles modeling used to evaluate New Source Review (NSR) and Prevention of Significant Deterioration (PSD) sources. However, Indiana has relied on U.S. EPA guidance “SO₂ NAAQS Designations Modeling Technical Assistance Document” in order to conduct an appropriate air dispersion modeling analysis for Duke - Cayuga to support 1-hour SO₂ designation recommendations.

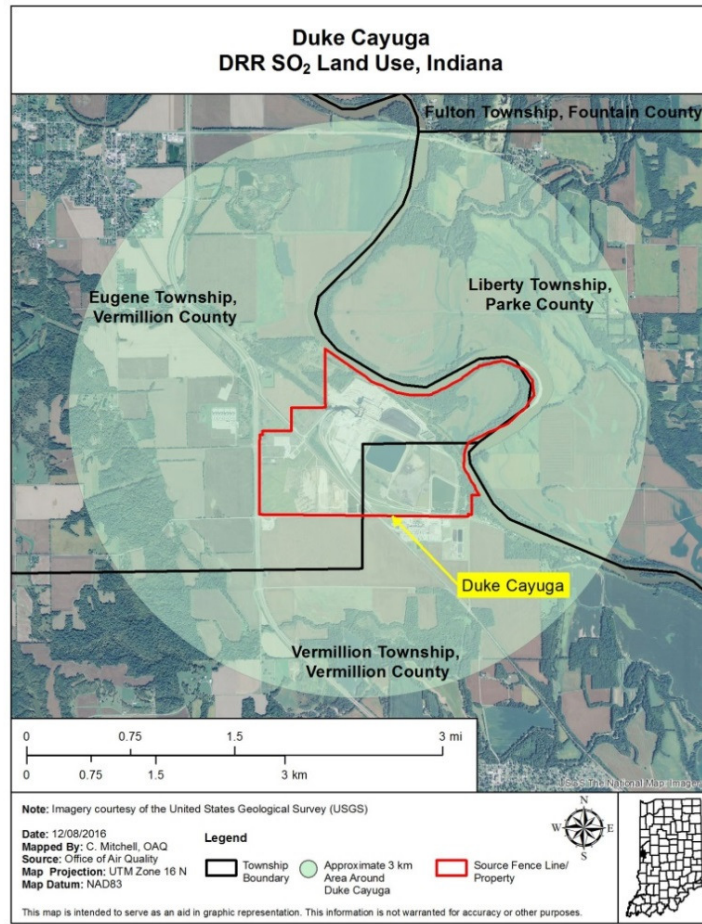
16.4.1 Model Selection

In accordance with Appendix A of Appendix W to 40 Code of Federal Regulations (CFR) Part 51, Indiana used the American Meteorological Society/Environmental Protection Agency Regulatory Model (AERMOD) version 15181. BPIPPRIME was used to account for any building downwash concerns.

16.4.2 Model Options

All regulatory default options within AERMOD were used to determine the air quality characteristics surrounding Duke. The area is considered primarily rural, based on the Auer’s Classification Land Use methodology with a vast majority of the land use types classified as agricultural rural (A2), undeveloped rural (A4) and water surfaces (A5). Therefore, a rural classification was used, as provided for in the Guideline on Air Quality Models, Section 7.2.3 (EPA, 2005b). No variation of the population selection was necessary. Figure 16.2 shows the 3-kilometer radius area surrounding Duke - Cayuga that was analyzed to determine the land use classification.

Figure 16.2 – Duke – Cayuga 3-km Radius to Determine Auer Land Use



16.4.3 AERMAP

The AERMOD terrain preprocessor mapping program, AERMAP, was used to determine all the terrain elevation heights for each receptor, building, and source locations using the Universal Transverse Mercator (UTM) coordinate system. The most recent AERMAP version 11103 assigned the elevations from the National Elevation Dataset (NED) using the North American Datum (NAD) 1983 as recommended in the, “40 CFR Part 51, Revision to the Guideline on Air Quality Models” Appendix W and later revised in the “AERMOD Implementation Guide.”

16.5 Meteorological Data

16.5.1 AERMET

As stated in 40 CFR Part 51, Appendix W, section 8.3.1.2 and the SO₂ NAAQS Designations Modeling TAD, Indiana used 2013-2015 National Weather Service (NWS) surface and upper air meteorological data processed with the latest version of the AERMOD meteorological data

preprocessor program AERMET (version 15181). Table 16.2 below lists surface and upper air meteorological stations used to conduct modeling

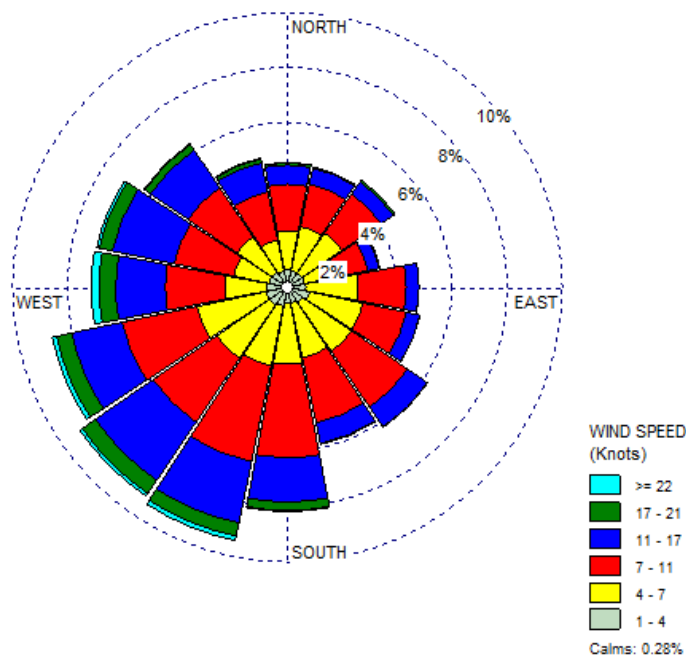
Table 16.2 – Duke – Cayuga NWS Stations/Onsite Meteorological Stations

| Facility | Surface Meteorology | Upper Air Meteorology |
|---------------|----------------------|-----------------------|
| Duke - Cayuga | Indianapolis, IN NWS | Lincoln, IL NWS |

16.5.2 Wind Rose

The Indianapolis, Indiana National Weather Service (NWS) surface meteorological data and the Lincoln, Illinois upper air meteorological data taken from 2012 through 2014 was used to determine the meteorological conditions for the area surrounding Duke - Cayuga in AERMOD. The Indianapolis NWS wind rose for the 3-year modeled period 2012-2014 is shown as Figure 16.3 below. The Indianapolis NWS wind rose depicts the predominant wind direction as from the southwest for the 3-year modeled period 2012-2014.

Figure 16.3 – Indianapolis 3-year Cumulative Wind Rose (2012 – 2014)



16.5.3 AERMINUTE/AERSURFACE

The 1-minute wind speeds and wind directions, taken from the Automated Surface Observing System (ASOS) NWS stations and onsite meteorological stations, were processed with the U.S. EPA 1-minute data processor program AERMINUTE version 15272.

The U.S. EPA program AERSURFACE version 13016 was used to determine the surface characteristics; albedo, Bowen ratio, and surface roughness for the Indianapolis, Indiana NWS meteorological tower location. Surface characteristics were determined at the NWS location for each of 12 wind direction sectors with a recommended default radius of one kilometer.

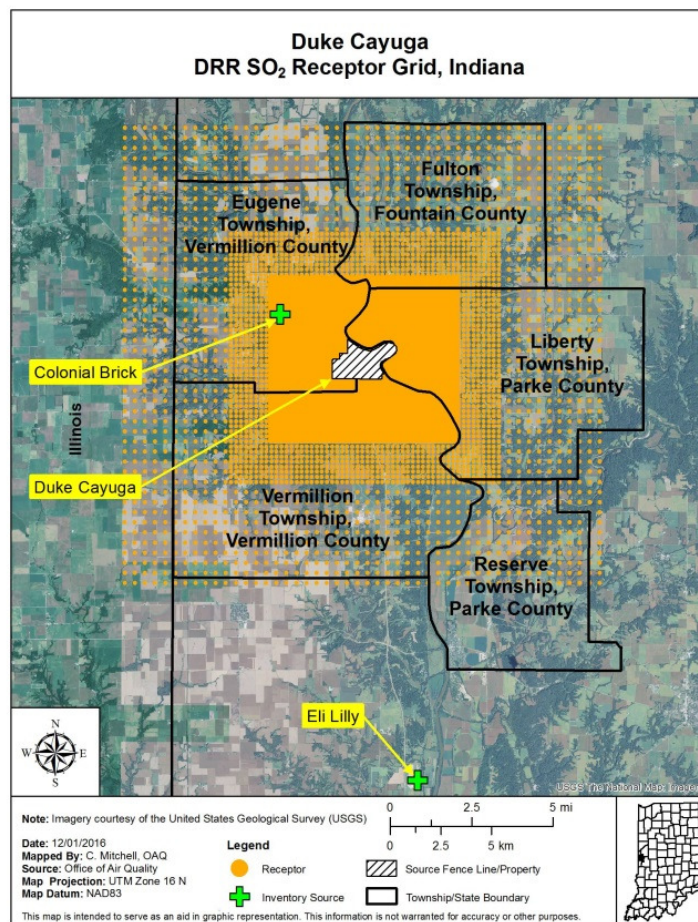
The albedo and the Bowen ratio surface characteristics were adjusted during the three winter months of January, February, and December in accordance with the U.S. EPA Region V document, “Regional Meteorological Data Processing Protocol,” dated May 6, 2011. Additionally, a dry or wet Bowen ratio value was used during months when soil moisture conditions were abnormally dry or wet; otherwise the Bowen ratio value for average soil moisture conditions was used. The surface roughness value for snow cover was used if more than half of the month had days with at least one inch of snow on the ground. Otherwise, the no snow cover surface roughness value was used.

16.6 Receptor Grid and Modeling Domain

The receptor grid and modeling domain was based on guidance provided in the memorandum “Updated Guidance for Area Designations for the 2010 Primary Sulfur Dioxide National Ambient Air Quality Standards”, dated March 20, 2015 and the SO₂ NAAQS Designations Modeling TAD. Indiana used a multi-nested rectangular receptor grid with appropriate spacing of receptors based on the distance from the modeled emission points to detect significant concentration gradients. The modeling domain extended out to include all sources and the appropriate distances to model maximum 1-hour SO₂ impacts to determine attainment designations for the area. Indiana used the following multi-nested rectangular receptor grid which are listed below and depicted in Figure 16.4:

- Receptor spacing at the fence line for each facility was placed every 50 meters.
- Receptor spacing at 100 meters was placed out to a distance of 3,000 meters (3 kilometers) beyond each facility.
- Receptor spacing at 250 meters was placed out to a distance of 5,000 meters (5 kilometers) beyond each facility.
- Receptor spacing at 500 meters was placed out to a distance of 10,000 meters (10 kilometers) beyond each facility.

Figure 16.4 – Duke – Cayuga Receptor Grid



Duke – Cayuga is largely fenced and has regular security patrols to keep unauthorized people off the property. Since this is the case, receptors were placed along the property line. Duke – Cayuga’s concentrations increase extending out from the property line, indicating that maximum modeled concentrations occur further away from the Duke – Cayuga property.

16.7 Stack Heights

The use of actual stack heights rather than relying on Good Engineering Practice (GEP) stack heights when modeling actual emissions was utilized in the analysis per the SO₂ NAAQS Designations Modeling TAD.

16.8 Temporally Varying Seasonal 1-Hour SO₂ Background

Temporally varying seasonal SO₂ background concentrations were developed in accordance with the recommended U.S. EPA guidance for establishment of such background concentrations in

Section 8.2 of 40 CFR Part 51, Appendix W and considered appropriate and representative of the area. The latest three years of SO₂ air quality monitoring data (2012-2014) was used.

The 99th percentile SO₂ concentrations by season (winter, spring, summer and fall) for each hour of the day were calculated to determine the temporally varying seasonal SO₂ background, which were directly input into the model and were part of the final modeled results.

Temporally varying seasonal 1-hour SO₂ background concentrations were taken from the Fountain County monitor for 2012 - 2014. The hourly seasonal SO₂ values used for representative background concentrations for the area surrounding Duke - Cayuga are listed below in Table 16.3.

Table 16.3 – Duke – Cayuga 99th Percentile Temporally Varying Seasonal SO₂ Background Values (ppb)

| | Hr 1 | Hr 2 | Hr 3 | Hr 4 | Hr 5 | Hr 6 | Hr 7 | Hr 8 |
|--------|------|------|------|------|------|------|------|------|
| Winter | 7.76 | 7.52 | 7.00 | 6.49 | 8.00 | 7.00 | 6.00 | 6.51 |
| Spring | 7.69 | 8.00 | 7.55 | 8.00 | 8.00 | 7.53 | 7.54 | 6.56 |
| Summer | 4.50 | 5.00 | 4.00 | 3.48 | 3.42 | 3.00 | 3.00 | 3.00 |
| Fall | 6.58 | 5.62 | 6.00 | 5.00 | 7.56 | 6.57 | 7.18 | 6.55 |

| | Hr 9 | Hr 10 | Hr 11 | Hr 12 | Hr 13 | Hr 14 | Hr 15 | Hr 16 |
|--------|------|-------|-------|-------|-------|-------|-------|-------|
| Winter | 8.55 | 9.60 | 9.98 | 9.00 | 9.00 | 8.26 | 7.65 | 8.30 |
| Spring | 8.63 | 9.00 | 10.00 | 8.00 | 8.63 | 9.00 | 9.00 | 7.64 |
| Summer | 6.22 | 7.24 | 8.62 | 8.00 | 9.00 | 8.00 | 6.57 | 6.60 |
| Fall | 6.60 | 6.63 | 9.00 | 8.67 | 8.00 | 7.62 | 9.00 | 8.68 |

| | Hr 17 | Hr 18 | Hr 19 | Hr 20 | Hr 21 | Hr 22 | Hr 23 | Hr 24 |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|
| Winter | 6.00 | 8.42 | 8.62 | 11.00 | 8.00 | 8.18 | 8.85 | 8.00 |
| Spring | 8.00 | 8.00 | 9.00 | 8.60 | 9.00 | 7.00 | 8.00 | 7.38 |
| Summer | 6.58 | 5.56 | 6.58 | 5.00 | 4.00 | 4.00 | 6.52 | 4.00 |
| Fall | 8.63 | 8.14 | 7.55 | 7.56 | 6.48 | 7.53 | 8.00 | 7.53 |

16.9 SO₂ Emissions Included in the Modeling Analysis

16.9.1 DRR Source: Duke - Cayuga Emissions

Duke - Cayuga has two units, Units BLR1 and BLR2 that have continuous emission monitoring (CEM) data for SO₂ from 2012 - 2014. This hourly CEM data from both units was formatted and used in the 1-hour SO₂ AERMOD model run. Total annual emissions from Duke - Cayuga from 2015 are approximately one-half of the emissions from 2012 through 2014 emissions.

Therefore, modeling the 2012-2014 emissions is conservative in nature. The auxiliary boiler will also be modeled based on the 2014 emissions reporting.

16.9.2 Inventoried SO₂ Sources Included in the Modeling

SO₂ sources from the surrounding area were evaluated to determine if their SO₂ emissions had a potential impact on the air quality surrounding the DRR source, beyond what is captured through background monitoring data. The latest available actual emissions over three years (2012-2014) were used. The following list of sources were included in the AERMOD run to determine overall air quality characteristics. Table 16.4 lists the inventory source to be included in the AERMOD run to determine overall air quality characteristics for the area surrounding Duke - Cayuga.

Table 16.4 – Duke – Cayuga Modeling Source Inventory

| Source | Source ID | Location | 2012-2014 SO ₂ Emissions (tpy) |
|----------------|-----------|-------------------|---|
| Eli Lilly | 165-00009 | Vermillion County | 1618.8 ^a |
| Colonial Brick | 165-00002 | Vermillion County | 76.5 ^b |

^a A short-term emission rate for the three-year (2012-2014) average was modeled for Eli Lilly.

^b A three-year (2012-2014) annual average was calculated for Colonial Brick. Colonial Brick was shut down in 2016. They still have an active Title V permit on file.

16.10 Modeling Results

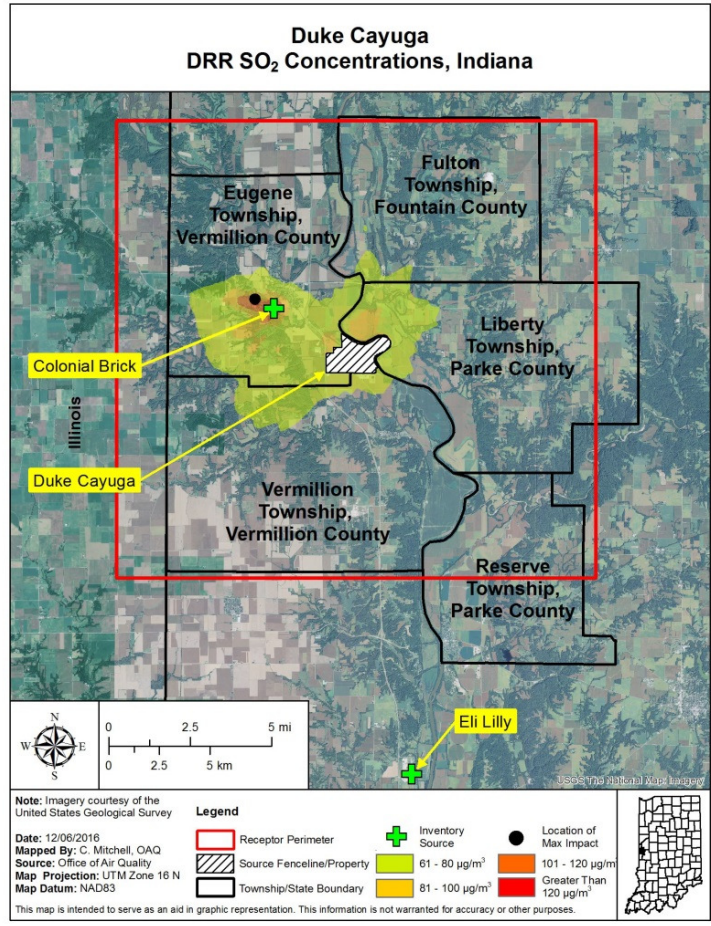
The 99th percentile of the 1-hour daily maximum modeled concentrations represents the fourth high of the 1-hour daily maximum SO₂ modeled concentrations and were averaged across three years to compare resulting concentrations to the 1-hour SO₂ NAAQS of 75 ppb (196.2 µg/m³). Modeled concentrations include representative temporally varying seasonal 1-hour SO₂ background values to determine the overall impact. The resulting concentrations were compared to the 1-hour SO₂ standard to indicate whether a modeled violation of the SO₂ NAAQS occurred. All concentrations fell below the 1-hour SO₂ NAAQS and were determined to attain the standard and the area surrounding Duke - Cayuga is recommended as attainment. The maximum predicted 99th percentile daily 1-hour SO₂ concentration is shown in Table 16.5. The overall maximum concentration was 176.4 µg/m³, occurring at UTM coordinates 458750.0 East, 4421750.0 North.

Table 16.5 – Duke – Cayuga Modeling Results

| Emission Scenarios | Total Modeled Concentration Including Seasonal Hourly Background (µg/m ³) | 1-Hour SO ₂ NAAQS (µg/m ³) | Facility Models Attainment |
|--------------------|---|---|----------------------------|
| Duke - Cayuga | 176.4 | 196.2 | Yes |

The concentration isopleths showing the maximum predicted 99th percentile daily 1-hour SO₂ concentration gradients can be found in Figure 16.5.

Figure 16.5 – Duke - Cayuga Modeling Results



ENCLOSURE 1

1-Hour SO₂ Background Determination

U.S. EPA revised the SO₂ National Ambient Air Quality Standard (NAAQS) by instituting a 1-hour primary standard of 75 parts per billion (ppb). Therefore, an analysis was necessary to determine ambient 1-hour SO₂ background concentrations representative for all regions in the state. This determination is needed in order to make attainment designations, attainment demonstrations and perform New Source Review (NSR) and Prevention of Significant Deterioration (PSD) modeling. Indiana has reviewed the 1-hour SO₂ monitoring and meteorological data from 2012 through 2014 to calculate representative ambient 1-hour SO₂ background concentrations. U.S. EPA's "SO₂ NAAQS Designations Modeling Technical Assistance Document, December 2013" was followed to calculate the background concentrations in order to eliminate overly conservative cumulative impacts from nearby major SO₂ emission sources when performing air quality dispersion modeling.

Overview

Indiana has 21 SO₂ monitors located throughout the state. Table 1 shows the 99th percentile for the years 2012, 2013, 2014, and 2015 and the 2012-2014 and 2013-2015 1-hour SO₂ design values for the 7 SO₂ monitors that the attainment designation are based on.

Table 1 - 1-Hour SO₂ Design Values for SO₂ Monitors (ppb) in Indiana

| County | Monitor ID | 99 th Percentile | | | | 2012-2014 Design Value | 2013-2015 Design Value |
|-------------|-------------|-----------------------------|------|------|------|------------------------------|------------------------------|
| | | 2012 | 2013 | 2014 | 2015 | | |
| Floyd | 18-043-1004 | 32.0 | 20.5 | 43.8 | 26.0 | 32 | 30 |
| Fountain | 18-045-0001 | 30.0 | 34.0 | 22.0 | 19.0 | 29 | 25 |
| Jasper | 18-073-0002 | 33.0 | 40.0 | 18.0 | 10.0 | 30 | 23 |
| Lake | 18-089-0022 | 47.0 | 43.2 | 53.1 | 35.0 | 48 | 44 |
| Porter | 18-127-0011 | 36.0 | 36.0 | 27.0 | 39.0 | 33 | 34 |
| Vanderburgh | 18-163-0021 | 16.5 | 18.6 | 32.3 | 18.0 | 22 | 23 |
| Vigo | 18-167-0018 | 72.5 | 79.1 | 85.0 | 71.0 | 79 | 78 |

Data Retrieval

Monitoring data for the SO₂ monitors near the DRR sources were retrieved from U.S. EPA's AirData database. The concentration data were supplied for each hour and day of every month from 2012 through 2014. Meteorological data was collected in order to correlate the wind

directions and concentrations for each hour of each day of every month. Meteorological data was either collected at a monitor near the monitoring site or the nearest National Weather Service (NWS) station or Automated Surface Observation Stations (ASOS). This data was collected and distributed by the Midwest Regional Climate Center (mrcc.isws.illinois.edu). The nearest meteorological data to each of the SO₂ monitors is summarized below.

Table 2 - Locations of SO₂ Monitors and Meteorological Stations for Background Analysis

| County/Site | Monitor ID | Monitor Location | Meteorological Station | Station Location |
|-------------------------------------|-------------------|-------------------------|--|-------------------------|
| Floyd Co. / New Albany | 18-043-1004 | 38.31° N 85.83° W | Charlestown State Park meteorological station | 38.39° N 85.66° W |
| Fountain Co. / North of S.R. 234 | 18-045-0001 | 39.96° N 87.42° W | Indianapolis NWS station | 39.79° N 86.18° W |
| Jasper Co. / Wheatfield | 18-073-0002 | 41.19° N 87.05° W | South Bend NWS station | 41.69° N 86.25° W |
| Lake Co. / Gary - IITRI | 18-089-0022 | 41.72° N 86.91° W | Gary IITRI meteorological station | 41.61° N 87.30° W |
| Porter Co. / Dunes Acres | 18-127-0011 | 41.63° N 87.10° W | Gary IITRI meteorological station | 41.61° N 87.30° W |
| Vanderburgh Co. / Buena Vista | 18-063-0021 | 38.01° N 87.58° W | Evansville NWS station | 38.05° N 87.52° W |
| Vigo Co. / Lafayette Ave | 18-167-0018 | 39.49° N 87.40° W | Indianapolis NWS station | 39.79° N 86.18° W |

Methodology for Determining Ambient SO₂ Background Concentrations

Each set of SO₂ data was paired with the corresponding meteorological conditions for every hour of the year in order to determine the wind direction for each hour that SO₂ concentrations were recorded. Data was processed in chronological order with daily and seasonal trends analyzed.

The initial analysis created pollution roses to determine the wind directions from which the highest SO₂ concentrations were coming. This analysis helped to identify the nearest upwind SO₂ emission sources impacting the SO₂ monitor. With those wind directions identified, SO₂ concentrations (10 ppb and above) resulting from SO₂ emission sources from those wind directions were removed from the analysis, in order to calculate a representative ambient SO₂ background concentration for each SO₂ monitor. This analysis helps to prevent double-counting SO₂ emission source impacts in an air quality modeling analysis. Once data for the SO₂ monitors were processed, the data was re-formatted in order to calculate the hourly-seasonal 99th percentile averages over a 3-year period, as detailed in U.S. EPA’s “SO₂ NAAQS Designations

Modeling Technical Assistance Document, December 2013 Section 8 – Background Concentrations”. The 99th percentile concentrations, based on each hour of the day and each of the four seasons of the year, were calculated for each SO₂ monitor.

In order to calculate the seasonal hourly 99th percentile average, the data was grouped by the seasonal months. Spring was represented by concentrations recorded in March, April and May; summer represented by June, July and August; fall represented by September, October and November and winter represented by December, January and February. Once this data was grouped by seasons, the 99th percentile was calculated for each hour of the day, making 24 separate 99th percentiles for each SO₂ monitoring site per season. The average of these 99th percentiles over the three-year period represents the hourly-seasonal 1-hour SO₂ background.

Summary

For purposes of the modeling analysis related to the DRR, adjusted 1-hour SO₂ background values were used for the Posey, Floyd, Sullivan, Vermillion, Jasper, Lake and Porter counties DRR sources. Calculations to determine adjusted 1-hour SO₂ background concentrations were made according to U.S. EPA’s “SO₂ NAAQS Designations Modeling Technical Assistance Document, February 2016 Section 8 – Background Concentrations”. This approach calls for the removal of SO₂ concentrations emitted from large SO₂ emission sources located directly upwind of a SO₂ monitor. This allows for more representative ambient background values to be determined, not overly conservative values that could possibly double-count direct SO₂ source impacts and 1-hour SO₂ background concentrations when modeling inventory sources.

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Enclosure 2
Lake County DRR Source Modeling Inventory
Point Sources

| | Company | Source ID | Source Description | East (X) (m) | North (Y) (m) | Stack Height (m) | Stack Temperature (K) | Exit Velocity (m/s) | Stack Diameter (m) | SO2 Emissions (tpy) | Emission Determination CEM/Varying/Annual |
|----|---------|-----------|------------------------------|-----------------|------------------|---------------------|--------------------------|------------------------|-----------------------|------------------------|--|
| 1 | AMUSA | 7 | Sinter Plant East Windbox | 463341 | 4612705 | 48.768 | 383.15 | 25.146 | 3.6576 | 355.17 | CEM |
| 2 | AMUSA | 26 | 4SP HMD South | 464015 | 4613844 | 7.9248 | 314.26 | 22.443439 | 2.2555 | 3.89 | CEM |
| 3 | AMUSA | 27 | 4SP HMD North | 464049 | 4613882 | 5.7912 | 314.26 | 22.23516 | 2.4384 | 3.89 | CEM |
| 4 | AMUSA | 37 | 4SP Secondary Vent | 464129 | 4613916 | 6.096 | 299.82 | 15.23492 | 4.8646 | 0.95 | CEM |
| 5 | AMUSA | 38 | 4SP Steelmaking Off Gas | 464111 | 4613786 | 45.72 | 338.71 | 22.9616 | 3.9624 | 27.3 | CEM |
| 6 | AMUSA | 101 | 101 | 464125 | 4612000 | 38.4048 | 519.26 | 18.81 | 1.676 | 4.71E-04 | CEM |
| 7 | AMUSA | 102 | 102 | 464115 | 4611990 | 38.4 | 519.26 | 18.81 | 1.676 | 4.71E-04 | CEM |
| 8 | AMUSA | 107 | 107 | 464100 | 4612030 | 67.06 | 672.04 | 7.596 | 3.3528 | 0.001052852 | CEM |
| 9 | AMUSA | 108 | 108 | 464090 | 4611930 | 67.06 | 672.04 | 7.596 | 3.353 | 0.001035227 | CEM |
| 10 | AMUSA | 134 | 5 BH 501-503 | 464897 | 4614738 | 68.58 | 407.04 | 14.1224 | 5.1816 | 338.15 | CEM |
| 11 | AMUSA | 141 | EAF Melting | 461960 | 4610940 | 43.5864 | 377.04 | 2.86512 | 10.2443 | 85.93 | CEM |
| 12 | AMUSA | 143 | EAF LMF | 461859 | 4610982 | 13.8684 | 340.37 | 18.39976 | 1.143 | 13.94 | CEM |
| 13 | AMUSA | 147 | 2SP 10 Furnace Off Gas | 463272 | 4612185 | 77.724 | 1922.04 | 13.49758 | 1.8288 | 28.02 | CEM |
| 14 | AMUSA | 148 | 2SP 20 Furnace Off Gas | 463383 | 4612297 | 73.152 | 1922.04 | 13.49758 | 1.8288 | 28.01 | CEM |
| 15 | AMUSA | 149 | 2SP Secondary Vent | 463461 | 4612335 | 64.008 | 302.04 | 8.712199 | 3.6576 | 11.2 | CEM |
| 16 | AMUSA | 152 | 2SP HMD | 463393 | 4612307 | 4.572 | 316.48 | 12.79144 | 3.81 | 0 | |
| 17 | AMUSA | 154 | 2SP LMF | 463202 | 4612155 | 18.288 | 339.82 | 10.24128 | 1.8288 | 20.01 | CEM |
| 18 | AMUSA | 166 | IH7 Casthouse Baghouse 2 (W) | 464670 | 4614630 | 4.572 | 310.93 | 33.67531 | 2.987 | 203.9 | CEM |
| 19 | AMUSA | 167 | IH7 Casthouse Baghouse 1 (E) | 464870 | 4614500 | 46.9392 | 327.59 | 16.03756 | 3.3528 | 203.9 | CEM |
| 20 | AMUSA | 170 | IH7 Stoves | 464800 | 4614500 | 70.104 | 533.15 | 14.1732 | 5.1816 | 398.77 | CEM |
| 21 | AMUSA | 195 | IH7 BFG Flare | 464870 | 4614490 | 55.7784 | 922.04 | 2 | 2.6518 | 136.9 | CEM |

Lake County DRR Source Modeling Inventory Point Sources

| | Company | Source ID | Source Description | East (X) (m) | North (Y) (m) | Stack Height (m) | Stack Temperature (K) | Exit Velocity (m/s) | Stack Diameter (m) | SO2 Emissions (tpy) | Emission Determination CEM/Varying/Annual |
|----|-----------|-----------|-------------------------------|-----------------|------------------|---------------------|--------------------------|------------------------|-----------------------|------------------------|--|
| 22 | Cokenergy | 201 | Cokenergy | 465354 | 4614325 | 89.9 | 422.04 | 20.33016 | 5.4864 | 5236 | CEM |
| 23 | IHCC | 220 | Boiler 504 | 464920 | 4614849 | 96.012 | 404.97 | 16.1544 | 3.048 | 236.25 | CEM |
| 24 | AMUSA | 45A | No. 1 Lime Kiln Bghse Stack A | 463894 | 4613596 | 21.3055 | 477.59 | 18.5674 | 0.9662 | 5.55 | CEM |
| 25 | AMUSA | 45B | No. 1 Lime Kiln Bghse Stack B | 463897 | 4613600 | 21.3055 | 477.59 | 18.5674 | 0.9662 | 5.55 | CEM |
| 26 | AMUSA | 45C | No. 2 Lime Kiln Bghse Stack A | 463883 | 4613607 | 21.3055 | 477.59 | 18.5674 | 0.9662 | 5.55 | CEM |
| 27 | AMUSA | 45D | No. 2 Lime Kiln Bghse Stack B | 463887 | 4613610 | 21.3055 | 477.59 | 18.5674 | 0.9662 | 5.55 | CEM |
| 28 | IHCC | IHCCCH1 | Charging-Battery A/B | 465174 | 4614512 | 18.2911 | 394.26 | 17.61134 | 2.7402 | 2.385 | 3-yr ave annual |
| 29 | IHCC | IHCCCH2 | Charging-Battery C/D | 465150 | 4614134 | 18.2911 | 394.26 | 17.61134 | 2.7402 | 2.385 | 3-yr ave annual |
| 30 | IHCC | IHCCPS | Pushing | 465154 | 4614232 | 7.7602 | 394.26 | 25.99944 | 0.8595 | 6.2 | 3-yr ave annual |
| 31 | IHCC | IHCCQ1 | Quenching A/B | 465264 | 4614353 | 18.3002 | 373.15 | 3.191256 | 11.9786 | 1.95 | 3-yr ave annual |
| 32 | IHCC | IHCCQ2 | Quenching C/D | 465258 | 4614315 | 18.3002 | 373.15 | 3.191256 | 11.9786 | 1.95 | 3-yr ave annual |
| 33 | IHCC | IHCCVS | IHCC Vent Stacks | 465166 | 4614224.5 | 25.3 | 983.15 | 18.37944 | 2.3896 | 2419.7 | CEM |
| 34 | | IHCC102 | | 465199.13 | 4614569.39 | 25.2984 | 983 | 12.246864 | 2.3866 | 0 | |
| 35 | | IHCC103 | | 465178.47 | 4614116.45 | 25.2984 | 983 | 12.246864 | 2.3866 | 0 | |
| 36 | | IHCC104 | | 465174.04 | 4614010.86 | 25.2984 | 983 | 12.246864 | 2.3866 | 0 | |
| 37 | | IHCC105 | | 465202.47 | 4614661.37 | 25.2984 | 983 | 12.246864 | 2.3866 | 0 | |
| 38 | | IHCC106 | | 465179.9 | 4614182.35 | 25.2984 | 983 | 12.246864 | 2.3866 | 0 | |
| 39 | | IHCC107 | | 465192.44 | 4614485.78 | 25.2984 | 983 | 12.246864 | 2.3866 | 0 | |
| 40 | | IHCC108 | | 465189.1 | 4614403.84 | 25.2984 | 983 | 12.246864 | 2.3866 | 0 | |
| 41 | | IHCC109 | | 465127.22 | 4614295.14 | 25.2984 | 983 | 12.246864 | 2.3866 | 0 | |
| 42 | | IHCC110 | | 465126.54 | 4614212.11 | 25.2984 | 983 | 12.246864 | 2.3866 | 0 | |
| 43 | | IHCC111 | | 465123.81 | 4614104.15 | 25.2984 | 983 | 12.246864 | 2.3866 | 0 | |

Enclosure 2
Lake County DRR Source Modeling Inventory
Point Sources

| | Company | Source ID | Source Description | East (X) (m) | North (Y) (m) | Stack Height (m) | Stack Temperature (K) | Exit Velocity (m/s) | Stack Diameter (m) | SO2 Emissions (tpy) | Emission Determination CEM/Varying/Annual |
|----|----------|-----------|--------------------------|-----------------|------------------|---------------------|--------------------------|------------------------|-----------------------|------------------------|--|
| 44 | | IHCC112 | | 465114.24 | 4614024.89 | 25.2984 | 983 | 12.246864 | 2.3866 | 0 | |
| 45 | | IHCC113 | | 465150.63 | 4614659.69 | 25.2984 | 983 | 12.246864 | 2.3866 | 0 | |
| 46 | | IHCC114 | | 465143.95 | 4614574.41 | 25.2984 | 983 | 12.246864 | 2.3866 | 0 | |
| 47 | | IHCC115 | | 465138.93 | 4614495.81 | 25.2984 | 983 | 12.246864 | 2.3866 | 0 | |
| 48 | | IHCC116 | | 465133.91 | 4614407.18 | 25.2984 | 983 | 12.246864 | 2.3866 | 0 | |
| 49 | AMIH | S1A | IH3 Stoves | 462621 | 4612774 | 65.2272 | 533.15 | 9.99744 | 3.2918 | 105.45 | CEM |
| 50 | AMIH | S1B | IH4 Casthouse Baghouse | 462629 | 4612930 | 22.7076 | 339.26 | 8.966201 | 3.6881 | 117.03 | CEM |
| 51 | AMIH | S1C | IH4 Stoves | 462629 | 4612787 | 62.1792 | 533.15 | 9.99744 | 3.9929 | 244.3 | CEM |
| 52 | AMIH | S1D | IH4 Bleeder | 462645 | 4612785 | 31.0896 | 922.04 | 5.916168 | 1.7242 | 138.7 | CEM |
| 53 | AMIH | S1E | IH3 Bleeder | 462624 | 4612765 | 31.0896 | 922.04 | 3.837432 | 1.7242 | 81.7 | CEM |
| 54 | AMIH | S301 | IH7 Granulator - Lafarge | 464750 | 4614550 | 99.44 | 336 | 5.479999 | 3.96 | 28.5 | CEM |
| 55 | AMIH | S3B | 3SP HMD Baghouse | 462734 | 4613566 | 8.8087 | 304.82 | 8.102599 | 1.204 | 54.65 | CEM |
| 56 | AMIH | S4A | HSM Reheat Furnace 1 | 462645 | 4614319 | 65.2272 | 977.59 | 8.74776 | 4.572 | 0 | |
| 57 | AMIH | S4B | HSM Reheat Furnace 2 | 462668 | 4614311 | 65.2272 | 977.59 | 8.74776 | 4.572 | 0 | |
| 58 | AMIH | S4C | HSM Reheat Furnace 3 | 462691 | 4614305 | 65.2272 | 977.59 | 8.74776 | 4.572 | 0 | |
| 59 | AMIH | S8E | No. 6 Boiler | 462286 | 4612566 | 46.9392 | 683.15 | 26.79192 | 3.048 | 180.5 | CEM |
| 60 | AMIH | S8G | No. 8 Boiler | 462273 | 4612540 | 46.9392 | 688.71 | 17.31264 | 3.5052 | 356.7 | CEM |
| 61 | Ironside | S8H | No. 9 Boiler | 462269 | 4612577 | 46.9392 | 683.15 | 26.79192 | 3.048 | 204.3 | CEM |
| 84 | US Steel | 94011 | Sinter Plant Windbox | 473218 | 4607057 | 56.388 | 385.93 | 20.23872 | 3.4442 | 534.9 | 3-yr ave annual |
| 85 | US Steel | 940541 | TBBH Boiler 1 | 472661 | 4607149 | 45.72 | 572.04 | 14.478 | 3.6576 | 72.18 | 3-yr ave annual |
| 86 | US Steel | 940542 | TBBH Boiler 2 | 472661 | 4607136 | 45.72 | 572.04 | 14.478 | 3.6576 | 124.14 | 3-yr ave annual |

Enclosure 2
Lake County DRR Source Modeling Inventory
Point Sources

| | Company | Source ID | Source Description | East (X) (m) | North (Y) (m) | Stack Height (m) | Stack Temperature (K) | Exit Velocity (m/s) | Stack Diameter (m) | SO2 Emissions (tpy) | Emission Determination CEM/Varying/Annual |
|-----|----------|--------------|--|-----------------|------------------|------------------------|-----------------------------|---------------------------|--------------------------|---------------------------|--|
| 87 | US Steel | 940543 | TBBH Boiler 3 | 472661 | 4607123 | 45.72 | 572.04 | 14.478 | 3.6576 | 126.2 | 3-yr ave annual |
| 88 | US Steel | 940545 | TBBH Boiler 5 | 472661 | 4607096 | 45.72 | 572.04 | 14.478 | 3.6576 | 63 | 3-yr ave annual |
| 89 | US Steel | 94053 | TBBH Boiler 6 | 472655 | 4607079 | 45.72 | 499.82 | 12.16152 | 3.6576 | 72.3 | 3-yr ave annual |
| 90 | US Steel | 94017 | 84 inch Hot Strip Mill Reheat Furnaces | 468755 | 4608468 | 49.6824 | 701.48 | 50.81016 | 2.4689 | 107.8 | Seasonal Varying |
| 91 | US Steel | 940121 | No. 4 BH Boiler 1 | 472592 | 4607817 | 35.3568 | 460.93 | 18.83664 | 2.8956 | 153.3 | Seasonal Varying |
| 92 | US Steel | 940122 | No. 4 BH Boiler 2 | 472592 | 4607792 | 35.3568 | 460.93 | 18.83664 | 2.8956 | 168.81 | Seasonal Varying |
| 93 | US Steel | 940123 | No. 4 BH Boiler 3 | 472592 | 4607767 | 35.3568 | 460.93 | 18.83664 | 2.8956 | 110.92 | Seasonal Varying |
| 94 | US Steel | 940401 | CPBH Boiler 8 | 474393 | 4606802 | 94.1832 | 535.93 | 5.66928 | 3.048 | 23.6 | Seasonal Varying |
| 95 | US Steel | 940402 | CPBH Boiler 9 | 474436 | 4606850 | 60.96 | 535.93 | 5.66928 | 2.8042 | 23.6 | Seasonal Varying |
| 96 | US Steel | 940403 | CPBH Boiler 10 | 474436 | 4606866 | 60.96 | 535.93 | 5.66928 | 2.8042 | 23.6 | Seasonal Varying |
| 97 | US Steel | 94070 | Tail Gas Incinerator | 474470 | 4606815 | 97.536 | 894.26 | 22.86 | 0.5791 | 1.2 | 3-yr ave annual |
| 98 | US Steel | 94026 | No. 2 Underfiring | 473903 | 4606522 | 106.68 | 368.71 | 3.2004 | 6.096 | 67.3 | 3-yr ave annual |
| 99 | US Steel | 94038 | CPBH Boiler 6 | 474362 | 4606775 | 40.5384 | 535.93 | 5.334 | 2.5908 | 23.6 | Seasonal Varying |
| 100 | US Steel | 94037 | CPBH Boilers 4 an 5 | 474337 | 4606775 | 40.5384 | 535.93 | 5.334 | 2.5908 | 23.6 | Seasonal Varying |
| 101 | US Steel | 94066 | No. 14 BF Casthouse | 472643 | 4607841 | 50.292 | 329.82 | 20.4216 | 3.9624 | 719.9 | Seasonal Varying |
| 102 | US Steel | 94039 | Coke Plant Boiler No. 7 | 474370 | 4606803 | 32.004 | 535.93 | 5.12064 | 2.5908 | 23.6 | 3-yr ave annual |
| 103 | US Steel | 94036 | Coke Plant Boiler No. 3 | 474315 | 4606782 | 39.3192 | 535.93 | 9.26592 | 1.8898 | 23.6 | 3-yr ave annual |
| 104 | US Steel | 94021 | No. 4 BF Stoves | 472694 | 4606861 | 68.58 | 314.82 | 3.47472 | 3.9014 | 53.9 | Seasonal Varying |
| 105 | US Steel | 94022 | No. 6 BF Stoves | 472697 | 4607006 | 68.58 | 319.82 | 8.13816 | 3.9014 | 92.2 | Seasonal Varying |
| 106 | US Steel | 94023 | No. 8 BF Stoves | 472701 | 4607166 | 76.2 | 313.71 | 5.88264 | 3.9014 | 59.4 | Seasonal Varying |
| 107 | US Steel | 94013BFSTOVE | #13 BF Stoves | 472696 | 4607680 | 76.2 | 325.37 | 6.21792 | 15.5143 | 101.7 | Seasonal Varying |

Enclosure 2
Lake County DRR Source Modeling Inventory
Point Sources

| | Company | Source ID | Source Description | East (X) (m) | North (Y) (m) | Stack Height (m) | Stack Temperature (K) | Exit Velocity (m/s) | Stack Diameter (m) | SO2 Emissions (tpy) | Emission Determination CEM/Varying/Annual |
|-----|----------|------------|---|-----------------|------------------|---------------------|--------------------------|------------------------|-----------------------|------------------------|--|
| 108 | US Steel | 94041 | No. 1 BOP Desulf Caster | 472325 | 4606631 | 24.384 | 299.82 | 22.82952 | 3.109 | 41.6 | 3-yr ave annual |
| 109 | US Steel | 94007 | Sinter Cooler | 473194 | 4607100 | 30.48 | 455.37 | 18.8976 | 5.4864 | 86.3 | 3-yr ave annual |
| 110 | US Steel | USPRECA | Precarbon #2 (by Coke Battery #2) includes CASP C | 473933 | 4606552 | 49.9872 | 499.98 | 9.99744 | 2.0117 | 3 | 3-yr ave annual |
| 111 | US Steel | USBFGFL | BFG Flare Stacks (closer to BF #4) | 472724 | 4606895 | 200.0098 | 922.04 | 9.99744 | 4.9987 | 90.3 | 3-yr ave annual |
| 112 | US Steel | 94045QBOP2 | No 2 QBOP Desulf Caster | 472524 | 4607641 | 16.764 | 331.48 | 16.3068 | 1.1582 | 0 | |
| 113 | US Steel | 940CB5 | Coke Battery #5 Underfire | 473200 | 4606400 | 76.2 | 499.82 | 4.38912 | 3.048 | 23.8 | 3-yr ave annual |
| 114 | US Steel | 940CB7 | Coke Battery #7 Underfire | 473200 | 4606600 | 76.2 | 533.15 | 5.6388 | 3.048 | 33.1 | 3-yr ave annual |
| 115 | US Steel | COGBYPROD | Coke Oven Gas Recovery | 473200 | 4606600 | 30.48 | 366.48 | 2.98704 | 1.0058 | 0 | |
| 116 | US Steel | 940CASPC | CASP C | 474393 | 4606802 | 16.764 | 366.48 | 3.048 | 2.0117 | 10.36 | 3-yr ave annual |
| 117 | US Steel | USCOGFLARE | COG stack Desulf | 473534.18 | 4606500.83 | 45.72 | 922.04 | 3.048 | 5.7912 | 69.6 | 3-yr ave annual |
| 118 | US Steel | US1BOPCAST | | 472477 | 4607429 | 24.4145 | 394.26 | 20.20824 | 2.4384 | 0 | |
| 132 | BP AMOCO | BP1 | 3SPS Boiler 1 | 459991.4 | 4613228.4 | 18.3948 | 508.36 | 7.7852016 | 0.8083 | 15.91 | 3-yr ave annual |
| 133 | BP AMOCO | BP2 | 3SPS Boiler 2 | 459991.4 | 4613237.1 | 18.3948 | 508.36 | 7.7852016 | 0.8083 | 15.76 | 3-yr ave annual |
| 134 | BP AMOCO | BP3 | 3SPS Boiler 3 | 459973.9 | 4613228.4 | 18.3948 | 508.36 | 7.7852016 | 0.8083 | 15.51 | 3-yr ave annual |
| 135 | BP AMOCO | BP4 | 3SPS Boiler 4 | 459973.9 | 4613237.1 | 18.3948 | 508.36 | 7.7852016 | 0.8083 | 16.68 | 3-yr ave annual |
| 136 | BP AMOCO | BP5 | 3SPS Boiler 6 | 459955.8 | 4613231.5 | 18.3948 | 508.36 | 7.7852016 | 0.8083 | 17.45 | 3-yr ave annual |
| 137 | BP AMOCO | BP6 | FCU 500 CAT | 460103 | 4612576 | 23.2258 | 567 | 10.451592 | 0.8361 | 25.1 | 3-yr ave annual |
| 138 | BP AMOCO | BP7 | 11 PS - H-1X | 459829.8 | 4613338.8 | 18.4877 | 496.94 | 2.3783544 | 0.8826 | 6.06 | 3-yr ave annual |
| 139 | BP AMOCO | BP9 | 11 PS - H-3 | 459861.8 | 4613314.7 | 15.329 | 607.12 | 3.5396424 | 0.3995 | 1.25 | 3-yr ave annual |
| 140 | BP AMOCO | BP10 | 11 PS - H-200 | 459792.5 | 4613422.1 | 18.209 | 536.13 | 3.0751272 | 0.9104 | 7.38 | 3-yr ave annual |
| 141 | BP AMOCO | BP11 | 11 PS- H-300 | 459792.5 | 4613443.9 | 18.209 | 536.13 | 2.4990552 | 0.8268 | 4.75 | 3-yr ave annual |

Enclosure 2
Lake County DRR Source Modeling Inventory
Point Sources

| | Company | Source ID | Source Description | East (X) (m) | North (Y) (m) | Stack Height (m) | Stack Temperature (K) | Exit Velocity (m/s) | Stack Diameter (m) | SO2 Emissions (tpy) | Emission Determination CEM/Varying/Annual |
|-----|----------|-----------|-------------------------------------|-----------------|------------------|------------------------|-----------------------------|---------------------------|--------------------------|---------------------------|--|
| 142 | BP AMOCO | BP12 | #1 CRU/ ARU PROCESS HEATER | 459703 | 4612854 | 16.258 | 514.53 | 0.4273296 | 1.1241 | 2.13 | 3-yr ave annual |
| 143 | BP AMOCO | BP13 | #2 CRU/ ARU PROCESS HEATER | 459666 | 4612852 | 15.6077 | 631.81 | 3.0470856 | 0.4831 | 1.1 | 3-yr ave annual |
| 144 | BP AMOCO | BP14 | FCU 600 CAT | 459945 | 4612578 | 14.8645 | 605.58 | 6.1222128 | 0.7432 | 16.25 | 3-yr ave annual |
| 145 | BP AMOCO | BP15 | ALKY | 460095 | 4612741.85 | 18.1161 | 962.68 | 6.094476 | 0.3066 | 1.55 | 3-yr ave annual |
| 146 | BP AMOCO | BP16 | DDU or South ? 800-04 | 459855.11 | 4613618.24 | 18.5806 | 962.68 | 6.094476 | 0.3809 | 90.97 | 3-yr ave annual |
| 147 | BP AMOCO | BP17 | FCU | 459721.53 | 4612637.23 | 18.5806 | 962.68 | 6.094476 | 0.3716 | 1.25 | 3-yr ave annual |
| 148 | BP AMOCO | BP18 | 4UF | 459550 | 4612830 | 18.5806 | 962.68 | 6.094476 | 0.6039 | 13.75 | 3-yr ave annual |
| 149 | BP AMOCO | BP19 | UIU | 459751.57 | 4612755.58 | 19.9742 | 962.68 | 6.094476 | 0.4274 | 7.4 | 3-yr ave annual |
| 150 | BP AMOCO | BP20 | VRU | 460280 | 4612423.82 | 18.1161 | 962.68 | 6.094476 | 0.1951 | 2.39 | 3-yr ave annual |
| 151 | BP AMOCO | BP21 | ARU - F200A, F-200B | 459993 | 4613060 | 18.5806 | 474.41 | 1.161288 | 1.0684 | 8.22 | 3-yr ave annual |
| 152 | BP AMOCO | BP22 | 4UF - F-1, F-8A, F-8B | 459707 | 4613011 | 15.9793 | 554.66 | 2.5270968 | 1.1241 | 4.64 | 3-yr ave annual |
| 153 | BP AMOCO | BP23 | 4UF - F-2 | 459635 | 4613011 | 19.7883 | 548.79 | 1.9510248 | 1.0684 | 3.86 | 3-yr ave annual |
| 154 | BP AMOCO | BP24 | 4UF - F-3 | 459645 | 4613011 | 18.3948 | 560.52 | 2.1646896 | 0.9755 | 4.14 | 3-yr ave annual |
| 155 | BP AMOCO | BP25 | 4UF - F-4, F-5, F-6 | 459665 | 4613011 | 17.1871 | 505.27 | 1.8022824 | 1.0684 | 4.31 | 3-yr ave annual |
| 156 | BP AMOCO | BP27 | New 12 PS Atmospheric Heater H-101A | 460629 | 4612809.3 | 18.3019 | 505.27 | 2.4804624 | 0.9941 | 21.4 | 3-yr ave annual |
| 157 | BP AMOCO | BP28 | New 12 PS Vacuum Heater H-102 | 460619.9 | 4612706.6 | 18.3948 | 496.01 | 2.3411688 | 0.9941 | 7.78 | 3-yr ave annual |
| 158 | BP AMOCO | BP30 | New Coker Heater | 460567 | 4612560 | 18.4877 | 506.81 | 2.1089112 | 0.6968 | 6.31 | 3-yr ave annual |
| 159 | BP AMOCO | BP31 | New Coker Heater | 460566 | 4612515 | 18.4877 | 506.81 | 2.1089112 | 0.6968 | 6.54 | 3-yr ave annual |
| 160 | BP AMOCO | BP32 | New Coker Heater | 460566 | 4612477 | 18.4877 | 506.81 | 2.1089112 | 0.6968 | 6 | 3-yr ave annual |
| 161 | BP AMOCO | BP33 | New Hydrogen Plant | 461343 | 4612750 | 9.2903 | 505.27 | 4.645152 | 1.0498 | 0 | |
| 162 | BP AMOCO | BP34 | New Hydrogen Plant | 461401 | 4612695 | 9.2903 | 505.27 | 4.645152 | 1.0498 | 0 | |

Enclosure 2
Lake County DRR Source Modeling Inventory
Point Sources

| | Company | Source ID | Source Description | East (X) (m) | North (Y) (m) | Stack Height (m) | Stack Temperature (K) | Exit Velocity (m/s) | Stack Diameter (m) | SO2 Emissions (tpy) | Emission Determination CEM/Varying/Annual |
|-----|----------|-----------|-------------------------------------|-----------------|------------------|---------------------|--------------------------|------------------------|-----------------------|------------------------|--|
| 163 | BP AMOCO | BP35 | COT1 and COT2 | 460224 | 4612806 | 11.6129 | 573.17 | 6.670548 | 0.576 | 52.52 | 3-yr ave annual |
| 164 | BP AMOCO | BP36 | New GOHT Heater | 459477.4 | 4613541.6 | 13.0064 | 628.73 | 4.3665648 | 0.3345 | 0 | |
| 165 | BP AMOCO | BP37 | New 12 PS Atmospheric Heater H-101B | 460629 | 4612839.8 | 18.3019 | 505.27 | 2.4804624 | 0.9941 | 0 | |
| 166 | BP AMOCO | BP39 | ISOM - H-1 | 459822 | 4612853 | 11.6129 | 517.62 | 2.6849832 | 0.7618 | 4.69 | 3-yr ave annual |
| 167 | BP AMOCO | BP42 | DDU - WB-301 and WB-301 | 459443 | 4613297 | 13.1922 | 644.16 | 5.9457336 | 0.3623 | 4.92 | 3-yr ave annual |
| 168 | BP AMOCO | BP43 | HU - B-501 | 459586 | 4613330 | 23.2258 | 505.27 | 5.8527696 | 0.641 | 2.23 | 3-yr ave annual |
| 169 | Carmeuse | KILN1A | Carmeuse 1 | 466117.95 | 4610027.09 | 24.3596 | 477.59 | 3.048 | 1.9812 | 8.76 | SO2 Limit |
| 170 | Carmeuse | KILN1B | | 466119.57 | 4610029.22 | 24.3596 | 477.59 | 3.048 | 1.9812 | 8.76 | SO2 Limit |
| 171 | Carmeuse | KILN1C | | 466121.19 | 4610031.35 | 24.3596 | 477.59 | 3.048 | 1.9812 | 8.76 | SO2 Limit |
| 172 | Carmeuse | KILN1D | | 466122.81 | 4610033.47 | 24.3596 | 477.59 | 3.048 | 1.9812 | 8.76 | SO2 Limit |
| 173 | Carmeuse | KILN1E | | 466124.43 | 4610035.6 | 24.3596 | 477.59 | 3.048 | 1.9812 | 8.76 | SO2 Limit |
| 174 | Carmeuse | KILN1F | | 466126.05 | 4610037.73 | 24.3596 | 477.59 | 3.048 | 1.9812 | 8.76 | SO2 Limit |
| 175 | Carmeuse | KILN2A | Carmeuse 2 | 466108.24 | 4610034.44 | 26.4932 | 477.59 | 3.048 | 1.9812 | 8.76 | SO2 Limit |
| 176 | Carmeuse | KILN2B | | 466109.85 | 4610036.58 | 26.4932 | 477.59 | 3.048 | 1.9812 | 8.76 | SO2 Limit |
| 177 | Carmeuse | KILN2C | | 466111.47 | 4610038.72 | 26.4932 | 477.59 | 3.048 | 1.9812 | 8.76 | SO2 Limit |
| 178 | Carmeuse | KILN2D | | 466113.09 | 4610040.86 | 26.4932 | 477.59 | 3.048 | 1.9812 | 8.76 | SO2 Limit |
| 180 | Carmeuse | KILN2F | | 466116.32 | 4610045.14 | 26.4932 | 477.59 | 3.048 | 1.9812 | 8.76 | SO2 Limit |
| 181 | Carmeuse | KILN3A | Carmeuse 3 | 466096.38 | 4610042.8 | 26.4932 | 477.59 | 3.048 | 1.9812 | 8.76 | SO2 Limit |
| 182 | Carmeuse | KILN3B | | 466097.99 | 4610044.93 | 26.4932 | 477.59 | 3.048 | 1.9812 | 8.76 | SO2 Limit |
| 183 | Carmeuse | KILN3C | | 466099.6 | 4610047.07 | 26.4932 | 477.59 | 3.048 | 1.9812 | 8.76 | SO2 Limit |
| 184 | Carmeuse | KILN3D | | 466101.22 | 4610049.2 | 26.4932 | 477.59 | 3.048 | 1.9812 | 8.76 | SO2 Limit |

Lake County DRR Source Modeling Inventory Point Sources

| | Company | Source ID | Source Description | East (X) (m) | North (Y) (m) | Stack Height (m) | Stack Temperature (K) | Exit Velocity (m/s) | Stack Diameter (m) | SO2 Emissions (tpy) | Emission Determination CEM/Varying/Annual |
|-----|----------|-----------|---------------------------------------|-----------------|------------------|---------------------|--------------------------|------------------------|-----------------------|------------------------|--|
| 185 | Carmeuse | KILN3E | | 466102.83 | 4610051.34 | 26.4932 | 477.59 | 3.048 | 1.9812 | 8.76 | SO2 Limit |
| 186 | Carmeuse | KILN3F | | 466104.44 | 4610053.47 | 26.4932 | 477.59 | 3.048 | 1.9812 | 8.76 | SO2 Limit |
| 187 | Carmeuse | KILN4A | Carmeuse 4 | 466086.05 | 4610050.06 | 28.956 | 477.59 | 3.048 | 1.9812 | 8.76 | SO2 Limit |
| 188 | Carmeuse | KILN4B | | 466087.66 | 4610052.19 | 28.956 | 477.59 | 3.048 | 1.9812 | 8.76 | SO2 Limit |
| 189 | Carmeuse | KILN4C | | 466089.27 | 4610054.33 | 28.956 | 477.59 | 3.048 | 1.9812 | 8.76 | SO2 Limit |
| 190 | Carmeuse | KILN4D | | 466090.88 | 4610056.46 | 28.956 | 477.59 | 3.048 | 1.9812 | 8.76 | SO2 Limit |
| 191 | Carmeuse | KILN4E | | 466092.49 | 4610058.6 | 28.956 | 477.59 | 3.048 | 1.9812 | 8.76 | SO2 Limit |
| 192 | Carmeuse | KILN4F | | 466094.1 | 4610060.73 | 28.956 | 477.59 | 3.048 | 1.9812 | 8.76 | SO2 Limit |
| 193 | Carmeuse | KILN5A | Carmeuse 5 | 466076.28 | 4610057.34 | 26.8224 | 477.59 | 3.048 | 1.9812 | 8.76 | SO2 Limit |
| 194 | Carmeuse | KILN5B | | 466077.89 | 4610059.47 | 26.8224 | 477.59 | 3.048 | 1.9812 | 8.76 | SO2 Limit |
| 195 | Carmeuse | KILN5C | | 466079.51 | 4610061.61 | 26.8224 | 477.59 | 3.048 | 1.9812 | 8.76 | SO2 Limit |
| 196 | Carmeuse | KILN5D | | 466081.13 | 4610063.75 | 26.8224 | 477.59 | 3.048 | 1.9812 | 8.76 | SO2 Limit |
| 197 | Carmeuse | KILN5E | | 466082.74 | 4610065.88 | 26.8224 | 477.59 | 3.048 | 1.9812 | 8.76 | SO2 Limit |
| 198 | Carmeuse | KILN5F | | 466084.36 | 4610068.02 | 26.8224 | 477.59 | 3.048 | 1.9812 | 8.76 | SO2 Limit |
| 199 | Koppers | KOPPER24 | | 437771.4 | 4630123.7 | 25.908 | 508.1 | 22.06752 | 1.524 | 569.8 | 3-yr ave annual |
| 200 | Koppers | KOPPER77 | | 437763 | 4630123.6 | 25.908 | 508.1 | 22.06752 | 1.524 | 569.8 | 3-yr ave annual |
| 201 | Koppers | KOPPER53 | | 437576.5 | 4630111.5 | 23.4696 | 794.2 | 14.23 | 0.76 | 333.6 | 3-yr ave annual |
| 202 | Koppers | KOPPER76 | | 437577.2 | 4630093.9 | 23.4696 | 777.6 | 9.31 | 0.76 | 312.5 | 3-yr ave annual |
| 203 | AMBH | AMSRC12 | Battery 2 Pushing Stack | 488266.6 | 4609400.9 | 64.008 | 1088.71 | 41.57472 | 1.524 | 0 | |
| 204 | AMBH | AM57 | BOF Hot Metal Desulf 1 Baghouse Stack | 488498.4 | 4609914.4 | 25.9111 | 305.37 | 12.94892 | 2.0513 | 0 | |
| 205 | AMBH | AM59 | BOF Hot Metal Desulf 2 Baghouse Stack | 488512 | 4609940.1 | 25.9111 | 305.37 | 5.887721 | 3.0389 | 0 | |
| 206 | AMBH | AM60 | BOF Hot Metal Desulf 3 Baghouse Stack | 488514.6 | 4609952.1 | 12.192 | 319.26 | 12.94892 | 2.664 | 0 | |

Lake County DRR Source Modeling Inventory Point Sources

| | Company | Source ID | Source Description | East (X) (m) | North (Y) (m) | Stack Height (m) | Stack Temperature (K) | Exit Velocity (m/s) | Stack Diameter (m) | SO2 Emissions (tpy) | Emission Determination CEM/Varying/Annual |
|-----|--------------|-----------|---------------------------------------|-----------------|------------------|---------------------|--------------------------|------------------------|-----------------------|------------------------|--|
| 207 | AMBH | P6 | AMBurns PwrStn Blr 8-12 | 488403 | 4609297 | 67.9704 | 505.37 | 13.939519 | 3.5113 | 4312.5 | Seasonal Varying |
| 208 | NIPSCO | PU78FGD | NIPSCO Bailly | 489738 | 4610321 | 146.304 | 327.59 | 26.634989 | 6.2484 | 1368.7 | CEM |
| 211 | LaFarge | LAFAR1 | | 465166 | 4614224.5 | 25.3 | 983.15 | 18.37944 | 2.39 | 98.45 | 3-yr ave annual |
| 212 | Safety Kleen | SK4 | | 460158.59 | 4610790.08 | 30.48 | 1080.37 | 6.767 | 1.3716 | 34.9 | 3-yr ave annual |
| 213 | Safety Kleen | SK7 | | 460162.05 | 4610772.05 | 30.48 | 1019.26 | 4.572 | 0.9693 | 21.36 | 3-yr ave annual |
| 214 | Safety Kleen | SK8 | | 460153.73 | 4610772.75 | 30.48 | 1055.37 | 7.132 | 0.8534 | 6 | 3-yr ave annual |
| 215 | Eco Service | 00242_2 | | 460128.5 | 4606396.7 | 10.668 | 810.93 | 15.651 | 1.3716 | 3.76 | 3-yr ave annual |
| 216 | Eco Service | 00242_3 | | 460053.5 | 4606385.4 | 91.44 | 334.26 | 12.89304 | 1.8288 | 251.29 | 3-yr ave annual |
| 225 | AMUSA | AMUSA166 | 2SP BOF Charge Aisle | 463400 | 4612140 | 4.572 | 316.48 | 33.6804 | 2.987 | 6.48 | 3-yr ave annual |
| 226 | AMBH | P7001 | 110 Plate Mill #1 & 2 Stack | 489029.6 | 4608811 | 54.5592 | 838.71 | 2.1336 | 4.4409 | 0.4 | 3-yr ave annual |
| 227 | AMBH | P6503 | 160 Plate Mill #1 Slab Reheat Furnace | 489014 | 4609043 | 54.2544 | 672.04 | 4.368802 | 3.1029 | 15.2 | 3-yr ave annual |
| 228 | AMBH | P6504 | 160 Plate Mill #2 Slab Reheat Furnace | 489035 | 4609043 | 54.2544 | 672.04 | 4.08432 | 3.2095 | 16.6 | 3-yr ave annual |
| 229 | AMBH | P6509 | 160 PM #5 IN/OUT REHEAT FURNACE | 489053.9 | 4609039 | 39.9288 | 783.15 | 12.476479 | 1.9507 | 0 | |
| 230 | AMBH | P6502 | 160 PM #7 IN/OUT REHEAT FURNACE | 489042.2 | 4608914 | 32.9184 | 783.15 | 9.987281 | 2.2372 | 0 | |
| 231 | AMBH | P6505 | 160 PM #8 BATCH FURNACE | 489042.2 | 4608894 | 50.9016 | 672.04 | 2.98704 | 1.7374 | 0 | |
| 232 | AMBH | P3018 | BATTERY #1 PECS | 488053.3 | 4608389 | 30.48 | 360.93 | 25.26585 | 2.4384 | 53.61 | 3-yr ave annual |
| 233 | AMBH | P3026 | #1 Underfire Coke Oven | 487967.9 | 4608346 | 76.8096 | 560.93 | 9.144 | 3.7795 | 1759.97 | Seasonal Varying |
| 234 | AMBH | P3024 | BATTERY #2 PECS | 488059.1 | 4608115 | 26.8224 | 360.93 | 25.26585 | 2.4384 | 60.7 | 3-yr ave annual |
| 235 | AMBH | P3027 | #2 Underfire Coke Oven | 487958.6 | 4608191 | 75.8952 | 560.93 | 9.144 | 4.0447 | 2261.91 | Seasonal Varying |
| 236 | AMBH | P3547 | C Furnace Stoves/Stacks (4 stoves) | 488244.3 | 4609339 | 61.2648 | 533.15 | 15.8496 | 3.4839 | 864.44 | Seasonal Varying |
| 237 | AMBH | P3560 | D Furnace Stoves/Stacks (4 stoves) | 488229.2 | 4609496 | 61.2648 | 533.15 | 14.894558 | 3.5936 | 1629.1 | Seasonal Varying |
| 238 | AMBH | P90A | HOT STRIP MILL #1 WALKING BEAM FCE E | 489029.2 | 4609235 | 96.012 | 810.93 | 7.061201 | 3.2004 | 21.8 | 3-yr ave annual |

Lake County DRR Source Modeling Inventory Point Sources

| | Company | Source ID | Source Description | East (X) (m) | North (Y) (m) | Stack Height (m) | Stack Temperature (K) | Exit Velocity (m/s) | Stack Diameter (m) | SO2 Emissions (tpy) | Emission Determination CEM/Varying/Annual |
|-----|---------|-----------|--|-----------------|------------------|---------------------|--------------------------|------------------------|-----------------------|------------------------|--|
| 239 | AMBH | P90B | HOT STRIP MILL #1 WALKING BEAM FCE W | 489009 | 4609235 | 96.012 | 810.93 | 7.061201 | 3.2004 | 21.8 | 3-yr ave annual |
| 240 | AMBH | P91A | HOT STRIP MILL #2 WALKING BEAM FCE E | 489051.1 | 4609236 | 96.012 | 810.93 | 7.02564 | 3.2004 | 11.3 | 3-yr ave annual |
| 241 | AMBH | P91B | HOT STRIP MILL #2 WALKING BEAM FCE W | 489030.1 | 4609235 | 96.012 | 810.93 | 7.02564 | 3.2004 | 11.3 | 3-yr ave annual |
| 242 | AMBH | P92A | HOT STRIP MILL #3 REHEAT FURNACE STACK E | 489069 | 4609236 | 41.4528 | 810.93 | 8.8392 | 3.9624 | 27.2 | 3-yr ave annual |
| 243 | AMBH | P92B | HOT STRIP MILL #3 REHEAT FURNACE STACK W | 489053.1 | 4609236 | 41.4528 | 810.93 | 8.8392 | 3.9624 | 27.2 | 3-yr ave annual |
| 254 | AMBH | P2501 | Power Station Boiler #7 | 488405.1 | 4609255 | 67.9704 | 505.37 | 14.43228 | 3.2004 | 879.84 | Seasonal Varying |
| 255 | AMBH | P3513 | SINTER PLANT WINDBOX SCRUBBER STACK | 488038.3 | 4609329 | 24.0792 | 322.04 | 13.9446 | 5.1816 | 702.78 | Seasonal Varying |
| 256 | AMBH | P4002 | STEELMAKING HMD STATION #1 | 488512.1 | 4609936 | 25.9111 | 305.37 | 12.948919 | 2.0513 | 10.7 | 3-yr ave annual |
| 257 | AMBH | P59 | STEELMAKING HMD STATION #2 | 488512 | 4609940 | 25.9111 | 305.37 | 5.887721 | 3.0389 | 10.7 | 3-yr ave annual |
| 260 | AMBH | P4008 | STEELMAKING HMD STATION #3 | 488514.6 | 4609952 | 12.192 | 319.26 | 12.948919 | 2.664 | 9.6 | 3-yr ave annual |
| 261 | AMBH | P3091 | Coke Oven Export Gas Flare | 487988 | 4608372 | 30.48 | 1922.04 | 9.397999 | 0.9144 | 1.8 | 3-yr ave annual |
| 262 | AMBH | P3540 | C Furnace BFG Flare (2 flareheads) | 488274.8 | 4609359 | 64.008 | 1088.71 | 41.57472 | 1.524 | 18.6 | 3-yr ave annual |
| 263 | AMBH | P3553 | D Furnace BFG Flare (2 flareheads) | 488278.3 | 4609495 | 64.008 | 1088.71 | 41.57472 | 1.524 | 18.64 | 3-yr ave annual |

AMUSA - ArcelorMittal - USA
 Cokenergy - Cokenergy, Inc
 AMIH - ArcelorMittal - Indiana Harbor
 Ironside - Ironside Energy, Inc
 US Steel - U.S. Steel - Gary Works
 BP AMOCO - BP Products - North America Inc.
 Carmeuse - Carmeuse Lime, Inc
 Koppers - Koppers Inc - Illinois
 AMBH - ArcelorMittal - Burns Harbor
 NIPSCO - NIPSCO Bailly Generating Station
 LaFarge - ISPAT Inland LaFarge North America
 Safety Kleen - Safety Kleen
 Eco Service - Eco Services Corp (formerly Rhodia, Solvay)

Lake County DRR Source Modeling Inventory Volume Sources

| | Company | Source ID | Source Description | East (X) | North (Y) | Release Height | Initial Horizontal Dimension | Initial Vertical Dimension | SO2 Emissions | Emission Determination CEM/Varying/Annual |
|----|---------|-----------|--------------------|----------|-----------|----------------|------------------------------|----------------------------|---------------|---|
| | | | | (m) | (m) | (m) | (m) | (m) | (tpy) | |
| 62 | AMIH | V3B1 | 3SP HMD Fugitives | 462672 | 4613541 | 16.15 | 2.23 | 7.51 | 0.278 | 3-yr ave annual |
| 63 | AMIH | V3B2 | 3SP HMD Fugitives | 462734 | 4613566 | 16.15 | 2.23 | 7.51 | 0.278 | 3-yr ave annual |
| 64 | AMIH | V3B3 | 3SP HMD Fugitives | 462717 | 4613529 | 16.15 | 2.23 | 7.51 | 0.278 | 3-yr ave annual |
| 65 | AMIH | V3B4 | 3SP HMD Fugitives | 462738 | 4613525 | 16.15 | 2.23 | 7.51 | 0.278 | 3-yr ave annual |
| 66 | AMIH | V1A1 | IH3 Casthouse | 462562 | 4612734 | 23.8 | 0.85 | 11.1 | 1.41 | 3-yr ave annual |
| 67 | AMIH | V1A2 | IH3 Casthouse | 462561 | 4612733 | 23.8 | 0.85 | 11.1 | 1.41 | 3-yr ave annual |
| 68 | AMIH | V1A3 | IH3 Casthouse | 462560 | 4612731 | 23.8 | 0.85 | 11.1 | 1.41 | 3-yr ave annual |
| 69 | AMIH | V1A4 | IH3 Casthouse | 462559 | 4612730 | 23.8 | 0.85 | 11.1 | 1.41 | 3-yr ave annual |
| 70 | AMIH | V1A5 | IH3 Casthouse | 462558 | 4612728 | 23.8 | 0.85 | 11.1 | 1.41 | 3-yr ave annual |
| 71 | AMIH | V1A6 | IH3 Casthouse | 462556 | 4612727 | 23.8 | 0.85 | 11.1 | 1.41 | 3-yr ave annual |
| 72 | AMIH | V1A7 | IH3 Casthouse | 462555 | 4612725 | 23.8 | 0.85 | 11.1 | 1.41 | 3-yr ave annual |
| 73 | AMIH | V1A8 | IH3 Casthouse | 462554 | 4612724 | 23.8 | 0.85 | 11.1 | 1.41 | 3-yr ave annual |
| 74 | AMIH | V1A9 | IH3 Casthouse | 462553 | 4612722 | 23.8 | 0.85 | 11.1 | 1.41 | 3-yr ave annual |
| 75 | AMIH | V1A10 | IH3 Casthouse | 462552 | 4612721 | 23.8 | 0.85 | 11.1 | 1.41 | 3-yr ave annual |
| 76 | AMIH | V1B1 | IH4 Casthouse | 462697 | 4612866 | 31.1 | 0.99 | 14.5 | 3.27 | 3-yr ave annual |
| 77 | AMIH | V1B2 | IH4 Casthouse | 462696 | 4612864 | 31.1 | 0.99 | 14.5 | 3.27 | 3-yr ave annual |
| 78 | AMIH | V1B3 | IH4 Casthouse | 462695 | 4612863 | 31.1 | 0.99 | 14.5 | 3.27 | 3-yr ave annual |
| 79 | AMIH | V1B4 | IH4 Casthouse | 462693 | 4612861 | 31.1 | 0.99 | 14.5 | 3.27 | 3-yr ave annual |
| 80 | AMIH | V1B5 | IH4 Casthouse | 462692 | 4612860 | 31.1 | 0.99 | 14.5 | 3.27 | 3-yr ave annual |
| 81 | AMIH | V1B6 | IH4 Casthouse | 462690 | 4612858 | 31.1 | 0.99 | 14.5 | 3.27 | 3-yr ave annual |
| 82 | AMIH | V1B7 | IH4 Casthouse | 462689 | 4612856 | 31.1 | 0.99 | 14.5 | 3.27 | 3-yr ave annual |

Lake County DRR Source Modeling Inventory Volume Sources

| | Company | Source ID | Source Description | East (X) | North (Y) | Release Height | Initial Horizontal Dimension | Initial Vertical Dimension | SO2 Emissions | Emission Determination |
|-----|----------|-----------|-------------------------|----------|-----------|----------------|------------------------------|----------------------------|---------------|------------------------|
| | | | | (m) | (m) | (m) | (m) | (m) | (tpy) | |
| 83 | AMIH | V1B8 | IH4 Casthouse | 462688 | 4612855 | 31.1 | 0.99 | 14.5 | 3.27 | 3-yr ave annual |
| 119 | US Steel | 221 | CB2UNDERFUG | 473900 | 4606300 | 19.9949 | 9.9974 | 9.9974 | 10.8 | |
| 120 | US Steel | 222 | CB5UNDERFUG | 473913 | 4606438 | 19.9949 | 9.9974 | 9.9974 | 1 | |
| 121 | US Steel | 447110 | #4 BF Casthouse Roof M | 472679.5 | 4606687.4 | 18.1051 | 4.2977 | 8.7996 | 6.32 | Emission Factor |
| 122 | US Steel | 447210 | #4 BF Casthouse Roof M | 472685.4 | 4606667.7 | 18.1051 | 4.2977 | 8.7996 | 6.32 | Emission Factor |
| 123 | US Steel | 447310 | #4 BF Casthouse Roof M | 472691.3 | 4606648 | 18.1051 | 4.2977 | 8.7996 | 6.32 | Emission Factor |
| 124 | US Steel | 447410 | #6 BF Casthouse Roof M | 472683 | 4606848 | 17.4986 | 4.2977 | 8.7996 | 6.34 | Emission Factor |
| 125 | US Steel | 447510 | #6 BF Casthouse Roof M | 472688.9 | 4606828.3 | 17.4986 | 4.2977 | 8.7996 | 6.34 | Emission Factor |
| 126 | US Steel | 447610 | #6 BF Casthouse Roof M | 472694.7 | 4606808.5 | 17.4986 | 4.2977 | 8.7996 | 6.34 | Emission Factor |
| 127 | US Steel | 447710 | #8 BF Casthouse Roof M | 472686.7 | 4606991.9 | 17.1999 | 4.2977 | 8.3972 | 5.9 | Emission Factor |
| 128 | US Steel | 447810 | #8 BF Casthouse Roof M | 472692.5 | 4606972.2 | 17.1999 | 4.2977 | 8.3972 | 5.9 | Emission Factor |
| 129 | US Steel | 447910 | #8 BF Casthouse Roof M | 472698.4 | 4606952.4 | 17.1999 | 4.2977 | 8.3972 | 5.9 | Emission Factor |
| 130 | US Steel | 448110 | #13 BF Casthouse RM | 472710.6 | 4607478.3 | 34.3997 | 6.3978 | 15.999 | 12.75 | Emission Factor |
| 131 | US Steel | 448210 | #13 BF Casthouse RM | 472713.1 | 4607461.2 | 34.3997 | 6.3978 | 15.999 | 12.75 | Emission Factor |
| 209 | AMBH | P133 | | 488222 | 4609449 | 50 | 16 | 3.6576 | 0 | |
| 210 | AMBH | P134 | | 488220 | 4609591 | 50 | 16 | 3.6576 | 0 | |
| 217 | AMIH | AMIH142 | | 461896 | 4610979 | 47.5488 | 4.9378 | 21.97 | 0 | |
| 218 | AMIH | AMIH165 | | 464750 | 4614615 | 21.9456 | 7.4981 | 1.4204 | 0 | |
| 219 | | F1C | | 462531 | 4612706 | 49.9994 | 15.999 | 12 | 37.5 | 3-yr ave annual |
| 220 | | F1D | | 462726 | 4612870 | 49.9872 | 15.999 | 12 | 69.5 | 3-yr ave annual |
| 221 | AMUSA | 171A | IH7 Casthouse Fugitives | 464721 | 4614598 | 21.9456 | 7.6352 | 19.56 | 0 | |
| 222 | AMUSA | 171B | IH7 Casthouse Fugitives | 464731 | 4614598 | 21.9456 | 7.6352 | 19.56 | 0 | |

Lake County DRR Source Modeling Inventory Volume Sources

| | Company | Source ID | Source Description | East (X) | North (Y) | Release Height | Initial Horizontal Dimension | Initial Vertical Dimension | SO2 Emissions | Emission Determination CEM/Varying/Annual |
|-----|---------|-----------|-------------------------|----------|-----------|----------------|------------------------------|----------------------------|---------------|---|
| | | | | (m) | (m) | (m) | (m) | (m) | (tpy) | |
| 223 | AMUSA | 171C | IH7 Casthouse Fugitives | 464741 | 4614598 | 21.9456 | 7.6352 | 19.559 | 0 | |
| 224 | AMUSA | 171D | IH7 Casthouse Fugitives | 464751 | 4614598 | 21.9456 | 7.6352 | 19.559 | 0 | |
| 244 | AMBH | PFE101 | | 488022.5 | 4608137.9 | 16.43 | 13.6 | 7.65 | 0.465817359 | 3-yr ave annual |
| 245 | AMBH | PFE102 | | 488023.4 | 4608163.5 | 16.43 | 13.6 | 7.65 | 0.465817359 | 3-yr ave annual |
| 246 | AMBH | PFE103 | | 488022.8 | 4608185.1 | 16.43 | 13.6 | 7.65 | 0.465817359 | 3-yr ave annual |
| 247 | AMBH | PFE104 | | 488023.1 | 4608208.7 | 16.43 | 13.6 | 7.65 | 0.465817359 | 3-yr ave annual |
| 248 | AMBH | PFE105 | | 488024.3 | 4608231.3 | 16.43 | 13.6 | 7.65 | 0.465817359 | 3-yr ave annual |
| 249 | AMBH | PFE201 | | 488012.9 | 4608305.6 | 16.43 | 13.6 | 7.65 | 0.465817359 | 3-yr ave annual |
| 250 | AMBH | PFE202 | | 488013.2 | 4608327.3 | 16.43 | 13.6 | 7.65 | 0.465817359 | 3-yr ave annual |
| 251 | AMBH | PFE203 | | 488012.7 | 4608349.1 | 16.43 | 13.6 | 7.65 | 0.465817359 | 3-yr ave annual |
| 252 | AMBH | PFE204 | | 488013.1 | 4608375.5 | 16.43 | 13.6 | 7.65 | 0.465817359 | 3-yr ave annual |
| 253 | AMBH | PFE205 | | 488013.9 | 4608397.5 | 16.43 | 13.6 | 7.65 | 0.465817359 | 3-yr ave annual |
| 258 | AMBH | BFDCHFUG | | 488240 | 4609560 | 24.7 | 21.4 | 3.5 | 14.53072061 | 3-yr ave annual |
| 259 | AMBH | BFCCHFUG | | 488242 | 4609426 | 24.7 | 21.4 | 3.5 | 14.53072061 | 3-yr ave annual |

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ENCLOSURE 3

Carmeuse Commissioner's Order



Indiana Department of Environmental Management

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Michael R. Pence
Governor

Carol S. Comer
Commissioner

STATE OF INDIANA)
COUNTY OF MARION) SS: BEFORE THE INDIANA DEPARTMENT
) OF ENVIRONMENTAL MANAGEMENT

IN THE MATTER OF:)
ORDER OF THE COMMISSIONER)
PURSUANT TO IC 13-14-2-1)
FOR CARMEUSE LIME INC.)

NOTICE AND ORDER OF THE COMMISSIONER OF THE DEPARTMENT OF ENVIRONMENTAL MANAGEMENT

This Notice and Order of the Commissioner of the Department of Environmental Management (“Order”) is issued pursuant to Indiana Code (“IC”) 13-14-1-9, IC 13-14-2-1, and IC 13-14-2-7. During the Commissioner’s review, it was determined that the Petition should be granted according to the terms specified below:

PETITION

Petitioner is Carmeuse Lime, Inc. (“Carmeuse” or “Petitioner”), a stationary lime manufacturing plant with Source I.D. Number 089-00112, located at 1 North Carmeuse Drive in Gary, Lake County, Indiana, and permitted under the Part 70 air operating permit program.

The United States Environmental Protection Agency (U.S. EPA) published the final Data Requirements Rule (DRR) for the 2010 1-hour SO₂ Primary National Ambient Air Quality Standard (NAAQS), in the *Federal Register* on August 21, 2015 (80 FR 51052). The DRR was promulgated in order to establish minimum requirements for air agencies to characterize 1-hour SO₂ air quality concentrations across the country, with an emphasis on doing so in the vicinity of sources that have the largest annual SO₂ emissions to aid in the implementation of the 2010 primary 1-hour SO₂ standard. Implementation of the new 1-hour SO₂ standard began in 2013 when U.S. EPA established nonattainment areas based on monitoring data. On March 2, 2015, U.S. EPA entered into a federal Consent Decree with the Sierra Club and Natural Resources Defense Council (NRDC) that established a timeline for the completion of air quality characterizations and designations in all remaining areas of the country. The Consent Decree required U.S. EPA to complete the designations in three additional rounds: Round 2 by July 2, 2016, Round 3 by December 31, 2017, and Round 4 by December 31, 2020.

On January 7, 2016, Indiana submitted to U.S. EPA a list of 11 stationary sources for air quality characterization pursuant to the DRR requirements as part of the Round 3 designation process. The DRR considers air dispersion modeling and ambient air monitoring appropriate ways to assess local SO₂ concentrations and the DRR also provides states with a third option to establish a permanent and federally enforceable facility-wide limit on SO₂ emissions from a

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listed source to below 2,000 tons per year. A source that limits its SO₂ emissions under the third option is not subject to the requirements for air quality characterization. Though the Petitioner is not one of the 11 stationary sources listed by IDEM and its SO₂ emissions are less than 2,000 tons per year, it has been identified by IDEM as a source that could impact overall SO₂ air quality in the area surrounding it.

On November 16, 2016, the Petitioner submitted a request to the Commissioner to impose permanent and enforceable SO₂ requirements on the Petitioner in order to ensure continued attainment of the 2010 1-hour SO₂ NAAQS in the area surrounding Carmeuse.

By January 13, 2017, the Indiana Department of Environmental Management ("IDEM") intends to recommend that Lake County be designated as attainment for the 2010 1-hour SO₂ NAAQS. The recommendation will be based on modeling that includes, among other requirements, permanent and enforceable SO₂ requirements at Carmeuse.

The Petitioner proposed that it be required to comply with emission rates for Rotary Kilns EU-1, EU-2, EU-3, EU-4, and EU-5 that would provide for modeled attainment of the 2010 1-hour SO₂ NAAQS.

FINDINGS

Pursuant to IC 13-14-2-1(b) and IC 13-14-2-7(1), the Commissioner may issue Orders to secure compliance with Indiana's environmental statutes and rules, and to impose emission limitations or other restrictions to demonstrate attainment of the ambient air quality standards, including the ambient air quality standard for SO₂ at 326 Indiana Administrative Code ("IAC") 1-3-4(b)(1)(A).

Petitioner's proposal and this Order are intended to support IDEM's intended recommendation that Lake County be designated as attainment for the 2010 1-hour SO₂ NAAQS.

Based on the foregoing information, IDEM finds the following:

1. Permanent and enforceable SO₂ emission requirements for Carmeuse are required in order to model continued attainment of the 2010 1-hour SO₂ NAAQS in areas surrounding the Petitioner.
2. Adding SO₂ emission requirements to the Petitioner's Part 70 Operating Permit is not adequately permanent to assure continued attainment of the 2010 1-hour SO₂ NAAQS. An Order of the Commissioner of IDEM is required to ensure SO₂ emission requirements remain permanent and enforceable, as required by 42 U.S.C. § 7407(d)(3)(E)(iii).
3. Approval by U.S. EPA of the Commissioner's Order into the Indiana State Implementation Plan ("SIP") is required to make the Order requirements federally enforceable. Upon approval into the Indiana SIP, the Order requirements become applicable requirements as defined in 326 IAC 2-7-1(6).
4. Based on modeling conducted by IDEM, the SO₂ emission rates in Order paragraph 2 are adequate to assure continued attainment of the 2010 1-hour SO₂ NAAQS.

ORDER

1. This Order approves the Petition submitted by the Petitioner according to the terms specified below. This Order imposes on Petitioner the SO₂ emission requirements described below.
2. Requirements:
 - a. The SO₂ emissions from Rotary Kilns EU-1, EU-2, EU-3, EU-4, and EU-5 shall not exceed nine and forty-eight hundredths (9.48) pounds per hour, each, calculated as a rolling seven hundred and twenty (720) operating hour average, per kiln.
3. The Petitioner shall comply with the requirements in Order paragraph 2, beginning seven (7) calendar days from the issuance of the permit modification required to allow the use of natural gas within the affected kilns, but no earlier than January 31, 2017.
4. As required by 326 IAC 2-7-2(d)(1) and 326 IAC 2-7-5, the Petitioner shall apply to incorporate these Order requirements as set forth in Order paragraphs 2 and 5 into its Part 70 Operating Permit within thirty (30) days of the effective date of U.S. EPA's approval of the requirements contained within this Commissioner's Order into the State Implementation Plan.
5. The Petitioner shall comply with the reporting, stack testing, compliance determination and recordkeeping requirements specified in this paragraph beginning seven (7) calendar days from the issuance of the permit modification required to allow the use of natural gas within the affected kilns, but no earlier than January 31, 2017.
 - a. Reporting: The Petitioner shall submit to IDEM, on a quarterly basis, a report of the SO₂ emissions in pounds per hour from each of Rotary Kilns #1 through #5 (EU-1 through EU-5) on a rolling seven hundred and twenty (720) operating hour average calculated for each kiln. Each report will be submitted not later than thirty (30) days after the end of the calendar quarter being reported.
 - b. Stack Testing: The Petitioner shall perform SO₂ testing of Rotary Kilns #1 through #5 (EU-1 through EU-5) utilizing methods approved by the Commissioner at least once every thirty (30) months from the date of the most recent valid stack test. The testing is required in order to develop the SO₂ scrubbing factors used to demonstrate compliance with the SO₂ emission rates in Order paragraph 2. Testing shall be conducted in accordance with the provisions of 326 IAC 3-6 (Source Sampling Procedures). Permit Condition C.8, Performance Testing, in Title V Permit No. T089-34191-00112 contains Petitioner's obligation with regard to the performance testing required herein. Representative sampling of the as-fed limestone, coal, engineered fuel (EF), and glycerin shall be conducted during each stack test run and the sulfur content analysis of the collected samples shall be included in the stack test report for development of the SO₂ scrubbing factor. Material sampling (as-fed during test) and analysis methods shall be included in the test protocol submitted to OAQ. Stack testing shall be conducted with limestone representative of the material processed in the kiln (dolomitic limestone or high calcium limestone). Testing shall be conducted for both dolomitic limestone and high calcium limestone if the kiln is used or is anticipated to be used to process both. The initial SO₂ stack test for each kiln shall occur no later than 180 days from the effective date as determined in Order paragraph 3. For kilns that process both dolomitic limestone and high calcium

limestone, the stack test for the second product processed in the kiln shall occur by the later of 180 days from the effective date as determined in Order paragraph 3 or 90 days after the second product is first processed, whichever occurs last.

- c. Compliance determination: Petitioner shall demonstrate compliance with the SO₂ emission rates in Order paragraph 2 above as follows:

Sampling, Analysis and Calculations:

- (i) Sampling: Each shipment of limestone, glycerin, engineered fuel (EF), and coal is sampled and analyzed by an independent laboratory, utilizing American Society for Testing and Materials (ASTM) standards for sampling and chemical analysis. The certified analyses that accompany each shipment shall be the source of the data of the sulfur content in both the limestone and coal calculation of the hourly SO₂ emissions for reporting. Either a certificate of analysis or certification that the EF complies with Carmeuse's specifications will be the source of the data of the sulfur content in the EF for calculation of the hourly SO₂ emissions for reporting. Information concerning the sulfur content of pipeline quality natural gas shall be the source of the data of the sulfur content in the natural gas. Pursuant to 326 IAC 7-4.1-2(c), the current sampling and analysis protocol to be used in lieu of certified analyses, certificates of analysis, or certification of compliance with Carmeuse's specifications for limestone, coal, glycerin, and/or EF is as follows:
- (a) The sample acquisition points shall be at locations where representative samples of the respective material shipments may be obtained.
 - (b) Minimum sample size shall be in accordance with ASTM specifications for representative samples in the size fraction and quantity delivered.
 - (c) Samples shall be composited and analyzed in accordance with ASTM specifications.
 - (1) For limestone, a sample shall be taken for each boat/barge load received and analyzed.
 - (2) For glycerin, a sample shall be taken for each truck load received and analyzed.
 - (3) For EF, analysis of a composite sample consisting of each truck load received per month.
 - (4) For coal, a sample shall be taken for each rail load received and analyzed.
 - (d) Preparation of the sample and sulfur content analysis, where applicable, shall be determined pursuant to 326 IAC 3-7-2(c), (d), and (e).
- (ii) For each kiln, the Petitioner shall calculate the SO₂ scrubbing factor for each product type as follows:

$$\text{Scrubbing Factor (SF)}_{\text{Kiln}(i) / \text{Product}(i)} = 1 - [\text{SO}_2, \text{stack test}(i) / (\text{S}_{\text{input STest}(i)} * 2 * 2000)]$$

Where, for purposes of this paragraph 5.c.(ii), $S_{\text{input STest}(i)}$ =

$$\begin{aligned} & [(\%S_{\text{limestone STest}(i)} \times \text{Usage}_{\text{limestone STest}(i)}) / 100] + \\ & [(\%S_{\text{coal STest}(i)} \times \text{Usage}_{\text{coal STest}(i)}) / 100] + \\ & [(\%S_{\text{glycerin STest}(i)} \times \text{Usage}_{\text{glycerin STest}(i)}) / 100] + \\ & [(\%S_{\text{EF STest}(i)} \times \text{Usage}_{\text{EF STest}(i)}) / 100] + \\ & [(S_{\text{natural gas STest}(i)} \times \text{Usage}_{\text{natural gas STest}(i)}) / (7000 \times 2000)] \end{aligned}$$

$\%S_{\text{STest}(i)}$ = weight percent sulfur in limestone, coal, glycerin or EF inputs, as applicable, as determined by sampling and analysis for the respective material input during the most recent valid stack test for Kiln(i) for the applicable product type (Product(i)).

$S_{\text{natural gas STest}(i)}$ = sulfur content of natural gas (grains/dscf) during the most recent valid stack test for Kiln(i) for the applicable product type (Product(i)).

$\text{Usage}_{\text{STest}(i)}$ = average limestone, coal, glycerin, EF or natural gas input to the kiln during the most recent valid stack test for Kiln(i) for the applicable product type (Product(i)) in tons/hr or dscf/hr as applicable.

The Petitioner shall recalculate the scrubbing factor within thirty (30) days after receiving the results of the most recent valid stack test for SO₂ for Kiln(i) for the applicable product type (Product(i)).

- (iii) The Petitioner shall calculate hourly SO₂ emissions (lb/hr) for each of Rotary Kilns #1 through #5 (EU-1 through EU-5) by the following calculations using the input values determined in Order paragraphs 5.c.(i) and 5.c.(ii) above:

$$SO_2 \text{ Emissions}_{\text{Kiln}(i)} \text{ (lb/hr)} = (1 - SF_{\text{Kiln}(i)/\text{Product}(i)}) \times S_{\text{input}} \times 2 \times 2000$$

Where

$SF_{Kiln(i)/Product(i)}$ = Scrubbing Factor value determined in Order paragraph 5.c.(ii) from most recent valid stack test for Kiln(i) for the applicable product type (Product(i)) for which the total sulfur input during the test was the same as or greater than the total sulfur input for the hour. If the total sulfur input for the hour is greater than the total sulfur input during the most recent valid stack test for Kiln(i) for the applicable product type (Product(i)), then the Scrubbing Factor value used shall be the value determined based on the results of the most recent prior valid stack test for Kiln(i) for the applicable product type (Product(i)) for which the total sulfur input during the test was the same as or greater than the total sulfur input for the hour.

Hour of operation is defined as any hour that fuel is being combusted within the affected kiln(s).

For the time period beginning seven (7) calendar days from the issuance of the permit modification required to allow the use of natural gas within the affected kilns, but no earlier than January 31, 2017 and the completion of the initial stack testing discussed in Order paragraph 5.b for each kiln and product type, Petitioner shall continue to use the existing scrubbing factors to calculate SO₂ emissions. However, following the development of new scrubbing factors based on the results of the initial stack tests for each kiln and product type, Petitioner shall recalculate the SO₂ emissions for the period beginning seven (7) calendar days from the issuance of the permit modification required to allow the use of natural gas within the affected kilns, but no earlier than January 31, 2017 to the date the new scrubbing factors were determined using the new scrubbing factors. If Petitioner has filed reports as required by Order paragraph 5.a based on the existing scrubbing factors, Petitioner shall submit revised reports based on the use of the new scrubbing factors.

When limestone or product is NOT present in a kiln, the SF shall be equal to zero (0).

For purposes of this paragraph 5.c.(iii), $S_{input} = [(\%S_{limestone} \times \text{Hourly Input}_{limestone}) / 100] + [(\%S_{coal} \times \text{Hourly Input}_{coal}) / 100] + [(\%S_{glycerin} \times \text{Hourly Input}_{glycerin}) / 100] + [(\%S_{EF} \times \text{Hourly Input}_{EF}) / 100] + [(S_{natural\ gas} \times \text{Hourly Input}_{natural\ gas}) / (7000 \times 2000)]$
 $\%S =$ weight percent sulfur in limestone, coal, glycerin or EF inputs, as applicable, as determined by the most recent vendor analysis or sampling, in accordance with 5.c.(i) - Sampling above.
 $S_{natural\ gas} =$ sulfur content of natural gas (grains/dscf).

Hourly Input = limestone, coal, glycerin, EF or natural gas input to the kiln in tons/hr or dscf/hr as applicable.

- (iv) The Petitioner shall calculate the rolling seven hundred and twenty (720) operating hour average SO₂ emissions (lbs/hr) for each Rotary Kiln #1 through #5 (EU-1 through EU-5) by adding the hourly SO₂ emissions calculated in Order paragraph 5.c.(iii) for each Rotary Kiln to the preceding seven hundred and nineteen (719) hours of operation for each rotary kiln, then divide by seven hundred and twenty (720) to derive the rolling average emissions per kiln per averaging period.
- d. Recordkeeping: The Petitioner shall maintain records of the sampling and analysis of raw material and fuels, certifications, other documentation, and the equations used to demonstrate compliance with the emission requirements in Order paragraph 2. These records shall be retained for a period of at least five (5) calendar years.

This Order shall apply to and be binding upon the Petitioner, its successors and assigns. No change in ownership, corporate, or partnership status of the Petitioner shall in any way alter its status or responsibilities under this Order.

Nothing in this Order shall prohibit future revisions to the emission rates in Order paragraph 2, including increases in such emission rates, provided such future revisions demonstrate continued attainment of the 1-hour SO₂ NAAQS, satisfy the requirements in Section 110(l) of the Clean Air Act (42 U.S.C. §7410(l)), and any necessary revisions to the applicable regulations and SIP are obtained.

EFFECTIVE DATE OF ORDER

Pursuant to IC 13-14-2-1(d), IC 4-21.5-3-1, IC 4-21.5-3-5(a)(6), and 40 CFR 51.102, IDEM will give notice of this Order to each entity to whom the Order is directed and affected neighbors by mailing and to the general public by publication.

Pursuant to IC 4-21.5-3-7(a)(3), IC 4-21.5-3-2(e), and IC 4-21.5-3-5, this Order may be appealed by a Petition for review within eighteen (18) days after the date affected persons were given notice of the Order by U.S. mail. Information on petitions for review of this Order can be found at IC 4-21.5-3-7 and 315 IAC 1-3-2.

Pursuant to IC 4-21.5-3-5(f) and IC 4-21.5-3-2(e), this Order is effective eighteen (18) days from mailing of the notice unless a Petition for review has been filed before or on the eighteenth (18th) day. However, the compliance date for the SO₂ emission requirements in Order paragraph 2 begins seven (7) calendar days from the issuance of the permit modification required to allow the use of natural gas within the affected kilns, but no earlier than January 31, 2017.

Pursuant to 40 CFR 51.103, IDEM will submit this Order to U.S. EPA as a revision to the Indiana SIP. Upon approval by the U.S. EPA, this Order will be part of the Indiana SIP.

Persons seeking judicial review of this Order may do so in accordance with IC 4-21.5-5.

If you have procedural or scheduling questions regarding your request for review, you may contact the Office of Environmental Adjudication at (317) 232-8591. If you have questions regarding this Order, please contact Betsy Zlatos, Office of Legal Counsel, by telephone at (317)233-5645 or email at bzlatos@idem.IN.gov.

Dated at Indianapolis, Indiana this 16th day of November, 2016.

A handwritten signature in black ink, appearing to read "Carol S. Comer", written over a horizontal line.

Carol S. Comer
Commissioner
Indiana Department of Environmental Management

ENCLOSURE 4

SABIC Commissioner's Order



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Michael R. Pence
Governor

Carol S. Comer
Commissioner

STATE OF INDIANA)
COUNTY OF MARION) SS: BEFORE THE INDIANA DEPARTMENT
) OF ENVIRONMENTAL MANAGEMENT

IN THE MATTER OF:)
ORDER OF THE COMMISSIONER)
PURSUANT TO IC 13-14-2-1)
FOR SABIC INNOVATIVE PLASTICS)
MT. VERNON, LLC)

NOTICE AND ORDER OF THE COMMISSIONER OF THE INDIANA DEPARTMENT OF ENVIRONMENTAL MANAGEMENT

On September 9, 2016, SABIC Innovative Plastics Mt. Vernon, LLC (SABIC) submitted a Petition to the Commissioner of the Indiana Department of Environmental Management (IDEM) that requested that the Commissioner limit the emissions of Sulfur Dioxide (SO₂) from SABIC's Mt. Vernon plant. The purpose of the petition request was to allow SABIC to limit its SO₂ emissions below the applicability threshold of the federal SO₂ Data Requirements Rule at 40 CFR 51 Subpart BB and concurrently ensure compliance with the 2010 1-hour SO₂ National Ambient Air Quality Standard (NAAQS). The Commissioner has determined that the Petition should be granted according to the terms specified below:

LEGAL BACKGROUND

SABIC Innovative Plastics Mt. Vernon, LLC owns a stationary integrated plastics and engineering resin manufacturing facility with Source I.D. Number 129-00002, located at 1 Lexan Lane in Mount Vernon, Posey County, Indiana, and permitted under the Part 70 air operating permit program.

The United States Environmental Protection Agency (U.S. EPA) published the final Data Requirements Rule (DRR) for the 2010 1-hour SO₂ Primary National Ambient Air Quality Standard (NAAQS), in the *Federal Register* on August 21, 2015 (80 FR 51052). The DRR was promulgated in order to establish minimum requirements for air agencies to characterize 1-hour SO₂ air quality concentrations across the country, with an emphasis on doing so in the vicinity of sources that have the largest annual SO₂ emissions to aid in the implementation of the 2010 primary 1-hour SO₂ standard. Implementation of the new 1-hour SO₂ standard began in 2013 when U.S. EPA established nonattainment areas based on monitoring data. On March 2, 2015, U.S. EPA entered into a federal Consent Decree with the Sierra Club and Natural Resources Defense Council (NRDC) that established a timeline for the completion of air quality characterizations and designations in all remaining areas of the country. The Consent Decree required U.S. EPA to complete the designations in three additional rounds: Round 2 by July 2, 2016, Round 3 by December 31, 2017, and Round 4 by December 31, 2020.

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On January 7, 2016, Indiana submitted to U.S. EPA a list of 11 stationary sources, including SABIC, for air quality characterization pursuant to the DRR requirements as part of the Round 3 designation process. The DRR considers air dispersion modeling and ambient air monitoring appropriate ways to assess local SO₂ concentrations and the DRR also provides states with a third option to establish a permanent and federally enforceable facility-wide limit on SO₂ emissions from a listed source to below 2,000 tons per year. A source that limits its SO₂ emissions under the third option is not subject to the requirements for air quality characterization.

Indiana informed U.S. EPA on June 30, 2016 that SABIC had selected the DRR modeling option to characterize the ambient air quality in the area. Subsequently, Indiana has learned that modifications made at the SABIC facility due to a Co-Gen project that was permitted as PSD/Significant Source Modification No.: 129-33998-00002 and issued on November 20, 2014 have resulted in the reduction of potential SO₂ emissions at the facility.

On September 9, 2016, SABIC submitted a request to the Commissioner to impose permanent and federally enforceable SO₂ emission limitations and emission rates on SABIC in order to ensure continued attainment of the SO₂ NAAQS in the area surrounding SABIC. SABIC proposed SO₂ emission limitations, applicable to specific emissions units and source-wide, as follows:

- a. Limitation on source-wide SO₂ emissions of 2,000 tons per year;
- b. Limitation on SO₂ emissions from 08-706 COS Vent Oxidizer and 08-708 COS Flare;
- c. Limitation on sulfur content of diesel fuel used in diesel-powered engines; and
- d. Limitation requiring coal-fired boilers (01-001 BW1-BOILER, 01-001 BW2-BOILER and 09-002 E-BOILER) at the facility to permanently cease operation prior to January 13, 2017.

Pursuant to IC 13-14-2-1(b) and IC 13-14-2-7(1), the Commissioner may issue Orders to secure compliance with Indiana's environmental statutes and rules, including the ambient air quality standard for SO₂ at 326 Indiana Administrative Code ("IAC") 1-3-4(b)(1)(A).

FINDINGS

Based on the foregoing information, IDEM, through its Commissioner, finds the following:

1. Permanent and enforceable SO₂ emission limitations and emission rates for SABIC are required that limit SO₂ emissions in order to provide assurance of attainment of the 2010 1-hour SO₂ NAAQS in the area surrounding SABIC's facility without continued assessment of the SO₂ concentrations through air dispersion modeling or ambient air monitoring.
2. Adding SO₂ emission limitations and emission rates to SABIC's Part 70 Operating Permit, while federally enforceable, is not permanent and, therefore, is not adequate to assure continued attainment of the SO₂ NAAQS. An Order of the Commissioner of IDEM (Order) is

required to ensure SO₂ emission limitations and emission rates remain permanent and enforceable, as required by 42 U.S.C. § 7407(d)(3)(E)(iii).

3. In addition, the approval by U.S. EPA of the Order into the Indiana State Implementation Plan ("SIP") is required to make the Order requirements permanent and federally enforceable. Upon approval into the Indiana SIP, the Order requirements become applicable requirements as defined in 326 IAC 2-7-1(6).

4. Based on modeling conducted by IDEM, the SO₂ emission limitations and emission rates proposed by SABIC were clarified and adjusted in order to assure continued attainment of the 1-hour SO₂ NAAQS. The annual source-wide SO₂ limitation of 2,000 tons was not necessary in order to demonstrate compliance with the DRR.

This Notice and Order of the Commissioner of the Indiana Department of Environmental Management (Order) is issued pursuant to Indiana Code (IC) 13-14-1-9, IC 13-14-2-1, and IC 13-14-2-7.

ORDER

1. SO₂ emission limitations and emission rates are set forth below for the following emission units: 01-101 NE BOILER, 01-014 BW GAS, 08-706 COS Vent Oxidizer, 08-707 COS Flare, 12-701 H-790, 03-007 H-520, 03-008 H-530A, 03-008 H-530B, 12-169 H-390, 13-049 H-900, 13-321 H-900B, 13-155 SC-1/2, 04-063 H-7090, 04-050 H-6060, 08-001 F-972, 19-001 COGEN, 19-002 AUX BOILER, 19-003 AUX2 BOILER, 19-004 CG1 BOILER, 09-106 R BOILER.

2. The COS Vent Oxidizer and the COS Flare shall not exceed the following SO₂ emission rates:

- a. 415 lb/hr, one (1) hour average; and
- b. 269.21 lb/hr, twenty-four (24) hour rolling average, based on daily coke usage and daily sulfur input.

3. The NE BOILER (01-101) shall not exceed an SO₂ emission rate of 0.15 lb/hr, one (1) hour average.

4. The BW GAS (01-014) shall not exceed an SO₂ emission rate of 0.15 lb/hr, one (1) hour average.

5. The H-790 (12-701) shall not exceed an SO₂ emission rate of 0.02 lb/hr, one (1) hour average.

6. The H-520 (03-007) shall not exceed an SO₂ emission rate of 0.0045 lb/hr, one (1) hour average.

7. The H-530A (03-008) shall not exceed an SO₂ emission rate of 27.8 lb/hr, one (1) hour average.

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8. The H-530B (03-008) shall not exceed an SO₂ emission rate of 27.8 lb/hr, one (1) hour average.
9. The H-390 (12-169) shall not exceed an SO₂ emission rate of 0.0102 lb/hr, one (1) hour average.
10. The H-900 (13-049) shall not exceed an SO₂ emission rate of 1.86 lb/hr, one (1) hour average.
11. The H-900B (13-321) shall not exceed an SO₂ emission rate of 0.0188 lb/hr, one (1) hour average.
12. The SC 1/2 (13-155) shall not exceed an SO₂ emission rate of 0.0008 lb/hr, one (1) hour average.
13. The H-7090 (04-063) shall not exceed an SO₂ emission rate of 0.00235 lb/hr, one (1) hour average.
14. The H-6060 (04-050) shall not exceed an SO₂ emission rate of 0.00153 lb/hr, one (1) hour average.
15. The F-972 (08-001) shall not exceed an SO₂ emission rate of 0.518 lb/hr, one (1) hour average.
16. The COGEN (19-001) shall not exceed an SO₂ emission rate of 1.17 lb/hr, one (1) hour average.
17. The AUX BOILER (19-002) shall not exceed an SO₂ emission rate of 0.15 lb/hr, one (1) hour average.
18. The AUX2 BOILER (19-003) shall not exceed an SO₂ emission rate of 0.15 lb/hr, one (1) hour average.
19. The CG1 BOILER (19-004), if constructed, shall not exceed an SO₂ emission rate of 0.15 lb/hr, one (1) hour average.
20. The R BOILER (09-106) shall not exceed an SO₂ emission rate of 0.11 lb/hr, one (1) hour average.
21. To achieve the SO₂ emission rate and emission limitation in Paragraph 2.a, daily sulfur input to the carbon monoxide generators, identified as COG1, COG2, COG3, COG4, COG5, COG6, COG7, COG8, COG9, COG10, COG11, COG12, COG13, COG14, COG15, and COG16, shall be limited to no more than 2.49 tons per day.
22. All site emergency generators and pumps, standby energy curtailment diesel generators and mobile diesel units, temporary and portable emergency generators shall operate on No. 2 diesel fuel containing 15 parts per million (ppm) by weight or less of sulfur.
23. SABIC shall comply with the SO₂ emission limitations and emission rates, and the No. 2 diesel fuel sulfur content limit, beginning January 13, 2017.

24. As required by 326 IAC 2-7-2(d)(1) and 326 IAC 2-7-5, SABIC shall apply to incorporate Order requirements, including reporting and recordkeeping requirements and methods to determine compliance, into its Part 70 Operating Permit within ninety (90) days of U.S. EPA approval of the Commissioner's Order into the Indiana SIP.

25. From January 13, 2017 until IDEM issues a Permit incorporating Order requirements, SABIC shall comply with the reporting and recordkeeping requirements and methods to determine compliance specified in this paragraph.

a. Reporting: SABIC shall submit to IDEM, on a quarterly basis, a report of the daily coke input and corresponding sulfur content for the COS Vent Oxidizer and COS Flare.

b. Recordkeeping: SABIC shall maintain records of daily coke input and corresponding sulfur content, and sulfur content of No. 2 diesel fuel.

c. Method to determine compliance: Compliance shall be determined on a daily basis, based on 326 IAC 3-5.

i. Daily sulfur input for the group of carbon monoxide generators (COG1-16), calculated by taking the daily coke usage and multiplying by the percent weight of corresponding sulfur content.

ii. The sulfur content of the coke used in the carbon monoxide generators shall be analyzed daily as received (vendor delivery analysis may be used, approved by IDEM on 08/01/2005) for each day the carbon monoxide generators operate.

iii. Actual fuel usage for natural gas, diesel and fuel oil and liquid waste fuel-fired emission units or, in the alternative, the maximum design fuel usage.

26. This Order shall apply to and be binding upon SABIC, its successors and assigns. No change in ownership, corporate, or partnership status of SABIC shall in any way alter its status or responsibilities under this Order.

27. The requirements of this Order supersede any less stringent requirements applicable to SABIC.

EFFECTIVE DATE OF ORDER

Pursuant to IC 13-14-2-1(d), IC 4-21.5-3-1, IC 4-21.5-3-5(a)(6), and 40 Code of Federal Regulations ("CFR") 51.102, IDEM will give notice of this Order to each entity to whom the Order is directed and affected neighbors by mailing and to the general public by web publication.

Pursuant to IC 4-21.5-3-7(a)(3), IC 4-21.5-3-2(e), and IC 4-21.5-3-5, this Order may be appealed by filing a Petition for review within eighteen (18) days after the date affected persons were given notice of the Order by U.S. mail. Information on petitions for review of this Order can be found at IC 4-21.5-3-7.

Pursuant to IC 4-21.5-3-5(f) and IC 4-21.5-3-2(e), the Order is effective eighteen (18) days from mailing of notice unless a Petition for review has been filed before or on the eighteenth (18th) day. However, the compliance date for the emission limitations in this Order is January 13, 2017.

Pursuant to 40 CFR 51.103, IDEM will submit this Order to U.S. EPA as a revision to the Indiana SIP. Upon approval by the U.S. EPA, this Order will be part of the Indiana SIP.

Persons seeking judicial review of this Order may do so in accordance with IC 4-21.5-5.

If you have procedural or scheduling questions regarding your request for review, you may contact the Office of Environmental Adjudication at (317) 232-8591. If you have questions regarding this Order, please contact Mark Derf, Office of Air Quality, by telephone at (317) 233-5682 or email at MDERF@idem.IN.gov.

Dated at Indianapolis, Indiana this 20th day of October, 2016.

A handwritten signature in cursive script that reads "Carol S. Comer". The signature is written in black ink and is positioned above a horizontal line.

Carol S. Comer
Commissioner
Indiana Department of Environmental Management

Attachment 3

U.S. Mineral Products (Isolatek) Discussion

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U.S. Mineral Products (Isolatek - Source ID: 069-00021)

The Indiana Department of Environmental Management (IDEM) excluded U.S. Mineral Products (USM) d/b/a Isolatek International, a mineral wool manufacturer near Huntington, Indiana in Huntington County, from its January 7, 2016 list of affected sources to be characterized under the Data Requirements Rule (DRR). Per the thresholds established within the DRR, USM's most current reported sulfur dioxide (SO₂) emissions were well below levels required for the rule to be applicable. However, United States Environmental Protection Agency (U.S. EPA) identified USM as an additional source to be characterized in its March 25, 2016 response to IDEM.

Indiana strongly objects to the inclusion of USM as an affected source under the DRR. The DRR defines applicable sources as stationary sources that had actual SO₂ emissions in 2014 of 2,000 tons or more, or have been identified by IDEM or U.S. EPA "as requiring further air quality characterization." (40 CFR § 51.1202). Indiana did not include USM on its list of sources subject to the DRR because its reported actual SO₂ emissions in 2014 were 164 tons, less than one tenth of the DRR threshold of 2,000 tons or more. According to U.S. EPA's calculations (based on an informal in-house 2007 stack test), USM's actual annual emissions would have been "approximately 444 tons of SO₂" in 2014. U.S. EPA also determined that 2014 was an abnormally low year for production and estimated 800 tons of SO₂ per year during normal production years, which is still less than half the DRR emission threshold. USM has seen a downturn since 2013 in its wool production (approximately 40,000 tons/year could be considered a prior normal), with a slight bounce back to 28,000 to 30,000 tons per year production over the last few years. This is still much lower than historic production, but should be considered the current normal production at the facility based upon current economic factors with the economy.

USM has operated the same equipment at its Huntington facility since 1982. In its March 25, 2016, letter, U.S. EPA indicated an emission factor of 21.6 lb SO₂ per ton of melt was appropriate for the USM cupola emissions. USM has historically used an emission factor of 8 lbs/ton based upon U.S. EPA's Compilation of Air Pollutant Emission Factors, AP-42.¹ As a result of a Clean Air Act (CAA) §114 information request, USM submitted to U.S. EPA, a summary sheet from stack tests previously conducted which included some engineering studies from 2007 and several pages from the 2007 study report for in-house testing of particulate matter (PM), nitrogen oxides (NO_x) and SO₂ at the facility. That study included an informational emission test for SO₂ for the cupola that was only performed in the downdraft ducts. The results were reported in the summary sheet and in the study report. USM does not consider 21.6 lbs/ton

¹ An emission factor of 0.2 lbs/hr was used from 2000 through 2005 as a result of an error in the data used for the annual emission calculation. When the correction was made in 2005, IDEM advised USM that it was not necessary to correct the prior emission statements.

to be a valid SO₂ emission factor due to problems with the cupola operation at the time of the informal test. It should be noted that IDEM did not review or approve of an SO₂ stack test protocol in 2007 for USM and had no compliance inspector present at the informal SO₂ test. According to production records available for the time period on and around the stack testing days in December 2007, the following may be concluded as summarized by USM:

On Dec 17th, the first day of the testing, both cupolas were idled in the morning for a period exceeding 2 hours each due to an electrical problem with a charge hoist. In addition, #1 cupola idled for 3 hours directly preceding the hoist issue due to a spinner motor failure. Typically, following an idle period of time, the cupola operating conditions take some time (could easily be several hours) to stabilize. Thus, the testing period started with less than normal conditions.

On Dec 18th, during the period of the testing for SO₂ data collection, #1 cupola went through a period of increased coke consumption and reduced melt rate. Both indicators were showing a variation from standard coke consumption and melt rate in the 10% - 20% order of magnitude. USM standard coke consumption is expected to be at ~320 – 340 lbs / ton of charge and the avg. melt rate at ~4.2 tons / hr. At the time of the stack test USM recorded an avg. of 360 – 380 lbs of coke / charge and a melt rate of ~3.9 tons / hr respectively. These variations are considered significant and clearly not normal operations. Those conditions are related and indicate that the operator was attempting to overcome the slower melt rate by adding additional coke to the charge. Based upon the increased coke consumption and slower melt rate, general operating conditions at the time of testing are best described as poor. The raw material receivers from that period of time indicate a higher than normal moisture content in received coke (10%-15% vs. standard of <7%) explaining the need for additional BTUs with every charge to evaporate the excess moisture. The low moisture content of coke is a critical factor to the cupola performance. During the period of time in 2007 around when the testing was performed, the USM coke supplier was struggling to provide a product with acceptable quality. The coke quality issues were caused by operational issues at the source. USM had no viable, alternative supply options at the time.

In order to resolve the emission factor issue, in 2016, USM conducted an engineering study of the cupola emissions. This consisted of an informational emission test that included SO₂ measured in the baghouse. That test indicated an SO₂ emission factor range of 9.22 to 9.36 lbs/ton. The results of the 2016 test confirm that the emission factor from AP-42 is appropriate to use for the USM mineral wool cupola operation. Additionally, the 164 tons of SO₂ reported as actual emissions for USM should be considered valid for DRR purposes. This is significantly lower than what U.S. EPA is attempting to rely upon in its analysis.

U.S. EPA identified the 2,000 ton threshold as an important indicator of the need for prioritized air quality characterization under the DRR. U.S. EPA set the threshold at a level “that prioritizes the resources that will be devoted to characterizing air quality near SO₂ sources nationally.” (80

FR 51061). That threshold is already on “the lower end of the range of thresholds” of sources that have the potential to contribute to violations of the National Ambient Air Quality Standard (NAAQS) (80 FR 51061). Furthermore, that threshold “strikes a reasonable balance between the need to characterize air quality near sources that have a higher likelihood of contributing to a NAAQS violation and the analytical burden on air agencies.” (80 FR 51061). U.S. EPA did not characterize the 2,000 ton threshold as an arbitrary number, but rather as an indicator of sources warranting prioritization of state and federal resources.

Because USM’s actual SO₂ emissions and total potential-to-emit SO₂ emissions remain well below the 2,000 ton applicability threshold, it is unreasonable to place it among the sources that should be prioritized to determine if it contributes to violations of the NAAQS. Including sources with actual SO₂ emissions of less than one-tenth the 2,000 ton threshold represents a misapplication of the intent of the DRR to prioritize sources and resources. Indiana believes that this reinterpretation of the DRR inappropriately broadens the scope and purpose of this phase of the DRR. There are numerous sources across the United States that fall into a similar category as USM. In Indiana alone, there are thirty five (35) sources with reported actual emissions between that of USM and the 2,000 ton threshold. Among these is a manufacturer of mineral wool, with very similar operational characteristics, with reported actual emissions greater than that of USM, and sources located in densely populated areas with as much as ten times the reported emissions of USM, which happens to be located in a sparsely populated rural area. Based on familiarity with how the dispersion model handles certain operations, it is safe to assume that some of these sources would clearly pose a greater threat to the NAAQS and human health than USM. Therefore, U.S. EPA’s identification of USM is clearly arbitrary and capricious.

Due to the time constraints that U.S. EPA has placed on states to implement the DRR, broadening the applicability of the DRR’s phased approach thwarts the rule’s intent to prioritize state and federal resources. IDEM does not question whether the DRR provides states or U.S. EPA the authority to identify sources with actual emissions below the 2,000 ton threshold as requiring further air quality characterization. However, if this is done, it should be done consistently and not arbitrarily. U.S. EPA did not use a systematic approach to identify sources below 2,000 tons that have the greatest probability to pose a risk to exceeding the NAAQS and threaten human health. Therefore, IDEM disagrees that USM should be arbitrarily subjected to further characterization under the DRR.

Table 1: U.S. Mineral Products (Isolatek) 2016 Stack Test Data

Table 1. Measured & Calculated Data-Melters' Process Line EU#1 & EU#2 CE#1 Baghouse

| Summary of Stack Gas Parameters and Test Results | | | | | |
|--|---|-----------|-----------|----------|--|
| 50668.0003 | | | | | |
| Isolatek | | | | | |
| Baghouse | | | | | |
| Page 1 of 2 | | | | | |
| | | 1-O2 | 2-O2 | O2 | |
| | RUN NUMBER | 4/28/2016 | 4/28/2016 | Average | |
| | RUN DATE | | | | |
| | RUN START | 11:30 | 12:50 | | |
| | RUN STOP | 12:18 | 13:48 | | |
| MEASURED DATA | | | | | |
| P _{static} | Stack Static Pressure, Inches H ₂ O | 0.00 | 0.00 | 0.00 | |
| y | Meter Box Correction Factor | 0.976 | 0.976 | 0.976 | |
| P _{bar} | Barometric Pressure, Inches Hg | 29.95 | 29.95 | 29.95 | |
| V _m | Sample Volume, ft ³ | 48.165 | 49.453 | 48.809 | |
| Dp ^{1/2} | Average Square Root Dp, (In. H ₂ O) ^{1/2} | 1.0948 | 1.1172 | 1.106 | |
| DH | Avg Meter Orifice Pressure, In. H ₂ O | 3.271 | 3.402 | 3.336 | |
| T _m | Average Meter Temperature, °F | 86.3 | 86.5 | 86.4 | |
| T _s | Average Stack Temperature, °F | 230.3 | 231.3 | 230.8 | |
| V _c | Condensate Collected, ml | 16.0 | 13.0 | 14.50 | |
| CO ₂ | Carbon Dioxide content, % by volume | 0.0 | 0.0 | 0.00 | |
| O ₂ | Oxygen content, % by volume | 20.8 | 20.8 | 20.8 | |
| N ₂ | Nitrogen content, % by volume | 79.2 | 79.2 | 79.2 | |
| C _o | Pitot Tube Coefficient | 0.84 | 0.84 | 0.84 | |
| | Circular Stack? 1=Y, 0=N: | 1 | 1 | | |
| A _s | Diameter or Dimensions, Inches: | 37.00 | 37.00 | 37.00 | |
| Q | Sample Run Duration, minutes | 48 | 48 | 48 | |
| D _n | Nozzle Diameter, Inches | 0.238 | 0.238 | 0.238 | |
| CALCULATED DATA | | | | | |
| A _n | Nozzle Area, ft ² | 0.000309 | 0.000309 | 0.000309 | |
| V _{m(Std)} | Standard Meter Volume, ft ³ | 45.82 | 47.05 | 46.44 | |
| V _{m(Std)} | Standard Meter Volume, m ³ | 1.298 | 1.332 | 1.315 | |
| Q _m | Average Sampling Rate, dscfm | 0.955 | 0.980 | 0.967 | |
| P _s | Stack Pressure, Inches Hg | 29.95 | 29.95 | 29.95 | |
| B _{ws} | Moisture, % by volume | 1.6 | 1.3 | 1.5 | |
| B _{w(Std)} | Moisture (at saturation), % by volume | 142.1 | 145.0 | 143.6 | |
| V _{w(Std)} | Standard Water Vapor Volume, ft ³ | 0.753 | 0.612 | 0.683 | |
| 1-B _{ws} | Dry Mole Fraction | 0.984 | 0.987 | 0.985 | |
| M _d | Molecular Weight (d.b.), lb/lb-mole | 28.83 | 28.83 | 28.83 | |
| M _s | Molecular Weight (w.b.), lb/lb-mole | 28.66 | 28.69 | 28.67 | |
| V _s | Stack Gas Velocity, ft/s | 70.5 | 72.0 | 71.2 | |
| A | Stack Area, ft ² | 7.5 | 7.5 | 7.5 | |
| Q _v | Stack Gas Volumetric flow, acfm | 31,587 | 32,238 | 31,912 | |
| Q _s | Stack Gas Volumetric flow, dscfm | 23,786 | 24,320 | 24,053 | |
| Q _h | Stack Gas Volumetric flow, dscmm | 674 | 689 | 681 | |
| I | Isokinetic Sampling Ratio, % | 97.0 | 97.4 | 97.2 | |

Table 2. PM, NO_x, CO, & SO₂ Emissions Test Results- Melters' Process Line EU#1 & EU#2 CE#1 Baghouse

| Summary of Stack Gas Parameters and Test Results | | | | | | |
|--|-----------|-----------|---------|--|--|--|
| 50668.0003 | | | | | | |
| Isolatek | | | | | | |
| US EPA Test Method 5 (PM), 6C (SO ₂), 7E (NO _x), 10 (CO), 15/16 (H ₂ S/COS), & 26A (HCL/HF) | | | | | | |
| Baghouse | | | | | | |
| Page 2 of 2 | | | | | | |
| RUN NUMBER | 1-02 | 2-02 | O2 | | | |
| RUN DATE | 4/28/2016 | 4/28/2016 | Average | | | |
| RUN START | 11:30 | 12:50 | | | | |
| RUN STOP | 12:18 | 13:48 | | | | |
| EMISSIONS DATA | | | | | | |
| Throughput (tons/hr) | 10.135 | 9.564 | 9.85 | | | |
| Sulfur Dioxide | | | | | | |
| SO ₂ Concentration PPM Dry | 393.67 | 368.85 | 381.26 | | | |
| E SO ₂ Emission Rate, lb/hr | 93.40 | 89.48 | 91.44 | | | |
| E SO ₂ Emission Rate, lb/ton | 9.22 | 9.36 | 9.29 | | | |

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Attachment 4

Alcoa Warrick Attainment Discussion

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ALCOA Warrick Power Plant (Source ID: 173-00007) and Warrick Operations (Source ID: 173-00002)

Aluminum Manufacturing Company of America (ALCOA) operates an aluminum manufacturing facility and power plant in Newburgh, Indiana, along the northern bank of the Ohio River in Anderson Township, Warrick County. The Indiana Department of Environmental Management (IDEM) believes Warrick Power Plant and Warrick Operations and the surrounding area should be designated attainment based on historical sulfur dioxide (SO₂) ambient monitoring data showing attainment of the SO₂ standard.

Warrick Power and Warrick Operations were determined to be sources subject to United States Environmental Protection Agency's Data Requirements Rule (DRR) based on actual 2014 SO₂ emissions of 4,993 tons and 3,500 tons, respectively. However, Warrick Operations shut down its smelter operations as of March 31, 2016, and has therefore ceased to generate potline point SO₂ emissions, potline smelter line source SO₂ emissions, or SO₂ emissions from the anode baking ring furnace. Warrick Operations currently operates a rolling mill that uses natural gas and will generate SO₂ emissions of less than one ton per year.

Historical SO₂ data from monitors operated by ALCOA prior to the shut-down of the smelter show attainment of the 2010 primary SO₂ 1-hour National Ambient Air Quality Standard (NAAQS). Tables 1 and 2 provide data from SO₂ monitors operated by ALCOA for several years prior to the smelting operation's shutdown. The tables also show data from the SO₂ monitor that IDEM operates in the region near the ALCOA Warrick facility.

As shown in the tables, all 99th percentile values since 2009 are below the 1-hour standard. In addition, the most recently available design value (2008 – 2010), and all recent partial-year design values, are also below the 1-hour standard. These low monitor values occurred during the time when the operations plant and the power plant were in full operation. As such, it is reasonable to conclude that the area surrounding the ALCOA Warrick facilities is in attainment of the 1-hour SO₂ NAAQS. As such, Indiana is recommending Anderson Township, Warrick County, Indiana as attainment.

Table 1: Warrick County SO₂ Monitor Data - 99th Percentile Values
(parts per billion) (2005 – 2016)

| Site ID | 2005 | 2006 | 2007 | 2008 | 2009 | 2010 | 2011 | 2012 | 2013 | 2014 | 2015 | 2016 |
|----------------|-----------------|------|------|------|------|------|-----------------|------|------|------|------|-----------------|
| IDEM Operated | | | | | | | | | | | | |
| 181630021 | 66 | 67 | 69 | 41 | 17 | 18.8 | 19.4 | 16.5 | 18.6 | 32.3 | 18 | 11 ^a |
| ALCOA Operated | | | | | | | | | | | | |
| 181730002 | 143 | 199 | 103 | 111 | 38 | 18 | Not Operational | | | | 23 | 36 ^b |
| 181730004 | Not Operational | | | | | | | | | | 63 | 57 ^b |
| 181730005 | Not Operational | | | | | | | | | | 46 | 42 ^b |
| 181730012 | Not Operational | | | | | | | | | | 59 | 62 ^b |

^a – Data through July 31, 2016.

^b – Data through June 30, 2016.

Table 2: Warrick County SO₂ Monitor Data – Design Values
(parts per billion) (2007 – 2016)

| Site ID | 2005 - 2007 | 2006 - 2008 | 2007 - 2009 | 2008 - 2010 | 2009 - 2011 | 2010 - 2012 | 2011 - 2013 | 2012 - 2014 | 2013 – 2015 | 2014 – 2016 |
|----------------|-----------------|----------------|----------------|----------------|-----------------|----------------|----------------|----------------|-----------------|-----------------|
| IDEM Operated | | | | | | | | | | |
| 181630021 | 67 | 59 | 43 | 26 | 18 | 18 | 18 | 22 | 23 | 21 |
| ALCOA Operated | | | | | | | | | | |
| 181730002 | 148 | 138 | 84 | 56 | Not Operational | | | | 23 ^a | 30 ^b |
| 181730004 | Not Operational | | | | | | | | 63 ^a | 60 ^b |
| 181730005 | Not Operational | | | | | | | | 46 ^a | 44 ^b |
| 181730012 | Not Operational | | | | | | | | 59 ^a | 61 ^b |

^a – Based on one year of data.

^b – Based on two years of data.

Attachment 5

ArcelorMittal – Burns Harbor SO₂ Air Quality Monitor
System Documentation

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U.S. EPA Confirmation Letter for Siting Methodologies of ArcelorMittal Burns Harbor SO₂ Monitor



UNITED STATES ENVIRONMENTAL PROTECTION AGENCY
REGION 5
77 WEST JACKSON BOULEVARD
CHICAGO, IL 60604-3590

AUG 5 2018

REPLY TO THE ATTENTION OF

AT-18J

Mr. Mark Derf
Office of Air Quality
Indiana Department of Environmental Quality
Indiana Government Center North
100 North Senate Avenue
Indianapolis, Indiana 46204

Dear Mr. Derf:

The purpose of this letter is to respond to your request for concurrence with the siting recommendation for a sulfur dioxide (SO₂) air quality monitor near the ArcelorMittal-Burns Harbor facility, located in Porter County, Indiana. The monitor is being sited in response to the designation process detailed in EPA's Data Requirements Rule for SO₂. This new monitor will supplement an existing monitor.

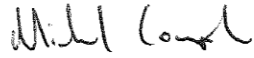
We have reviewed your June 2016 Monitoring Protocol document and, based on the air quality modeling conducted by the facility and IDEM, agree that the western boundary of the ArcelorMittal facility is the best location for a monitor. Additionally, based on information provided to Region 5 by IDEM, the availability of land on the western border that would be considered ambient air and available for lease is extremely limited. This resulted in your recommendation that the existing lead monitor site is the best available location. This site is represented by the green dot in Figure 13.3 of the IDEM protocol document. Region 5 agrees that the placement of a monitor at the location of the existing lead site is acceptable. This will augment the existing SO₂ monitor located on the eastern edge of the facility.

While this letter confirms our agreement that the addition of a single monitor located at the existing lead monitor site is acceptable based on air quality modeling conducted in accordance with EPA's Monitoring Technical Assistance Document and site specific accessibility information, this letter does not confirm that the proposed site will meet each of the monitor siting requirements specified in 40 CFR part 58 Appendix E. Prior to beginning installation, IDEM should evaluate and ensure this site will meet those criteria and provide Region 5 with the results of your monitor siting assessment showing that all criteria will be able to be met at this proposed location.

Recycled/Recyclable • Printed with Vegetable Oil Based Inks on 50% Recycled Paper (20% Postconsumer)

Thank you for the advanced coordination on this issue. If you have any questions or need additional information, please contact Randy Robinson at 312 353-6713 or Jesse McGrath at 312 886-1532.

Sincerely,

A handwritten signature in black ink, appearing to read "Michael Compher". The signature is written in a cursive style with a large initial "M" and a long, sweeping underline.

Michael Compher
Chief
Air Monitoring and Analysis Section

Enclosures

U.S. EPA's Approval of IDEM's 2017 Ambient Air Monitoring Network Plan



UNITED STATES ENVIRONMENTAL PROTECTION AGENCY
REGION 5
77 WEST JACKSON BOULEVARD
CHICAGO, IL 60604-3590

OCT 31 2016

REPLY TO THE ATTENTION OF:
AT-18J

Mr. Keith Baugues
Assistant Commissioner
Office of Air Quality
Indiana Department of Environmental Management
100 North Senate Avenue
Indianapolis, IN 46204-2251

Dear Mr. Baugues:

The U.S. Environmental Protection Agency has reviewed the Indiana Department of Environmental Management's 2017 Ambient Air Monitoring Network Plan and approves the plan and proposed changes to your network of air quality monitors, but for the following:

- Lead emissions from the Crane Division Naval Surface Warfare Center have increased from the time of IDEM's original waiver from 1.2 tons/year to 2.3 tons/year. In light of this increase, EPA requires that IDEM either operate a lead monitor at this facility, or request a waiver which demonstrates that lead values will not exceed 50% of the NAAQS.
- EPA has reviewed the analyses in Appendix B and does not approve exclusion of the PM_{2.5} Federal Equivalent Method data at sites 18-141-0015 or 18-163-0021 from comparison to the NAAQS. Where IDEM determines specific daily values are erroneous and can identify the causes of the error, IDEM should invalidate the specific data, rather than exclude all data from comparison to the NAAQS.

EPA evaluated the plan, as well as information about monitoring sites submitted to the Air Quality System database, and confirmed, with the above exceptions, that IDEM's network meets the siting and operation requirements of 40 CFR Part 58.

Additionally, EPA has reviewed and approves IDEM's lead monitoring waivers in Appendix D for the ALCOA Warrick Power Plant in Warrick County, and Ardagh Glass Inc. in Randolph County, as per 40 CFR Part 58 Appendix D section 4.5(ii).

If you determine that changes to your monitoring network are needed due to unplanned circumstances or revisions to the federal ambient monitoring and quality assurance requirements, the modifications must be reviewed and approved by EPA.

If you have any questions, please contact Michael Compher, Air Monitoring and Analysis Section Chief, at (312) 886-5745.

Sincerely,

A handwritten signature in blue ink, appearing to read "Ed Nam".

Ed Nam
Acting Director
Air and Radiation Division

Clean Air Engineering Certifications for ArcelorMittal Burns Harbor's SO₂ Monitor



Ambient SO₂ Monitoring System Factory Acceptance Test Protocol and Checklist

1

2 **Clean Air Project Information**

| | |
|------------------------|-------------------------------|
| Project Number: | 13075 |
| Project Manager: | Jack Demkovich |
| Purchaser: | ArcelorMittal |
| Installation Location: | Port of Indiana, Burns Harbor |

3 **System Information**

| | |
|-----------------------|-------------------------|
| System Type: | SO ₂ Ambient |
| System Serial Number: | N/A |
| System Site ID: | TBD |
| Date Installed: | 12-7-17 |

4 **FAT Test Information**

| | |
|------------------------|-----------------------------|
| Test Date: | 12/8 - 12/13/2016 |
| Test Site: | Final Installation Location |
| Test Supervisor: | Jack Demkovich |
| Test Engineer: | Jack Demkovich |
| Witness & Affiliation: | -- |
| | |
| | |
| | |

5 **Instructions:**

- 6 Use check boxes to acknowledge completion of each step.
- 7 Note status of each completed test as follows: PASS/FAIL/SEE COMMENTS.
- 8 A Comments page is included at the end of the document.
- 9 Comments are required for any test marked FAIL and for deviations from this checklist.
- 10 Comments must reference a form line number.
- 11 Test Engineer(s) and Witness(es) to sign this form upon completion.

12 **System Documentation**

13 *Attach the following documents for inspection*

- 14 Major Component Serial ID list
- 15 Calibration Reference Certifications
- 16 Project Drawings
- 17 QAPP *Draft version subject to final approval by IDEM*

18 **System Documentation:** PASS FAIL SEE COMMENTS

19

20 **System Physical Inspection**

- 21 Primary system components are available for inspection
- 22 Shelter dimensions match construction drawings
- 23 Shelter interior layout matches construction drawings
- 24 Shelter construction materials correspond to construction specifications
- 25 Shelter electrical service matches construction specifications
- 26 Voltage: 240 Phase: 1 Current: 100A @ 240V
- 27 Shelter HVAC matches construction specifications:
- 28 Heat BTU: _____ Cooling BTU: 2 ton SN: L163362236
- 29 Site specific labeling (if applicable) is installed & meets specification
- 30 Analyzer #1 Mfg: THERMO Model: 43i Gas: SO2
- 31 Analyzer #2 Mfg: N/A Model: N/A Gas: N/A
- 32 Analyzer #3 Mfg: N/A Model: N/A Gas: N/A
- 33 Calibrator Mfg: THERMO Model: 146i
- 34 Logger Mfg: AGILAIRE Model: 8872
- 35 UPS Mfg: APC Model: SMART UPS 1500
- 36 Other Mfg: N/A Model: N/A
- 37 Other Mfg: N/A Model: N/A
- 38 Other Mfg: N/A Model: N/A
- 39 Number of PCs supplied = Server PC (Pittsburgh), Logger PC & Monitor
- 40 I/O components include:
- 41 Ethernet switch
- 42 Cellular Modem, Carrier: ATT Number: 2245323513
- 43 Cloud Backup, Provider: Wellkeeper Number: 5056972685

44

45

46 **Physical Inspection:** PASS FAIL SEE COMMENTS

47 **Component IP Address List**

| 48 | IP Verified | Component | IP Address |
|----|-------------------------------------|-----------------|--|
| 49 | <input checked="" type="checkbox"/> | MODEM | 192.168.13.31:9191 |
| 50 | <input checked="" type="checkbox"/> | AGILAIRE LOGGER | 192.168.13.101 |
| 51 | <input checked="" type="checkbox"/> | 43i | 192.168.13.102 |
| 52 | <input checked="" type="checkbox"/> | 146i | 192.168.13.103 |
| 53 | <input type="checkbox"/> | | |
| 54 | <input type="checkbox"/> | | |
| 55 | <input type="checkbox"/> | | |
| 56 | <input type="checkbox"/> | | |
| 57 | <input type="checkbox"/> | | |
| 58 | <input type="checkbox"/> | | |
| 59 | IP Verification: | | PASS <input checked="" type="checkbox"/> FAIL <input type="checkbox"/> SEE COMMENTS <input type="checkbox"/> |

61 **HVAC Operation Verification**

| | | | |
|----|-------------------------------------|---|--|
| 62 | <input checked="" type="checkbox"/> | Set HVAC temperature to 25°C (78°F) | |
| 63 | <input checked="" type="checkbox"/> | Energize sampling system | |
| 64 | <input checked="" type="checkbox"/> | Initiate sampling (all shelter-housed components must be operational) | |
| 65 | <input checked="" type="checkbox"/> | Allow system to operate for at least 3 days | |
| 66 | <input checked="" type="checkbox"/> | Retrieve hourly data logs at completion of the test period | |
| 67 | <input checked="" type="checkbox"/> | Verify HVAC operation: | |
| 68 | | • Start Date & Time: <u>12-10-16, 09:00</u> | |
| 69 | | • End Date & Time: <u>12-13-16, 08:00</u> | |
| 70 | | • Min cabinet temperature: <u>24.7</u> | |
| 71 | | • Max cabinet temperature: <u>25.1</u> | |
| 72 | <input checked="" type="checkbox"/> | All data within ±2°C (3.6°F): | |
| 73 | <input checked="" type="checkbox"/> | All data within 20° to 30°C, (68° to 86°F): | |
| 74 | HVAC Operation Verified: | | PASS <input checked="" type="checkbox"/> FAIL <input type="checkbox"/> SEE COMMENTS <input type="checkbox"/> |

75 **Sampling System Inspection**

- 76 Sampling system is complete with:
- 77 Inverted Funnel Inlet
- 78 Support System
- 79 Calibration Tee at Funnel
- 80 Filter
- 81 Moisture Trap
- 82 All components Teflon or glass
- 83 All components are new and clean
- 84 Exhaust tubing installed
- 85 All system interconnecting tubing is installed
- 86 Funnel inlet is 3 to 6 m (10-20 ft) above ground: 3.84
- 87 Inlet distance to nearest obstruction: m: 1.1 DISTANCE TO ROOF TOP
- 88 Sample Flow Rate L/min: 0.495
- 89 Sample Line Vacuum inHg: 0.16
- 90 Tubing ID (1/8 inch): cm: 0.318
- 91 Estimated Length (25 ft): cm: 520
- 92 Volume of tubing: cm³: 41.3
- 93 Volume of Trap/Filter: cm³: 50.0 total vol= 91.3
- 94 Calculate residence time: sec: 11.06
- 95 Residence time < 20 seconds? YES

Sampling System Inspection: PASS FAIL SEE COMMENTS

96

97

98 **System Startup and Communication Verification**

- 99 Energize all system components and allow system to fully start up
- 100 Open calibration gas regulator
- 101 Enter Agilaire logger software
- 102 Use a remote PC with Team Viewer to verify connectivity
- 103 Verify logger time and date, reset if necessary
- 104 Verify EnviroNics 7000 operating temperature is 300°C
- 105 Verify EnviroNics 7000 output pressure is set to 25psi
- 106 Verify EnviroNics 7000 dewpoint indicator is BLUE
- 107 Verify no alarms are present on the Thermo 146i
- 108 Verify no alarms are present on the Thermo 43i

| | | Logger | Instrument | Units | %Diff | PASS (<1%) |
|-----|--|--------|------------|---------|-------|-------------------------------------|
| 109 | <input checked="" type="checkbox"/> Verify the following parameters are updating and logger and instrument displays agree: | | | | | |
| 110 | | | | | | |
| 111 | <input checked="" type="checkbox"/> SO2 - Thermo 43i - Logger display | 2.09 | 2.08 | ppb | 0.5% | <input checked="" type="checkbox"/> |
| 112 | <input checked="" type="checkbox"/> SO2 Internal Temp (SO2INTTP) | 35 | 35 | °C | 0.0% | <input checked="" type="checkbox"/> |
| 113 | <input checked="" type="checkbox"/> SO2 Chamber Temp (SO2CHMTP) | 45.3 | 45.3 | °C | 0.0% | <input checked="" type="checkbox"/> |
| 114 | <input checked="" type="checkbox"/> SO2 Chamber Press (SO2CHMPR) | 730.6 | 730.6 | mmHg | 0.0% | <input checked="" type="checkbox"/> |
| 115 | <input checked="" type="checkbox"/> SO2 Sample Flow (SO2FLOW) | 0.494 | 0.494 | l/min | 0.0% | <input checked="" type="checkbox"/> |
| 116 | <input checked="" type="checkbox"/> SO2 PMT Volts (SO2PMTVT) | -721.5 | -721.5 | V | 0.0% | <input checked="" type="checkbox"/> |
| 117 | <input checked="" type="checkbox"/> SO2 Flash Volts (SO2FLSVT) | 1006.2 | 1006 | V | 0.0% | <input checked="" type="checkbox"/> |
| 118 | <input checked="" type="checkbox"/> SO2 Lamp Intensity (SO2LUNT) | 92.0 | 92.0 | % | 0.0% | <input checked="" type="checkbox"/> |
| 119 | <input checked="" type="checkbox"/> SO2 Background (SO2BCKGR) | 2.11 | 2.11 | ppb | 0.0% | <input checked="" type="checkbox"/> |
| 120 | <input checked="" type="checkbox"/> SO2 Cal Coefficient (SO2COEFF) | 1.012 | 1.012 | N/A | 0.0% | <input checked="" type="checkbox"/> |
| 121 | <input checked="" type="checkbox"/> Cal Gas Concentration (CALGAS) | 400.0 | 400 | ppb | 0.0% | <input checked="" type="checkbox"/> |
| 122 | <input checked="" type="checkbox"/> Cal Gas Target Flow (CALTARG) | 37.7 | 37.70 | scc/min | 0.0% | <input checked="" type="checkbox"/> |
| 123 | <input checked="" type="checkbox"/> Cal Gas Actual Flow (CALACTL) | 37.7 | 37.66 | scc/min | 0.1% | <input checked="" type="checkbox"/> |
| 124 | <input checked="" type="checkbox"/> Cal Gas Zero Gas Target Flow (CALZTRG) | 2000 | 2000 | scc/min | 0.0% | <input checked="" type="checkbox"/> |
| 125 | <input checked="" type="checkbox"/> Cal Gas Zero Gas Actual Flow (CALZACT) | 1996 | 1996 | scc/min | 0.0% | <input checked="" type="checkbox"/> |
| 126 | <input checked="" type="checkbox"/> Cal Gas Total Target Flow (CALTOTTG) | 2000 | 2000 | scc/min | 0.0% | <input checked="" type="checkbox"/> |
| 127 | <input checked="" type="checkbox"/> Cal Gas Total Actual Flow (CALTOTAC) | 1996 | 1996 | scc/min | 0.0% | <input checked="" type="checkbox"/> |
| 128 | <input checked="" type="checkbox"/> Cal Gas Pressure (CALGSPRS) | 1873.9 | 1862 | scc/min | 0.6% | <input checked="" type="checkbox"/> |
| 129 | <input checked="" type="checkbox"/> Sample Line Vacuum (SMPLNVAC) | 0.16 | N/A | inHg | N/A | <input checked="" type="checkbox"/> |
| 130 | <input checked="" type="checkbox"/> AC Power Loss (ACPWRLOSS) | 0.7 | N/A | V | N/A | <input checked="" type="checkbox"/> |
| 131 | <input checked="" type="checkbox"/> Low UPS Battery (LOWBATT) | 1 | N/A | V | N/A | <input checked="" type="checkbox"/> |
| 132 | <input checked="" type="checkbox"/> Cal Zero Gas Pressure (ZAGPRESS) | 26.5 | 26.5 | psi | 0.0% | <input checked="" type="checkbox"/> |
| 133 | <input checked="" type="checkbox"/> Shelter Temperature (SHLTTEMP) | 25.9 | N/A | °C | N/A | <input checked="" type="checkbox"/> |
| 134 | System Startup Successful: PASS <input checked="" type="checkbox"/> FAIL <input type="checkbox"/> SEE COMMENTS <input type="checkbox"/> | | | | | |

135 *System should be running for at least 24 hours and be calibrated before calibration verification*

136 **Multipoint Calibration Verification**

- 137 Trigger the Multipoint Calibration cycle through the logger
 138 Allow the calibration cycles to complete
 139 Complete a Multipoint Calibration form using logger data
 140 Attach completed form to this document

141 **Multipoint Calibration Verified:** PASS FAIL SEE COMMENTS

142

143 **One-Point Quality Control (Precision) Check Verification**

- 144 Trigger the One-Point Quality Control Check through the logger
 145 Allow the cycle to complete
 146 Complete a One-Point QC Check form using logger data
 147 Attach completed form to this document

148 **One-Point QC Check Verified:** PASS FAIL SEE COMMENTS

149

150 **Data Validation (DV) Check Verification**

- 151 Trigger the Data Validation Check through the logger
 152 Allow the cycle to complete
 153 Complete a Data Validation check form using logger data
 154 Attach completed form to this document

155 **DV Check Verified:** PASS FAIL SEE COMMENTS

156

157 **Automated Span Drift Verification**

- 158 Allow the system to operate for at least 24 hours
 159 Allow at least one automated cycle to complete
 160 Manually poll Calibration Results from logger into AirVision
 161 Attach Calibration Report generated through AirVision to this document

162 **Automated Span Verified:** PASS FAIL SEE COMMENTS

163

164 **Automated Zero Drift Verification**

- 165 Allow the system to operate for at least 24 hours
 166 Allow at least one automated cycle to complete
 167 Manually poll Calibration Results from logger into AirVision
 168 Attach Calibration Report generated through AirVision to this document

168 **Automated Zero Verified:** PASS FAIL SEE COMMENTS

169

170 **Shelter Ambient Temperature Sensor Calibration Verification**

- 171 Perform a shelter temp sensor calibration per the SOP
 172 Complete the Shelter TC Calibration form
 173 Attach completed form to this document

174 **Shelter Temp Sensor Cal Verified:** PASS FAIL SEE COMMENTS

175 **Data Backup Verification**

176 *Allow system to run under normal operation conditions for 3 days*

177 **Agilaire 8872 Logger Backup**

178 Open folder "C:\SQL_Database_Backups_for_AVTrend" on the Agilaire 8872 Logger

179 AVData.bak file is present in folder

180 Date modified of AVData.bak is the current date, time modified is 04:30

181 Open folder "Weekly_Backups"

182 All files are named "8872_AVBackup_MMDDYY_hhmmss"

183 Date modified of newest file is the most recent Sunday

184 No files older than 14 days old

185 No more than two files in folder

186 Open Z: drive

187 AVData.bak file is only file present in Z:

188 Date modified of AVData.bak is the current date, time modified is 04:30

189 **Agilaire 8872 Logger Backup:** PASS FAIL SEE COMMENTS

190

191 **AirVision Server Backup**

192 Open the folder "C:\SQL_Database_Backups_For_AirVision" on the AirVision Server

193 AVData.bak file is present in folder

194 Date modified of AVData.bak is the current date, time modified is 04:30

195 Open folder "Weekly_Backups"

196 All files are named "Server_AVBackup_MMDDYY_hhmmss"

197 Date modified of newest file is the most recent Sunday

198 No files older than 14 days old

199 No more than two files in folder

200 **AirVision Server Backup:** PASS FAIL SEE COMMENTS

201

202 **Dropbox Backup**

203 Open the folder "C:\Users\mrclean\Dropbox (CleanAir)\13075_ArcelorMittal_SO2

204 **_Backup_Data_SERVER"** on the AirVision Server

205 AVData.bak file is present in folder

206 Date modified of AVData.bak is the current date, time modified is 04:30

207 In the Dropbox folder, open "13075_ArcelorMittal_SO2_Backup_Data_TEXT"

208 1-Minute_Data folder is present

209 5-Minute_Data folder is present

210 Hourly_Data folder is present

211 Open "1-Minute_Data" folder

212 Several .CSV files are present, all with format "RAW_1MIN_Data_Mmddyyyy.csv"

213 Date modified of most recent file is the current date, time modified is XX:XX

214 When file is opened, opens Excel, is populated, and is easily readable

215 Open "5-Minute_Data" folder

216 Several .CSV files are present, all with format "RAW_5MIN_Data_Mmddyyyy.csv"

217 Date modified of most recent file is the current date, time modified is XX:XX

218 When file is opened, opens Excel, is populated, and is easily readable

219 Open "Hourly_Data" folder

220 Several .CSV files are present, all with format "RAW_HOUR_Data_Mmddyyyy.csv"

221 Date modified of most recent file is the current date, time modified is XX:XX

222 When file is opened, opens Excel, is populated, and is easily readable

223 **Dropbox Backup Verified:** PASS FAIL SEE COMMENTS

System Equipment List

PROJECT: ArcelorMittal USA / Job No: 13073
 INSTALLATION LOCATION: Burns Harbor, IN
 STATION ID: _____

| ITEM | EQUIPMENT | MANUFACTURER | MODEL | SERIAL NUMBER | OPERATIONAL DATE |
|------|------------------------------------|-----------------------|-------------------------|---------------|------------------|
| 1 | SO2 Analyzer | Thermo Scientific | 43iTLE | 1162320006 | 12/10/2016 |
| 2 | Gas Dilution Calibrator | Thermo Scientific | 146i | 1162320005 | 12/10/2016 |
| 3 | Data Control System | Agilair | 8872 | 0609 | 12/10/2016 |
| 4 | Zero Air Generator (ZAG) | EnviroNics | 7000 | 7223 | 12/10/2016 |
| 5 | Temperature Probe | Agilair | R5-232 Air Temp Sensor | RTD-01 | 12/10/2016 |
| 6 | Cylinder Gas Pressure Transmitter | Ashcroft | GC35 | 6600057 R | 12/10/2016 |
| 7 | Cylinder Gas Regulator | Scott Specialty Gases | 51215A660 | 817334 | 12/10/2016 |
| 8 | ZAG Output Pressure Transmitter | Dwyer | 628-09-GH-P1-E1-S1 | 13075PT1 | 12/10/2016 |
| 9 | Sample Vacuum Pressure Transmitter | ControllerSensors | 860-0.00/30.00-I-12-I-P | 8100040 | 12/10/2016 |
| 10 | Uninterruptible Power Supply | APC | SUA1500RM2U | A50733130756 | 12/10/2016 |
| 11 | | | | | |
| 12 | | | | | |
| 13 | | | | | |
| 14 | | | | | |
| 15 | | | | | |

Transfer Standard Certification Schedule

PROJECT: ArcelorMittal USA / Job No: 13075

INSTALLATION LOCATION: Burns Harbor, IN

STATION ID: _____

| ITEM | EQUIPMENT | MANUFACTURER | MODEL | SERIAL NUMBER | CYLINDER NUMBER | CERTIFICATION DATE | RECERTIFICATION DATE |
|------|---------------------------|-------------------|--------|---------------|-----------------|--------------------|----------------------|
| 1 | Gas Dilution Calibrator | Thermo Scientific | 146i | 1162320005 | -- | 11/29/2016 | 5/29/2017 |
| 2 | Station SO2 Gas Standard | Airgas | N/A | -- | CC7590 | 11/29/2016 | 5/29/2017 |
| 3 | Digital Thermometer | Omega | HH370 | 160407973 | -- | 12/5/2016 | 12/5/2017 |
| 4 | Temperature Probe | Omega | RS-232 | RTD-01 | -- | 12/8/2016 | 6/8/2017 |
| 5 | Audit Gas Standard | Airgas | N/A | -- | -- | -- | -- |
| 6 | Audit UHP Zero Air | Airgas | N/A | -- | -- | -- | -- |
| 7 | Audit Dilution Calibrator | EnviroNics | 6100 | -- | -- | -- | -- |
| 8 | | | | | | | |
| 9 | | | | | | | |
| 10 | | | | | | | |
| 11 | | | | | | | |
| 12 | | | | | | | |
| 13 | | | | | | | |
| 14 | | | | | | | |
| 15 | | | | | | | |

**INDIANA DEPARTMENT OF ENVIRONMENTAL MANAGEMENT
OFFICE OF AIR QUALITY**

CERTIFICATION - AIR MASS FLOW METER

Cert Type Agency Cert Date Recert Date Performed By
 90 CLEAN AIR ENGINEERING 28-NOV-2016 28-MAY-2017 ALDAVIDS

Transfer Standard
 Flow Meter SN Brand Model Calibrator SN Brand Model
 1162320005-A THERMO 1461 1162320005 THERMO 1461

Previous Flow Meter Certification **Primary Flow Standard**
 Slope Intercept Cert Date Standard SN Brand Model Type
 1.00000 0.00000 378+ / 790+ FLUKE / AIR MOLBLOC MASS FLOW

| Air/Dil Meter Setting | Std Flow (L/min) | Curve Flow (L/min) | Pct Diff (%) | Pass/Fail | Current Curve Flow (L/min) | Prev Curve Flow (L/min) | Pct Diff (%) |
|--------------------------|---------------------|-----------------------|-----------------|-----------|-------------------------------|----------------------------|-----------------|
| 0.538 | 0.5380 | 0.5380 | 0.0 | PASS | 0.5380 | 0.5380 | 0.0 |
| 2.009 | 2.0090 | 2.0090 | 0.0 | PASS | 2.0090 | 2.0090 | 0.0 |
| 3.427 | 3.4270 | 3.4270 | 0.0 | PASS | 3.4270 | 3.4270 | 0.0 |
| 4.838 | 4.8380 | 4.8380 | 0.0 | PASS | 4.8380 | 4.8380 | 0.0 |
| 6.245 | 6.2450 | 6.2450 | 0.0 | PASS | 6.2450 | 6.2450 | 0.0 |
| 7.685 | 7.6850 | 7.6850 | 0.0 | PASS | 7.6850 | 7.6850 | 0.0 |
| 9.199 | 9.1990 | 9.1990 | 0.0 | PASS | 9.1990 | 9.1990 | 0.0 |
| | | | | | | | |

Comments: FLOWS ENTERED INTO MFC TABLE FOR SLOPE INTERCEPT OF 1/0. 4 FLOWS CHECKED AFTERWARDS AND FOUND TO ALL BE WITHIN 1% OF ACTUAL FLOW. CERTIFICATION GOOD TILL 11/28/17 DUE TO THIS BEING A BENCH CALIBRATOR.

Slope Intercept Corr Coef
 1.00000 0.00000 1.00000

RECERTIFICATION IS DUE: 28-MAY-2017

**INDIANA DEPARTMENT OF ENVIRONMENTAL MANAGEMENT
OFFICE OF AIR QUALITY**

CERTIFICATION - GAS MASS FLOW METER

Cert Type Agency Cert Date Recert Date Performed By
 90 CLEAN AIR ENGINEERING 28-NOV-2016 28-MAY-2017 ALDAVIDS

Transfer Standard

| | | | | | |
|---------------|--------|-------|---------------|--------|-------|
| Flow Meter SN | Brand | Model | Calibrator SN | Brand | Model |
| 1162320005-G | THERMO | 146I | 1162320005 | THERMO | 146I |

Previous Flow Meter Certification

| | | |
|---------|-----------|-----------|
| Slope | Intercept | Cert Date |
| 1.00000 | 0.00000 | |

Primary Flow Standard

| | | | |
|-------------|---------------------|-------|-----------|
| Standard SN | Brand | Model | Type |
| 378+ / 788+ | FLUKE / GAS MOLBLOC | | MASS FLOW |

| Gas Meter Setting | Std Flow (cc/min) | Curve Flow (cc/min) | Pct Diff (%) | Pass/Fail | Current Curve Flow (cc/min) | Prev Curve Flow (cc/min) | Pct Diff (%) |
|-------------------|-------------------|---------------------|--------------|-----------|-----------------------------|--------------------------|--------------|
| 2.608 | 2.6080 | 2.6080 | 0.0 | PASS | 2.6080 | 2.6080 | 0.0 |
| 10.069 | 10.0690 | 10.0690 | 0.0 | PASS | 10.0690 | 10.0690 | 0.0 |
| 17.471 | 17.4710 | 17.4710 | 0.0 | PASS | 17.4710 | 17.4710 | 0.0 |
| 24.819 | 24.8190 | 24.8190 | 0.0 | PASS | 24.8190 | 24.8190 | 0.0 |
| 32.142 | 32.1420 | 32.1420 | 0.0 | PASS | 32.1420 | 32.1420 | 0.0 |
| 39.532 | 39.5320 | 39.5320 | 0.0 | PASS | 39.5320 | 39.5320 | 0.0 |
| 48.100 | 48.1000 | 48.1000 | 0.0 | PASS | 48.1000 | 48.1000 | 0.0 |
| | | | | | | | |

Comments

FLows ENTERED INTO MFC TABLE FOR SLOPE/INTERCEPT OF 1/0. 4 FLOWS CHECKED AFTERWARDS AND FOUND TO BE LESS THAN 0.1% DIFFERENT FROM TRUE FLOW. CERT GOOD UNTIL 11/28/17 DUE TO THIS BEING A BENCH CALIBRATOR THAT WILL BE AT ONE STATION.

| | | |
|---------|-----------|-----------|
| Slope | Intercept | Corr Coef |
| 1.00000 | 0.00000 | 1.00000 |

RECERTIFICATION IS DUE: 28-MAY-2017

**INDIANA DEPARTMENT OF ENVIRONMENTAL MANAGEMENT
OFFICE OF AIR QUALITY**

CERTIFICATION - SO₂, DILUTION WITH MASS FLOW

Cert Type Agency Cert Date Recert Date Performed By
 10 CLEAN AIR ENGINEERING 29-NOV-2016 29-MAY-2017 ALDAVIDS

Transfer Standard

| | | | | | | |
|---------------|--------|-------|--------------|--------|-----------|----------------|
| Calibrator SN | Brand | Model | Cylinder SN | Brand | Prev Conc | Prev Cert Date |
| 1162320005 | THERMO | 1461 | CLEAN CC7590 | AIRGAS | | |

Transfer Analyzer

| | | | | | | |
|------------|-------------|-------|---------|-----------|------------------|-------------------|
| SN | Brand | Model | Slope | Intercept | Calibration Date | Verification Date |
| 0524312232 | THERMO E.C. | 431 | 1.00138 | -0.00050 | 29-NOV-2016 | 13-DEC-2006 |

Primary Standard

| | | | | | | |
|---------------|-------|-------|-------------|------|-------------|---------------|
| Calibrator SN | Brand | Model | Standard SN | Type | Brand | Concentration |
| 462-S | API | 700E | ND47923 | | AIR LIQUIDE | 49.0800 |

Mass Flow Meter Last Certification

| | | | | | | | | | | | |
|-----------|---------|---------------|---------|----------------------------|---------|---------------|---------|----------------------|--|-------------|------|
| Gas Slope | 1.00000 | Gas Intercept | 0.00000 | Analyzer Zero Resp (volts) | -0.0003 | Avg Calc Conc | 10.6100 | Pct Diff Avg vs Prev | | **Pass/Fail | FAIL |
| Air Slope | 1.00000 | Air Intercept | 0.00000 | | | | | | | | |

| Gas | Air/Dilution | Gas (cc/min) | Total (cc/min) | Analyzer Resp (volts) | Meas Conc (ppm) | Calc Conc (ppm) | Pct Diff for Avg Conc | *Pass/Fail |
|-------|--------------|--------------|----------------|-----------------------|-----------------|-----------------|-----------------------|------------|
| 45.00 | 2.00 | 45.00 | 2,045.0 | 0.234 | 0.234 | 10.62 | 0.1 | PASS |
| 40.00 | 3.00 | 40.00 | 3,040.0 | 0.141 | 0.140 | 10.66 | 0.4 | PASS |
| 32.00 | 3.00 | 32.00 | 3,032.0 | 0.112 | 0.112 | 10.58 | -0.2 | PASS |
| 25.00 | 3.00 | 25.00 | 3,025.0 | 0.088 | 0.088 | 10.60 | -0.1 | PASS |
| 25.00 | 4.00 | 25.00 | 4,025.0 | 0.066 | 0.066 | 10.58 | -0.3 | PASS |

Comments **Certified Cylinder Concentration (ppm): 10.6100 Recertification is Due: 29-MAY-2017**

* PASS if Pct Diff of Avg vs Calc is less than + - 4.0%. All data points must PASS for a valid certification.
 ** PASS if Pct Diff of Current vs Previous is less than + - 5.0%. If Fail, see Comment.

**INDIANA DEPARTMENT OF ENVIRONMENTAL MANAGEMENT
OFFICE OF AIR QUALITY**

CERTIFICATION - TEMPERATURE PROBE

Cert Type Agency Cert Date Recert Date Performed By
 98 CLEAN AIR ENGINEERING 05-DEC-2016 05-DEC-2017 ALDAVIDS

Transfer Standard

SN Brand Model Prev Cert Date
 160407973 OMEGA HH370

Primary Std SN Brand Type
 35060-1 ISOTECH THERMOMETER

| Test Ranges | Transfer Std (C) | Primary Std (C) | Difference (C) | Pass/Fail | Met Use Pass/Fail |
|----------------------|------------------|-----------------|----------------|-----------|-------------------|
| LOW (-5.0 to +5.0) C | 0.0 | 0.0 | 0.0 | PASS | PASS |
| AMBIENT | 26.3 | 26.4 | -0.1 | PASS | PASS |
| HIGH (35 to 45) C | 46.2 | 46.4 | -0.2 | PASS | PASS |

Note: All differences must be within +/- 1.0 C or a correction factor is required. For meteorological audits all differences must be +/- 0.2 C or a correction factor is required.

Comments



Certificate of Calibration

Customer: CLEAN AIR ENGINEERING
 Customer P.O.: 01356-44-13075
 Instrument: Omega HH370
 Order Number: WC00274278
 Description: Digital Thermometer
 Serial Number: 160407973
 Equipment I.D.#: WC274278
 Incident Number: new

Cal-3

Omega Engineering, Inc. hereby certifies that the above instrumentation has been calibrated and tested to meet or exceed the published specifications. This calibration and testing was performed using instrumentation and standards that are traceable to the National Institute of Standards and Technology. Omega Engineering, Inc. is in compliance with ISO 10012-1, ISO 9001 and ANSI/NCSL Z540-1-1994. This certificate shall not be reproduced, except in full, without the written consent of Omega Engineering, Inc.

CALIBRATION INFORMATION

Cal Date: 04-Oct-16 Temperature: 22°C ± 5°C
 Cal Due Date: 04-Oct-17 Humidity: Below 80%

Absolute Uncertainty: ± 0.19 F
 Comments:

Pass: Y Technician: DL Seals OK: N/A
 Procedure: QAP-2100 Certificate #: WC274278

STANDARDS USED FOR CALIBRATION

| Asset Number | Description | NIST Traceable Number | Cal Date | Due Date |
|--------------|--|-----------------------|----------|----------|
| RE-098-14 | IET HARS-X-6-0-01 Resistance Simulator | 10NNRE09814 | 8-Apr-16 | 8-Apr-17 |

David Jansen
 Metrology Technician:

[Signature]
 Quality Assurance Inspector:

OMEGA Engineering, Inc., One Omega Circle, P.O. Box 336, Bridgeport, NJ 08014-0336 Telephone: (856) 467-4200 Fax: (856) 467-1212

www.omega.com e-mail: info@omega.com

WC3 - 06/05A



Calibration Results

| | | | |
|------------------|-----------------------|----------------|--------------|
| Customer: | CLEAN AIR ENGINEERING | Result: | PASS |
| P.O. Number: | 01356-44-13075 | Cal Date: | 04-Oct-16 |
| Order Number: | WC00274278 | Cal Due Date: | 04-Oct-17 |
| Instrument: | Omega HH370 | Technician: | DL |
| Description: | Digital Thermometer | Temperature: | 22 °C ± 5 °C |
| Serial Number: | 160407973 | Humidity: | Below 80% |
| Equipment I.D.#: | WC274278 | Condition F/L: | AS-LEFT |
| Incident Number: | new | Procedure: | QAP-2100 |
| | | Certificate #: | WC274278 |

Standards Used

| Asset # | Description | NIST Traceable Number | Cal Date | Due Date |
|-----------|--|-----------------------|----------|----------|
| RE-098-14 | IET HARS-X-6-0.01 Resistance Simulator | 10NNRE09814 | 8-Apr-16 | 8-Apr-17 |

Test Data

| Test Description | True Value | Test Result | Lower limit | Upper limit | |
|----------------------------|------------|-------------|-------------|-------------|------|
| Pt100 RTD Temperature Test | | | | | |
| -130.0 DegreeF | | -130.0 | -130.9 | -129.1 | Pass |
| 32.0 DegreeF | | 31.8 | 31.2 | 32.8 | Pass |
| 212.0 DegreeF | | 211.8 | 211.0 | 213.0 | Pass |
| 392.0 DegreeF | | 391.7 | 390.8 | 393.2 | Pass |
| 554.0 DegreeF | | 553.5 | 552.6 | 555.4 | Pass |

End of Test Data



Airgas USA, LLC

2039 BELLAIRE AVE
ROYAL OAK, MI 48067
248-309-8020
Airgas.com

CERTIFICATE OF ANALYSIS Grade of Product: EPA Protocol

| | | | |
|------------------|-------------------------------|---------------------|----------------|
| Customer: | CLEAN AIR ENGINEERING | Reference Number: | 32-400770445-1 |
| Part Number: | E02NI99E15A0576 | Cylinder Volume: | 144.3 CF |
| Cylinder Number: | CC7590 | Cylinder Pressure: | 2015 PSIG |
| Laboratory: | 112 - Royal Oak-32 (SAP) - MI | Valve Outlet: | 660 |
| PGVP Number: | B62016 | Certification Date: | Oct 03, 2016 |
| Gas Code: | SO2,BALN | | |

Expiration Date: Oct 03, 2020

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a volume/volume basis unless otherwise noted.

Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

| ANALYTICAL RESULTS | | | | | |
|--------------------|-------------------------|----------------------|-----------------|----------------------------|------------------------|
| Component | Requested Concentration | Actual Concentration | Protocol Method | Total Relative Uncertainty | Assay Dates |
| SULFUR DIOXIDE | 10.00 PPM | 10.02 PPM | G1 | +/- 1% NIST Traceable | 09/15/2016, 10/03/2016 |
| NITROGEN | Balance | | | | |

| CALIBRATION STANDARDS | | | | | |
|-----------------------|-----------|-------------|-----------------------------------|-------------|-----------------|
| Type | Lot ID | Cylinder No | Concentration | Uncertainty | Expiration Date |
| NTRM | 130603-28 | CC403839 | 16.82 PPM SULFUR DIOXIDE/NITROGEN | +/-0.9% | May 31, 2019 |

| ANALYTICAL EQUIPMENT | | |
|-------------------------|----------------------|-----------------------------|
| Instrument/Make/Model | Analytical Principle | Last Multipoint Calibration |
| E/N 54 Nicolet 6700 SO2 | FTIR | Sep 23, 2016 |

Triad Data Available Upon Request




Approved for Release

