

**PROCESS POLLUTANT DETERMINATION  
FOR COMPLIANCE EMISSION TESTING**

**BANBURY MIXER NO. 7  
TEST DATE OCTOBER 24, 2013**

**Prepared For:**

**THE GOODYEAR TIRE AND RUBBER COMPANY  
1901 GOODYEAR BOULEVARD  
DANVILLE, VIRGINIA 24541**

**Prepared By:**

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CHARLOTTE, NORTH CAROLINA**

**CEC Project 132-066**

**November 22, 2013**




**Civil & Environmental Consultants, Inc.**

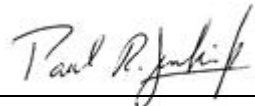
## REPORT CERTIFICATION

This report, testing details, and approach have been developed under the supervision (including review) of the persons named below. Results contained in this report relate only to the sources tested and the parameters included in the test program. CEC operates in conformance with the requirements of ASTM D7036-04 (Reapproved 2011).

Date 11/22/13

Signature   
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## 1.0 INTRODUCTION

Civil & Environmental Consultants, Inc. (CEC) of Charlotte, North Carolina was contracted by The Goodyear Tire and Rubber Company (Goodyear) to conduct a compliance test on Banbury Mixer No. 7 (ID. No. EU-007) located in Danville, Virginia. The results of the total particulate matter (PM) and particulate matter less than 10 microns (PM10) sampling and the documentation provided in this report will be used to determine compliance with Title V Permit No. SCRO30106 issued by the Commonwealth of Virginia Department of Environmental Quality (VDEQ).

The emission testing on the fabric filter exhaust of Banbury Mixer No. 7 was performed on October 24, 2013. Three 2-hour sampling runs were conducted for total particulate matter and PM10. United States Environmental Protection Agency (US EPA) Methods 1 through 5 and 202 were used for the determination of total particulate matter concentrations and emission rates. US EPA Method 201A and 202 were used for the determination of PM10. The test runs were conducted concurrently during normal plant operations. The sampling and analytical procedures used in this test program were those established by the US EPA and VDEQ in standard reference test methods and appropriate sampling and analytical procedures.

<b>Table 1 – List of Project Participants The Goodyear Tire &amp; Rubber Company Danville, Virginia Facility</b>			
<b>Participant</b>	<b>Title</b>	<b>Affiliation</b>	<b>Contact</b>
W. Quentin Best	Senior Professional	CEC, Inc.	Telephone: 980.237.0373 Facsimile: 980.237.0372 <a href="mailto:qbest@cecinc.com">qbest@cecinc.com</a>
Bryan L. Starnes	Project Manager	CEC, Inc.	
Joshua A. Jones, QSTI	Assistant Project Manager	CEC, Inc.	
Graham R. Guse	Technician	CEC, Inc.	
Kevin M. Dunham	Technician	CEC, Inc.	
Carlton Williams	Regional Environmental Manager North America - Commercial Plts	The Goodyear Tire & Rubber Company	Telephone: 330.796.0811 Mobile: 864.978.3170 <a href="mailto:carlton_williams@goodyear.com">carlton_williams@goodyear.com</a>

Mr. Carlton Williams of Goodyear was responsible for coordinating the referenced process and for the collection of process operations data. This data is presented in Appendix F.

This report contains the results of the emission tests conducted during the test program. Copies of reference method field data sheets, sample analysis data, example calculations and equipment calibration records are included as appendices to this report.

## 2.0 SUMMARY OF TEST RESULTS

This section presents a summary of the particulate matter sampling. Detailed sampling results and example calculations for the test program can be found in Appendix A. Field data sheets and sample recovery documentation are presented in Appendix B. Appendix C contains the laboratory report. Appendix D presents copies of the current reference method equipment calibration records. Appendix E contains copies of the Qualified Stack Test Individual (QSTI) certifications for CEC testing personnel. Appendix F contains documentation of the production during the compliance test.

### 2.1 SAMPLING RESULTS

The summary of the results for the tests performed at the Banbury Mixer No. 7 is presented in Table 2 below. The emission rates presented in the following tables were calculated based upon emission stream conditions measured during the test period. The calculations were conducted in accordance with the appropriate test methods.

<b>Table 2 – Particulate Matter and PM10 Sampling Results</b>					
<b>Fabric Filter Exhaust from Banbury Mixer No. 7</b>					
Total Particulate Matter	Average Emission Rate				
	Run 1	Run 2	Run 3	Average	Limit
gr/dscf*	0.00082	0.00065	0.00077	0.00075	0.01
lb/hr**	0.068	0.057	0.066	0.064	
PM10					
gr/dscf*	0.00096	0.00045	0.00016	0.00031***	0.01
lb/hr**	0.079	0.034	0.013	0.024***	

\* gr/dscf = grains per dry standard cubic foot

\*\* lb/hr = pound per hour

\*\*\* Average based on Runs 2 and 3

Goodyear has been issued Title V Permit No. SCO30106 by VDEQ. The applicable emission limit for particulate matter at the Banbury Mixer is 0.01 grains per dry standard cubic foot (gr/dscf). The results of the Banbury Mixer No. 7 test program demonstrate that the tested unit was in compliance with the applicable air emission limit for total particulate matter and PM10.

## 2.2 SAMPLING DATES AND TIMES

Table 3 presents the sampling dates and times for the process tested at the Goodyear, Danville, Virginia facility.

<b>Table 3 – Sampling Dates and Times The Goodyear Tire &amp; Rubber Company Danville, Virginia Facility</b>			
<b>Sample Location</b>	<b>Run 1</b>	<b>Run 2</b>	<b>Run 3</b>
Banbury Mixer No. 7	10/24/13	10/24/13	10/24/13
	0955-1210	1343-1554	1630-1844

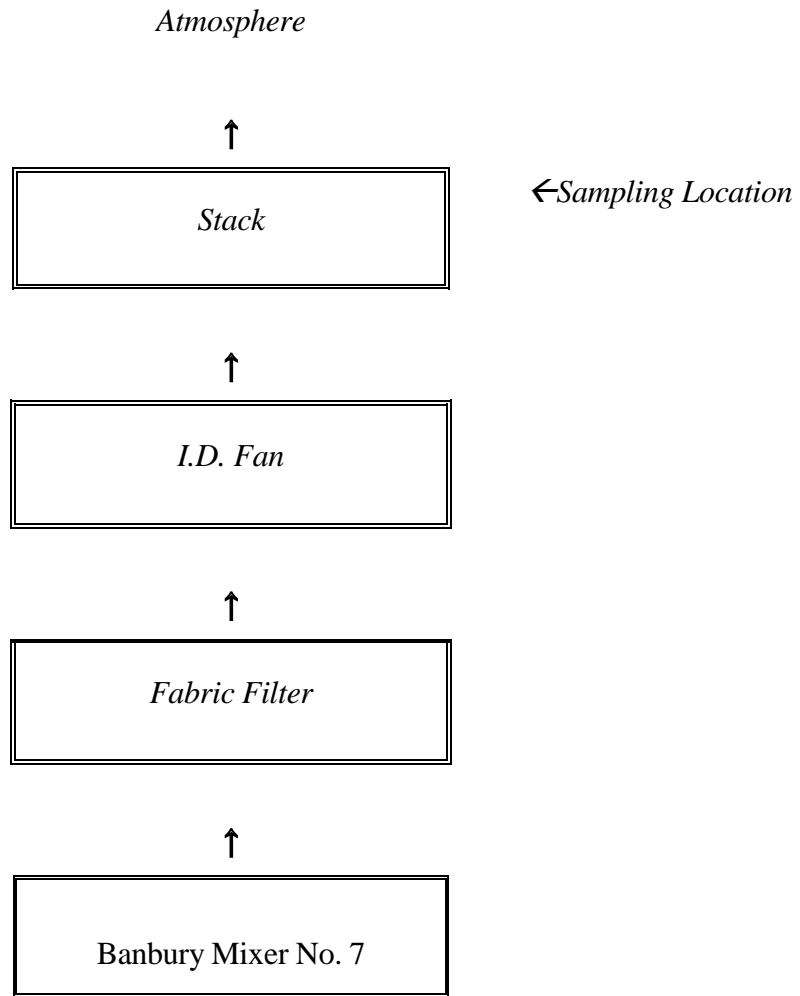
### 3.0 PROCESS DESCRIPTION

The Goodyear facility operates nine Banbury mixers. Banbury No. 7 was chosen as a representative of the nine Banbury mixers.

Figure 1 details the air-flow schematic for the referenced system. Production data and control device parameters during the sampling were recorded by Goodyear personnel and are presented in Appendix F. The sampling was performed during material processing.



## Banbury Mixer No. 7



**Figure 1 - Process Air Flow Schematic**

## **4.0 SUMMARY OF THE REFERENCE TEST METHODS**

This section describes the sampling strategy, sampling and analytical methods, and quality assurance/quality control procedures implemented during this project.

### **4.1 SAMPLING STRATEGY**

The US EPA methods that were utilized in this sampling program were:

- Method 1 for the location of sampling ports and points, and determination of cyclonic flow;
- Method 2 for velocity / volumetric flow rate determination, and assignment of dry molecular weight of the stack gas;
- Method 4 for the determination of moisture in the stack gas;
- Method 5 for the determination of particulate matter;
- Method 201A for the determination of PM10, and
- Method 202 for the determination of condensable particulate matter.

These test methods are available in the Code of Federal Regulations Volume 40, Part 60, US EPA's web site [www.epa.gov/ttn/emc/](http://www.epa.gov/ttn/emc/), and/or by request from CEC.

### **4.2 SAMPLING AND ANALYTICAL PROCEDURES**

A sampling and analysis synopsis for these methods is discussed briefly in the following subsections.

#### **4.2.1 US EPA Method 1-Sampling Point Determination**

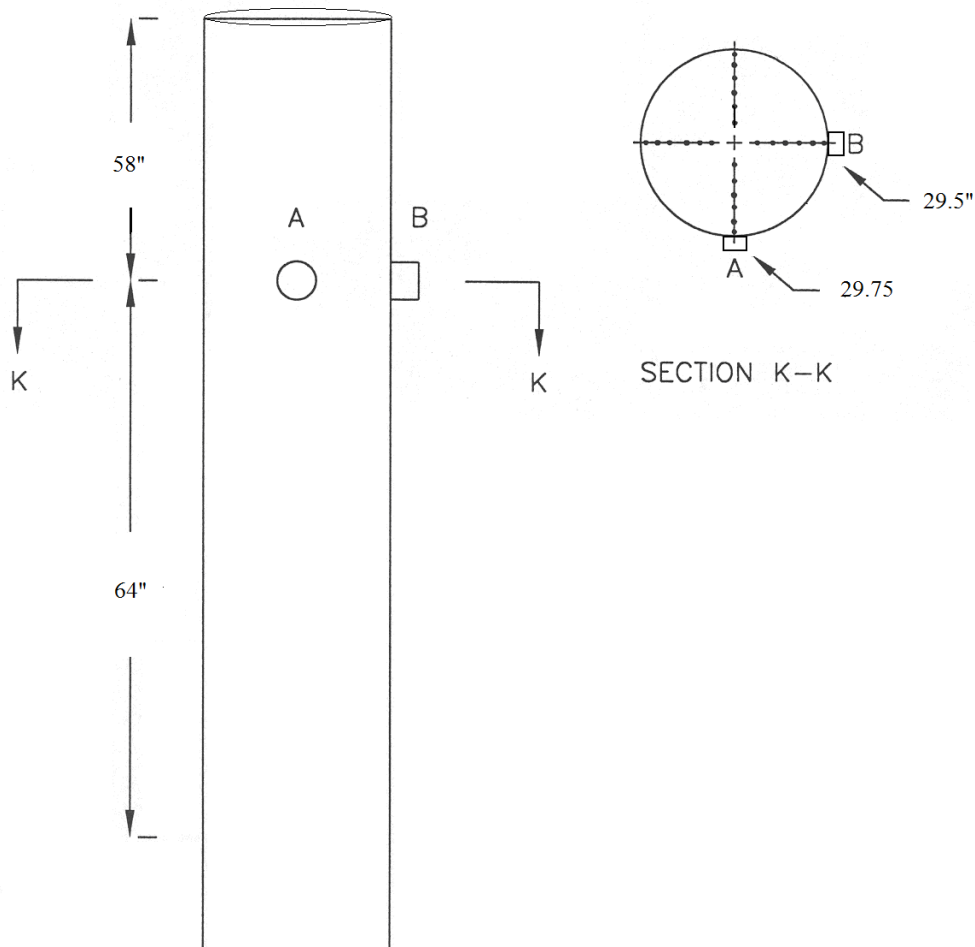
For this test program, the US EPA Method 1 was used to determine the appropriateness of the existing ports as the sampling location at the Banbury Mixer No. 7 stack. The duct diameters upstream and downstream from the sampling ports were determined prior to sampling. The number of traverse points was chosen with respect to sampling port location. For particulate traverses, Method 1 specifies a minimum of 8 traverse points for sampling ports located  $>8/2$  downstream/upstream stack diameters from flow disturbances and a maximum of 24 traverse points when located  $>2/0.5$  downstream/ upstream stack diameters from flow disturbances.

The dimensions of the stack and the location of the sampling ports and points are detailed in Figure 2. Method 1 sampling criteria was maintained. The Banbury Mixer No. 7 Exhaust Stack was a circular duct divided into 24 equal traverse areas with ports labeled A and B (twelve sample points per port). During the Method 5/202 and 201A/202 sampling runs, the individual points were sampled for a period of five (5) minutes, which yielded a total test of 120 minutes.

The Banbury Mixer No. 7 sampling location was determined to be less than 20° and in compliance with US EPA Method 1, Section 11.4.2 for cyclonic flow. A copy of this data can be found in Appendix B.

### Banbury Mixer No. 7 Exhaust Stack

Table 4 – Stack Diameter and Upstream/Downstream Measurements for Banbury Mixer No.7 Exhaust Stack The Goodyear Tire & Rubber Company Danville, Virginia Facility- Method 1				
System	Stack Diameter (inches)	Upstream (inches)	Downstream (inches)	Total number of sampling points per run
Banbury Mixer No. 7 Stack	29.75/29.5	58	64	24



*Not to Scale*

**Figure 2 - Location of Sampling Ports and Points**

#### 4.2.2 US EPA Method 2 Velocity and Volumetric Flow Rate Determination

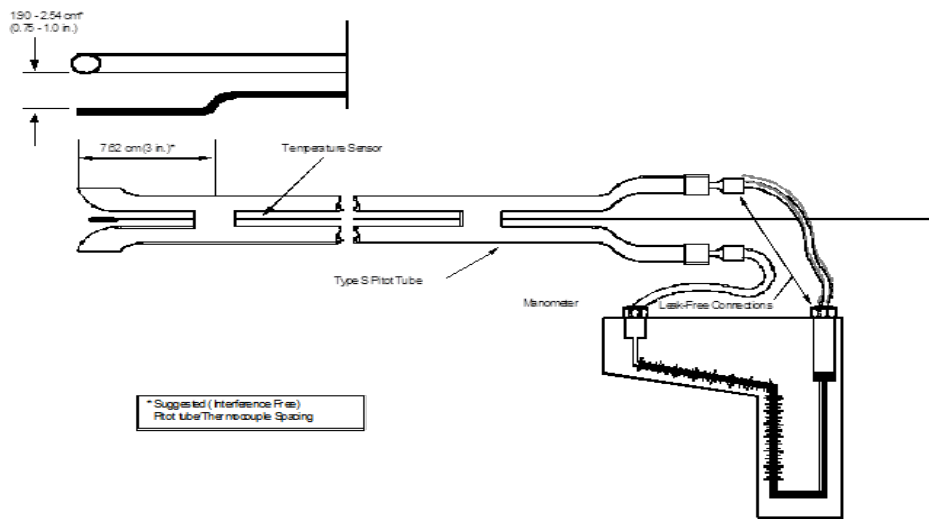
Method 2 was used for determining the average gas velocity from measurements of gas density and the average velocity head with a Type S (Stausscheibe or reverse type) pitot tube (0.84 coefficient). This method is applicable for quantifying gas flows for stacks that are 12 inches and over in diameter which meet the criteria of Method 1.

During this project, the sampling locations met the criteria detailed in Method 1. Gas stream density was assigned a value per Method 2 Section 8.6. Moisture determination was performed by Method 4. The velocity traverses were performed using Method 2 where the principal components of the gas velocity measurement system were sequentially:

- A calibrated stainless steel Type S pitot tube and Type K thermocouple;
- Leak-free interface tubing between pitot tube and differential pressure gauge;
- A 0 to 10 inch inclined manometer; and
- An NIST traceable pyrometer.

The apparatus was set-up according to manufacturer and reference method recommendations. Pre-test and post-test leak checks were conducted using procedures outlined in Method 2, Section 8.0. Velocity head and temperature measurements were performed during each sampling run at the traverse points specified by Method 1. The effluent gas temperature was measured with chromel-alumel thermocouples equipped with a digital temperature indicator. The atmospheric and static pressure of each stack was also determined during each sample run. The volumetric flow rate calculations used were those specified in Method 2, Section 12. Figure No. 3 show a typical S-type Pitot tube velocity measurement system.

CEC conducted measurements of the face opening alignments, external tubing diameter, and base-to-opening plane distances of the pitot tubes. These measurements meet the design criteria in US EPA Method 2 for a Type “S” pitot tube, and therefore a baseline coefficient value of 0.84 inches was assigned to the Pitot tube. Verification of these measurements were recorded onto a pitot tube calibration worksheet and presented in Appendix D of the final report.



**Figure 3 - S-Type Pitot Velocity Measurements System**

#### **4.2.3 US EPA Method 3 Molecular Weight Rate Determination**

Method 3 is applicable for determining carbon dioxide and oxygen concentrations and dry molecular weight of a sample from a gas stream of a fossil-fuel combustion process. This method may also be applicable to other processes where it has been determined that compounds other than carbon dioxide, oxygen, carbon monoxide, and nitrogen are not present in concentrations sufficient to affect the results. However, US EPA Method 2, Section 8.6 states that “For processes emitting essentially air, an analysis needs not be conducted; use a dry molecular weight of 29.0.” The Banbury mixer was emitting essentially air, therefore the emission rate calculations were based on a dry molecular weight of 29.0.

#### **4.2.4 US EPA Method 4 Moisture Determination**

Method 4 involves the determination of stack gas moisture. The moisture content is used to correct the emission concentration or mass emission rate to a dry basis. EPA Method 4 and *Field Procedure 4* of the QA Handbook were used to measure stack gas moisture content. *Field Procedure 4* provides detailed information on the application of Method 4.

Preliminary flue gas moisture content (for purposes of setting the isokinetic flow rate) was determined using wet bulb/dry bulb thermometers and partial pressure, vapor and saturated vapor pressure equations. This technique is described in Method 4 and is summarized below:

- Moisten the wet bulb thermometer wick with deionized water;
- Insert both thermometers into the flue gas stream and monitor the wet bulb temperature;
- When the wet bulb temperature has stabilized, record both the wet bulb and dry bulb thermometer temperatures; and
- Calculate the flue gas moisture content (PMV) using the appropriate equations.

The moisture content for emission rate calculations was determined in conjunction with the Method 5 isokinetic sampling train. The reference method involves the withdrawal of gaseous and particulate pollutants from the emission source at an isokinetic rate using a Method 5 sampling system. The sampling and analytical procedure for reference Method 4 will be discussed in detail in Section 4.2.5 with the isokinetic sampling procedures.

#### **4.2.5 US EPA Method 5 Particulate Matter Sampling and Analysis**

Testing for total particulate matter was performed according to US EPA Methods 5 and 202. Gaseous and particulate pollutants were withdrawn isokinetically from the emission source and collected in a multi-component sampling train. In principle, filterable particulate matter includes any material that was condensed at or above the filtration temperature of approximately 250 degrees Fahrenheit and was collected on a tared glass fiber filter. The condensable particulate matter (CPM) is collected in the dry impinger system after the filterable particulate matter has been collected on the filter. The CPM is collected in the condenser system/ water drop out impinger and CPM filter. The gaseous components are bubbled through a measured volume of chilled deionized water to determine the moisture content of the emission source. The principal components of the sampling system were sequentially:

- A stainless steel sample nozzle and borosilicate probe liner;
- A heated (248°F ±25°F) probe and filter assembly with tared glass fiber filter;

- An impinger train consisting of a dry and wet impinger system. The dry impinger system consisted of a condenser and a dropout impinger; followed by an empty modified Greenburg Smith impinger and a CPM filter. Following the CPM filter, the wet impinger system consisted of two impingers. The first containing 100 ml of deionized water followed by a final impinger containing 200 grams of silica gel; and
- A metering system capable of maintaining an isokinetic sampling rate and accurately determining the sample volume according to specifications in APTD-0581.

After the test run, the impingers were weighed to determine moisture. The collected condensate measurements were recorded on the Method 4 moisture determination data analysis form. An impinger stem was added to the dropout impinger so that the stem extended below the water level. Nitrogen purged deionized water was added to the impinger to ensure the water level was over the stem for the duration of the purge. The sampling train was reassembled and connected to an ultra-high purity nitrogen gas cylinder for a one hour purge with nitrogen at 14 liters per minute.

The tared filter, which collected the filterable particulate matter sample, was carefully removed from the glass filter support and sealed in a Petri dish. The nozzle, probe liner, and front filter-half of the filter assembly were brushed and rinsed with acetone into a glass storage container which was sealed and the liquid level was marked.

After the purge, liquid in the dropout impinger and backup impinger was collected into a clean sampling container (CPM container No. 1). The back filter-half, condenser, dropout impinger, backup impinger, the front half of the CPM filter assembly and connecting glassware were twice rinsed with deionized water into CPM container No.1. Following the water rinses, the glassware was rinsed once with acetone and rinsed twice with hexane and was recovered into CPM Container No.2. The CPM filter was removed from the filter holder and sealed in a labeled Petri dish. The sample containers were transported to Enthalpy Analytical, Inc. in Durham, North Carolina for gravimetric analysis. Documentation of the laboratory analysis and chain-of-custody can be found in Appendix C. The condensable fractions of the sample runs were train blank corrected.



#### **4.2.6 US EPA Method 201A Particulate Matter Less Than 10 Microns (PM10) Sampling and Analysis**

Testing for PM10 was performed according to US EPA Methods 201A and 202. Gaseous and particulate pollutants were withdrawn at a predetermined constant flow rate through an in-stack sizing device. In principle, particulate matter is extracted at a constant flow rate through an in-stack sizing device with well-defined limits to minimize variations with isokinetic sampling. The in-stack sizing device separates particles with nominal aerodynamic diameters of 10 micrometers and the final fraction was collected on a tared quartz fiber filter housed in a stainless steel impactor. The condensable particulate matter (CPM) is collected in the dry impinger system after the PM10 has been collected on the filter. The CPM is collected in the condenser system/ water drop out impinger and CPM filter. The gaseous components are bubbled through a measured volume of chilled deionized water to determine the moisture content of the emission source. The principal components of the sampling system were sequentially:

- A stainless steel sample nozzle and PM10 sizing heads with tared quartz fiber filter;
- A heated (248°F ±25°F) stainless steel probe liner;
- An impinger train consisting of a dry and wet impinger system. The dry impinger system consisted of a condenser and a dropout impinger; followed by an empty modified Greenburg Smith impinger and a CPM filter. Following the CPM filter, the wet impinger system consisted of two impingers. The first containing 100 ml of deionized water followed by a final impinger containing 200 grams of silica gel; and
- A metering system capable of maintaining an isokinetic sampling rate and accurately determining the sample volume according to specifications in APTD-0581.

After the test run, the impingers were weighed to determine moisture. The collected condensate measurements were recorded on the Method 4 moisture determination data analysis form. An impinger stem was added to the dropout impinger so that the stem extended below the water level. Nitrogen purged deionized water was added to the impinger to ensure the water level was over the stem for the duration of the purge. The sampling train was reassembled and connected to an ultra-high purity nitrogen gas cylinder for a one hour purge with nitrogen at 14 liters per minute.

The tared PM10 filter was carefully removed from the stainless steel filter support and sealed in a petri dish. The sizing head and front filter-half of the filter assembly were brushed and rinsed with acetone into a separate glass storage container (PM10 fraction) which was sealed and the liquid level was marked. The fraction greater than 10 microns was discarded.

After the purge, liquid in the dropout impinger and backup impinger was collected into a clean sampling container (CPM container No. 1). The back filter-half, condenser, dropout impinger, backup impinger, the front half of the CPM filter assembly and connecting glassware were twice rinsed with deionized water into CPM container No.1. Following the water rinses, the glassware was rinsed once with acetone and rinsed twice with hexane and was recovered into CPM Container No. 2. The CPM filter was removed from the filter holder and sealed in a labeled Petri dish. The sample containers were transported to Enthalpy Analytical, Inc. in Durham, North Carolina for gravimetical analysis. Documentation of the laboratory analysis and chain-of-custody can be found in Appendix C. The condensable fractions of the sample runs were train blank corrected.

## 5.0 QUALITY ASSURANCE / QUALITY CONTROL RESULTS

CEC has established quality assurance and quality control (QA/QC) guidelines for providing quality sampling and analytical data from source tests. These QA/QC procedures were implemented to ensure the acceptability and reliability of the data generated.

In summary, an appropriate degree of data quality was maintained throughout this project. Leak checks and isokinetic QA criteria were met for the full sampling run. The sampling trains were leak checked prior to and immediately after sampling. Leak rates for the isokinetic sampling trains were less than the maximum criterion of 0.02 cubic feet per minute. The sampling rates were also within the 100%  $\pm$ 10% criterion established for isokinetic sampling. Quality control procedures for the particulate matter determinations have included the analysis of acetone rinse blanks. The result of the method blank is reported in Appendix C with the laboratory data.

Method 201A is typically paired with Method 202 for the determination of condensable particulate matter which is considered to be PM<sub>2.5</sub>. However, per Method 201A, the Method 202 sampling is only required for evaluating sources when the emission source operates at a temperature over 85 degrees F. The backhalf sampling trains were analyzed and included in the data even though the stack temperature did not exceed 85 degrees. Please note due to the cold day and high wind on the day of testing the backhalf requirement for the 202 portion of the sampling train was not maintained above 65 degrees F.

Method 201A has a requirement that point for point isokinetic sampling is required. Sampling run number 1 failed to meet the point per point isokinetic requirement. Due to the variability in the flow and nozzle selection, there were six out of the 24 points that were not isokinetic. The method allows up to five data point to be outside of 100  $\pm$  20 %. The run data is presented, but not included in the average for the PM<sub>10</sub> data.

<b>Table 5 – Quality Assurance and Quality Control Data – Method 5</b>					
<b>Banbury Mixer No. 7</b>		Run 1	Run 2	Run 3	<b>Criteria</b>
Leak Checks	Method 5	0.002	0.005	0.001	< 0.020 cu. ft.
Isokinetics		101.3	102.6	100.6	100 ± 10%
Post Meter Calibration – Alternative Method 4 Post-Test Calibration (ALT-009) Post Meter Calibration			Meter Box 300.390 Avg. Y = 0.975		0.986 ± 0.05
Leak Checks	Method 201A	0.002	0.001	0.001	< 0.020 cu. ft.
Isokinetics		97.4	109.4	101.2	100 ± 20%
Post Meter Calibration – Alternative Method 4 Post-Test Calibration (ALT-009) Post Meter Calibration			Meter Box 300.392 Avg. Y = 0.957		0.990 + 0.05

Field data and final laboratory results were entered into CEC's air quality data system by a staff professional, and reviewed by a project manager for verification of data. After QC review by the project manager, a senior professional verified the final report for completeness and reasonableness of data. The report was returned to the staff professional for review and preparation of the final draft. The report requires the signature of the staff professional and a project manager before release to the client. Data and final reports are archived in a secured area for a minimum period of seven years.

CEC's field and laboratory test equipment has been maintained and calibrated in accordance with quality assurance procedures established by the US EPA in the QA handbook. Equipment calibrations including pre-test and post-test calibration data are presented in Appendix D

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**APPENDIX A**

**SUMMARY OF RESULTS AND EXAMPLE CALCULATIONS**

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## The Goodyear Tire &amp; Rubber Company Danville, Virginia

CEC Project No. 132-066

Banbury Mixer No. 7

## SUMMARY OF RESULTS

## EPA METHOD 5 and 202

## Determination of Total Particulate Concentrations and Emission Rates

Run Number	1	2	3	Average
Sample Identification	132066-01	132066-02	132066-03	----
Date:	10/24/2013	10/24/2013	10/24/2013	----
$\theta$ Net Time of Test, minutes	120.0	120.0	120.0	----
Sample Time, 24-hour clock	0955-1210	1343-1554	1630-1844	----
$P_{bar}$ Barometric Pressure, in. Hg	29.62	29.62	29.56	29.60
$P_g$ Static Pressure, in. H <sub>2</sub> O	-0.250	-0.250	-0.250	-0.250
$P_s$ Stack Pressure, Absolute, in. Hg	29.602	29.602	29.542	29.582
$V_M$ Actual Meter Volume Sampled, cu. ft.	84.709	88.336	86.523	86.523
$\Delta H$ Avg. Delta H, in. H <sub>2</sub> O	1.61	1.74	1.73	1.69
$T_M$ Avg. Gas Meter Temp., Deg. F	71.7	76.1	67.7	71.8
$V_{m(STD)}$ Volume Sampled at Stand. Cond., cu. ft.	82.436	85.292	84.695	84.141
$V_C$ Volume of Water Collected, ml	-2.1	-8.0	-2.4	-4.2
$V_{wc(std)}$ Volume of Water Vapor at Std. Cond., SCF	-0.10	-0.38	-0.11	-0.20
$W_C$ Volume of Water Collected in Silica Gel, g	13.90	22.20	20.50	18.87
$V_{wsg(std)}$ Vol. of Water Vapor in Silica Gel at Std. Cond., SCF	0.66	1.05	0.97	0.89
$B_{WS1}$ Moisture Content of Gas Stream	0.007	0.008	0.010	0.008
$P_{MV1}$ Calculated Percent Moisture in Stack	0.7	0.8	1.0	0.8
$P_{MV1S}$ Saturated Percent Moisture in Stack	2.3	2.7	2.5	2.5
$P_{MV1R}$ Reported Percent Moisture in Stack	0.7	0.8	1.0	0.8
$M_{FD1}$ Mole Fraction of Dry Gas	0.993	0.992	0.990	0.992
$M_d$ Mole. Wt. Stack Gas, Dry Basis, lb/lb mole	29.0	29.0	29.0	29.0
$M_s$ Mole. Wt. Stack Gas, Wet Basis, lb/lb mole	28.926	28.914	28.890	28.910
$C_p$ Pitot Tube Coefficient	0.84	0.84	0.84	0.84
$\Delta PS$ Avg. Sqrt. Delta P, in. H <sub>2</sub> O	0.608	0.645	0.633	0.629
$T_s$ Avg. Stack Temp., Deg. F	67.0	72.0	70.4	69.8
$V_s$ Avg. Stack Velocity, ft/sec	34.2	36.5	35.8	35.5
A Area Stack, ft <sup>2</sup>	4.787	4.787	4.787	4.787

## The Goodyear Tire &amp; Rubber Company Danville, Virginia

CEC Project No. 132-066

Banbury Mixer No. 7

## SUMMARY OF RESULTS

## EPA METHOD 5 and 202

## Determination of Total Particulate Concentrations and Emission Rates

Run Number		1	2	3	Average
Q <sub>SD</sub>	Gas Volume Flow, Dry Std. Cond. CFM	9685	10215	10018	9972
Q <sub>A</sub>	Actual Gas Volume Flow, CFM	9836	10484	10294	10205
Q <sub>SW</sub>	Gas Volume Flow, Wet Std. Cond., CFM	9750	10295	10119	10055
D <sub>n</sub>	Sample Nozzle Diameter, inches	0.248	0.244	0.248	0.247
A <sub>n</sub>	Area of Nozzle, ft <sup>2</sup>	0.00034	0.00032	0.00034	0.00033
I	Percent Isokinetic	101.3	102.6	100.6	101.5
Mb #	Meter Box Number	300.390	300.390	300.390	---
ΔH@	ΔH@ of Meter Box @ 0.75 SCFM	1.956	1.956	1.956	---
Y <sub>qa</sub>	Alt. Mthd 5 Posttest Calibration (ALT-009)	0.970	0.971	0.983	0.975
Y	Meter Calibration Factor	0.986	0.986	0.986	---

CEC Project No. 132-066

The Goodyear Tire & Rubber Company Danville, Virginia  
Banbury Mixer No. 7

Summary of Results  
EPA Methods 5 and 202  
Determination of Total Particulate Concentrations and Emission Rates

Run Number		1	2	3	Average
	Sample Identification	132066-01	132066-02	132066-03	
<b>Filterable Particulate Matter (PM) Concentration and Emission Rates</b>					
$m_f$	Particulate Catch, mg	2.8	2.0	2.4	2.4
$C_s$	PM Concentration, gr/dscf	0.00052	0.00036	0.00044	0.00044
$C_{sm}$	PM Concentration, mg/dscm	1.20	0.83	1.00	1.01
$C_{AW}$	PM Emission Rate, lbs/hr	0.044	0.032	0.038	0.038
<b>Condensable Particulate Matter (CPM) Concentration and Emission Rates</b>					
$m_{cpm}$	CPM Catch, mg	1.6	1.6	1.8	1.7
$C_{sc}$	CPM Concentration, gr/dscf	0.00030	0.00029	0.00033	0.00031
$C_{sm}$	CPM Concentration, mg/dscm	0.69	0.66	0.75	0.70
$C_{AWc}$	CPM Emission Rate, lbs/hr	0.025	0.025	0.028	0.026
<b>Total Particulate Matter (TPM) Concentration and Emission Rates</b>					
$C_{sT}$	TPM Concentration, gr/dscf	0.00082	0.00065	0.00077	0.00075
$C_{sm}$	TPM Concentration, mg/dscm	1.88	1.49	1.75	1.71
$C_{AWT}$	TPM Emission Rate, lbs/hr	0.068	0.057	0.066	0.064



The Goodyear Tire & Rubber Company Danville, Virginia  
Banbury Mixer No. 7

CEC Project No. 132-066

Summary of Results  
EPA Methods 5 and 202

Determination of Total Particulate Concentrations and Emission Rates

**Example Calculations Run 1**

Stack Pressure, Absolute, in. Hg $P_S = P_{bar} + (P_g / 13.6) =$	29.602
Volume Sampled at Stand. Cond., cu. ft. $V_m(std) = (V_m * Y * (P_{bar} + DH / 13.6) * T_{std}) / (P_{std} * (T_m + 460)) =$	82.436
Method 4 Calculations:	
Volume of Water Vapor at Std. Cond., SCF $V_{WC(std)} = 0.04706 * V_C =$	-0.10
Vol. of Water Vapor in Silica Gel at Std. Cond., SCF $V_{wsg(std)} = 0.04715 * W_C =$	0.66
Moisture Content of Gas Stream $B_{WS1} = (V_{WC(std)} + V_{wsg(std)}) / (V_m(std) + V_{WC(std)} + V_{wsg(std)}) =$	0.007
Percent Moisture in Stack $P_{MV1} = 100 * (V_{WC(std)} + V_{wsg(std)}) / (V_m(std) + V_{WC(std)} + V_{wsg(std)}) =$	0.7
Saturated Stack Moisture using Stack Temperature (°F): Note if %S <sub>VP</sub> > 100% = 100%	
$P_{MV1S} = \%S_{VP} = (100/P_S) * 10^{(6.6921 - (3144/(T+390.86)))}$	2.3
Reported Stack Moisture according to Method 4 Section 12.1.7 In saturated or moisture laden gas streams, the lower B <sub>ws</sub> (PMV1 or PMV1S) is considered correct	0.7
Mole Fraction of Dry Gas $M_{FD1} = (100 - P_{MV}) / 100 =$	0.993
Mole. Wt. Stack Gas, Dry Basis, lb/lb mole M <sub>d</sub> is assigned a value per EPA Method 2, Section 8.6 =	29.0
Mole. Wt. Stack Gas, Wet Basis, lb/lb mole $M_S = M_d * (1 - B_{ws}) + 18.0 * B_{ws} =$	28.926
Avg. Stack Velocity, ft/sec $VS = 85.49 * CP * \sqrt{DP_{avg}} * \sqrt{(TS + 460) / (PS * MS)} =$	34.2
Gas Volume Flow, Dry Std. Cond. CFM $Q_{SD} = (60 \text{ sec/min} * (1 - B_{ws}) * V_s * A * ((T_{std} * P_s) / (T_{s(abs)} * P_{std})))$	9685
Actual Gas Volume Flow, CFM $Q_A = V_S * A * 60 \text{ sec/min} =$	9836
Gas Volume Flow, Wet Std. Cond., CFM $Q_{SW} = Q_{SD} * [1/(1 - B_{ws})] =$	9750
Area of Nozzle, ft <sup>2</sup>	

**The Goodyear Tire & Rubber Company Danville, Virginia  
Banbury Mixer No. 7**

**CEC Project No. 132-066**

Summary of Results  
EPA Methods 5 and 202

Determination of Total Particulate Concentrations and Emission Rates

**Example Calculations Run 1**

$$A_n = ((D_n / 2)^2 * 3.14159) / 144 = 0.00034$$

Percent Isokinetic

$$I = (0.0945 * (TS + 460) * V_m (STD)) / (q * VS * PS * (1 - Bws) * A_n) = 101.3$$

Alternative Method 5 Posttest Calibration (ALT-009) Criteria:  $(Y \pm 0.05)$

$$Y_{qa} = (0/V_m) * ((0.319 * T_m) / (\Delta H @ * (P_b + (\Delta H_{avg} / 13.6)))) * (29/M_d)^{1/2} * (\Delta H_{avg})^{1/2} = 0.970$$

Filterable Particulate Matter (PM) Concentration and Emission Rates

Filterable Particulate Concentration, gr/dscf (At Standard Conditions)

$$C_s = 0.015432358 \text{ grain} / 1 \text{ mg} * m_n / V_{STD} = 0.00052$$

Filterable Particulate Matter Concentration, mg/dscm

$$C_{sm} = \text{mass (mg)} / (V_{mstd} (\text{dscf}) * 0.028316847) = 1.20$$

Filterable Particulate Emission Rate, lbs/hr (At Standard Conditions)

$$C_{AW} = 60 \text{ min/hr} / 7000 \text{ grain/lb} * C_s * Q_{sd} = 0.044$$

Standard Conditions 68 Deg. F, 29.92 in. Hg

Pstd = 29.92 in. Hg

Tstd = 528 °R

TEST RESULTS and DATA ANALYSIS SHEET

Location: Banbury Mixer # 7 Start Time: 9:55 RUN No. 1  
 Date: 24-Oct-2013 End Time: 12:10 JOB No. 132-066

STACK DATA	Molecular Weight	EQUIPMENT	AVERAGE TEST DATA
% Moisture: <u>2</u> % est.	%CO2: <u>0.00</u> %	METER BOX: <u>300.392</u>	Average ΔP: <u>0.45</u> in H <sub>2</sub> O
Barometric: <u>29.65</u> in Hg	%O2: <u>20.90</u> %	Y: <u>0.990</u>	Average T <sub>m</sub> : <u>525.5</u> °R
Static Press: <u>-0.25</u> in H <sub>2</sub> O	%N2/CO: <u>79.10</u> %	ΔH@: <u>1.912</u> in H <sub>2</sub> O	Average T <sub>s</sub> : <u>526.8</u> °R
Stack Press: <u>29.63</u> in Hg	Md: <u>28.84</u> lb/lb-mole	Cp': <u>0.765</u> S/N -	Average ΔH: <u>0.51</u> in H <sub>2</sub> O
Stack Area: <u>4.8</u> ft <sup>2</sup>	Actual Mw: <u>28.77</u> lb/lb-mole	Cp: <u>0.765</u> S/N -	T <sub>std</sub> : <u>528.00</u> °R
# of Points: <u>24</u> points	Run Time: <u>115.00</u> min	Nozzle Dia: <u>0.193</u> inches	P <sub>std</sub> : <u>29.92</u> in Hg

<PM <sub>2.5</sub> Filter Analysis	<PM <sub>2.5</sub> Recovery Analysis	Moisture Analysis
Container 1: <u>0</u> mg	Container 4: <u>2.2</u> mg	Container 6: <u>207.3</u> g
C1 + Filter Tare: _____ mg	Cont. 4 Tare: _____ mg	Silica Gel Tare: <u>200</u> g
Acetone V <sub>aw1</sub> : _____ ml	Acetone V <sub>aw4</sub> : _____ ml	M <sub>sg</sub> : <u>7.3</u> g
Acetone W <sub>a1</sub> : _____ mg	Acetone W <sub>a4</sub> : _____ mg	V <sub>wsg(std)</sub> : <u>0.344</u> scf
(Filter) M <sub>1</sub> : <u>0.00</u> mg	(PM <sub>2.5</sub> ) M <sub>4</sub> : <u>2.200</u> mg	Container 5: <u>-1.7</u> ml
>PM <sub>10</sub> Recovery Analysis	PM <sub>2.5-10</sub> Recovery Analysis	V <sub>wc(std)</sub> : <u>-0.080</u> scf
Container 2: _____ mg	Container 3: <u>0.62</u> mg	V <sub>ws</sub> : <u>0.264</u> scf
Cont. 2 Tare: _____ mg	Cont. 3 Tare: _____ mg	B <sub>ws</sub> : <u>0.006</u> H <sub>2</sub> O
Acetone V <sub>aw2</sub> : _____ ml	Acetone V <sub>aw3</sub> : _____ ml	Actual % H <sub>2</sub> O: <u>0.6</u> %
Acetone W <sub>a2</sub> : _____ mg	Acetone W <sub>a3</sub> : _____ mg	Acetone Blank Analysis
(PM <sub>2.5</sub> ) M <sub>2</sub> : _____ mg	(PM <sub>10-2.5</sub> ) M <sub>3</sub> : <u>0.620</u> mg	Container 7: <u>2300.1</u> mg
		Container 7 Tare: <u>2299.9</u> mg
		Acetone Density ρ <sub>a</sub> : <u>0.000791</u> mg/ml
		Blank Volume V <sub>aw</sub> : <u>200</u> ml
		Blank Conc. C <sub>a</sub> : <u>1.264222503</u> mg <sub>f</sub> /mg <sub>v</sub>

CALCULATIONS AND DATA ANALYSIS

V<sub>m</sub>: 46.150 acf - [Actual Sample Volume]  
 V<sub>ms</sub>: 45.545 dscf - [Corrected Sample Volume (std)]  
 V<sub>ws</sub>: 0.264 scf - [Volume of Water Vapor]      μ: 184.362 mpoise - [Actual Gas Viscosity]  
 Q<sub>Sst</sub>: 0.396 dscfm - [Corrected Dry Sampling Rate (std)]      C: 1.0651 [Cunningham Correction Factor]  
 Q<sub>s</sub>: 0.401 acfm - [Actual Final Sampling Rate]      D<sub>50</sub>: 10.911 μmeter - D50 for Cyclone 1  
 I: 97.405 % - [Percent Isokinetic Sampling]      D<sub>50IV</sub>: 2.339 μmeter - D50 for Cyclone IV  
 N<sub>re</sub>: 3044 [Actual Reynolds Number]      Q<sub>sd(stack)</sub>: 574,797 dscf/hr - [Dry Stack Flow Rate (std)]  
 V<sub>s(avg)</sub>: 33.80 fps - [Average Stack Velocity]      Q<sub>sw(stack)</sub>: 578,123 scf/hr - [Wet Stack Flow Rate (std)]

Concentrations

PM<sub>10</sub>: 0.00096 gr/dscf

Emission Rates

PM<sub>10</sub>: 0.0785 lb/hr

TEST RESULTS and DATA ANALYSIS SHEET

Location: Banbury Mixer # 7 Start Time: 13:43:00 RUN No. 2  
 Date: 24-Oct-2013 End Time: 15:50:00 JOB No. 132-066

STACK DATA	Molecular Weight	EQUIPMENT	AVERAGE TEST DATA
% Moisture: <u>2</u> % est.	%CO2: <u>0.00</u> %	METER BOX: <u>300.392</u>	Average ΔP: <u>0.39</u> in H <sub>2</sub> O
Barometric: <u>29.62</u> in Hg	%O2: <u>20.90</u> %	Y: <u>0.990</u>	Average T <sub>m</sub> : <u>530.9</u> °R
Static Press: <u>-0.25</u> in H <sub>2</sub> O	%N2/CO: <u>79.10</u> %	ΔH@: <u>1.912</u> in H <sub>2</sub> O	Average T <sub>s</sub> : <u>531.9</u> °R
Stack Press: <u>29.60</u> in Hg	Md: <u>28.84</u> lb/lb-mole	Cp': <u>0.765</u> S/N <u>-</u>	Average ΔH: <u>0.55</u> in H <sub>2</sub> O
Stack Area: <u>4.8</u> ft <sup>2</sup>	Actual Mw: <u>28.75</u> lb/lb-mole	Cp: <u>0.765</u> S/N <u>-</u>	T <sub>std</sub> : <u>528.00</u> °R
# of Points: <u>24</u> points	Run Time: <u>108.00</u> min	Nozzle Dia: <u>0.1940</u> inches	P <sub>std</sub> : <u>29.92</u> in Hg

<PM <sub>2.5</sub> Filter Analysis	<PM <sub>2.5</sub> Recovery Analysis	Moisture Analysis
Container 1: <u>0</u> mg	Container 4: <u>1</u> mg	Container 6: <u>208.4</u> g
C1 + Filter Tare: _____ mg	Cont. 4 Tare: _____ mg	Silica Gel Tare: <u>200</u> g
Acetone V <sub>aw1</sub> : _____ ml	Acetone V <sub>aw4</sub> : _____ ml	M <sub>sg</sub> : <u>8.4</u> g
Acetone W <sub>a1</sub> : _____ mg	Acetone W <sub>a4</sub> : _____ mg	V <sub>wsg(std)</sub> : <u>0.395</u> scf
(Filter) M <sub>1</sub> : <u>0.000</u> mg	(PM <sub>2.5</sub> ) M <sub>4</sub> : <u>1.000</u> mg	Container 5: <u>-0.4</u> ml
>PM <sub>10</sub> Recovery Analysis	PM <sub>2.5-10</sub> Recovery Analysis	V <sub>wc(std)</sub> : <u>-0.019</u> scf
Container 2: _____ mg	Container 3: <u>0.31</u> mg	V <sub>ws</sub> : <u>0.377</u> scf
Cont. 2 Tare: _____ mg	Cont. 3 Tare: _____ mg	B <sub>ws</sub> : <u>0.008</u> H <sub>2</sub> O
Acetone V <sub>aw2</sub> : _____ ml	Acetone V <sub>aw3</sub> : _____ ml	Actual % H <sub>2</sub> O: <u>0.8</u> %
Acetone W <sub>a2</sub> : _____ mg	Acetone W <sub>a3</sub> : _____ mg	Acetone Blank Analysis
(PM <sub>2.5</sub> ) M <sub>2</sub> : _____ mg	(PM <sub>10-2.5</sub> ) M <sub>3</sub> : <u>0.310</u> mg	Container 7: _____ mg
		Container 7 Tare: _____ mg
		Acetone Density ρ <sub>a</sub> : _____ mg/ml
		Blank Volume V <sub>aw</sub> : _____ ml
		Blank Conc.C <sub>a</sub> : _____ mg <sub>r</sub> /mg <sub>v</sub>

CALCULATIONS AND DATA ANALYSIS

V<sub>m</sub>: 45.949 acf - [Actual Sample Volume]  
 V<sub>ms</sub>: 44.847 dscf - [Corrected Sample Volume (std)]  
 V<sub>ws</sub>: 0.377 scf - [Volume of Water Vapor] μ: 185.33 mpoise - [Actual Gas Viscosity]  
 Q<sub>Sst</sub>: 0.415 dscfm - [Corrected Dry Sampling Rate (std)] C: 1.070 [Cunningham Correction Factor]  
 Q<sub>s</sub>: 0.426 acfm - [Actual Final Sampling Rate] D<sub>50</sub>: 10.52 μmeter - D50 for Cyclone 1  
 I: 109.4 % - [Percent Isokinetic Sampling] D<sub>50IV</sub>: 2.207 μmeter - D50 for Cyclone IV  
 N<sub>re</sub>: 3180 [Actual Reynolds Number] Q<sub>sd(stack)</sub>: 531,069 dscf/hr - [Dry Stack Flow Rate (std)]  
 V<sub>s(avg)</sub>: 31.64 fps - [Average Stack Velocity] Q<sub>sw(stack)</sub>: 535,528 scf/hr - [Wet Stack Flow Rate (std)]

Concentrations

PM<sub>10</sub>: 0.00045 gr/dscf

Emission Rates

PM<sub>10</sub>: 0.0342 lb/hr

TEST RESULTS and DATA ANALYSIS SHEET

Location: <u>Banbury Mixer # 7</u>	Start Time: <u>16:30:00</u>	RUN No. <u>3</u>
Date: <u>24-Oct-2013</u>	End Time: <u>18:48:00</u>	JOB No. <u>132-066</u>

STACK DATA	Molecular Weight	EQUIPMENT	AVERAGE TEST DATA
% Moisture: <u>2</u> % est.	%CO2: <u>0.00</u> %	METER BOX: <u>300.392</u>	Average ΔP: <u>0.46</u> in H <sub>2</sub> O
Barometric: <u>29.56</u> in Hg	%O2: <u>20.90</u> %	Y: <u>0.990</u>	Average T <sub>m</sub> : <u>525.8</u> °R
Static Press: <u>-0.25</u> in H <sub>2</sub> O	%N2/CO: <u>79.10</u> %	ΔH@: <u>1.912</u> in H <sub>2</sub> O	Average T <sub>s</sub> : <u>530.2</u> °R
Stack Press: <u>29.54</u> in Hg	Md: <u>28.84</u> lb/lb-mole	Cp: <u>0.765</u> S/N <u>-</u>	Average ΔH: <u>0.54</u> in H <sub>2</sub> O
Stack Area: <u>4.8</u> ft <sup>2</sup>	Actual Mw: <u>28.73</u> lb/lb-mole	Cp: <u>0.765</u> S/N <u>-</u>	T <sub>std</sub> : <u>528.00</u> °R
# of Points: <u>24</u> points	Run Time: <u>128.00</u> min	Nozzle Dia: <u>0.1930</u> inches	P <sub>std</sub> : <u>29.92</u> in Hg

<u>&lt;PM<sub>2.5</sub> Filter Analysis</u>	<u>&lt;PM<sub>2.5</sub> Recovery Analysis</u>	<u>Moisture Analysis</u>
Container 1: <u>0</u> mg	Container 4: <u>0</u> mg	Container 6: <u>214.9</u> g
C1 + Filter Tare: _____ mg	Cont. 4 Tare: _____ mg	Silica Gel Tare: <u>200</u> g
Acetone V <sub>aw1</sub> : _____ ml	Acetone V <sub>aw4</sub> : _____ ml	M <sub>sg</sub> : <u>14.9</u> g
Acetone W <sub>a1</sub> : _____ mg	Acetone W <sub>a4</sub> : _____ mg	V <sub>wsg(std)</sub> : <u>0.701</u> scf
(Filter) M <sub>1</sub> : <u>0.000</u> mg	(PM <sub>2.5</sub> ) M <sub>4</sub> : <u>0.000</u> mg	Container 5: <u>-3.7</u> ml
<u>&gt;PM<sub>10</sub> Recovery Analysis</u>	<u>PM<sub>2.5-10</sub> Recovery Analysis</u>	V <sub>wc(std)</sub> : <u>-0.174</u> scf
Container 2: _____ mg	Container 3: <u>0.55</u> mg	V <sub>ws</sub> : <u>0.527</u> scf
Cont. 2 Tare: _____ mg	Cont. 3 Tare: _____ mg	B <sub>ws</sub> : <u>0.010</u> H <sub>2</sub> O
Acetone V <sub>aw2</sub> : _____ ml	Acetone V <sub>aw3</sub> : _____ ml	Actual % H <sub>2</sub> O: <u>1.0</u> %
Acetone W <sub>a2</sub> : _____ mg	Acetone W <sub>a3</sub> : _____ mg	<u>Acetone Blank Analysis</u>
(PM <sub>2.5</sub> ) M <sub>2</sub> : _____ mg	(PM <sub>10-2.5</sub> ) M <sub>3</sub> : <u>0.550</u> mg	Container 7: _____ mg
		Container 7 Tare: _____ mg
		Acetone Density ρ <sub>a</sub> : _____ mg/ml
		Blank Volume V <sub>aw</sub> : _____ ml
		Blank Conc. C <sub>a</sub> : _____ mg <sub>f</sub> /mg <sub>v</sub>

**CALCULATIONS AND DATA ANALYSIS**

V <sub>m</sub> : <u>54.206</u> acf - [Actual Sample Volume]	μ: <u>184.769</u> mpoise - [Actual Gas Viscosity]
V <sub>ms</sub> : <u>53.31</u> dscf - [Corrected Sample Volume (std)]	C: <u>1.070</u> [Cunningham Correction Factor]
V <sub>ws</sub> : <u>0.527</u> scf - [Volume of Water Vapor]	D <sub>50</sub> : <u>10.47</u> μmeter - D50 for Cyclone 1
Q <sub>Sst</sub> : <u>0.417</u> dscfm - [Corrected Dry Sampling Rate (std)]	D <sub>50IV</sub> : <u>2.19</u> μmeter - D50 for Cyclone IV
Q <sub>s</sub> : <u>0.428</u> acfm - [Actual Final Sampling Rate]	Q <sub>sd(stack)</sub> : <u>582,079</u> dscf/hr - [Dry Stack Flow Rate (std)]
I: <u>101.2</u> % - [Percent Isokinetic Sampling]	Q <sub>sw(stack)</sub> : <u>587,835</u> scf/hr - [Wet Stack Flow Rate (std)]
N <sub>re</sub> : <u>3202</u> [Actual Reynolds Number]	
V <sub>s(avg)</sub> : <u>34.69</u> fps - [Average Stack Velocity]	

**Concentrations**

PM<sub>10</sub>: 0.00016 gr/dscf

**Emission Rates**

PM<sub>10</sub>: 0.0132 lb/hr

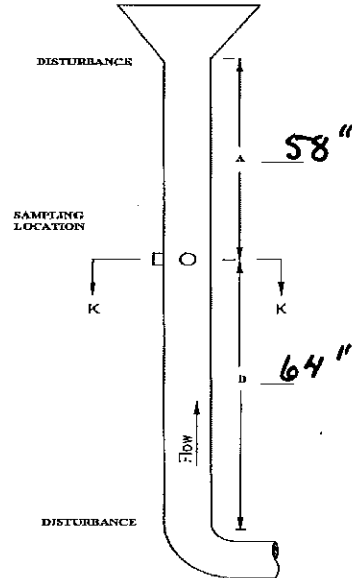
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**APPENDIX B**  
**FIELD DATA SHEETS**

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## EPA Method 1 Determination of Sampling Ports and Points

Client Goodyear Tire & Rubber Company City/State Danville, VA  
 Sampling Location Banbury Mixer #7 Stack Date 10/23/13  
 Sampling Location Dimensions, in inches: Port A Port B  
 From Far Wall to Outside of Port 35.75 / 35.50  
 Nipple Length 6.0 6.0  
 Depth of Duct 29.75 29.50  
 Width (Rectangular Duct)         



**Equivalent Diameter Calculation (DE):**

$$DE = \frac{2 \times \text{Length} \times \text{Width}}{\text{Length} + \text{Width}} = \frac{2(-)(-)}{(-) + (-)} = \underline{\quad}$$

**Distance to Ports From Nearest Flow Disturbance:**

Upstream - A      Downstream - B  
 Dimensions in Inches      58"      64"  
 Duct Diameters      1.97      2.17  
 Stack Area, in Square Feet      4787  
 Calculations By WGS

*Schematic of Sampling Location*

	4	6	8	10	12
1	6.7	4.4	3.2	2.6	2.1
2	25.0	14.6	10.5	8.2	6.7
3	75.0	29.6	19.4	14.6	11.8
4	93.3	70.4	32.3	22.6	17.7
5		85.4	67.7	34.2	25.0
6		95.6	80.6	65.8	35.6
7			89.5	77.4	64.4
8			96.8	85.4	75.0
9				91.8	82.3
10				97.4	88.2
11					93.3
12					97.9

	2	3	4	5	6	7	8
1	25.0	16.7	12.5	10.0	8.3	7.1	6.3
2	75.0	50.0	37.5	30.0	25.0	21.4	18.8
3		83.3	62.5	50.0	41.7	35.7	31.3
4			87.5	70.0	58.3	50.0	43.8
5				90.0	75.0	64.3	56.3
6					91.7	78.6	68.8
7						92.9	81.3
8							93.8
9							
10							
11							
12							

Point	% of Stack ID	Stack ID, in.	Distance From Inside Wall, in.	Nipple Length, in.	Distance From Outside of Port, in.
1	2.1	29.50	0.62	6.0	6.62 → 7.0
2	6.7		1.98		7.98
3	11.8		3.48		9.48
4	17.7		5.22		11.22
5	25.0		7.38		13.38
6	35.6		10.5		16.5
7	64.4		19.0		25.0
8	75.0		22.13		28.13
9	82.3		24.28		30.28
10	88.2		26.02		32.02
11	93.3		27.52		33.52
12	97.9		28.88		34.88 → 34.5

Stack Diameter = 12 - 24 inches Relocate to 0.50 inches from stack wall  
 Stack Diameter > 24 inches Relocate to 1.00 inches from stack wall

Audited by: 10 (Personnel)      Date: 11/18/13      Completeness       Legibility       Accuracy   
 Audited by: WGS (Team Leader)      Date: 11/11/13      Specifications       Reasonableness

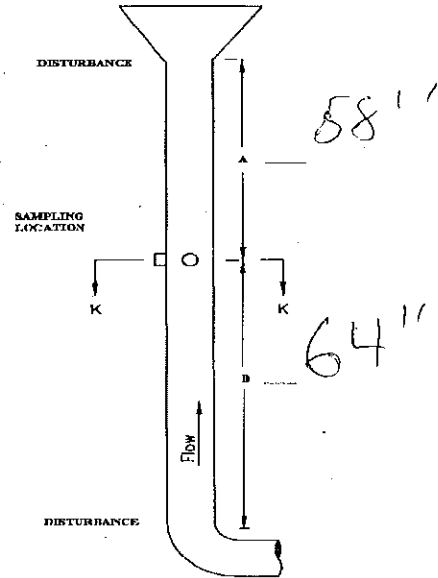


## EPA Method 1 Determination of Sampling Ports and Points

Client Goodyear Tire & Rubber Company City/State Danville, VA  
 Sampling Location Banbury Mixer #7 Stack Date 10/23/13

**Sampling Location Dimensions, in inches:**

From Far Wall to Outside of Port 35.75 / 35.50  
 Nipple Length 6.0 / 6.0  
 Depth of Duct 29.75 / 29.50 = 29.625  
 Width (Rectangular Duct) -



**Equivalent Diameter Calculation (DE):**

$$DE = \frac{2 \times \text{Length} \times \text{Width}}{\text{Length} + \text{Width}} = \frac{2(-)(-)}{(-)+(-)} = -$$

**Distance to Ports From Nearest Flow Disturbance:**

	Upstream - A	Downstream - B
Dimensions in Inches	<u>58"</u>	<u>64"</u>
Duct Diameters	<u>1.95"</u>	<u>2.15"</u>
Stack Area, in Square Feet	<u>4.787</u>	<u>(29.625)</u>

Calculations By JAJ

*Schematic of Sampling Location*

	4	6	8	10	12
1	6.7	4.4	3.2	2.6	2.1
2	25.0	14.6	10.5	8.2	6.7
3	75.0	29.6	19.4	14.6	11.8
4	93.3	70.4	32.3	22.6	17.7
5		85.4	67.7	34.2	25.0
6		95.6	80.6	65.8	35.6
7			89.5	77.4	64.4
8			96.8	85.4	75.0
9				91.8	82.3
10				97.4	88.2
11					93.3
12					97.9

Point	% of Stack ID	Stack ID, in.	Distance From Inside Wall, in.	Nipple Length, in.	Distance From Outside of Port, in.
1	2.1	29.50	0.62	6.0	6.62 → 7.00
2	6.7		1.98		7.98
3	11.8		3.50		10.50
4	17.7		5.24		11.24
5	25.0		7.41		13.41
6	35.6		10.55		16.55
7	64.4		19.08		25.08
8	75.0		27.22		28.22
9	82.3		24.38		30.38
10	88.2		26.13		32.13
11	93.3		27.64		33.64
12	97.9		29.00		35.00 → 34.5
1'					

	2	3	4	5	6	7	8
1	25.0	16.7	12.5	10.0	8.3	7.1	6.3
2	75.0	50.0	37.5	30.0	25.0	21.4	18.8
3		83.3	62.5	50.0	41.7	35.7	31.3
4			87.5	70.0	58.3	50.0	43.8
5				90.0	75.0	64.3	56.3
6					91.7	78.6	68.8
7						92.9	81.3
8							93.8
9							
10							
11							
12							

Stack Diameter = 12 - 24 inches Relocate to 0.50 inches from stack wall  
 Stack Diameter > 24 inches Relocate to 1.00 inches from stack wall

Audited by: MY (Personnel) Date: 11/11/13 Completeness  Legibility  Accuracy   
 Audited by: WAS (Team Leader) Date: 11/18/13 Specifications  Reasonableness





## EPA Method 2 Determination of Stack Gas Velocity, Volumetric Flow Rate and Cyclonic Flow

Client Goodyear  
 Sampling Location Banding Mixer #7 Stack  
 Run Date 10/23/13  
 Barometric Pressure, in. Hg 29.55  
 Static Pressure, in. H<sub>2</sub>O -0.40  
 Pitot Tube Coefficient 0.84

City, State Danville, VA  
 Operators [Signature]  
 Time 1:50  
 Pitot Tube I.D. No. 200711  
 Date Calibrated 1511  
 Leak Check, in. H<sub>2</sub>O <0.1 @ 3.5/-3.0

### Field Data

Traverse Point Number	Velocity Head Δp Inches H <sub>2</sub> O		Stack Temperature °F		Cyclonic Flow Determination			
	A	B	A	B	A		B	
					Ap, at 0° Reference		Angle Which Yields a Null Ap	
1	0.59	0.57	73	73	0.11	0.08	8°	8°
2	0.55	0.59	74	73	0.11	0.09	8°	9°
3	0.50	0.55	74	74	0.14	0.09	10°	10°
4	0.53	0.50	75	74	0.12	0.10	14°	10°
5	0.52	0.38	75	74	0.13	0.11	12°	14°
6	0.45	0.30	75	74	0.11	0.14	13°	15°
7	0.30	0.44	75	74	0.05	0.09	10°	12°
8	0.26	0.45	75	74	∅	0.06	∅	10°
9	0.25	0.43	75	74	∅	0.06	∅	9°
10	0.20	0.40	75	74	∅	0.07	∅	9°
11	0.15	0.38	75	74	∅	0.06	∅	11°
12	0.13	0.36	75	74	∅	0.08	∅	30°
Averages		0.408	74.25				was 4.68 9.3	

Stack Temperature, Dry, °F (A) — Stack Temperature, Wet °F (B) —  
 Difference (A - B) — Preliminary Percent Moisture 2

Comments \_\_\_\_\_

Audited by: ME (Personnel) Date: 11/18/13 Completeness  Legibility  Accuracy   
 Audited by: WGB (Team Leader) Date: 11/13/13 Specifications  Reasonableness



Isokinetic Field Data Sheet - EPA Method 5/20

Client The Goodyear Tire and Rubber Company

Run Number 1

City/State Danville, VA

Date 10/24/13

Sampling Location Unit No. 7 - Bunking Mixer

Operators WOB/BLS JAS

Bar. Press., In. Hg 29.62

NOMOGRAPH SET-UP: K Factor 4.24

LEAK CHECKS

Static Press., In. H<sub>2</sub>O -0.25

ΔH @ 1.956 Y = 0.986 Avg. ΔP 0.41

Pre-Test 0.002 @ 14 In. Hg.

Meter Box No. 300.390

Meter Temp. 45.63 Ref. ΔP ---

Post-Test 0.002 @ 5.0 In. Hg.

Sample Box No. D

Stack Temp. 45.65 Desired Nozzle 0.26

Pre-Test Pitot <0.1 @ 9.2/46 In. H<sub>2</sub>O

Probe/Pitot No. 200.077

Pitot Coeff. 0.84 Nozzle No. 300.192

Post-Test Pitot <0.1 @ 16.0/30 In. H<sub>2</sub>O

Probe Temp. Setting 250

% Moisture 2 Nozzle Calibration 248, 248, 247

Observer ---

Sample ID No. 132066-01

C Factor --- Nozzle Diameter 248

Agency VADEQ

Filter No. 5822

Start Time 0955 End Time 1210

Sample Point	Clock Time	Dry Gas Meter Cubic Feet	Pitot Reading ΔP In. H <sub>2</sub> O	Orifice Setting ΔH Inches H <sub>2</sub> O		Dry Gas Meter Temp. °F	Pump Vacuum Inches Hg	Stack Temp °F	Probe Temp °F	Filter Exhaust °F	CFM Filter Exhaust °F	Impinger Temp °F
				Ideal	Actual							
A1	0	975.900	0.15	0.64	0.65	58	1	61	253	264	52	52
2	5	978.10	0.18	0.76	0.75	62	1	62	244	270	52	44
3	10	980.61	0.24	1.02	1.00	62	1	63	255	265	52	43
4	15	983.22	0.24	1.02	1.00	63	1	65	253	261	52	44
5	20	986.24	0.30	1.27	1.25	65	1	65	248	265	53	45
6	25	989.31	0.30	1.27	1.25	65	1	65	246	265	54	45
7	30	992.40	0.41	1.74	1.75	67	1	66	249	264	54	46
8	35	996.10	0.41	1.74	1.75	68	1	66	250	258	57	46
9	40	999.71	0.55	2.33	2.35	70	1	66	250	264	57	48
10	45	3.94	0.55	2.33	2.35	71	1	67	245	262	58	49
11	50	8.42	0.55	2.33	2.35	72	1	67	250	261	58	50
12	55	12.65	0.55	2.33	2.35	72	1	68	250	258	58	50
B1	60	17.015	0.40	1.70	1.70	73	1	68	245	244	58	55
2	65	20.75	0.40	1.70	1.70	75	1	66	250	246	60	51
3	70	24.38	0.40	1.70	1.70	75	1	68	249	248	61	52
4	75	27.91	0.40	1.70	1.70	75	1	69	250	251	61	52
5	80	31.83	0.40	1.70	1.70	74	1	69	249	249	61	52
6	85	35.69	0.40	1.70	1.70	76	1	69	245	250	61	58
7	90	39.31	0.29	1.23	1.25	79	1	69	248	253	66	51
8	95	42.47	0.29	1.23	1.25	79	1	69	246	250	59	51
9	100	45.70	0.37	1.57	1.55	80	1	70	238	244	59	51
10	105	49.24	0.42	1.78	1.80	80	1	70	251	251	60	50
11	110	52.97	0.44	1.87	1.85	80	1	70	249	245	60	50
12	115	56.90	0.44	1.87	1.85	80	1	70	250	246	60	50
	120	60.609										
		84.709	0.378		1.606	71.7		67.0				

Comments:

Isokinetic Check:

Audited by: WOB (Personnel) Date: 11/18/13 Completeness  Legibility  Accuracy

Audited by: WOB (Team Leader) Date: 11/11/13 Specifications  Reasonableness



Isokinetic Field Data Sheet - EPA Method 5/202

Client The Goodyear Tire and Rubber Company

Run Number 2

City/State Danville, VA

Date 10/24/13

Sampling Location Unit No. 7 - Bamberg Mixer

Operators WOB/BLS JAJ

Bar. Press., In. Hg 29.62

NOMOGRAPH SET-UP: K Factor 4.100/4.062

LEAK CHECKS

Static Press., In. H<sub>2</sub>O -0.25

$\Delta H @ 1.956 \quad Y = 0.986$

Avg.  $\Delta P$  0.378

Pre-Test 0.003 @ 14.0 In. Hg.

Meter Box No. 300.370

Meter Temp. 85

Ref.  $\Delta P$  —

Post-Test 0.005 @ 6.5 In. Hg.

Sample Box No. D

Stack Temp. 70

Desired Nozzle 0.256

Pre-Test Pitot <0.1 @ 49.0/4.1 In. H<sub>2</sub>O

Probe/Pitot No. 200.080

Pitot Coeff. 0.84

Nozzle No. 300.488

Post-Test Pitot <0.1 @ 17.0/3.2 In. H<sub>2</sub>O

Probe Temp. Setting 250

% Moisture 2

Nozzle Calibration 0.243, 0.244, 0.245

Sample ID No. 132066-02

C Factor —

Nozzle Diameter 0.244

Observer —

Filter No. 5623

Start Time 1343

End Time 1554

Agency VADEQ

Sample Point	Clock Time	Dry Gas Meter Cubic Feet	Pitot Reading $\Delta P$ In. H <sub>2</sub> O	Orifice Setting $\Delta H$ Inches H <sub>2</sub> O		Dry Gas Meter Temp. °F	Pump Vacuum Inches Hg	Stack Temp °F	Probe Temp °F	Filter Exhaust °F	Impinger Filter Exhaust °F	Impinger Temp °F
				Ideal	Actual							
A1	0	64.468	0.52	2.13	2.15	69	1	68	245	248	57	55
2	5	68.60	0.49	2.00	2.00	72	1	71	253	249	58	59
3	10	72.50	0.49	2.00	2.00	72	1	71	254	250	59	59
4	15	76.45	0.45	1.85	1.85	72	1	70	249	250	60	64
5	20	80.44	0.45	1.85	1.85	72	1	71	247	250	62	65
6	25	84.30	0.45	1.85	1.85	72	1	72	243	245	65	65
7	30	88.21	0.45	1.85	1.85	72	1	73	247	250	64	64
8	35	92.70	0.49	2.00	2.00	74	1	72	243	254	65	63
9	40	95.69	0.45	1.85	1.85	76	1	72	245	251	65	63
10	45	99.58	0.42	1.72	1.70	78	1	70	248	250	65	62
11	50	103.41	0.42	1.72	1.70	80	1	72	245	255	65	62
12	55	107.31	0.15	0.62	0.62	80	1	70	243	255	65	61
B1	60	109.483	0.325	1.34	1.30	77	1	73	241	250	60	57
2	65	112.90	0.24	0.98	0.98	78	1	73	243	249	61	56
3	70	115.62	0.21	0.85	0.85	78	1	74	247	257	61	55
4	75	118.22	0.24	0.98	0.98	78	1	73	244	262	60	56
5	80	121.02	0.28	1.14	1.10	77	1	73	242	255	60	56
6	85	124.44	0.34	1.38	1.40	78	1	72	246	260	60	57
7	90	127.41	0.47	1.91	1.90	77	3	73	252	257	60	57
8	95	131.434	0.57	2.32	2.30	77	4	74	247	249	61	58
9	100	135.69	0.58	2.36	2.35	78	4	74	245	261	62	59
10	105	139.94	0.56	2.28	2.30	80	3.5	73	243	257	62	61
11	110	144.27	0.57	2.32	2.30	80	3.5	72	240	262	63	61
12	115	148.46	0.59	2.40	2.40	79	3.5	72	249	258	64	62
1	120	152.804	0.426	✓	✓	76.08	✓	72.0	✓			
		888336	0.43	✓	1.74	76.08	✓	72.0	✓			

Comments:

Isokinetic Check: OK

Audited by: M (Personnel) Date: 11/8/13 Completeness  Legibility  Accuracy   
 Audited by: WOB (Team Leader) Date: 11/11/13 Specifications  Reasonableness



Isokinetic Field Data Sheet - EPA Method 5/20

Client The Goodyear Tire and Rubber Company

Run Number 3

City/State Danville, VA

Date 10/24/13

Sampling Location Unit No. 7 - Banding Mixer

Operators WOB/BES JAJ

Bar. Press., In. Hg 29.56

NOMOGRAPH SET-UP: K Factor 4.239

LEAK CHECKS

Static Press., In. H<sub>2</sub>O -.25

AH @ 1956 Y = 0.986

Avg. ΔP 0.426

Pre-Test 0.005 @ 13.0 In. Hg.

Meter Box No. 360.390

Meter Temp. 70

Ref. ΔP -

Post-Test 0.001 @ 5 In. Hg.

Sample Box No. 0

Stack Temp. 72

Desired Nozzle 0.252

Pre-Test Pitot <0.1 @ +6.5/-4.1 In. H<sub>2</sub>O

Probe/Pitot No. 200.077

Pitot Coeff. 0.84

Nozzle No. 360.192

Post-Test Pitot <0.1 @ 8.3/3.7 In. H<sub>2</sub>O

Probe Temp. Setting 250

% Moisture 2

Nozzle Calibration 1,248, 248, 247

Sample ID No. 132066-03

C Factor -

Nozzle Diameter 1.248

Observer -

Filter No. 5624

Start Time 16:30

End Time 16:44

Agency VADEQ

Sample Point	Clock Time	Dry Gas Meter Cubic Feet	Pitot Reading ΔP In. H <sub>2</sub> O	Orifice Setting ΔH Inches H <sub>2</sub> O		Dry Gas Meter Temp. °F	Pump Vacuum Inches Hg	Stack Temp °F	Probe Temp °F	Filter Exhaust °F	Impinger Filter Exhaust °F	Impinger Temp °F
				Ideal	Actual							
A1	0	<del>153.075</del> 153.075	0.20	0.85	0.85	67	1	70	252	248	55	54
2	5	155.80	0.20	0.85	0.85	67	1	70	255	251	55	54
3	10	158.35	0.28	1.19	1.20	68	1	70	254	250	55	52
4	15	161.41	0.28	1.19	1.20	69	1	71	252	251	55	51
5	20	164.39	0.32	1.36	1.35	69	1	71	254	256	55	52
6	25	167.60	0.34	1.44	1.45	69	1	71	252	254	55	52
7	30	170.81	0.39	1.65	1.65	69	1	71	250	260	54	53
8	35	174.35	0.57	2.42	2.40	69	2	71	246	254	57	53
9	40	178.68	0.58	2.46	2.45	69	2	71	248	252	57	53
10	45	183.19	0.56	2.37	2.35	69	2	71	249	260	56	55
11	50	187.34	0.56	2.37	2.35	70	2	70	245	250	58	56
12	55	191.65	0.55	2.33	2.35	70	2	71	249	257	59	56
B1	60	195.939	0.38	1.35	1.35	66	1	71	252	256	55	54
2	65	199.06	0.31	1.31	1.30	67	1	71	255	252	55	54
3	70	202.19	0.42	1.78	1.80	67	1	71	246	246	56	55
4	75	206.17	0.44	1.87	1.85	67	1	71	247	258	56	58
5	80	209.93	0.46	1.95	1.95	67	1.5	71	251	256	57	60
6	85	213.64	0.45	1.91	1.90	67	1.5	70	246	257	56	60
7	90	217.35	0.46	1.95	1.95	67	1.5	70	245	255	56	60
8	95	221.24	0.32	1.36	1.35	67	1	69	244	253	56	60
9	100	224.38	0.40	1.70	1.70	67	1	70	257	250	56	60
10	105	227.96	0.45	1.91	1.90	66	1	69	251	248	55	60
11	110	231.82	0.48	2.04	2.05	64	1.5	69	251	246	56	60
12	115	235.78	0.49	2.08	2.10	64	1.5	68	248	246	56	60
	120	239.74										
		86.523	0.409	1.733	1.705	67.705		70.338				

Comments:

Isokinetic Check: 100.141

Audited by: 10 (Personnel) Date: 11/13/13 Completeness  Legibility  Accuracy

Audited by: WOB (Team Leader) Date: 11/11/13 Specifications  Reasonableness



Methods 5 & 202 and Sample Recovery – Data Analysis

Client Name Goodyear Project Number 132-066  
 City/State Danville, VA Sample Date 10/24/13  
 Sampling Location Banbury Mixer No. 7 Samples Recovered BU  
 Clean-Up Box Number M5/202 Recovery Date 10/24/13  
 Chain of Custody: Date Received 10/15/13 Received By PRJ Locked?

Equipment Documentation

Run Number	1	2	3
Sample ID Number	132-066-01	132-066-02	132-066-03
Sample Box Number	D	D	D
Probe Number	200.077 300.192	200.080 300.488	200.077 300.192

Sample Recovery – Fraction 1

Filter Container #	<del>BU 5622</del> 5622	5623	5624
Particulate Description	None visible	None visible	None visible
Filter Container Sealed?	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>

Sample Recovery – Fraction 2

Probe Rinse Container #	132066-01	132066-02	132066-03	Acetone
Rinsing Solution	Acetone	Acetone	Acetone	Acetone
Sample Container Sealed?	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	
Liquid Level Marked?	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	

Analysis of Moisture and Sample Recovery – Fraction 3

Reagent Recovery Container	132066-01	132066-02	132066-03	DI H <sub>2</sub> O
Imp. Absorbing Solution	DI H <sub>2</sub> O	DI H <sub>2</sub> O	DI H <sub>2</sub> O	DI H <sub>2</sub> O
Description of Reagent	clear	clear	clear	
Reagent Level Marked?	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	
Final Volume, ml	97.9	92.0	97.6	
Initial Volume, ml	100	100	100	
Net Condensed Volume, ml	-2.1	-8.0	-2.4	
N <sub>2</sub> Purge	1 hour - 14 LPM	1 hour - 14 LPM	1 hour - 14 LPM	
Rinse twice with DI H <sub>2</sub> O	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	
Rinse twice with Acetone	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	
Rinse twice with hexane	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	

Analysis of Moisture and Sample Recovery – Silica Gel

Silica Gel Recovery Container #	1	2	3
Percent Silica Gel Spent	25%	30%	30%
Final Weight, g	213.9	222.2	220.5
Initial Weight, g	200	200	200
Net Absorbed Water, g	13.9	22.2	20.5
Total Moisture Collected, g	11.8	14.2	18.1

200 mL BU Reagent Blanks

Absorbing Reagent Blank (500 mL)	DI H <sub>2</sub> O	Absorbing Blank ID#	132066-09
Rinsing Reagent Blank (200 mL)	Acetone	Rinsing Blank ID #	132066-08
Rinsing Reagent Blank (200 mL)	Hexane	Rinsing Blank ID #	132066-10
Analyst Initials	BLJ	Reviewer Initials	

Balance ID	Wt. (200 mg)	Wt. (500 mg)	Wt. (1,000 mg)
10/23/13	200.0	500.0	1000.0
10/24/13	200.0	499.9	999.9

Audited by: PR (Personnel) Date: 11/18/13 Completeness  Legibility  Accuracy   
 Audited by: LODB (Team Leader) Date: 11/11/13 Specifications  Reasonableness



Method 5 & 202 - Moisture Determination and Sample Recovery

Client Name Goodyear  
 City/State Danville, VA  
 Sampling Location Painbow Mixer No. 7

Project Number: 132-066  
 Sample Date: 10/24/13  
 Samples Recovered by: bv  
 Recovery Date: 10/24/13

Moisture Recovery by weight

Run No.:	Impinger Bottle Weight	Initial wt. (mg)	Final Wt (mg)	Difference (gain) wt.	
1	1 <sup>st</sup> Imp. Bottle	479.8	481.5	-0.7	-2.1
	2 <sup>nd</sup> Imp. Bottle	608.7	609.4	0.7	
	3 <sup>rd</sup> Imp. Bottle	700.2	698.1	-2.1	
	4 <sup>th</sup> Imp. Bottle	796.7	810.6	13.9	
	5 <sup>th</sup> Imp. Bottle				
	6 <sup>th</sup> Imp. Bottle				TC = 11.80 grams

Run No.:	Impinger Bottle Weight	Initial wt. (mg)	Final Wt (mg)	Difference (gain) wt.	
2	1 <sup>st</sup> Imp. Bottle	485.1	484.1	-1.0	-8.0
	2 <sup>nd</sup> Imp. Bottle	596.8	597.4	0.6	
	3 <sup>rd</sup> Imp. Bottle	709.4	701.8	-7.6	
	4 <sup>th</sup> Imp. Bottle	806.4	828.6	22.2	
	5 <sup>th</sup> Imp. Bottle				
	6 <sup>th</sup> Imp. Bottle				TC = 14.2 grams

Run No.:	Impinger Bottle Weight	Initial wt. (mg)	Final Wt (mg)	Difference (gain) wt.	
3	1 <sup>st</sup> Imp. Bottle	479.3	479.4	0.1	-2.4
	2 <sup>nd</sup> Imp. Bottle	606.8	607.2	0.4	
	3 <sup>rd</sup> Imp. Bottle	691.0	688.1	-2.9	
	4 <sup>th</sup> Imp. Bottle	794.1	814.6	20.5	
	5 <sup>th</sup> Imp. Bottle				
	6 <sup>th</sup> Imp. Bottle				TC = 18.1 grams

Run No.:	Impinger Bottle Weight	Initial wt. (mg)	Final Wt (mg)	Difference (gain) wt.	
	1 <sup>st</sup> Imp. Bottle				
	2 <sup>nd</sup> Imp. Bottle				
	3 <sup>rd</sup> Imp. Bottle				
	4 <sup>th</sup> Imp. Bottle				
	5 <sup>th</sup> Imp. Bottle				
	6 <sup>th</sup> Imp. Bottle				

Audited by: fw (Personnel)

Date: 11/18/13 Completeness  Legibility  Accuracy

Audited by: was (Team Leader)

Date: 11/11/13 Specifications  Reasonableness



Civil & Environmental Consultants, Inc.

**EPA Method 2**

**Determination of Stack Gas Velocity, Volumetric Flow Rate and Cyclonic Flow**

Client Goodyear Tire & Rubber Company  
 Sampling Location Banbury # 7  
 Run Date 10/24/13  
 Barometric Pressure, in. Hg -0.25 29.65  
 Static Pressure, in. H<sub>2</sub>O ↓  
 Pitot Tube Coefficient 0.765

City, State Danville VA  
 Operators WBS, JAT  
 Time 0800  
 Pitot Tube I.D. No. 200,302/0799  
 Date Calibrated 6/22/13  
 Leak Check, in. H<sub>2</sub>O <0.1 @ 3.8/-3.9

**Field Data**

Traverse Point Number	Velocity Head Δp Inches H <sub>2</sub> O		Stack Temperature °F		Cyclonic Flow Determination		
	A	B	A	B	Δp, at 0° Reference	Angle Which Yields a Null Δp	
1	1	0.63	0.62	57	62		
2	1	0.64	0.62	59	62		
3	2	0.60	0.50	60	62		
4	2	0.60	0.50	61	62		
5	3	0.58	0.36	61	62		
6	3	0.57	0.35	61	62		
7	4	0.33	0.49	61	62		
8	4	0.33	0.48	61	62		
9	5	0.26	0.44	60	60		
10	5	0.26	0.45	60	60		
11	6	0.20	0.42	—	—		
12	6	0.19	0.41	—	—		
Averages		0.451	0.457				

Stack Temperature, Dry, °F (A) — Stack Temperature, Wet °F (B) —  
 Difference (A - B) — Preliminary Percent Moisture 2

Comments \_\_\_\_\_

Audited by: WBS (Personnel) Date: 11/18/13 Completeness — Legibility ✓ Accuracy ✓  
 Audited by: WBS (Team Leader) Date: 11/12/13 Specifications ✓ Reasonableness ✓



PRELIMINARY TEST DATA SHEET

Location: Banbury Mixer # 7 Start Time: 9:00:00 RUN No. 1  
 Date: 24-Oct-2013 End Time: 9:20:00 JOB No. 132-066

STACK DATA		Head Config.	PRE-TEST CALCULATIONS		EQUIPMENT	
PM <sub>10</sub> & PM <sub>2.5</sub> (1), PM <sub>10</sub> Only (2), PM <sub>2.5</sub> Only (3)		2				
% Moisture: <u>2</u> % est.	%CO <sub>2</sub> : <u>0.00</u> %	Viscosity μ <sub>s</sub> : <u>181.47</u> mpoise	METER BOX: <u>300.392</u>			
Barometric: <u>29.65</u> in Hg	%O <sub>2</sub> : <u>20.90</u> %	Cunningham: <u>1.0664</u>	Y: <u>0.990</u>			
Static Press: <u>-0.25</u> in H <sub>2</sub> O	%N <sub>2</sub> /CO: <u>79.10</u> %	D <sub>50LL</sub> : <u>10.68</u> μm	ΔH@: <u>1.912</u> in H <sub>2</sub> O			
Stack Press: <u>29.63</u> in Hg	M <sub>d</sub> : <u>28.84</u> lb/lb-mole	[N <sub>re</sub> >3162] D <sub>50LL</sub> : <u>-</u> μm	Estimated T <sub>m</sub> : <u>52</u> °F			
Stack Area: <u>4.79</u> ft <sup>2</sup>	Est. M <sub>w</sub> : <u>28.62</u> lb/lb-mole	D <sub>50T</sub> : <u>10.84</u> μm	Cp': <u>0.765</u> S/N			
Stack Area: <u>689.3</u> in <sup>2</sup>		Estimated Q <sub>s</sub> : <u>0.3979</u> acfm	Cp: <u>0.765</u> S/N			
STANDARD CONDITIONS	T <sub>std</sub> : <u>68</u> °F	Estimated N <sub>re</sub> : <u>3085</u>	Nozzle Dia: <u>0.193</u> inches			
	P <sub>std</sub> : <u>29.92</u> inches Hg	Estimated ΔH: <u>0.508</u> in H <sub>2</sub> O	Nozzle Area: <u>0.00020</u> ft <sup>2</sup>			


PRELIMINARY TRAVERSE

NOZZLE SELECTION

Sample Point	Cyclonic Flow Check	Preliminary ΔP (in. H <sub>2</sub> O)			Stack Temperature (°F)
	Null Angle °	ΔP <sub>m</sub>	ΔP <sub>s</sub>	ΔP <sub>s2</sub>	
1	8.0	0.630	0.630	0.672	57.0
2	8.0	0.640	0.640	0.683	59.0
3	10.0	0.600	0.600	0.640	60.0
4	14.0	0.600	0.600	0.640	61.0
5	12.0	0.580	0.580	0.619	61.0
6	13.0	0.570	0.570	0.608	61.0
7	10.0	0.330	0.330	0.352	61.0
8	0.0	0.330	0.330	0.352	61.0
9	0.0	0.260	0.260	0.277	60.0
10	0.0	0.260	0.260	0.277	60.0
11	0.0	0.200	0.200	0.213	60.0
12	0.0	0.190	0.190	0.203	60.0
13	8.0	0.620	0.620	0.662	62.0
14	9.0	0.620	0.620	0.662	62.0
15	10.0	0.500	0.500	0.534	62.0
16	10.0	0.500	0.500	0.534	62.0
17	14.0	0.360	0.360	0.384	62.0
18	15.0	0.350	0.350	0.373	62.0
19	12.0	0.490	0.490	0.523	62.0
20	10.0	0.480	0.480	0.512	62.0
21	9.0	0.440	0.440	0.469	60.0
22	9.0	0.450	0.450	0.480	60.0
23	11.0	0.420	0.420	0.448	60.0
24	30.0	0.410	0.410	0.437	60.0
	9.3	0.451	0.451	0.481	60.708

Nozzle S/N	Diam. Dn (in)	Vn (fps)	V <sub>min</sub> (fps)	V <sub>max</sub> (fps)	ΔP <sub>min</sub> (inches H <sub>2</sub> O)	ΔP <sub>max</sub> (inches H <sub>2</sub> O)
	0.125	77.82	59.09	95.58	1.33	3.48
	0.138	63.85	47.53	79.03	0.86	2.38
	0.154	51.27	36.97	64.19	0.52	1.57
	0.178	38.38	25.79	49.08	0.25	0.92
	<b>0.193</b>	32.64	20.55	42.41	<b>0.16</b>	<b>0.69</b>
	0.200	30.40	18.40	39.82	0.13	0.60
	0.220	25.12	12.85	33.75	0.06	0.43
	0.250	19.45	9.73	27.29	0.04	0.28
	0.253	19.00	9.50	26.77	0.03	0.27
	0.274	16.20	8.10	23.62	0.02	0.21
	0.296	13.88	6.94	20.82	0.02	0.17
	0.320	11.87	5.94	17.81	0.01	0.12

NOTE: This spreadsheet contains circular references, therefore, iterative calculation must be turned on in Excel. In the 2010 version of Excel, the iterative calculation selection is located in File/Options/Formulas.

(absolute °)  
  
 Test Personnel (signature/date) 10/24/13

  
 Project Leader (signature/date) 11/21/13 Review



Location: Banbury Mixer # 7

Start Time: 9:55

RUN No. 1

Date: 24-Oct-2013


End Time: 12:10

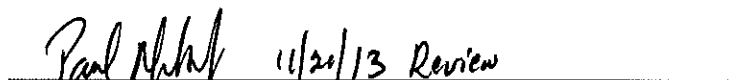
JOB No. 132-066

STACK DATA		EQUIPMENT		ESTIMATES		+/- 50°F ΔH	
% Moisture: <u>2</u> % est.	METER BOX: <u>300.392</u>	Ts (°F): <u>60.71</u>	Tm (°F): <u>52</u>	Ts-50°: <u>10.7083333</u>	Ts+50°: <u>110.708</u>	Est. Qs: <u>0.3979</u> cfm	Est. Qs: <u>0.4328</u>
Barometric: <u>29.65</u> in Hg	Y: <u>0.990</u>	Est. μs: <u>181.47</u> mpoise	Est. ΔH: <u>0.508</u> in H <sub>2</sub> O	Est. μs: <u>157.534386</u>	Est. ΔH: <u>0.621</u>	Est. μs: <u>181.53</u>	Est. ΔH: <u>0.423</u>
Static Press: <u>-0.25</u> in H <sub>2</sub> O	ΔH@: <u>1.912</u> in H <sub>2</sub> O	<b>LEAK CHECKS</b>					
Stack Press: <u>29.63</u> in Hg	Cp: <u>0.765</u> S/N <u>-</u>						
%CO <sub>2</sub> : <u>0.00</u> %	Cp: <u>0.765</u> S/N <u>-</u>	DGM initial	<u>292.88</u>	<u>339.04</u>	cf		
%O <sub>2</sub> : <u>20.90</u> %	Nozzle Dia: <u>0.1930</u> inches	DGM final	<u>292.886</u>	<u>339.042</u>	cf		
%N <sub>2</sub> /CO: <u>79.10</u> %	Stack Area: <u>4.8</u> ft <sup>2</sup>	Time	<u>1</u>	<u>1</u>	min.		
M <sub>d</sub> : <u>28.84</u> lb/lb-mole	# of Points: <u>24</u> points	Leak Rate	<u>0.0060</u>	<u>0.0020</u>	cfm		
Est. M <sub>v</sub> : <u>28.62</u> lb/lb-mole	Run Time: <u>120.00</u> min	Vacuum	<u>15</u>	<u>5</u>	in. Hg		
T <sub>std</sub> : <u>528</u> °R	P <sub>std</sub> : <u>29.92</u> in Hg						

Sample Point	Clock Time (min)	Dry Gas Meter Reading (ft <sup>3</sup> )	Pitot ΔP ("H <sub>2</sub> O)	Gas Temperatures (°F)			Orifice Press. ΔH (in H <sub>2</sub> O)		Pump Vac. (in Hg)	Gas Temps (°F)			Qs (acfm)	D <sub>50</sub> [10 μm]	D <sub>50</sub> [2.5 μm]	Pt. Iso
				DGM			Ideal	Actual		Probe	Filter	Imp. Exit				
				Inlet	Outlet	Stack										
1	5.75	292.9000	0.640	58.0	58.0	65	0.505	0.500	1	175	58	41	0.4174	10.54	2.21	83.24%
2	11.50	295.2400	0.620	59.0	59.0	65	0.506	0.510	1	218	54	46	0.4113	10.65	2.25	83.33%
3	16.75	297.5500	0.520	59.0	59.0	65	0.506	0.510	1	225	54	46	0.4115	10.65	2.24	91.02%
4	22.00	299.6600	0.520	60.0	60.0	65	0.507	0.510	1	230	55	47	0.4165	10.55	2.22	92.14%
5	26.25	301.8000	0.330	61.0	61.0	65	0.508	0.510	1	230	55	48	0.4128	10.62	2.24	114.62%
6	30.50	303.5200	0.340	61.0	61.0	65	0.508	0.510	1	230	56	48	0.4032	10.80	2.30	110.29%
7	35.75	305.2000	0.520	62.0	62.0	65	0.509	0.510	1	234	58	48	0.4072	10.73	2.27	90.07%
8	41.00	307.3000	0.520	63.0	63.0	66	0.508	0.510	1	236	59	49	0.4130	10.63	2.24	91.27%
9	45.75	309.4300	0.420	63.0	63.0	66	0.508	0.510	1	246	60	49	0.4157	10.58	2.22	102.23%
10	50.50	311.3700	0.430	65.0	65.0	66	0.510	0.520	1	242	61	49	0.4163	10.57	2.22	101.17%
11	54.75	313.3200	0.340	65.0	65.0	66	0.510	0.510	1	245	61	50	0.4199	10.51	2.20	114.77%
12	59.00	315.0800	0.350	67.0	67.0	65	0.514	0.520	1	245	60	49	0.4050	10.77	2.29	109.20%
13	64.75	316.7870	0.640	67.0	67.0	67	0.510	0.510	1	243	58	53	0.4019	10.86	2.32	79.98%
14	70.50	319.0700	0.620	67.0	67.0	67	0.510	0.510	1	245	58	50	0.3714	11.48	2.56	75.10%
15	76.25	321.1800	0.610	68.0	68.0	68	0.509	0.510	1	245	58	50	0.4330	10.31	2.16	88.19%
16	82.00	323.6400	0.610	68.0	68.0	68	0.509	0.500	1	249	60	49	0.2394	15.70	4.35	48.75%
17	87.50	325.0000	0.590	69.0	69.0	69	0.508	0.500	1	244	63	51	0.4876	9.49	1.96	100.89%
18	93.00	327.6500	0.590	70.0	70.0	70	0.507	0.500	1	244	63	53	0.3956	11.02	2.39	81.78%
19	97.25	329.8000	0.340	70.0	70.0	69	0.509	0.500	1	245	65	52	0.5253	9.00	1.84	143.16%
20	101.75	332.0100	0.360	71.0	71.0	69	0.510	0.510	1	245	66	52	0.4212	10.53	2.21	111.57%
21	105.25	333.8900	0.240	72.0	72.0	70	0.509	0.520	1	250	67	53	0.4610	9.89	2.05	149.38%
22	109.00	335.4900	0.250	72.0	72.0	70	0.509	0.510	1	250	67	54	0.2958	13.54	3.40	93.92%
23	112.00	336.5900	0.160	72.0	72.0	70	0.509	0.500	1	245	65	56	0.4033	10.87	2.33	160.08%
24	115.00	337.7900	0.170	72.0	72.0	70	0.509	0.500	1	245	68	55	0.4235	10.50	2.20	163.06%
		339.0500														

Actual Run Time	V <sub>m</sub>	ΔP (avg)	T <sub>m</sub> (avg)		T <sub>s</sub> (avg)		Max Vac.	ΔH (avg)	V <sub>s</sub> (avg)	Run ISO
			525.5 °R	526.8 °R	65.9 °F	67.1 °F				
115.00 min	46.150 cf	0.447 in H <sub>2</sub> O	65.9 °F	67.1 °F	1	0.508 in H <sub>2</sub> O	33.889 fps	98.63%		

  
Test Personnel (signature/date) 10/24/13

  
Project Leader (signature/date) 11/21/13 Review

Client:		The Goodyear Tire and Rubber Company		EPA Method OTM 27 Sampling Calculations		Date: 10/29/13	
City/State:		Danville, VA		CEC Project No.: 132-066		Operators: WQB	
Sampling Location:		Unit		Run No.: 1		Operational Condition: Normal	
Initialization Parameters:							
Meter Box No.:	300, 372	Probe/Pitot No.:	200, 302	Pre-Test	0.004	15	
Sample Box No.:		Probe Temp. Setting:	250	Post-Test	0.002	5	
Sample ID No.:	132066-04	Filter No.:	3288	Start Volume:	9.55		
DGM Coefficient?	Y	Number Of Points:	24	Start Time:	1/12/0		
Orifice Coefficient?		Nozzle Diameter:	1.93	End Time:			
Pitot Coefficient?		Actual Meter Temp.:	58.2	Pitot Lk: >3.0 in. H2O	Positive		
Barometric Press.?	29.65	Est. Moisture:	2%	Pre-Test Pitot <0.1	6.7	3.1	in. H2O
Static Pressure?	-2.25	O2 Content:	21%	Post-Test Pitot <0.1	6.8	3.1	in. H2O
Run Duration?	120 min.	CO2 Content:	0%	Intermediate Lk Chk	1	2	3
		DH	505	Vac., in. Hg			
Ts Avg. stack temp. -	60.1	DH+50	473	DGM init, Cf			
Ts+50 Avg. stack temp. +50	116.1	DH-50	862	DGM finl, Cf			
Ts-50 Avg. stack temp. -50	10.1			Leak Rate, cfm			
Pt. MC		Run Time		Pt Beg			
No. %	ΔP	'DP bf	Run Time	Vol.	Incr.	Run	Meter
			Actual	Vol.	Vol.	Vol.	Temp.
1	0.64		5.45	0.51	279.00	5.8	58
2	0.62		11.50	0.51	275.27	5.4	54
3	0.52		16.45	0.51	277.55	5.4	54
4	0.52		22.00	0.51	289.66	6.0	60
5	0.33		26.15	0.51	301.90	6.1	61
6	0.34		30.30	0.51	303.52	6.1	61
7	0.52		35.45	0.51	305.20	6.2	62
8	0.52		41.00	0.51	307.30	6.3	63
9	0.42		45.25	0.52	309.43	6.3	63
10	0.43		50.30	0.51	311.37	6.5	65
11	0.34		54.45	0.51	313.32	6.5	65
12	0.35		59.00	0.52	315.08	6.5	65
13	0.64		64.75	0.51	316.787	6.7	67
14	0.62		70.50	0.51	319.01	6.7	67
15	0.61		76.25	0.51	320.16	6.8	68
16	0.61		82.00	0.51	322.01	6.8	68
17	0.54		87.75	0.50	323.64	6.8	68
18	0.54		93.50	0.50	325.00	6.9	69
19	0.34		99.25	0.50	327.45	7.0	70
20	0.34		105.00	0.50	329.90	7.0	70
21	0.24		110.75	0.51	332.01	7.1	71
22	0.25		116.50	0.51	333.67	7.1	71
23	0.40		122.25	0.51	335.49	7.2	72
24	0.17		128.00	0.51	337.79	7.2	72
End			115		339.03		

PRELIMINARY TEST DATA SHEET

Location: Banbury Mixer # 7  
 Date: 24-Oct-2013

Start Time: 9:55  
 End Time: 12:10

RUN No. 2  
 JOB No. 132-066

STACK DATA		Head Config.	PRE-TEST CALCULATIONS		EQUIPMENT	
PM <sub>10</sub> & PM <sub>2.5</sub> (1), PM <sub>10</sub> Only (2), PM <sub>2.5</sub> Only (3)		2				
% Moisture: <u>2</u> % est.	%CO <sub>2</sub> : <u>0.00</u> %	Viscosity μ <sub>s</sub> : <u>183.71</u> mpoise	METER BOX: <u>300.392</u>			
Barometric: <u>29.62</u> in Hg	%O <sub>2</sub> : <u>20.90</u> %	Cunningham: <u>1.0679</u>	Y: <u>0.990</u>			
Static Press: <u>-0.25</u> in H <sub>2</sub> O	%N <sub>2</sub> /CO: <u>79.10</u> %	D <sub>50LL</sub> : <u>10.65</u> μm	ΔH@: <u>1.912</u> in H <sub>2</sub> O			
Stack Press: <u>29.60</u> in Hg	M <sub>d</sub> : <u>28.84</u> lb/lb-mole	[N <sub>re</sub> >3162] D <sub>50LL</sub> : <u>-</u> μm	Estimated T <sub>m</sub> : <u>75</u> °F			
Stack Area: <u>4.79</u> ft <sup>2</sup>	Est. M <sub>w</sub> : <u>28.62</u> lb/lb-mole	D <sub>50T</sub> : <u>10.82</u> μm	Cp': <u>0.765</u> S/N			
Stack Area: <u>689.3</u> in <sup>2</sup>		Estimated Q <sub>s</sub> : <u>0.4060</u> acfm	Cp: <u>0.765</u> S/N			
STANDARD CONDITIONS	T <sub>std</sub> : <u>68</u> °F	Estimated N <sub>re</sub> : <u>3052</u>	Nozzle Dia: <u>0.194</u> inches			
	P <sub>std</sub> : <u>29.92</u> inches Hg	Estimated ΔH: <u>0.532</u> in H <sub>2</sub> O	Nozzle Area: <u>0.00021</u> ft <sup>2</sup>			

PRELIMINARY TRAVERSE

NOZZLE SELECTION

Sample Point	Cyclonic Flow Check Null Angle °	Preliminary ΔP (in. H <sub>2</sub> O)			Stack Temperature (°F)
		ΔP <sub>m</sub>	ΔP <sub>s</sub>	ΔP <sub>s2</sub>	
1	8.0	0.640	0.640	0.683	70.0
2	8.0	0.620	0.620	0.662	70.0
3	10.0	0.520	0.520	0.555	70.0
4	14.0	0.520	0.520	0.555	70.0
5	12.0	0.330	0.330	0.352	70.0
6	13.0	0.340	0.340	0.363	70.0
7	10.0	0.520	0.520	0.555	70.0
8	0.0	0.520	0.520	0.555	70.0
9	0.0	0.420	0.420	0.448	70.0
10	0.0	0.430	0.430	0.459	70.0
11	0.0	0.340	0.340	0.363	70.0
12	0.0	0.350	0.350	0.373	70.0
13	8.0	0.640	0.640	0.683	70.0
14	9.0	0.620	0.620	0.662	70.0
15	10.0	0.610	0.610	0.651	70.0
16	10.0	0.610	0.610	0.651	70.0
17	14.0	0.590	0.590	0.630	70.0
18	15.0	0.590	0.590	0.630	70.0
19	12.0	0.340	0.340	0.363	70.0
20	10.0	0.360	0.360	0.384	70.0
21	9.0	0.240	0.240	0.256	70.0
22	9.0	0.250	0.250	0.267	70.0
23	11.0	0.160	0.160	0.171	70.0
24	30.0	0.170	0.170	0.181	70.0
	9.3	0.447	0.447	0.477	70.000

Nozzle S/N	Diam. Dn (in)	Vn (fps)	V <sub>min</sub> (fps)	V <sub>max</sub> (fps)	ΔP <sub>min</sub> (inches H <sub>2</sub> O)	ΔP <sub>max</sub> (inches H <sub>2</sub> O)
	0.125	79.39	60.31	97.50	1.36	3.55
	0.138	65.14	48.53	80.61	0.88	2.43
	0.154	52.31	37.75	65.47	0.53	1.60
	0.172	41.93	28.82	53.30	0.31	1.06
	<b>0.194</b>	32.96	20.70	42.85	<b>0.16</b>	<b>0.69</b>
	0.200	31.01	18.84	40.60	0.13	0.62
	0.220	25.63	13.19	34.40	0.07	0.44
	0.250	19.85	9.92	27.82	0.04	0.29
	0.253	19.38	9.69	27.29	0.04	0.28
	0.274	16.52	8.26	24.07	0.03	0.22
	0.296	14.16	7.08	21.24	0.02	0.17
	0.320	12.11	6.06	18.17	0.01	0.12

NOTE: This spreadsheet contains circular references, therefore, iterative calculation must be turned on in Excel. In the 2010 version of Excel, the iterative calculation selection is located in File/Options/Formulas.

(absolute °)

*[Signature]* 10/24/13

Test Personnel (signature/date)

*[Signature]* 11/21/13

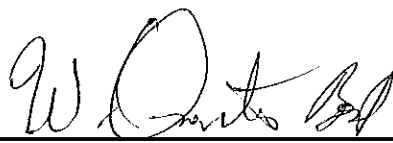
Project Leader (signature/date)


Location: Banbury Mixer #7 Start Time: 13:43 RUN No. 2  
Date: 24-Oct-2013 End Time: 15:50 JOB No. 132-066

STACK DATA		EQUIPMENT		ESTIMATES		+/- 50°F ΔH		
% Moisture: 2 % est.	METER BOX: 300.392	Ts (°F): 70	Tm (°F): 75	Ts-50°: 20	Ts+50°: 120	Est. Qs: 0.4060 cfm	Est. Qs: 0.4408	
Barometric: 29.62 in Hg	Y: 0.990	Est. μs: 183.71 mpoise	Est. ΔH: 0.532 in H <sub>2</sub> O	Est. μs: 159.737497	Est. ΔH: 0.649	Est. μs: 183.759225	Est. ΔH: 0.4661	
Static Press: -0.25 in H <sub>2</sub> O	ΔH@: 1.912 in H <sub>2</sub> O	Est. ΔH: 0.532 in H <sub>2</sub> O	<b>LEAK CHECKS</b>				DGM initial	0
Stack Press: 29.60 in Hg	Cp': 0.765 S/N -	DGM final					0.002	0
%CO <sub>2</sub> : 0.00 %	Cp: 0.765 S/N -	Time	1	1	1	min.		
%O <sub>2</sub> : 20.90 %	Nozzle Dia: 0.1940 inches	Leak Rate	0.0020	0.0010	0.0010	cfm		
%N <sub>2</sub> /CO: 79.10 %	Stack Area: 4.8 ft <sup>2</sup>	Vacuum	14	6	6	in. Hg		
M <sub>d</sub> : 28.84 lb/lb-mole	# of Points: 24 points							
Est. M <sub>w</sub> : 28.62 lb/lb-mole	Run Time: 120.00 min							
T <sub>std</sub> : 528 °R	P <sub>std</sub> : 29.92 in Hg							

Sample Point	Clock Time (min)	Dry Gas Meter Reading (ft <sup>3</sup> )	Pitot ΔP ("H <sub>2</sub> O)	Gas Temperatures (°F)			Orifice Press. ΔH (in H <sub>2</sub> O)		Pump Vac. (in Hg)	Gas Temps (°F)			Qs (acfm)	D <sub>50</sub> [10 μm]	D <sub>50</sub> [2.5 μm]	Pt. Iso
				Inlet	Outlet	Stack	Ideal	Actual		Probe	Filter	Imp. Exit				
1	3.25	339.5010	0.200	65.0	65.0	68	0.527	0.530	1	240	58	55	0.4069	10.78	2.30	143.15%
2	6.50	340.8000	0.190	67.0	67.0	70	0.525	0.520	1	240	59	55	0.3852	11.23	2.47	138.80%
3	9.75	342.0300	0.190	68.0	68.0	70	0.526	0.500	1	232	61	54	0.3751	11.45	2.55	135.15%
4	12.75	343.2300	0.180	70.0	70.0	70	0.528	0.500	1	240	63	54	0.3306	12.52	2.97	122.39%
5	16.75	344.2100	0.290	70.0	70.0	70	0.528	0.500	1	241	64	54	0.3087	13.14	3.23	90.03%
6	20.75	345.4300	0.290	71.0	71.0	70	0.529	0.510	1	239	65	55	0.3460	12.12	2.81	100.91%
7	25.50	346.8000	0.420	72.0	72.0	72	0.526	0.510	1	239	65	55	0.4048	10.87	2.34	97.92%
8	30.50	348.7000	0.450	73.0	73.0	73	0.525	0.510	1	239	65	54	0.4575	9.98	2.08	106.80%
9	35.75	350.9600	0.490	74.0	74.0	73	0.526	0.510	1	236	65	54	0.4791	9.66	2.00	107.20%
10	41.00	353.4500	0.500	74.0	74.0	74	0.524	0.520	1	237	64	54	0.4935	9.47	1.95	109.21%
11	46.50	356.0100	0.580	74.0	74.0	73	0.526	0.520	1	235	63	54	0.4941	9.45	1.95	101.61%
12	52.00	358.7000	0.570	75.0	75.0	74	0.525	0.520	1	236	63	54	0.5180	9.15	1.87	107.35%
13	57.50	361.5200	0.560	72.0	72.0	74	0.522	0.750	1	230	63	55	0.4343	10.37	2.17	90.81%
14	63.00	363.8700	0.550	73.0	73.0	74	0.523	0.750	1	230	62	57	0.4907	9.51	1.96	103.53%
15	68.00	366.5300	0.460	72.0	72.0	74	0.522	0.650	1	230	61	57	0.4614	9.94	2.07	106.44%
16	73.00	368.8000	0.460	72.0	72.0	74	0.522	0.600	1	229	60	55	0.4369	10.33	2.16	100.80%
17	77.00	370.9500	0.300	71.0	71.0	73	0.523	0.500	1	228	63	52	0.4064	10.86	2.33	116.19%
18	81.00	372.5500	0.300	71.0	71.0	73	0.523	0.500	1	228	63	52	0.4064	10.86	2.33	116.19%
19	85.75	374.1500	0.420	71.0	71.0	73	0.523	0.500	1	229	62	51	0.4384	10.29	2.15	105.95%
20	90.50	376.2000	0.430	71.0	71.0	73	0.523	0.600	1	229	62	51	0.4706	9.78	2.03	112.40%
21	95.25	378.4000	0.400	71.0	71.0	72	0.525	0.600	1	230	61	54	0.4057	10.86	2.33	100.55%
22	100.00	380.3000	0.400	71.0	71.0	72	0.525	0.500	1	230	61	55	0.4056	10.86	2.33	100.53%
23	104.00	382.2000	0.310	71.0	71.0	72	0.525	0.550	1	231	61	56	0.4056	10.86	2.33	114.21%
24	108.00	383.8000	0.310	71.0	71.0	72	0.525	0.550	1	231	61	56	0.4183	10.62	2.25	117.78%
		385.4500														

Actual Run Time	V <sub>m</sub>	ΔP (avg)	T <sub>m</sub> (avg)		T <sub>s</sub> (avg)		Max Vac.	ΔH (avg)	V <sub>s</sub> (avg)		Run ISO
			530.9 °R	71.3 °F	531.9 °R	72.2 °F			1	0.550 in H <sub>2</sub> O	
108.00 min	45.949 cf	0.385 in H <sub>2</sub> O	530.9 °R	71.3 °F	531.9 °R	72.2 °F	1	0.550 in H <sub>2</sub> O	31.712	fps	110.36%

  
Test Personnel (signature/date) 10/24/13

  
Project Leader (signature/date) 11/21/13 Review



PRELIMINARY TEST DATA SHEET

Location: **Banbury Mixer # 7** Start Time: **13:43** RUN No. **3**  
 Date: **24-Oct-2013** End Time: **15:30** JOB No. **132-066**

STACK DATA			Head Config.	PRE-TEST CALCULATIONS			EQUIPMENT			
PM <sub>10</sub> & PM <sub>2.5</sub> (1), PM <sub>10</sub> Only (2), PM <sub>2.5</sub> Only (3)			2	Viscosity μ <sub>s</sub> : <b>184.19</b> mpoise			METER BOX: <b>300.392</b>			
% Moisture: <b>2</b>	% est.	%CO <sub>2</sub> : <b>0.00</b>	%	Cunningham: <b>1.0683</b>	D <sub>50LL</sub> : <b>10.64</b> μm			Y: <b>0.990</b>		
Barometric: <b>29.56</b>	in Hg	%O <sub>2</sub> : <b>20.90</b>	%	[N <sub>re</sub> >3162] D <sub>50LL</sub> : <b>-</b>	μm			ΔH@: <b>1.912</b> in H <sub>2</sub> O		
Static Press: <b>-0.25</b>	in H <sub>2</sub> O	%N <sub>2</sub> /CO: <b>79.10</b>	%	D <sub>50T</sub> : <b>10.82</b>	μm			Estimated T <sub>m</sub> : <b>68</b> °F		
Stack Press: <b>29.54</b>	in Hg	M <sub>d</sub> : <b>28.84</b>	lb/lb-mole	Estimated Q <sub>s</sub> : <b>0.4080</b>	acfm			Cp': <b>0.765</b> S/N		
Stack Area: <b>4.79</b>	ft <sup>2</sup>	Est. M <sub>w</sub> : <b>28.62</b>	lb/lb-mole	Estimated N <sub>re</sub> : <b>3042</b>				Cp: <b>0.765</b> S/N		
Stack Area: <b>689.3</b>	in <sup>2</sup>			Estimated ΔH: <b>0.526</b>	in H <sub>2</sub> O			Nozzle Dia: <b>0.193</b> inches		
STANDARD CONDITIONS		T <sub>std</sub> : <b>68</b>	°F				Nozzle Area: <b>0.00020</b> ft <sup>2</sup>			
		P <sub>std</sub> : <b>29.92</b>	inches Hg							

PRELIMINARY TRAVERSE

Sample Point	Cyclonic Flow Check Null Angle °	Preliminary ΔP (in. H <sub>2</sub> O)			Stack Temperature (°F)
		ΔP <sub>m</sub>	ΔP <sub>s</sub>	ΔP <sub>s2</sub>	
1	8.0	0.200	0.200	0.213	72.0
2	8.0	0.190	0.190	0.203	72.0
3	10.0	0.190	0.190	0.203	72.0
4	14.0	0.180	0.180	0.192	72.0
5	12.0	0.290	0.290	0.309	72.0
6	13.0	0.290	0.290	0.309	72.0
7	10.0	0.420	0.420	0.448	72.0
8	0.0	0.450	0.450	0.480	72.0
9	0.0	0.490	0.490	0.523	72.0
10	0.0	0.500	0.500	0.534	72.0
11	0.0	0.580	0.580	0.619	72.0
12	0.0	0.570	0.570	0.608	72.0
13	8.0	0.560	0.560	0.598	72.0
14	9.0	0.550	0.550	0.587	72.0
15	10.0	0.460	0.460	0.491	72.0
16	10.0	0.460	0.460	0.491	72.0
17	14.0	0.300	0.300	0.320	72.0
18	15.0	0.300	0.300	0.320	72.0
19	12.0	0.420	0.420	0.448	72.0
20	10.0	0.430	0.430	0.459	72.0
21	9.0	0.400	0.400	0.427	72.0
22	9.0	0.400	0.400	0.427	72.0
23	11.0	0.310	0.310	0.331	72.0
24	30.0	0.310	0.310	0.331	72.0
	9.3	0.385	0.385	0.411	72.000

NOZZLE SELECTION

Nozzle S/N	Diam. Dn (in)	Vn (fps)	V <sub>min</sub> (fps)	V <sub>max</sub> (fps)	ΔP <sub>min</sub> (inches H <sub>2</sub> O)	ΔP <sub>max</sub> (inches H <sub>2</sub> O)
	0.125	79.79	60.62	97.99	1.37	3.57
	0.138	65.47	48.78	81.01	0.88	2.44
	0.154	52.57	37.96	65.79	0.54	1.61
	0.172	42.14	28.98	53.56	0.31	1.07
	0.188	35.28	22.82	45.55	0.19	0.77
	<b>0.193</b>	<b>33.47</b>	<b>21.15</b>	<b>43.46</b>	<b>0.17</b>	<b>0.70</b>
	0.220	25.76	13.29	34.57	0.07	0.44
	0.250	19.95	9.97	27.95	0.04	0.29
	0.253	19.48	9.74	27.42	0.04	0.28
	0.274	16.61	8.30	24.19	0.03	0.22
	0.296	14.23	7.12	21.35	0.02	0.17
	0.320	12.18	6.09	18.26	0.01	0.12

NOTE: This spreadsheet contains circular references, therefore, iterative calculation must be turned on in Excel. In the 2010 version of Excel, the iterative calculation selection is located in File/Options/Formulas.

(absolute °)

*W. D. Best* 10/24/13  
 Test Personnel (signature/date)

*Paul Alford* 11/21/13 Review  
 Project Leader (signature/date)

Location: Banbury Mixer # 7

Start Time: 16:30

RUN No. 3

Date: 24-Oct-2013

End Time: 18:48

JOB No. 132-066

STACK DATA		EQUIPMENT		ESTIMATES		+/- 50°F ΔH	
% Moisture: <u>2</u> % est.	METER BOX: <u>300.392</u>	Ts (°F): <u>72</u>	Tm (°F): <u>68</u>	Ts-50°: <u>22</u>	Ts+50°: <u>122</u>		
Barometric: <u>29.56</u> in Hg	Y: <u>0.990</u>	Est. Qs: <u>0.4080</u> cfm		Est. Qs: <u>0.4427</u>	Est. Qs: <u>0.4681</u>		
Static Press: <u>-0.25</u> in H <sub>2</sub> O	ΔH@: <u>1.912</u> in H <sub>2</sub> O	Est. μ <sub>s</sub> : <u>184.19</u> mpoise		Est. μ <sub>s</sub> : <u>160.213105</u>	Est. μ <sub>s</sub> : <u>184.239679</u>		
Stack Press: <u>29.54</u> in Hg	Cp': <u>0.765</u> S/N -	Est. ΔH: <u>0.526</u> in H <sub>2</sub> O		Est. ΔH: <u>0.641</u>	Est. ΔH: <u>0.439</u>		
%CO <sub>2</sub> : <u>0.00</u> %	Cp: <u>0.765</u> S/N -	<b>LEAK CHECKS</b>					
%O <sub>2</sub> : <u>20.90</u> %	Nozzle Dia: <u>0.1930</u> inches	DGM initial	<u>0</u>	<u>0</u>	<u>0</u>	<u>0</u>	cf
%N <sub>2</sub> /CO: <u>79.10</u> %	Stack Area: <u>4.8</u> ft <sup>2</sup>	DGM final	<u>0.015</u>	<u>0.001</u>	<u>0.001</u>	<u>0.001</u>	cf
M <sub>d</sub> : <u>28.84</u> lb/lb-mole	# of Points: <u>24</u> points	Time	<u>1</u>	<u>1</u>	<u>1</u>	<u>1</u>	min.
Est. M <sub>w</sub> : <u>28.62</u> lb/lb-mole	Run Time: <u>120.00</u> min	Leak Rate	<u>0.0150</u>	<u>0.0010</u>	<u>0.0010</u>	<u>0.0010</u>	cfm
T <sub>std</sub> : <u>528</u> °R	P <sub>std</sub> : <u>29.92</u> in Hg	Vacuum	<u>13</u>	<u>5</u>	<u>5</u>	<u>5</u>	in. Hg

Sample Point	Clock Time (min)	Dry Gas Meter Reading (ft <sup>3</sup> )	Pitot ΔP ("H <sub>2</sub> O)	Gas Temperatures (°F)			Orifice Press. ΔH (in H <sub>2</sub> O)		Pump Vac. (in Hg)	Gas Temps (°F)			Qs (acfm)	D <sub>50</sub> [10 μm]	D <sub>50</sub> [2.5 μm]	Pt. Iso
				Inlet	Outlet	Stack	Ideal	Actual		Probe	Filter	Imp. Exit				
1	6.25	387.0000	0.640	68.0	68.0	70	0.530	0.730	1	235	62	60	0.4229	10.52	2.21	83.79%
2	12.50	389.6000	0.620	67.0	67.0	70	0.529	0.650	1	236	59	59	0.4676	9.80	2.03	94.13%
3	18.25	392.4700	0.510	67.0	67.0	71	0.527	0.510	1	242	60	57	0.4487	10.10	2.11	99.51%
4	24.00	395.0000	0.510	67.0	67.0	71	0.527	0.500	1	240	61	56	0.4203	10.58	2.23	93.21%
5	28.75	397.3700	0.350	67.0	67.0	71	0.527	0.500	1	241	62	57	0.4143	10.69	2.27	110.92%
6	33.50	399.3000	0.350	67.0	67.0	71	0.527	0.550	1	241	62	57	0.4187	10.61	2.24	112.09%
7	39.25	401.2500	0.510	68.0	68.0	72	0.526	0.600	1	240	62	57	0.4346	10.34	2.17	96.29%
8	45.00	403.7000	0.510	68.0	68.0	72	0.526	0.600	1	240	62	57	0.4612	9.92	2.06	102.19%
9	50.25	406.3000	0.460	67.0	67.0	71	0.527	0.500	1	240	61	56	0.4273	10.45	2.19	99.79%
10	55.75	408.5000	0.470	67.0	67.0	71	0.527	0.500	1	240	61	56	0.4265	10.47	2.20	98.52%
11	60.75	410.8000	0.400	67.0	67.0	71	0.527	0.550	1	241	62	57	0.4386	10.26	2.15	109.82%
12	65.75	412.9500	0.410	67.0	67.0	71	0.527	0.550	1	241	62	58	0.4488	10.10	2.10	110.99%
13	72.00	415.1500	0.630	65.0	65.0	71	0.525	0.700	1	242	64	59	0.4179	10.62	2.25	83.38%
14	78.25	417.7000	0.630	65.0	65.0	71	0.525	0.550	1	242	65	60	0.4587	9.94	2.07	91.52%
15	84.50	420.5000	0.630	66.0	66.0	71	0.526	0.600	1	242	65	61	0.4578	9.96	2.07	91.35%
16	90.75	423.3000	0.610	66.0	66.0	71	0.526	0.600	1	242	65	61	0.4742	9.71	2.01	96.16%
17	96.50	426.2000	0.550	66.0	66.0	71	0.526	0.600	1	231	64	61	0.4799	9.63	1.99	102.48%
18	102.50	428.9000	0.560	66.0	66.0	71	0.526	0.600	1	234	64	61	0.4939	9.43	1.94	104.54%
19	107.25	431.8000	0.350	65.0	65.0	69	0.529	0.500	1	235	60	59	0.4079	10.78	2.30	109.41%
20	112.00	433.7000	0.360	65.0	65.0	69	0.529	0.500	1	235	60	59	0.4079	10.78	2.30	107.88%
21	116.00	435.6000	0.250	64.0	64.0	69	0.528	0.400	1	235	60	58	0.3575	11.83	2.70	113.46%
22	120.00	437.0000	0.250	64.0	64.0	69	0.528	0.400	1	236	60	58	0.3703	11.54	2.59	117.51%
23	124.00	438.4500	0.250	64.0	64.0	69	0.528	0.400		238	60	57	0.3448	12.14	2.82	109.41%
24	128.00	439.8000	0.250	64.0	64.0	69	0.528	0.400		238	60	57	0.3591	11.80	2.68	113.94%
		441.2060														

Actual Run Time	V <sub>m</sub>	ΔP (avg)	T <sub>m</sub> (avg)		T <sub>s</sub> (avg)		Max Vac.	ΔH (avg)	V <sub>s</sub> (avg)		Run ISO
			525.8 °R	530.2 °R	66.1 °F	70.5 °F					
128.00 min	54.206 cf	0.461 in H <sub>2</sub> O					1	0.541 in H <sub>2</sub> O	34.758	fps	101.98%

*[Signature]*  
Test Personnel (signature/date) 10/24/13

*[Signature]*  
Project Leader (signature/date) 11/21/13 Review

Client:		The Goodyear Tire and Rubber Company		EPA Method OTM 27 Sampling Calculations		CEC Project No.: 132-066		Date: 10/21/13		Operators: WQB/JAV	
City/State:		Danville, VA		Run No.: 3		Operational Condition: Normal		Leak Check, <0.020 Cf			
Sampling Location:		Unit		Pre-Test		Post-Test		Start Volume		End Time	
Initialization Parameters:		Probe/Pitot No.: 200-302		Filter No.: 3250		Number Of Points: 24		Nozzle Diameter:		Actual Meter Temp.:	
Meter Box No.: 300392		Probe Temp. Setting: 250		Number Of Points: 24		Nozzle Diameter:		Actual Meter Temp.:		Est. Moisture:	
Sample ID No.: 132066-06		Filter No.: 3250		Number Of Points: 24		Nozzle Diameter:		Actual Meter Temp.:		Est. Moisture:	
DGM Coefficient? 0.990		Filter No.: 3250		Number Of Points: 24		Nozzle Diameter:		Actual Meter Temp.:		Est. Moisture:	
Office Coefficient? 0.765		Filter No.: 3250		Number Of Points: 24		Nozzle Diameter:		Actual Meter Temp.:		Est. Moisture:	
Pitot Coefficient? 0.956		Filter No.: 3250		Number Of Points: 24		Nozzle Diameter:		Actual Meter Temp.:		Est. Moisture:	
Barometric Press.? 29.56		Filter No.: 3250		Number Of Points: 24		Nozzle Diameter:		Actual Meter Temp.:		Est. Moisture:	
Static Pressure? 1.25		Filter No.: 3250		Number Of Points: 24		Nozzle Diameter:		Actual Meter Temp.:		Est. Moisture:	
Run Duration? 120 min.		Filter No.: 3250		Number Of Points: 24		Nozzle Diameter:		Actual Meter Temp.:		Est. Moisture:	
T <sub>s</sub> Avg. stack temp. 72 °F		Filter No.: 3250		Number Of Points: 24		Nozzle Diameter:		Actual Meter Temp.:		Est. Moisture:	
T <sub>s+50</sub> Avg. stack temp. +50 122 °F		Filter No.: 3250		Number Of Points: 24		Nozzle Diameter:		Actual Meter Temp.:		Est. Moisture:	
T <sub>s-50</sub> Avg. stack temp. -50 22 °F		Filter No.: 3250		Number Of Points: 24		Nozzle Diameter:		Actual Meter Temp.:		Est. Moisture:	
Pt. MC		Run Time		Stack Temp.		Rate ΔH		Actual ΔH		Pt Beg Vol.	
No. %		Time		Temp.		ΔH		ΔH		Vol.	
1	2	0.64	6.25	6.15	70	0.73	389.60	0.65	392.47	6.8	235
2	2	0.62	12.50	12.30	70	0.51	595.00	0.51	595.00	6.7	236
3	2	0.51	18.25	18.15	71	0.50	397.37	0.50	397.37	6.7	240
4	2	0.51	24.00	24.00	71	0.50	399.30	0.55	401.25	6.7	241
5	2	0.35	29.75	29.45	71	0.60	403.76	0.60	406.30	6.8	240
6	2	0.35	35.50	35.30	71	0.50	408.50	0.50	410.80	6.7	240
7	2	0.51	41.25	41.15	72	0.55	412.95	0.55	415.15	6.7	241
8	2	0.51	47.00	46.00	72	0.70	417.70	0.55	420.50	6.5	242
9	2	0.46	52.75	52.45	71	0.60	423.30	0.60	426.20	6.6	242
10	2	0.40	58.50	58.15	71	0.60	428.90	0.60	431.80	6.6	242
11	2	0.41	64.25	63.45	71	0.60	434.50	0.60	437.40	6.6	242
12	2	0.41	70.00	69.15	71	0.50	440.10	0.50	443.00	6.5	242
13	2	0.63	75.75	75.00	69	0.40	445.70	0.40	448.60	6.4	242
14	2	0.63	81.50	80.15	69	0.40	451.30	0.40	454.20	6.4	242
15	2	0.63	87.25	85.45	69	0.40	456.90	0.40	459.80	6.4	242
16	2	0.61	93.00	91.15	69	0.40	462.50	0.40	465.40	6.4	242
17	2	0.53	98.75	96.45	69	0.40	468.10	0.40	471.00	6.4	242
18	2	0.56	104.50	102.15	69	0.40	473.70	0.40	476.60	6.4	242
19	2	0.35	110.25	107.15	69	0.40	479.30	0.40	482.20	6.4	242
20	2	0.36	116.00	112.00	69	0.40	484.90	0.40	487.80	6.4	242
21	2	0.27	121.75	117.15	69	0.40	490.50	0.40	493.40	6.4	242
22	2	0.25	127.50	122.00	69	0.40	496.10	0.40	499.00	6.4	242
23	2	0.25	133.25	127.00	69	0.40	501.70	0.40	504.60	6.4	242
24	2	0.25	139.00	132.00	69	0.40	507.30	0.40	510.20	6.4	242
End											

CPM #4

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24



201A  
Methods 8 & 202 and Sample Recovery - Data Analysis  
BY

Client Name Goodyear  
 City/State Danville, VA  
 Sampling Location Banbury Mber, No. 7  
 Clean-Up Box Number M201A/202  
 Chain of Custody: Date Received 10/24/13

Project Number 132066  
 Sample Date 10/24/13  
 Samples Recovered BU  
 Recovery Date 10/24/13  
 Received By Locked?

Equipment Documentation

Run Number	1	2	3	Field Blank
Sample ID Number	132066-04	132066-05	132066-06	132066-07
Sample Box Number	H	H	H	-
Probe Number	200.302	200.303	200.302	200.303

CCT-

Sample Recovery - Fraction 1

Filter Container #	3288	3289	3290	NA
Particulate Description	None visible	None visible	None visible	-
Filter Container Sealed?	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	-

Sample Recovery - Fraction 2

Probe Rinse Container #	132066-04	132066-05	132066-06	132066-07
Rinsing Solution	Acetone	Acetone	Acetone	Acetone
Sample Container Sealed?	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	NA <input checked="" type="checkbox"/> BU
Liquid Level Marked?	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	NA <input checked="" type="checkbox"/> BUS

Analysis of Moisture and Sample Recovery - Fraction 3

Reagent Recovery Container	132066-04	132066-05	132066-06	132066-07
Imp. Absorbing Solution	DI H <sub>2</sub> O	DI H <sub>2</sub> O	DI H <sub>2</sub> O	DI H <sub>2</sub> O
Description of Reagent	clear	clear	clear	clear
Reagent Level Marked?	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>
Final Volume, ml	98.3	99.6	96.3	100
Initial Volume, ml	100	100	100	100
Net Condensed Volume, ml	-1.7	-0.4	-3.7	0
N <sub>2</sub> Purge	1 hour - 14 LPM	1 hour - 14 LPM	1 hour - 14 LPM	1 hour - 14 LPM
Rinse twice with DI H <sub>2</sub> O	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>
Rinse twice with Acetone	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>
Rinse twice with hexane	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>

Analysis of Moisture and Sample Recovery - Silica Gel

Silica Gel Recovery Container #	4	5	6	4
Percent Silica Gel Spent	20%	20%	25%	0%
Final Weight, g	207.7	208.4	214.9	200
Initial Weight, g	200	200	200	200
Net Absorbed Water, g	7.3	8.4	14.9	0
Total Moisture Collected, g	5.6	8.0	11.2	0

200 mL BU

Reagent Blanks

Absorbing Reagent Blank (500 mL)	DI H <sub>2</sub> O	Absorbing Blank ID#	132066-09
Rinsing Reagent Blank (200 mL)	Acetone	Rinsing Blank ID #	132066-08
Rinsing Reagent Blank (200 mL)	Hexane	Rinsing Blank ID #	132066-10
Analyst Initials	BU	Reviewer Initials	

Balance ID	Wt. (200 mg)	Wt. (500 mg)	Wt. (1,000 mg)
10/23/13	200.0	500.0	1000.0
10/24/13	200.0	499.9	999.9

Audited by: AK (Personnel) Date: 11/18/13 Completeness  Legibility  Accuracy   
 Audited by: BU (Team Leader) Date: 11/12/13 Specifications  Reasonableness



201A  
Method 8 & 202 - Moisture Determination and Sample Recovery

Client Name Goodyear  
City/State Danville, VA  
Sampling Location Banbury Mixer No. 7

Project Number: 132-066  
Sample Date: 10/29/13  
Samples Recovered by: BY  
Recovery Date: 10/24/13

Moisture Recovery by weight

DI H<sub>2</sub>O  
80 ml added  
before purge  
1348 -  
1448  
K<sub>2</sub> purg.

Run No.: 1	Impinger Bottle Weight	Initial wt. (mg)	Final Wt (mg)	Difference (gain) wt.	
1 <sup>st</sup> Imp. Bottle		481.5	481.4	-0.1	▶ -1.70
2 <sup>nd</sup> Imp. Bottle		592.8	592.1	-0.7	
3 <sup>rd</sup> Imp. Bottle		660.4	659.5	-0.9	
4 <sup>th</sup> Imp. Bottle		794.8	802.1	7.3	
5 <sup>th</sup> Imp. Bottle					
6 <sup>th</sup> Imp. Bottle					TC = 5.60 grams

DI H<sub>2</sub>O  
80 ml added  
before purge

Run No.: 2	Impinger Bottle Weight	Initial wt. (mg)	Final Wt (mg)	Difference (gain) wt.	
1 <sup>st</sup> Imp. Bottle		480.8	480.1	-0.7	▶ -0.40
2 <sup>nd</sup> Imp. Bottle		593.6	594.0	0.4	
3 <sup>rd</sup> Imp. Bottle		701.8	701.7	-0.1	
4 <sup>th</sup> Imp. Bottle		802.0	810.4	8.4	
5 <sup>th</sup> Imp. Bottle					
6 <sup>th</sup> Imp. Bottle					TC = 8.00 grams

DI H<sub>2</sub>O  
80 ml added  
before purge

Run No.: 3	Impinger Bottle Weight	Initial wt. (mg)	Final Wt (mg)	Difference (gain) wt.	
1 <sup>st</sup> Imp. Bottle		361.8	361.8	0.0	▶ -3.70
2 <sup>nd</sup> Imp. Bottle		594.1	595.0	0.9	
3 <sup>rd</sup> Imp. Bottle		707.1	702.5	-4.6	
4 <sup>th</sup> Imp. Bottle		796.8	811.7	14.9	
5 <sup>th</sup> Imp. Bottle					
6 <sup>th</sup> Imp. Bottle					TC = 11.20 grams

DI H<sub>2</sub>O 80ml added  
before purge

Run No.: Field Blank	Impinger Bottle Weight	Initial wt. (mg)	Final Wt (mg)	Difference (gain) wt.	
1 <sup>st</sup> Imp. Bottle		482.3	481.5	-	
2 <sup>nd</sup> Imp. Bottle		591.6 → 670.2	659.0	-	
3 <sup>rd</sup> Imp. Bottle		660.4	660.4	0	
4 <sup>th</sup> Imp. Bottle		794.8	794.8	0	
5 <sup>th</sup> Imp. Bottle					
6 <sup>th</sup> Imp. Bottle			"After purge"		

Audited by: 10 (Personnel) Date: 11/18/13 Completeness T Legibility ✓ Accuracy ✓  
Audited by: LOBS (Team Leader) Date: 11/12/13 Specifications ✓ Reasonableness ✓



Civil & Environmental Consultants, Inc.

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**APPENDIX C**  
**LABORATORY DATA**

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# Civil & Environmental Consultants, Inc. - Charlotte

2030 S. Tryon Street, Suite 3E  
Charlotte, NC 28203

Goodyear  
Danville, VA  
Client # 132-066

Analytical Report  
(1013-06)

*EPA Method 5*  
Particulate Matter

*EPA Method 202*  
Condensable Particulate Matter

*EPA Modified Method 201A*  
Particulate Matter

NELAP accredited in the state of Virginia under Laboratory ID # 460155, Certificate # 2453.



**Enthalpy Analytical, Inc.**

Phone: (919) 850 - 4392 / Fax: (919) 850 - 9012 / [www.enthalpy.com](http://www.enthalpy.com)  
800-1 Capitola Drive Durham, NC 27713-4385

I certify that to the best of my knowledge all analytical data presented in this report:

- Have been checked for completeness
- Are accurate, error-free, and legible
- Have been conducted in accordance with approved protocol, and that all deviations and analytical problems are summarized in the appropriate narrative(s)

This analytical report was prepared in Portable Document Format (.PDF) and contains 20 pages.

*Michael Steven Schapira*

QA Review Performed by: Michael Steven Schapira

Report Issued: 11/11/13



# Summary of Results



Company	Civil & Env. Consultants
Analyst	KTH / JMD
Parameters	EPA Method 5

Client #	132-066
Job #	1013-06
# Samples	3 Samples + Blanks

Compound	Sample ID / Particulate Matter (PM) Weight (mg)		
	<b>132066-01</b>	<b>13206-02</b>	<b>132066-03</b>
	<b>M5/202-R1</b>	<b>M5/202-R2</b>	<b>M5/202-R3</b>
Net Filter Catch	0.0	0.7	0.6
Net Front Rinse	2.8	1.3	1.8
Total Particulate	2.8	2.0	2.4

Company	Civil & Env. Consultants
Analyst	KTH / JMD
Parameters	EPA Method 202

Client #	132-066
Job #	1013-06
# Samples	6 Runs + blanks

Compound	Sample ID / Condensable Particulate Matter (CPM) Weight (mg)		
	<b>132066-01</b>	<b>132066-02</b>	<b>132066-03</b>
	<b>M5/202-R1</b>	<b>M5/202-R2</b>	<b>M5/202-R3</b>
Net Organic Catch	2.2	1.8	1.6
Corrected Inorganic	1.4	1.8	2.2
TB Corrected CPM	1.6	1.6	1.8
	<b>132066-04</b>	<b>132066-05</b>	<b>132066-06</b>
	<b>M201A/202-R1</b>	<b>M201A/202-R2</b>	<b>M201A/202-R3</b>
Net Organic Catch	3.2	1.1	0.9
Corrected Inorganic	1.0	1.8	0.8
TB Corrected CPM	2.2	1.0	0.0
	<b>132066-07</b>		
	<b>M202-FTB</b>		
Organic Catch	0.8	If Train Blank CPM is >2.0 mg,	
Inorganic Catch	1.2	then sample correction is 2.0 mg.	
CPM	2.0		



Company	Civil & Env. Consultants
Analyst	JMD/KTH
Parameters	Modified EPA Method 201A

Client #	132-066
Job #	1013-06
# Samples	3 runs

Sample Fraction	Sample ID / Catch Weight (mg)		
	<b>132066-04</b>	<b>132066-05</b>	<b>132066-06</b>
	<b>M201A/202-R1</b>	<b>M201A/202-R2</b>	<b>M201A/202-R3</b>
Filter Catch	-0.18	-0.12	-0.25
Acetone Rinses	0.62	0.31	0.55
Total particulate (mg)	0.62	0.31	0.55

# Results



**EPA Method 5 - Particulate Determination - Data Analysis**

Company	Civil & Env. Consultants
Analyst	KTH / JMD
Parameters	EPA Method 5

Client #	132-066
Job #	1013-06
# Samples	3 Samples + Blanks

**Analysis of Particulate Recovery**

Sample ID	<i>M5/202-R1</i>		<i>M5/202-R2</i>		<i>M5/202-R3</i>	
Filter ID	5622	Dates	5623	Dates	5624	Dates
Final wt. (g) 1st	0.3592	11/6/13 8P	0.3566	11/6/13 8P	0.3569	11/6/13 8P
Final wt. (g) 2nd	0.3591	11/7/13 2P	0.3572	11/7/13 2P	0.3570	11/7/13 2P
Filter tare (g)	0.3591	10/21/13	0.3565	10/21/13	0.3564	10/21/13
Net filter catch (mg)	0.0		0.7		0.6	
Beaker number	7457	Dates	7458	Dates	7459	Dates
Final wt (g) 1st	2.28684	11/7/13 9A	2.27812	11/7/13 9A	2.29131	11/7/13 9A
Final wt (g) 2nd	2.28686	11/7/13 4P	2.27812	11/7/13 4P	2.29128	11/7/13 4P
Beaker tare (g)	2.28394	10/30/13	2.27668	10/30/13	2.28930	10/30/13
Acetone vol (mL)	149		155		172	
Acetone blank (g)	0.0001		0.0001		0.0002	
Net front rinse (mg)	2.8		1.3		1.8	
<b>Total particulate (mg)</b>	<b>2.8</b>		<b>2.0</b>		<b>2.4</b>	

**Blank Acetone Analysis**

Blank beaker number	7472			Dates
Blank volume (mL)	214	Date		Final wt (g) 1st
Beaker tare (g)	2.29990	10/30/13		Final wt (g) 2nd
Max acetone residue (g)	0.0017			Acetone residue (g)
				2.30008
				2.30011
				0.0002

**In-House Blank Acetone Analysis**

Blank beaker number	7473			Dates
Blank volume (mL)	200	Date		Final wt (g) 1st
Beaker tare (g)	2.28666	10/30/13		Final wt (g) 2nd
Max acetone residue (g)	0.0016			Acetone residue (g)
				2.28681
				2.28682
				0.0002

Company Civil & Environmental Consultants  
Analyst KTH / JMD  
Parameters EPA Method 202

Client # 132-086  
Job # 1013-06  
# Samples 6 Runs + blanks

Analysis of Condensible Particulate Recovery

Sample ID Number	M202-FTB	M51202-R1	M51202-R2	M51202-R3
<b>Organic</b>				
Beaker Number	7469	7463	7464	7465
Initial Hexane/Acetone Volume, mL	184	216	245	282
Lab Hexane Volume, mL	165	165	165	165
Final Weight, g	2.2797	2.3012	2.3027	2.2768
Reweight, Final, g	2.2797	2.3011	2.3027	2.2767
Beaker Tare, g	2.2789	2.2989	2.3009	2.2751
Net Organic Catch, mg	0.8	2.2	1.8	1.6
<b>Inorganic</b>				
Beaker Number	7606	7600	7601	7602
Final Weight, g	2.2853	2.2872	2.2925	2.2884
Reweight, Final, g	2.2851	2.2871	2.2924	2.2882
Beaker Tare, g	2.2839	2.2857	2.2905	2.2860
Sample H2O volume, mL	222	252	314	279
Added H2O, Filter Extraction, mL	75	75	75	75
Removed Pre-aliquot, mL	0.5	0.5	0.5	0.5
Pre-aliquot CF	1.002	1.002	1.001	1.001
Resuspended Volume, mL	100.0	100.0	100.0	100.0
Removed Post-aliquot, mL	0.5	0.5	0.5	0.5
Post-aliquot CF	1.01	1.01	1.01	1.01
Net Inorganic, mg	1.2	1.4	1.8	2.2
Ammonium Correction, mg	0.0	0.0	0.0	0.0
Corrected Inorganic, mg	1.2	1.4	1.8	2.2
Condensible Particulate Matter, mg	2.0	3.6	3.6	3.8
TB Corrected CPV, mg		1.6	1.6	1.8

Client Blank Analyses

Type Blank	Hexane	H2O	Acetone
Beaker Number	7470	7607	7472
Dry Residue Weight, g	2.2782	2.2870	2.3001
Reweight, Final, g	2.2782	2.2869	2.3001
Tare weight, g	2.2780	2.2863	2.2999
Hexane Residue, g	0.0002	0.0006	0.0002
Hexane Volume, mL	218	200	214
Max. Hexane Residue, g	0.0001	0.0002	0.0002

In-House Blank Analyses

Type Blank	Hexane	H2O	Acetone
Beaker Number	7471	7608	7473
Dry Residue Weight, g	2.2947	2.2724	2.2868
Reweight, Final, g	2.2942	2.2724	2.2868
Tare weight, g	2.2936	2.2721	2.2867
Hexane Residue, g	0.0006	0.0002	0.0002
Hexane Volume, mL	225	250	200
Max. Hexane Residue, g	0.0001	0.0003	0.0002

Company: Civil & Environmental Consultants  
 Analyst: KTH / JMD  
 Parameters: EPA Method 202

Client #: 132-066  
 Job #: 1013-06  
 # Samples: 6 Runs + blanks

Analysis of Condensable Particulate Recovery

Sample ID Number		M202-FTB		M201A/202-R1		M201A/202-R2		M201A/202-R3	
<b>Organic</b>									
Beaker Number	7466	7466	7467	7468	7466	7467	7468	7466	7467
Initial Hexane/Acetone Volume, mL	184	261	311	356	165	165	165	165	165
Lab Hexane Volume, mL	165	165	165	165	165	165	165	165	165
Final Weight, g	2.2797	2.2840	2.3052	2.2766	2.2797	2.2840	2.2766	2.2797	2.2840
Reweigh, Final, g	2.2797	2.2840	2.3052	2.2766	2.2797	2.2840	2.2766	2.2797	2.2840
Beaker Tare, g	2.2789	2.2809	2.3040	2.2757	2.2789	2.2809	2.2757	2.2789	2.2809
Net Organic Catch, mg	0.8	3.2	1.1	0.9	0.8	1.1	0.8	0.8	1.1
<b>Inorganic</b>									
Beaker Number	7606	7603	7604	7605	7606	7603	7604	7605	7606
Final Weight, g	2.2853	2.2648	2.2986	2.2919	2.2853	2.2648	2.2986	2.2919	2.2853
Reweigh, Final, g	2.2851	2.2647	2.2983	2.2918	2.2851	2.2647	2.2983	2.2918	2.2851
Beaker Tare, g	2.2839	2.2637	2.2966	2.2910	2.2839	2.2637	2.2966	2.2910	2.2839
Sample H2O volume, mL	222	247	302	297	222	247	302	297	222
Added H2O, Filter Extraction, mL	75	75	75	75	75	75	75	75	75
Removed Pre-aliquot, mL	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
Pre-aliquot CF	1.002	1.002	1.001	1.001	1.002	1.002	1.001	1.001	1.002
Resuspended Volume, mL	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0
Removed Post-aliquot, mL	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
Post-aliquot CF	1.01	1.01	1.01	1.01	1.01	1.01	1.01	1.01	1.01
Net Inorganic, mg	1.2	1.0	1.8	0.8	1.2	1.0	1.8	0.8	1.2
Ammonium Correction, mg	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Corrected Inorganic, mg	1.2	1.0	1.8	0.8	1.2	1.0	1.8	0.8	1.2
Condensable Particulate Matter, mg	2.0	4.2	2.9	1.7	2.0	4.2	2.9	1.7	2.0
TB Corrected CPY, mg	2.0	2.2	1.0	0.0	2.0	2.2	1.0	0.0	2.0

Client Blank Analyses

Type Blank	Hexane	H2O	Acetone
Beaker Number	7470	7607	7472
Dry Residue Weight, g	2.2782	2.2870	2.3001
Reweigh, Final, g	2.2782	2.2869	2.3001
Tare weight, g	2.2780	2.2863	2.2999
Hexane Residue, g	0.0002	0.0006	0.0002
Water Volume, mL	218	200	214
Max. Hexane Residue, g	0.0001	0.0002	0.0002

In-House Blank Analyses

Type Blank	Hexane	H2O	Acetone
Beaker Number	7477	7608	7473
Dry Residue Weight, g	2.2947	2.2724	2.2868
Reweigh, Final, g	2.2942	2.2724	2.2868
Tare weight, g	2.2936	2.2721	2.2867
Hexane Residue, g	0.0006	0.0002	0.0002
Water Volume, mL	225	250	200
Max. Hexane Residue, g	0.0001	0.0003	0.0002

Company	Civil & Environmental Consultants
Analyst	KTH / JMD
Parameters	EPA Method 202

Client #	132-066
Job #	1013-06
# Samples	6 Runs + blanks

MDL 0.09 (mg Ammonium)

MDL 0.26 (mg Sulfate)

Blank titrant amount (Vtb) 0.03

NH<sub>4</sub>OH normality 0.1

Lot # Sigma Aldrich 318620

Sample ID	Volume Resuspended (mL)	Titration Aliquot Vol (mL)	NH <sub>4</sub> OH Titration Vol (mL)	Aliquot Factor (mL rec'd/aliqu mL)	SO <sub>4</sub> Catch (mg)	Ammonium equivalent (mg)
M202-FTB	100	99.5	0.00	1.01	0.26 ND	0.09 ND
M5/202-R1	100	99.5	0.05	1.01	0.26 ND	0.09 ND
M5/202-R2	100	99.5	0.00	1.01	0.26 ND	0.09 ND
M5/202-R3	100	99.5	0.04	1.01	0.26 ND	0.09 ND
M201A/202-R1	100	99.5	0.05	1.01	0.26 ND	0.09 ND
M201A/202-R2	100	99.5	0.00	1.01	0.26 ND	0.09 ND
M201A/202-R3	100	99.5	0.03	1.01	0.26 ND	0.09 ND

Company	Civil & Env. Consultants
Analyst	JMD/KTH
Parameters	Modified EPA Method 201A

Client #	132-066
Job #	1013-06
# Samples	3 runs

Sample ID	M201A/202-R1		M201A/202-R2		M201A/202-R3	
Filter ID	3288	Dates	3289	Dates	3290	Dates
Final wt. (g) 1st	0.11072	11/6/13 8P	0.11047	11/6/13 8P	0.11139	11/6/13 8P
Final wt. (g) 2nd	0.11073	11/7/13 2P	0.11048	11/7/13 2P	0.11139	11/7/13 2P
Final Tare Weight (g)	0.11091	5/20/13	0.11060	5/20/13	0.11164	5/20/13
Net filter catch (mg)	-0.18		-0.12		-0.25	
Acetone Rinses						
Beaker number	7460	Dates	7461	Dates	7462	Dates
Final wt (g) 1st	2.28768	11/7/13 9A	2.27855	11/7/13 9A	2.28928	11/7/13 9A
Final wt (g) 2nd	2.28768	11/7/13 4P	2.27852	11/7/13 4P	2.28925	11/7/13 4P
Beaker tare (g)	2.28700	10/30/13	2.27808	10/30/13	2.28860	10/30/13
Acetone vol (mL)	67		136		104	
Blank Correction (g)	0.00006		0.00013		0.00010	
PM Catch (mg)	0.62		0.31		0.55	
<b>Total particulate (mg)</b>	<b>0.62</b>		<b>0.31</b>		<b>0.55</b>	

#### Client Blank Acetone Analysis

Blank beaker number	7472	Dates
Final wt (g) 1st	2.30008	11/7/13 9A
Final wt (g) 2nd	2.30011	11/7/13 4P
Beaker tare (g)	2.29990	10/30/13
Acetone residue (g)	0.00021	
Blank volume (mL)	214	
Max acetone residue (g)	0.00169	

#### Laboratory Blank Acetone Analysis

Blank beaker number	7473	Dates
Final wt (g) 1st	2.28681	11/7/13 9A
Final wt (g) 2nd	2.28682	11/7/13 4P
Beaker tare (g)	2.28666	10/30/13
Acetone residue (g)	0.00015	
Blank volume (mL)	200	
Max acetone residue (g)	0.00158	

# Narrative Summary





## Enthalpy Analytical Narrative Summary

<b>Company</b>	Civil & Env. Consultants, Inc.	<b>Client #</b>	132-066
<b>Analyst</b>	KTH / JMD	<b>Job #</b>	1013-06
<b>Parameters</b>	EPA Method 5	<b># Samples</b>	3 and Blanks

**Custody** Jim Beach received the samples on 10/28/13 after being relinquished by Civil & Environmental Consultants, Inc. of Charlotte, NC. The samples were received at ambient temperature and were in good condition. Prior to, during, and after analysis, the samples were kept under lock with access only to authorized personnel by Enthalpy Analytical, Inc.

**Analysis** The samples were analyzed for particulate matter using the analytical procedures in EPA Method 5, Determination of Particulate Matter Emissions from Stationary Sources (40 CFR Part 60, Appendix A).

The filter fractions were weighed on Balance 2 (Mettler Model AB265-S, Serial # 1125163272) and the rinse fractions were weighed on Balance 8 (Sartorius Model ME 5-F, Serial # 23104965). Each balance is certified by Mettler Toledo through July 31, 2014.

**QC Notes** The catch weights were adjusted by a corresponding reagent blank correction value. A mathematically determined (theoretical) maximum value was calculated and compared with the actual value measured for the blank. The lower of the two values was used as the blank correction value, which was then factored by the sample volume divided by the blank volume, and subtracted from the sample catch weight.

**Reporting Notes** Gravimetric analyses are considered to be accurate to  $\pm 0.5$  mg. Therefore, negative catch weights between 0 and  $-0.5$  mg are set to zero and no investigation is undertaken. Negative catch weights less than  $-0.5$  mg are investigated. The only fraction with a negative catch weight was the filter for *Run 1*, which was in the hundredths of a milligram negative. No further action was taken, beyond treating it as a zero when determining the final catch weight.

These analyses met the requirements of the TNI Standard. Any deviations from the requirements of the reference method or TNI Standard have been stated above.

The results presented in this report are representative of the samples as provided to the laboratory.



## Enthalpy Analytical Narrative Summary

<b>Company</b>	Civil & Env. Consultants, Inc.
<b>Analyst</b>	KTH / JMD
<b>Parameters</b>	EPA Method 202

<b>Client #</b>	132-066
<b>Job #</b>	1013-06
<b># Samples</b>	6 and Blanks

**Custody** Jim Beach received the samples on 10/28/13 after being relinquished by Civil & Environmental Consultants, Inc. of Charlotte, NC. The samples were received at ambient temperature and were in good condition. Prior to, during, and after analysis, the samples were kept under lock with access only to authorized personnel by Enthalpy Analytical, Inc.

**Analysis** The samples were analyzed for Condensable Particulate Matter using the analytical procedures in EPA Method 202, Determination of Condensable Particulate Emissions from Stationary Sources (40 CFR Part 51, Appendix M).

All samples were weighed on Balance 8 (Sartorius Model ME 5-F, Serial # 23104965), certified by Mettler Toledo through July 31, 2014.

**QC Notes** A field blank (train blank) was received from each source and analyzed with these samples. The method specifies that blank corrections are accomplished by subtracting the particulate mass determined for the 'Field Train Blank' or 2 mg (whichever is less) from the sample weight.

Acetone, water, and hexane reagent blanks were received and analyzed with these samples. Results are reported for each of these blanks, but none are used to blank correct the associated sample results.

The inorganic results for the samples were corrected for the ammonium ions used to precipitate the sulfate, per the formula in the Method (Section 12.2.1).

**Reporting Notes** Gravimetric analyses are considered to be accurate to  $\pm 0.5$  mg. Therefore, negative catch weights between 0 and  $-0.5$  mg are set to zero and no investigation is undertaken. Negative catch weights less than  $-0.5$  mg are investigated. There were no fractions with negative catch weights for this set of Method 202 samples with the exception of the client hexane blank.

These analyses met the requirements of the TNI Standard. Any deviations from the requirements of the reference method or TNI Standard have been stated above.

The results presented in this report are representative of the samples as provided to the laboratory.



## Enthalpy Analytical Narrative Summary

<b>Company</b>	Civil & Env. Consultants
<b>Analyst</b>	KTH / JMD
<b>Parameters</b>	Modified EPA Method 201A

<b>Client #</b>	132-066
<b>Job #</b>	1013-06
<b># Samples</b>	3 Runs

**Custody** Jim Beach received the samples on 10/28/13 after being relinquished by Civil & Environmental Consultants, Inc. The samples were received in good condition at ambient temperature. Prior to, during, and after analysis, the samples were kept under lock with access only to authorized personnel by Enthalpy Analytical, Inc.

**Analysis** The samples were analyzed for particulate matter using EPA Method 201A, Determination of PM<sub>10</sub> and PM<sub>2.5</sub> Emissions (Constant Sampling Rate Procedures).

Each sample consisted of just one filter and one acetone rinse fraction.

Filter *3288* (part of the *Run 1* sample) appeared very slightly damaged, but the other two filters did not appear to be damaged.

All samples were weighed on Balance 2 (Mettler Model AB265-S, Serial #1125163272) or on Balance 8 (Sartorius Model ME 5-F, Serial #23104965), both certified by Mettler Toledo through July 31, 2014.

**QC Notes** Gravimetric analyses are considered to be accurate to  $\pm 0.5$  mg. Therefore, negative catch weights between 0 and  $-0.5$  mg are displayed as measured, but treated as zero for determination of the total catch weight. No investigation is undertaken for negative masses less than half a milligram.

All three filter samples showed negative catch weights less than 0.5 mg. No filter pieces were obvious as present in the rinse fractions.

Negative catch greater than 0.5 mg magnitude would have been investigated were there any.

**Reporting Notes** These analyses met the requirements of the TNI Standard. Any deviations from the requirements of the reference method and/or the TNI Standard have been stated above.

The results presented in this report are representative of the samples as provided to the laboratory.



## General Reporting Notes

(continued)

- The Sample ID *LCS* represents a Laboratory Control Sample. Clean matrix, similar to the client sample matrix, prepared and analyzed by the laboratory using the same reagents, spiking standards and procedures used for the client samples. The LCS is used to assess the control of the laboratory's analytical system. Whenever spikes are prepared for our client projects, two spikes are retained as LCSs. The LCSs are labeled with the associated project number and kept in-house at the appropriate temperature conditions. When the project samples are received for analysis, the LCSs are analyzed to confirm that the analyte could be recovered from the media, separate from the samples which were used on the project and which may have been affected by source matrix, sample collection and/or sample transport.
- **Significant Figures:** Where the reported value is much greater than unity (1.00) in the units expressed, the number is rounded to a whole number of units, rather than to 3 significant figures. For example, a value of 10,456.45 ug catch is rounded to 10,456 ug. There are five significant digits displayed, but no confidence should be placed on more than two significant digits.
- **Manual Integration:** The data systems used for processing will flag manually integrated peaks with an "M". There are several reasons a peak may be manually integrated. These reasons will be identified by the following two letter designations on sample chromatograms, if provided in the report. The peak was *not integrated* by the software "NI", the peak was *integrated incorrectly* by the software "II" or the *wrong peak* was integrated by the software "WP". These codes will accompany the analyst's manual integration stamp placed next to the compound name on the chromatogram.



# Sample Custody





**This Is The Last Page  
Of This Report.**



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**APPENDIX D**  
**2013 EQUIPMENT CALIBRATIONS**

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## QUALITY ASSURANCE AND EQUIPMENT CALIBRATION PROCEDURES

**General.** Field or laboratory test equipment purchased or fabricated by Civil and Environmental Consultants, Inc. (CEC) is assigned a unique, permanent identification number. New items for which calibration is required are calibrated before initial field use. Equipment whose calibration status may change with use or with time is inspected in the field before testing begins, and again upon return from field use. When an item of equipment is found to be out of calibration, it is adjusted and recalibrated or retired from service. CEC's equipment is periodically recalibrated, regardless of the outcome of these regular inspections.

Calibrations are conducted in accordance with United States Environmental Protection Agency (US EPA) specifications. CEC follows the calibration procedures outlined in EPA Reference Methods found in the Code of Federal Regulations (Volume 40, Part 60) and those recommended in the Quality Assurance Handbook for Air Pollution Measurement Systems: Volume III (EPA/600/R-94/038c). When the Reference Methods do not detail procedures, CEC uses methods such as those prescribed by the American Society for Testing and Materials (ASTM).

Data obtained during calibrations are recorded on standardized forms, which are verified for completeness and accuracy by the Quality Assurance Manager. Data reduction and subsequent calculations are performed using CEC's Air Quality Data System. Calibration calculations are performed by an environmental scientist, independently audited by the Project Manager, and reviewed by the Quality Assurance Manager for verification of data. Copies of calibration data are included in the test or project report.

**Inspection and Maintenance.** An effective preventative program is necessary to ensure equipment performance quality prior to, during, and following the source test. Equipment returning from the field is inspected before it is returned to storage. During the course of these inspections, items are cleaned, repaired, reconditioned, and recalibrated when necessary.

Equipment that is transported to the field for a test project is inspected again prior to being packed. CEC performs these quality assurance checks prior to departure for the project site to detect equipment problems, which may occur during periods of storage. CEC transports adequate back-up equipment to the project site so as to minimize delays in the test schedule.

**Calibration.** Source sampling equipment that requires calibration includes nozzles, pitot tubes, thermometers, flow meters, dry gas meters, and barometers. The following sections briefly describe the calibration procedures followed by CEC.

**Nozzles.** Probe nozzles are uniquely and permanently identified at the time of purchase or fabrication; with the exception for glass nozzles. (Glass nozzles are not uniquely identified due to their fragile status.) Nozzles are calibrated before initial field use and prior to the source test. The inside diameter of the nozzle is measured to the nearest 0.001 inch precision micrometer. Three measurements are made using different

diameters. If the difference between the high and the low measurements do not exceed 0.004 inch, the average of the three measurements is used. If the difference exceeds this amount, or when the nozzle becomes nicked, dented, or corroded, the nozzle is reshaped, sharpened, and recalibrated. Regardless of usage, nozzles are inspected on a yearly basis.

**Pitot Tubes.** CEC Type S Pitot tubes have been constructed and calibrated using those recommendations in accordance with EPA Reference Method 2, Section 10.1. CEC Type S Pitot tubes  $C_p$  coefficients have been determined according to Method 2, Section 10.1. CEC standard Pitot tubes have been assigned a  $C_p$  coefficient of 0.99 according to Calibration Procedure 2. Pitot tubes are visually inspected prior to field use. If the inspection indicates damage, the calibration is rechecked. Regardless of usage, CEC Pitot tubes are inspected and recalibrated on a yearly basis.

**Dry Gas Meter and Orifice.** Console metering systems receive a full calibration at the time of purchase and annually, thereafter. Post-test calibrations are performed after the source test. Approved Alternative Method 5 Post-Test Calibration (ALT-009) may be used to determine a post-test calibration on the console metering systems instead of reference post-test method. If the calibration factor,  $\gamma$  (gamma), deviates by more than five percent per the reference post-test method, the meter is recalibrated and the meter coefficient (initial or recalibrated) that yields the lowest sample volume for the test runs is used. Standard practice at CEC is to recalibrate the dry gas meter when the  $\gamma$  is found to be outside the range of  $\gamma \pm 3\%$ .

**Barometer.** Field barometers are compared to a reference mercury barometer and are deemed acceptable when they agree to within  $\pm 0.1$  inches Hg. This barometric pressure is corrected for pressure and temperature. Prior to and following the sampling program, the field barometer is verified against the referenced barometer.

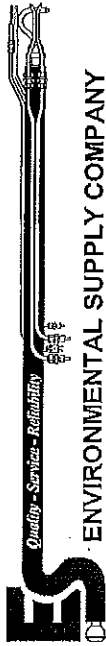
**Thermometers.** New thermometers, pyrometers and thermocouples purchased or fabricated by CEC are calibrated using the procedures described by US EPA Test Protocol. Calibration tolerance limits are as follow:

Impinger Temperature Gauge	$\pm 1^\circ\text{C}$ or $2^\circ\text{F}$
Dry Gas Meter Temperature Gauge	$\pm 3^\circ\text{C}$ or $5.4^\circ\text{F}$
Stack Thermocouples	$\pm 1.5\%$ of absolute temperature

Thermometers and thermocouples are inspected and calibrated prior to and following the field test. Regardless of usage, CEC thermometers and thermocouples are inspected and recalibrated on a yearly basis.

**Laboratory Equipment.** CEC, Inc. has a written quality assurance document that covers calibration and maintenance of laboratory equipment. This includes calibration of the analytical balance against Class S weights. Calibration of thermometers, barometers, and wet test meters are traceable to NIST. A copy of our quality assurance document may be obtained by written request.





**ENVIRONMENTAL SUPPLY COMPANY**

**METHOD 5 DRY GAS METER CALIBRATION USING CRITICAL ORIFICES**

- 1) Select three critical orifices to calibrate the dry gas meter which bracket the expected operating range.
- 2) Record barometric pressure before and after calibration procedure.
- 3) Run at tested vacuum (from Orifice Calibration Report), for a period of time necessary to achieve a minimum total volume of 5 cubic feet.
- 4) Record readings in outlined boxes below, other columns are automatically calculated.

METER PART #: 300.321		DATE: 1/30/2013		METER SERIAL #: 1523437		INITIAL BAROMETRIC PRESSURE (in Hg): 29.21		FINAL AVG (P <sub>bar</sub> ): 29.20		IF Y VARIATION EXCEEDS 2.00%, CRIFICE SHOULD BE RECALIBRATED					
ORIFICE #	RUN #	K' FACTOR (AVG)	TESTED VACUUM (in Hg)	DGM READINGS (FT <sup>3</sup> )		TEMPERATURES °F		ELAPSED TIME (MIN) θ	DGM ΔH (in H <sub>2</sub> O)	V <sub>m</sub> (STD)	Y VARIATION (%)				
				INITIAL	FINAL	NET (V <sub>m</sub> )	AMBIENT					DGM INLET	DGM OUTLET	DGM AVG	
#56	1	0.2882	23	470.50	474.95	4.05	74.0	74	74	74	74	74	4.007	1.024	1.638
	2	0.2882	23	474.95	479.00	4.05	74.0	73	74	73	74	74	4.007	1.023	1.640
	3	0.2882	23	479.00	483.05	4.05	74.0	73	74	73	74	74	4.007	1.021	1.640
AVG = 1.023												0.42			
#54	1	0.4269	21	445.70	453.37	8.27	75	76	75	76	76	76	8.095	1.015	1.679
	2	0.4269	21	453.37	462.23	8.26	75	76	75	76	75	75	8.066	1.015	1.680
	3	0.4269	21	462.23	470.51	8.28	75	76	75	76	75	75	8.085	1.012	1.680
AVG = 1.014												-0.43			
#52	1	0.6069	20	359.50	368.30	9.20	68.0	68	68	69	69	69	9.257	1.016	1.806
	2	0.6069	20	368.30	374.98	6.18	68.0	69	70	69	70	70	6.172	1.021	1.803
	3	0.6069	20	374.98	391.18	6.20	68.0	70	71	70	71	71	6.172	1.020	1.799
AVG = 1.019												0.05			
#51	1	0.6704	19	388.00	399.12	11.12	71	72	73	72	73	73	11.047	1.020	1.744
	2	0.6704	19	399.12	410.23	11.11	71	72	73	72	73	73	11.047	1.021	1.744
	3	0.6704	19	410.23	421.35	11.12	71	72	73	72	73	73	11.047	1.020	1.744
AVG = 1.021												0.25			
#48	1	0.8138	17	429.10	439.34	6.24	74.0	76	76	76	76	76	6.172	1.020	1.779
	2	0.8138	17	439.34	445.52	6.29	74	76	77	76	77	77	6.085	1.014	1.777
	3	0.8138	17	445.52	441.92	6.30	74	77	77	77	77	77	6.089	1.012	1.776
AVG = 1.015												-0.28			

USING THE CRITICAL ORIFICES AS CALIBRATION STANDARDS:  
 The following equations are used to calculate the standard volumes of air passed through the DGM, V<sub>m</sub> (std), and the critical orifice, V<sub>c</sub> (std), and the DGM calibration factor, Y. These equations are automatically calculated in the spreadsheet above.

$$(1) V_m (std) = K_1 V_m \frac{P_{bar} + (\Delta H / 13.6)}{T_m}$$

$$(2) V_c (std) = K' \sqrt{\frac{P_{bar} \theta}{T_{amb}}}$$

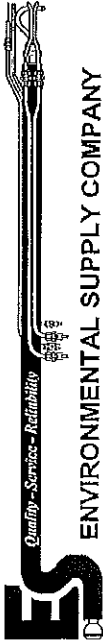
$$(3) Y = \frac{V_c (std)}{V_m (std)} = \text{DGM calibration factor}$$

$$\text{AVERAGE } \Delta H_c = 1.729$$

$$\text{AVERAGE DRY GAS METER CALIBRATION FACTOR, } Y = 1.018$$

$$\Delta H_c = \left( \frac{0.75 \theta}{V_m (std)} \right)^2 \Delta H \left( \frac{V_m (std)}{V_m} \right)$$

= Net volume of gas sample passed through DGM, corrected to standard conditions  
 K<sub>1</sub> = 17.64 R/in. Hg (English), 0.3688 K/inm Hg (Metric)  
 T<sub>amb</sub> = Absolute DGM avg. temperature (°R - English, °K - Metric)  
 = Volume of gas sample passed through the critical orifice, corrected to standard conditions  
 T<sub>amb</sub> = Absolute ambient temperature (°R - English, °K - Metric)  
 K = Average K factor from Critical Orifice Calibration



**METHOD 5 DRY GAS METER CALIBRATION USING CRITICAL ORIFICES**

- 1) Select three critical orifices to calibrate the dry gas meter which bracket the expected operating range.
- 2) Record barometric pressure before and after calibration procedure.
- 3) Run at tested vacuum (from Orifice Calibration Report), for a period of time necessary to achieve a minimum total volume of 5 cubic feet.
- 4) Record readings in outlined boxes below, other columns are automatically calculated.

DATE: 1/10/2013		METER SERIAL #: 12454586		INITIAL BAROMETRIC PRESSURE (in Hg): 29.64		FINAL AVG (P <sub>bar</sub> ): 29.63		IF Y VARIATION EXCEEDS 2.00%, CRIFICE SHOULD BE RECALIBRATED									
METER PART #: S-209/300.045		CRITICAL ORIFICE SET SERIAL #: 1374		TEMPERATURES °F		ELAPSED TIME (MIN)		DGM ΔH (in H <sub>2</sub> O)									
ORIFICE #	RUN #	K' FACTOR (AVG)	TESTED VACUUM (in Hg)	DGM READINGS (FT)		DGM INLET		DGM OUTLET		DGM AVG	ELAPSED TIME (MIN)	DGM ΔH (in H <sub>2</sub> O)	V <sub>m</sub> (STD)	V <sub>c</sub> (STD)	Y VARIATION (%)	ΔH <sub>m</sub>	
				INITIAL	FINAL	INITIAL	FINAL	INITIAL	FINAL								INITIAL
#56	1	0.2882	16	485.80	491.28	5.48	79.5	79.5	80	80	15.00	0.40	5.317	5.557	1.045	1.580	
	2	0.2882	16	491.28	496.76	5.48	80.5	80.5	81	81	15.00	0.40	5.307	5.556	1.047	1.588	
	3	0.2882	16	496.76	502.25	5.49	82.0	82.0	83	83	15.00	0.40	5.302	5.550	1.047	1.587	
													AVG =		1.046	0.49	
#54	1	0.4269	16	504.71	512.38	8.18	84.5	84.5	86	86	15.00	0.56	7.874	8.213	1.043	1.734	
	2	0.4269	16	512.38	521.09	8.21	86.5	86.5	87	87	15.00	0.56	7.874	8.209	1.043	1.728	
	3	0.4269	16	521.09	529.31	8.22	87.5	87.5	88	88	15.00	0.56	7.869	8.206	1.043	1.727	
													AVG =		1.043	0.14	
#52	1	0.6069	16	535.30	547.04	11.74	89.5	89.5	90	90	15.00	2.00	11.227	11.561	1.039	1.780	
	2	0.6069	16	547.04	558.81	11.77	90.0	90.0	90	90	15.00	2.00	11.245	11.562	1.037	1.778	
	3	0.6069	16	558.81	570.58	11.77	90.0	90.0	90	90	15.00	2.00	11.245	11.564	1.037	1.778	
													AVG =		1.038	-0.35	
#51	1	0.6704	16	584.70	597.65	12.96	89.5	89.5	90	90	15.00	2.50	12.409	12.691	1.039	1.823	
	2	0.6704	16	597.65	610.55	12.93	89.5	89.5	89	89	15.00	2.50	12.380	12.692	1.041	1.823	
	3	0.6704	16	610.55	623.55	12.96	89.0	89.0	89	89	15.00	2.50	12.420	12.699	1.039	1.822	
													AVG =		1.040	-0.16	
#48	1	0.8138	15	632.90	646.59	15.69	89.0	89.0	89	89	15.00	3.60	15.077	15.669	1.039	1.783	
	2	0.8138	15	646.59	664.25	15.66	89.0	89.0	89	89	15.00	3.60	15.048	15.674	1.042	1.782	
	3	0.8138	15	664.25	679.95	15.70	89.0	89.0	89	89	15.00	3.60	15.027	15.677	1.039	1.781	
													AVG =		1.040	-0.12	

USING THE CRITICAL ORIFICES AS CALIBRATION STANDARDS:  
 The following equations are used to calculate the standard volumes of air passed through the DGM, V<sub>m</sub> (std), and the critical orifice, V<sub>c</sub> (std), and the DGM calibration factor, Y. These equations are automatically calculated in the spreadsheet above.

(1)  $V_m (std) = K_1 V_x \frac{P_{bar} + (\Delta H / 13.6)}{T_m}$       AVERAGE ΔH<sub>m</sub> = 1.740

(2)  $V_c (std) = K' \sqrt{\frac{P_{bar} \theta}{T_{amb}}}$       ΔH<sub>m</sub> =  $\left( \frac{0.75 \theta}{V_c (std)} \right)^2 \Delta H \left( \frac{V_m (std)}{V_m} \right)$

(3)  $Y = \frac{V_c (std)}{V_m (std)}$       AVERAGE DRY GAS METER CALIBRATION FACTOR, Y = 1.041

**Meter Console Information**

Console Number:	300.392 A
Dry Gas Meter Number:	978295
Calibration Date:	1/2/2013
Expiration Date:	12/28/2013

**Calibration Condition**

Time:	1330
Barometric Pressure (P <sub>b</sub> ):	29.20
Calibration Technician:	JJ
Wet Test Meter ID:	11088
Wet Test Meter Verification Date:	4/1/2012

Pass Positive Leak Check?	8.5	Yes
Pass Negative Leak Check?	0.000	Yes

DGM Orifice Setting (P <sub>m</sub> ) in H <sub>2</sub> O	Console Meter				Wet Test Meter				Run Time							
	Vacuum Setting (2-4 in Hg)	Meter Initial Volume (V <sub>di</sub> ) cubic feet	Meter Final Volume (V <sub>df</sub> ) cubic feet	Sample Volume (V <sub>m</sub> ) cubic feet	Outlet Temp. Initial (T <sub>di</sub> ) °F	Outlet Temp. Final (T <sub>df</sub> ) °F	Outlet Temp. Average (T <sub>da</sub> ) °F	Wet Test Initial Volume (V <sub>wi</sub> ) cubic feet	Wet Test Final Volume (V <sub>wf</sub> ) cubic feet	Wet Test Temp. Initial (T <sub>wi</sub> ) °F	Wet Test Temp. Final (T <sub>wf</sub> ) °F	Wet Test Temp. Average (T <sub>wa</sub> ) °F	Minutes	Seconds	Hundreds	Elapsed minutes
0.5	3.0	908.18	913.25	5.070	75	75	75.0	0	5	65	65	65.0	13.0	7.0	50.0	13.122
1.0	3.0	902	907.15	5.150	77	77	77.0	1	6	65	65	65.0	9.0	12.0	50.0	9.205
1.5	3.0	854.83	865	10.170	70	71	70.5	0	10	65	65	65.0	15.0	24.0	50.0	15.405
2.0	3.0	866.14	877.421	11.281	71	73	72.0	1	12	65	65	65.0	14.0	25.0	50.0	14.422
3.0	3.0	878.44	888.69	10.250	73	75	74.0	0	10	65	65	65.0	10.0	32.0	50.0	10.538
4.0	3.0	890.74	900.975	10.235	76	77	76.5	0	10	65	65	65.0	8.0	55.0	50.0	8.9217

Thermocouple Simulator:

Thermocouple Simulator Setting		Meter Box Thermocouple Calibration:		
F°	Probe	Stack	Filter	Auxiliary
0	1	1	0	0
50	48	48	48	48
75	74	75	75	74
100	98	99	98	98
200	202	199	201	201
300	299	301	299	299
500		502	0.2%	
1000		1003	0.1%	
1500		1499	0.2%	
1900				

Tolerance Range	
Stack	1.5 % ± Absolute (°F or °C)
Filter	± 5.4° F
Meter	± 5.4° F
Exit	± 2.0° F
Auxiliary	± 5.4° F

0.990 γ Average 1.912 ΔH@ Average

$$\gamma = V_w * P_b * (T_d + 460) / V_d * (P_b + \Delta H / 13.6) * (T_w + 460)$$

$$\Delta H_{\theta} = ((0.0519 * \Delta H) / (P_b * (T_d + 460))) * (((T_w + 460) * \theta) / (V_w * \gamma^2))$$

Note: For Calibration Factor γ, the ratio of the calibration meter to dry gas meter, acceptable tolerance of individual values from the average is ±0.02.  
 Note: For ΔH<sub>θ</sub>, orifice pressure differential that equates to 0.75 cfm (0.0212 m<sup>3</sup>/min) at standard temperature and pressure, acceptable tolerance of individual values from the average is ±0.2 inches (5.1mm) H<sub>2</sub>O.

Meter Console Information

Console Number:	300.388.D
Dry Gas Meter Number:	977111
Calibration Date:	1/3/2013
Expiration Date:	12/29/2013

Calibration Condition

Time:	1200
Barometric Pressure (P <sub>b</sub> ):	29.58
Calibration Technician:	JJ
Wet Test Meter ID:	11088
Wet Test Meter Verification Date:	4/1/2012

Pass Positive Leak Check?	8.1
Pass Negative Leak Check?	0

DGM Orifice Setting		Vacuum Setting			Meter Initial Volume		Meter Final Volume		Sample Volume		Outlet Temp.		Outlet Temp. Average		Wet Test Initial Volume		Wet Test Final Volume		Wet Test Volume		Wet Test Temp. Initial		Wet Test Temp. Final		Wet Test Temp. Average		Run Time			
(P <sub>m</sub> )	in. H <sub>2</sub> O	in. Hg	(2-4 in Hg)	(V <sub>ai</sub> )	(V <sub>af</sub> )	(V <sub>si</sub> )	(V <sub>sf</sub> )	(V <sub>si</sub> )	(V <sub>sf</sub> )	(T <sub>ai</sub> )	(T <sub>af</sub> )	(T <sub>av</sub> )	(V <sub>wi</sub> )	(V <sub>wf</sub> )	(V <sub>w</sub> )	(T <sub>wi</sub> )	(T <sub>wf</sub> )	(T <sub>wa</sub> )	Minutes	Seconds	Hundreds	Elapsed	Minutes	Seconds	Hundreds	Elapsed	Minutes	Seconds	Hundreds	Elapsed
0.5	3.0	3.0	3.0	823.5	828.75	5.250	5.250	0	5	71	70	70.5	0	5	5.000	63	63	63.0	13.0	10.0	0.0	13.167	0.0	0.0	0.0	13.167	0.0	0.0	0.0	13.167
1.0	3.0	3.0	3.0	816.255	822.47	6.215	6.215	0	6	73	73	73.5	0	6	6.000	63	63	63.0	11.0	5.0	0.0	11.083	0.0	0.0	0.0	11.083	0.0	0.0	0.0	11.083
1.5	3.0	3.0	3.0	751.835	761.835	10.190	10.190	0	10	65	67	66.0	0	10	10.000	63	63	63.0	14.0	55.0	0.0	14.917	0.0	0.0	0.0	14.917	0.0	0.0	0.0	14.917
2.0	3.0	3.0	3.0	762.86	784.38	21.520	21.520	0	21	67	70	68.5	0	21	21.000	63	63	63.0	27.0	16.0	0.0	27.267	0.0	0.0	0.0	27.267	0.0	0.0	0.0	27.267
3.0	3.0	3.0	3.0	787.48	797.74	10.260	10.260	0	10	72	74	73.0	0	10	10.000	63	63	63.0	10.0	30.0	0.0	10.5	0.0	0.0	0.0	10.5	0.0	0.0	0.0	10.5
4.0	3.0	3.0	3.0	798.78	815.23	16.450	16.450	0	16	74	75	74.5	0	16	16.000	63	63	63.0	14.0	36.0	0.0	14.6	0.0	0.0	0.0	14.6	0.0	0.0	0.0	14.6

Thermocouple Simulator:

DGM Orifice Setting	DGM Factor	Δγ	Orifice Meter	ΔH <sub>Q</sub>	Orifice Meter	ΔH <sub>Q</sub>	ΔH <sub>Q</sub> @ Average
in. H <sub>2</sub> O	0.965	-0.015	1.941	0.055	in. H <sub>2</sub> O	1.886	ΔH <sub>Q</sub> @ Average
1	0.982	0.002	1.900	0.014			
1.5	0.983	0.003	1.884	-0.001			
2	0.981	0.001	1.895	0.009			
3	0.986	0.006	1.843	-0.043			
4	0.984	0.004	1.851	-0.035			

0.980 γ Average 1.886 ΔH<sub>Q</sub>@ Average

$$\gamma = V_w * P_b * (T_d + 460) / V_d * (P_b + \Delta H / 15.6) * (T_w + 460)$$

$$\Delta H_{Q@} = ((0.0319 * \Delta H) / (P_b * (T_d + 460))) * (((T_w + 460) * \theta) / V_w)^2$$

Note: For Calibration Factor γ, the ratio of the calibration meter to dry gas meter, acceptable tolerance of individual values from the average is ±0.02.  
 Note: For ΔH<sub>Q</sub>, orifice pressure differential that equates to 0.75 cfm (0.0212 m<sup>3</sup>/min) at standard temperature and pressure, acceptable tolerance of individual values from the average is ±0.2 inches (5.1mm) H<sub>2</sub>O.

Thermocouple Simulator Setting		Meter Box Thermocouple Calibration:		
F°	Probe	Stack	Filter	Auxiliary
0	1	2	1	2
50	49	50	50	49
75	73	74	74	75
100	99	99	99	99
200	200	200	200	199
300	302	302	301	301
500	505	505	-0.5%	
1000		1006	-0.4%	
1500		1503	-0.2%	
1900				

Tolerance Range	
Stack	± 1.5% ± Absolute (°R or °K)
Filter	± 5.4° F
Meter	± 5.4° F
Exit	± 2.0° F
Auxiliary	± 5.4° F

Meter Console Information

Console Number:	300.390 G
Dry Gas Meter Number:	978295
Calibration Date:	1/4/2013
Expiration Date:	12/30/2013

Calibration Condition

Time:	1230
Barometric Pressure (P <sub>b</sub> ):	29.47
Calibration Technician:	JJ
Wet Test Meter ID:	11088
Wet Test Meter Verification Date:	4/1/2012

Pass Positive Leak Check?	7.7
Pass Negative Leak Check?	0.000

Meter				Console Meter				Wet Test Meter				Run Time					
DGM Orifice Setting (P <sub>m</sub> ) in. H <sub>2</sub> O	Vacuum Setting (2.4 in Hg)	Initial Volume (V <sub>i</sub> ) cubic feet	Meter Final Volume (V <sub>f</sub> ) cubic feet	Sample Volume (V <sub>m</sub> ) cubic feet	Outlet Temp. Initial (T <sub>oI</sub> ) °F	Outlet Temp. Final (T <sub>oF</sub> ) °F	Outlet Temp. Average (T <sub>oA</sub> ) °F	Wet Test Initial Volume (V <sub>wI</sub> ) cubic feet	Wet Test Final Volume (V <sub>wF</sub> ) cubic feet	Wet Test Volume (V <sub>w</sub> ) cubic feet	Wet Test Temp. Initial (T <sub>wI</sub> ) °F	Wet Test Temp. Final (T <sub>wF</sub> ) °F	Wet Test Temp. Average (T <sub>wA</sub> ) °F	Minutes	Seconds	hundreds	Elapsed
0.5	3.0	96	106.35	10.350	72	72	72.0	0	10	10.000	61	61	61.0	26.0	14.0	50.0	26.238
1.0	3.0	84.88	95.22	10.340	74	73	73.5	0	10	10.000	61	61	61.0	18.0	37.0	50.0	18.622
1.5	3.0	34.66	45.01	10.350	72	74	73.0	0	10	10.000	61	61	61.0	15.0	32.0	50.0	15.538
2.0	3.0	46.05	59.305	13.215	64	66	65.0	0	13	13.000	61	61	61.0	17.0	20.0	50.0	17.338
3.0	3.0	60.33	72.59	12.260	67	71	69.0	0	12	12.000	61	61	61.0	13.0	29.0	50.0	13.488
4.0	3.0	73.6	83.84	10.240	71	73	72.0	0	10	10.000	61	61	61.0	9.0	6.0	50.0	9.105

Thermocouple Simulator:

DGM Orifice Setting (P <sub>m</sub> ) in. H <sub>2</sub> O	DGM Factor	DGM Factor Δγ	Orifice Meter ΔH <sub>g</sub> in. H <sub>2</sub> O	Orifice Meter ΔH <sub>g</sub> in. H <sub>2</sub> O	Orifice Meter ΔΔH <sub>g</sub> in. H <sub>2</sub> O
0.5	0.985	-0.001	1.901	-0.055	
1	0.988	0.002	1.910	-0.046	
1.5	0.985	-0.002	1.996	0.041	
2	0.986	0.000	1.991	0.035	
3	0.986	0.000	2.105	0.149	
4	0.987	0.001	1.831	-0.124	

0.986 γ Average 1.956 ΔH@ Average

$$\gamma = V_w * P_b * (T_d + 460) / V_d * (P_b + \Delta H / 13.6) * (T_w + 460)$$

$$\Delta H_{\text{avg}} = ((0.0319 * \Delta H) / (P_b * (T_d + 460))) * (((T_w + 460) * \theta) / V_w)^2$$

Note: For Calibration Factor γ, the ratio of the calibration meter to dry gas meter, acceptable tolerance of individual values from the average is ±0.02.  
 Note: For ΔH<sub>g</sub>, orifice pressure differential that equates to 0.75 cfm (0.0212 m<sup>3</sup>/min) at standard temperature and pressure, acceptable tolerance of individual values from the average is ±0.2 inches (5.1mm) H<sub>2</sub>O.

Thermocouple Simulator Setting						Meter Box Thermocouple Calibration:					
F°	Probe	Stack	Filter	Exit	Auxiliary	F°	Probe	Stack	Filter	Exit	Auxiliary
0	0	0	0	0	1	0	0	0	0	0	1
50	49	50	50	50	50	75	74	73	73	74	73
100	99	100	99	99	99	200	202	200	201	201	201
300	299	303	299	299	299	500	500	501	501	501	501
1000		1004	0.1%			1500		1502	0.2%		
1900											

Tolerance Range	
Stack	± 1.5 % ± Absolute (°R or °K)
Filter	± 5.4° F
Meter	± 5.4° F
Exit	± 2.0° F
Auxiliary	± 5.4° F



Meter Console Information

Console Number:	300.241.H
Dry Gas Meter Number:	12834597
Calibration Date:	1/3/2013
Expiration Date:	12/29/2013

Calibration Condition

Time:	900
Barometric Pressure (P <sub>b</sub> ):	29.41
Calibration Technician:	JJ
Wet Test Meter ID:	11088
Wet Test Meter Verification Date:	4/1/2012

Pass Positive Leak Check? 9.4  
 Pass Negative Leak Check? 0.000

Yes  
 Yes

DGM Orifice Setting (P <sub>m</sub> ) in. H <sub>2</sub> O	Meter			Console Meter			Wet Test Meter			Run Time			
	Vacuum Setting (2-4 in. Hg)	Initial Volume (V <sub>is</sub> ) cubic feet	Meter Final Volume (V <sub>ef</sub> ) cubic feet	Sample Volume (V <sub>m</sub> ) cubic feet	Outlet Temp. Initial (T <sub>di</sub> ) °F	Outlet Temp. Average (T <sub>da</sub> ) °F	Wet Test Initial Volume (V <sub>wi</sub> ) cubic feet	Wet Test Final Volume (V <sub>wf</sub> ) cubic feet	Wet Test Temp. Initial (T <sub>wi</sub> ) °F	Wet Test Temp. Average (T <sub>wa</sub> ) °F	Minutes	Seconds	Elapsed minutes
0.5	3.0	966.1	971.16	5.060	70	70.0	0	5	63	63.0	12.0	24.0	12.405
1.0	3.0	957.995	965.09	7.095	70	70.0	0	7	63	63.0	12.0	21.0	12.355
1.5	3.0	908.73	919.74	11.010	65	65.5	0	11	63	63.0	15.0	45.0	15.755
2.0	3.0	920.745	930.8	10.055	67	67.5	0	10	63	63.0	12.0	36.0	12.605
3.0	3.0	932.835	942.88	10.045	68	68.5	0	10	63	63.0	10.0	21.0	10.355
4.0	3.0	944.91	955.975	11.065	69	69.5	0	11	63	63.0	9.0	50.0	9.8383

Thermocouple Simulator: t-207319

DGM Orifice Setting (P <sub>m</sub> ) in. H <sub>2</sub> O	DGM Factor	DGM Δγ	Orifice Meter ΔH <sub>ef</sub>	Orifice Meter ΔH <sub>ie</sub>	ΔH <sub>ie</sub> @
0.5	1.000	0.002	1.723	1.744	-0.021
1	0.997	-0.001	1.744	1.737	-0.028
1.5	1.000	0.002	1.737	1.787	0.022
2	0.998	0.000	1.787	1.806	0.041
3	0.999	0.000	1.806	1.793	0.028
4	0.997	-0.002	1.793		

0.998 γ Average 1.765 ΔH@ Average

$$\gamma = V_w * P_b * (T_d + 460) / V_d * (P_b + \Delta H / 13.6) * (T_w + 460)$$

$$\Delta H_{ef} = ((0.0319 * \Delta H) / (P_b * (T_d + 460))) * ((T_w + 460) * \theta) / V_w * \gamma^2$$

Note: For Calibration Factor γ, the ratio of the calibration meter to dry gas meter, acceptable tolerance of individual values from the average is ±0.02.  
 Note: For ΔH<sub>ef</sub>, orifice pressure differential that equates to 0.75 cfm (0.0312 m³/min) at standard temperature and pressure, acceptable tolerance of individual values from the average is ±0.2 inches (5.1mm) H<sub>2</sub>O.

Thermocouple Simulator Setting						Meter Box Thermocouple Calibration:					
F°	Probe	Stack	Filter	Exit	Auxiliary	F°	Probe	Stack	Filter	Exit	Auxiliary
0	0	0	0	0	0	0	0	0	0	0	0
50	49	49	49	49	49	50	49	49	49	49	49
75	73	73	73	73	73	75	73	73	73	73	73
100	98	98	98	98	98	100	98	98	98	98	98
200	199	199	199	199	199	200	199	199	199	199	199
300	300	300	300	300	300	300	300	300	300	300	300
500	500	500	500	500	500	500	500	500	500	500	500
1000	1000	1002	1002	1002	1002	1000	1002	1002	1002	1002	1002
1500	1500	1500	1500	1500	1500	1500	1500	1500	1500	1500	1500
1900	1900	1901	1901	1901	1901	1900	1901	1901	1901	1901	1901

Tolerance Range	
Stack	± 1.5% ± Absolute (°R or °K)
Filter	± 5.4° F
Meter	± 5.4° F
Exit	± 2.0° F
Auxiliary	± 5.4° F



METHOD 5 CRITICAL ORIFICE CALIBRATION

CRITICAL ORIFICE SET SIZE: 1374

REFERENCE DRY GAS METER  
SERIAL NUMBER: 8324249

LEAK CHECK:  Failed  Passed

DATE: 7/25/00  
GAS METER PIN: S-200

Barometric Pressure

CRITICAL VACUUM (in Hg)

DCM READINGS (ft<sup>3</sup>)  
INITIAL FINAL NET (V<sub>2</sub>)

TEMPERATURES (°F)  
DCM INLET DCM OUTLET DGM AVG

ELAPSED TIME (MIN)

DCM ΔH (in H<sub>2</sub>O)

K FACTOR VARIATION (%)

AVG VOLUME FLOW RATE (CFY/MIN)

AVG VOLUME FLOW RATE (LITERS/MIN)

ORIFICE #	RUN #	TESTED VACUUM (in Hg)	Barometric Pressure (in Hg)	DCM READINGS (ft <sup>3</sup> )		NET (V <sub>2</sub> )	TEMPERATURES (°F)		DCM INLET	DCM OUTLET	DGM AVG	ELAPSED TIME (MIN)	DCM ΔH (in H <sub>2</sub> O)	K FACTOR	K FACTOR VARIATION (%)	AVG VOLUME FLOW RATE (CFY/MIN)	AVG VOLUME FLOW RATE (LITERS/MIN)
				INITIAL	FINAL		INITIAL	FINAL									
#48 SS	1	14	18	553.643	559.783	6.335	58.0	58.7	59.2	59.7	62.88	6.00	0.71	0.8763	0.19	1.05	29.80
	2	14	18	559.783	566.105	6.222	58.6	59.2	70.5	65.8	65.38	5.00	2.71	0.8125	-0.45	1.05	29.80
	3	14	18	566.105	572.441	6.336	58.0	70.4	72.5	59.0	70.24	6.00	3.71	0.8134	-0.55	1.05	29.80
#51 SS	1	14	18.5	572.441	578.582	6.121	59.0	70.4	72.5	59.3	70.50	7.00	2.46	0.8710	0.10	0.98	24.71
	2	14	18.5	578.582	584.887	6.225	59.1	72.4	74.5	59.7	71.50	7.00	2.46	0.8704	0.00	0.98	24.71
	3	14	18.5	584.887	590.214	6.327	59.1	73.1	74.5	70.2	72.23	7.00	2.46	0.8697	-0.20	0.98	24.71
#52 SS	1	18	18	590.214	597.474	6.360	58.4	73.0	75.1	70.7	74.2	8.00	2.16	0.8075	0.10	0.73	22.45
	2	18	19	597.474	603.551	6.077	58.1	74.4	76.5	71.2	74.6	8.00	2.16	0.8068	-0.03	0.73	22.45
	3	18	19	603.551	609.897	6.346	58.1	74.8	75.1	71.5	72.1	8.00	2.16	0.8067	-0.02	0.73	22.45
#54 SS	1	15	21	609.897	615.457	5.560	57.5	68.1	68.5	68.1	68.4	10.00	0.88	0.4264	-0.10	0.56	15.79
	2	15	21	615.457	621.056	5.579	57.6	68.3	68.9	68.1	68.3	10.00	0.88	0.4277	0.21	0.56	15.79
	3	15	21	621.056	626.602	5.565	57.6	68.3	68.5	68.3	68.63	10.00	0.88	0.4264	-0.11	0.56	15.79
#55 SS	1	16	22	626.602	631.725	4.525	57.2	69.1	69.5	69.5	69.4	12.00	0.42	0.2881	-0.62	0.38	10.65
	2	16	22	631.725	637.354	4.525	58.0	69.5	70.1	69.4	69.3	12.00	0.42	0.2882	0.01	0.38	10.65
	3	16	22	637.354	643.179	4.625	58.3	70.0	70.6	69.6	70.03	12.00	0.42	0.2882	0.01	0.38	10.65

USING THE CRITICAL ORIFICES AS CALIBRATION STANDARDS:  
Calculate the standard volume of air passed through the DGM and the critical orifices, and calculate the DGM calibration factor, Y, using the equations in US EPA Method 5, Section 7.2.3.3 (these equations are programmed on the spreadsheet included with each orifice set).

AVG K FACTOR = 0.8138  
AVG K FACTOR = 0.8704  
AVG K FACTOR = 0.8068  
AVG K FACTOR = 0.4264  
AVG K FACTOR = 0.4263  
AVG K FACTOR = 0.2882

$K_1 = V_{std} \cdot R_{in} \cdot H_1 \cdot (E_{in})^{1.875}$   
 $= 0.00458 \cdot K_{in} \cdot H_1 \cdot (E_{in})^{1.875}$   
 $K_2 = V_{std} \cdot R_{in} \cdot H_2 \cdot (E_{in})^{1.875}$   
 $= 0.00458 \cdot K_{in} \cdot H_2 \cdot (E_{in})^{1.875}$   
 $T_{amb} =$  Absolute ambient temperature, °R (English), °K (Metric)  
 $T_{ref} =$  Absolute DGM avg. temperature, °R (English), °K (Metric)

Critical Orifice Set number 1374 Yes calibrated in accordance with the Code of Federal Regulations, Title 40, Part 60, Appendix A, Method 5, Section 7.2

Signature: *David Ball...*  
Date: 7/25/00

# CERTIFICATE OF CALIBRATION

This certifies that your American AL-20 Wet Test Meter  
Serial No. 11088

Has been calibrated with a American Bell Prover  
Serial No. 277

It is traceable to the N.I.S.T., Reference No. 11200311

Rate of Flow                      % of Proof

60 CFH                              100.0 %

**Calibrated by Carl Poe Co., Inc.**

4600 Allen Street Houston, Texas 77007

(713) 861-3816 \* Fax: (713) 861-8299

January 26, 2012

Date

*Charles Cook*  
Signature

Date: 01/07/13  
 Barometric Pressure: 29.44  
 In. Hg:

Reference Thermometer:  
 Tegam NIST Calibrator Serial No.: 3075 100.122

Reference Thermometer:  
 Tegam NIST Calibrator Serial No.: 3075 100.122

Reference Thermometer:  
 Tegam NIST Calibrator Serial No.: 3075 100.122

Asset Number	Cal. By	Temp. One	Reference Temp. One	Percent Difference	Passed	Temp. Two	Reference Temp. Two	Percent Difference	Passed	Temp. Three	Reference Temp. Three	Percent Difference	Passed
200.021	JJ	55.0	64.0	-0.2%	Yes	150.0	155.0	0.8%	Yes	326.0	328.0	0.3%	Yes
200.063	JJ	85.0	64.0	-0.2%	Yes	149.0	165.0	1.0%	Yes	310.0	308.0	-0.3%	Yes
200.064	JJ	55.0	64.0	-0.2%	Yes	148.0	151.0	0.5%	Yes	324.0	326.0	0.3%	Yes
200.005	JJ	55.0	64.0	-0.2%	Yes	157.0	161.0	0.8%	Yes	254.0	255.0	0.1%	Yes
200.015	JJ	54.0	64.0	0.0%	Yes	154.0	160.0	1.0%	Yes	249.0	246.0	-0.4%	Yes
200.016	JJ	54.0	64.0	0.0%	Yes	145.0	148.0	0.5%	Yes	250.0	253.0	0.4%	Yes
200.017	JJ	64.0	64.0	0.0%	Yes	142.0	145.0	0.5%	Yes	290.0	287.0	-0.4%	Yes
200.076	JJ	64.0	64.0	0.0%	Yes	147.0	151.0	0.7%	Yes	249.0	247.0	-0.3%	Yes
200.077	JJ	64.0	64.0	0.0%	Yes	145.0	156.0	1.1%	Yes	310.0	308.0	-0.3%	Yes
200.079	JJ	64.0	64.0	0.0%	Yes	150.0	154.0	0.7%	Yes	338.0	340.0	0.3%	Yes
200.080	JJ	64.0	64.0	0.0%	Yes	158.0	160.0	0.3%	Yes	303.0	303.0	0.0%	Yes
200.300	JJ	64.0	64.0	0.0%	Yes	155.0	154.0	-0.2%	Yes	301.0	310.0	1.2%	Yes
200.301	JJ	64.0	64.0	0.0%	Yes	155.0	162.0	1.1%	Yes	311.0	315.0	0.5%	Yes
200.302	JJ	64.0	64.0	0.0%	Yes	151.0	148.0	-0.5%	Yes	333.0	327.0	-0.8%	Yes
200.303	JJ	64.0	64.0	0.0%	Yes	156.0	154.0	-0.3%	Yes	305.0	303.0	-0.3%	Yes
200.008	JJ	64.0	64.0	0.0%	Yes	135.0	140.0	0.8%	Yes	277.0	274.0	-0.4%	Yes
200.105	JJ	64.0	64.0	0.0%	Yes	141.0	140.0	-0.2%	Yes	260.0	265.0	0.7%	Yes
200.118	JJ	64.0	64.0	0.0%	Yes	151.0	155.0	0.7%	Yes	318.0	321.0	0.4%	Yes
200.119	JJ	65.0	64.0	-0.2%	Yes	139.0	140.0	0.2%	Yes	302.0	307.0	0.7%	Yes
200.120	JJ	64.0	64.0	0.0%	Yes	160.0	159.0	-0.2%	Yes	296.0	302.0	0.8%	Yes
200.121	JJ	64.0	64.0	0.0%	Yes	148.0	155.0	1.1%	Yes	295.0	303.0	1.0%	Yes
200.093 7	JJ	66.0	67.0	0.2%	Yes	148.0	155.0	1.1%	Yes	302.0	305.0	0.4%	Yes
200.094 7	JJ	66.0	67.0	0.2%	Yes	144.0	140.0	-0.7%	Yes	278.0	285.0	0.9%	Yes
200.310 7	JJ	66.0	67.0	0.2%	Yes	167.0	170.0	0.5%	Yes	296.0	305.0	1.2%	Yes
200.112 7	JJ	66.0	67.0	0.2%	Yes	151.0	155.0	0.7%	Yes	300.0	305.0	0.7%	Yes
200.709 8	JJ	65.0	67.0	0.4%	Yes	147.0	150.0	0.5%	Yes	291.0	285.0	-0.8%	Yes
200.705 8	JJ	65.0	67.0	0.4%	Yes	145.0	140.0	-0.8%	Yes	283.0	285.0	0.3%	Yes
200.041 8	JJ	66.0	67.0	0.4%	Yes	166.0	164.0	-0.3%	Yes	300.0	305.0	0.7%	Yes
200.108 8	JJ	65.0	67.0	0.4%	Yes	178.0	180.0	0.3%	Yes	301.0	305.0	0.5%	Yes
200.109 8	JJ	65.0	67.0	0.4%	Yes	155.0	155.0	0.0%	Yes	288.0	305.0	0.9%	Yes
200.045 8	JJ	65.0	67.0	0.4%	Yes	157.0	170.0	0.5%	Yes	279.0	285.0	0.8%	Yes
200.013 10	JJ	65.0	67.0	0.4%	Yes	145.0	150.0	0.8%	Yes	281.0	285.0	0.5%	Yes
200.014 10	JJ	66.0	67.0	0.2%	Yes	155.0	155.0	0.0%	Yes	290.0	285.0	-0.7%	Yes
200.050 11	JJ	66.0	67.0	0.2%	Yes	160.0	169.0	0.2%	Yes	278.0	285.0	0.9%	Yes
200.051 11	JJ	66.0	67.0	0.2%	Yes	138.0	140.0	0.3%	Yes	287.0	285.0	-0.3%	Yes
200.052 11	JJ	66.0	67.0	0.2%	Yes	143.0	148.0	0.8%	Yes	290.0	285.0	-0.7%	Yes
200.053 11	JJ	66.0	67.0	0.2%	Yes	144.0	143.0	-0.1%	Yes	273.0	285.0	0.9%	Yes
200.098 14	JJ	66.0	67.0	0.2%	Yes	153.0	155.0	0.3%	Yes	300.0	305.0	0.7%	Yes
200.099 14	JJ	65.0	67.0	0.4%	Yes	161.0	159.0	-0.3%	Yes	287.0	285.0	-0.3%	Yes
200.111 15	JJ	65.0	67.0	0.4%	Yes	148.0	155.0	1.1%	Yes	298.0	305.0	0.9%	Yes
200.110 15	JJ	65.0	67.0	0.4%	Yes	181.0	155.0	0.7%	Yes	305.0	305.0	0.0%	Yes
200.081 15	JJ	65.0	67.0	0.4%	Yes	138.0	140.0	0.3%	Yes	302.0	305.0	0.4%	Yes

PROBES





TYPE "S" PITOT TUBE CALIBRATION FORM														
Date:	1/7/13		Specifications:											
Calibrator:	JJ		A.) Pitot tube assembly must be level.											
			B.) If pitot tube is damaged explain under comments section.											
			C.) $Z = A \sin g$ ( $<0.125$ ) and $W = A \sin q$ ( $<0.03125$ )											
			D.) $a < 10^\circ$ and $b < 5^\circ$											
Pitot Tubes Attached to Probes														
I.D. Length	a1°	a2°	b1°	b2°	g°	q°	A, in.	Z, in.	W, in.	PA, in.	PB, in.	Dt, in.	Pass/Fail	Cal. Date
200.021 2'	1.0	1.0	0.5	0.5	0.5	1.5	0.948	0.008	0.02482	0.474	0.474	0.376	Pass	1/7/13
200.063 2'	1.2	1.5	2.7	1.1	3.8	0.6	0.862	0.057	0.00903	0.431	0.431	0.372	Pass	1/7/13
200.064 2'	0.5	0.0	1.5	1.0	1.0	1.0	0.892	0.016	0.01557	0.446	0.446	0.380	Pass	1/7/13
200.074 2'	0.5	0.5	1.0	0.0	1.5	1.0	0.916	0.024	0.01599	0.458	0.458	0.365	Pass	1/7/13
200.005 3'	0.1	0.4	0.8	0.3	1.1	1.1	0.930	0.018	0.01785	0.465	0.465	0.388	Pass	1/7/13
200.015 3'	1.0	1.0	2.0	1.0	1.0	1.0	0.925	0.016	0.01614	0.463	0.463	0.382	Pass	1/7/13
200.016 3'	1.0	0.0	0.5	0.5	1.0	0.5	0.925	0.016	0.00807	0.463	0.463	0.372	Pass	1/7/13
200.017 3'	1.5	1.2	2.0	2.0	1.2	1.9	0.935	0.020	0.03100	0.468	0.468	0.379	Pass	1/7/13
200.076 3'	1.5	1.1	0.7	1.1	2.0	0.5	0.926	0.032	0.00808	0.463	0.463	0.386	Pass	1/7/13
200.077 3'	0.6	0.6	0.5	0.2	2.2	0.2	0.930	0.036	0.00325	0.465	0.465	0.378	Pass	1/7/13
200.079 3'	0.5	0.9	0.9	0.3	1.2	1.0	0.944	0.020	0.01648	0.472	0.472	0.378	Pass	1/7/13
200.080 3'	0.4	0.7	2.2	1.4	1.6	1.0	0.971	0.027	0.01695	0.486	0.486	0.373	Pass	1/7/13
200.300 3'	0.0	0.0	1.0	1.0	0.5	1.0	0.933	0.008	0.01628	0.467	0.467	0.370	Pass	1/7/13
200.301 3'	0.5	1.0	1.0	1.0	0.5	0.0	0.923	0.008	0.00000	0.462	0.462	0.378	Pass	1/7/13
200.302 3'	1.0	0.0	1.0	0.5	1.5	0.0	0.940	0.025	0.00000	0.470	0.470	0.377	Pass	1/7/13
200.303 3'	0.0	0.0	0.0	0.0	0.5	1.0	0.940	0.008	0.01641	0.470	0.470	0.375	Pass	1/7/13
200.008 5'	0.2	0.8	0.6	0.5	1.5	1.0	0.983	0.026	0.01716	0.492	0.492	0.371	Pass	1/7/13
200.105 5'	1.0	1.0	0.5	0.5	1.0	1.5	0.921	0.016	0.02411	0.461	0.461	0.373	Pass	1/7/13
200.118 5'	0.0	0.5	0.0	0.0	0.5	0.5	0.953	0.008	0.00832	0.477	0.477	0.380	Pass	1/7/13
200.119 5'	0.0	0.0	1.0	1.0	1.5	0.5	0.990	0.026	0.00864	0.495	0.495	0.376	Pass	1/7/13
200.120 5'	0.0	1.0	0.5	0.5	1.0	0.0	0.931	0.016	0.00000	0.466	0.466	0.380	Pass	1/7/13
200.121 5'	0.5	0.0	0.5	0.0	2.0	1.0	0.925	0.032	0.01614	0.463	0.463	0.376	Pass	1/7/13
200.093 7'	0.5	0.5	0.0	0.0	0.5	1.0	0.998	0.009	0.01742	0.499	0.499	0.386	Pass	1/7/13
200.094 7'	0.0	0.5	1.0	0.0	2.0	0.0	0.934	0.033	0.00000	0.467	0.467	0.382	Pass	1/7/13
200.310 7'	1.0	1.0	0.0	0.0	0.5	1.0	0.981	0.009	0.01712	0.491	0.491	0.385	Pass	1/7/13
200.112 7'	1.3	2.0	0.0	1.1	0.0	0.9	0.987	0.000	0.01550	0.494	0.494	0.385	Pass	1/7/13
200.709 8'	0.7	2.0	1.0	2.0	0.5	0.7	0.954	0.008	0.01166	0.477	0.477	0.374	Pass	1/7/13
200.705 8'	2.0	0.0	1.0	0.0	0.6	0.9	0.941	0.010	0.01478	0.471	0.471	0.380	Pass	1/7/13
200.041 8'	1.0	0.0	1.0	1.0	0.4	0.8	0.980	0.007	0.01368	0.490	0.490	0.386	Pass	1/7/13
200.108 8'	1.1	1.3	1.4	1.0	1.1	0.5	0.951	0.018	0.00830	0.476	0.476	0.382	Pass	1/7/13
200.109 8'	1.2	1.4	0.0	2.0	1.3	0.0	0.962	0.022	0.00000	0.481	0.481	0.374	Pass	1/7/13
200.045 8'	1.0	1.0	1.5	1.4	0.9	0.00	0.947	0.015	0.00000	0.474	0.474	0.750	Pass	1/7/13
200.013 10'	0.8	1.1	0.0	0.0	0.7	0.0	0.972	0.012	0.00000	0.486	0.486	0.379	Pass	1/7/13
200.014 10'	0.7	1.0	1.1	0.0	0.6	0.5	0.967	0.010	0.00844	0.484	0.484	0.380	Pass	1/7/13
200.050 11'	1.5	1.3	2.0	1.0	0.0	0.0	0.966	0.000	0.00000	0.483	0.483	0.373	Pass	1/7/13
200.051 11'	2.0	2.5	1.2	1.0	0.0	1.3	0.981	0.000	0.02226	0.491	0.491	0.386	Pass	1/7/13
200.052 11'	2.0	1.0	2.0	1.0	1.2	1.1	0.925	0.019	0.01776	0.463	0.463	0.383	Pass	1/7/13
200.053 11'	2.0	3.0	0.0	1.1	0.0	0.7	0.962	0.000	0.01175	0.481	0.481	0.379	Pass	1/7/13
200.098 14'	2.0	1.0	2.0	0.0	1.4	1.4	0.955	0.023	0.02333	0.478	0.478	0.388	Pass	1/7/13
200.099 14'	1.0	1.2	2.0	0.0	1.1	1.1	0.938	0.018	0.01801	0.469	0.469	0.379	Pass	1/7/13
200.111 15'	2.0	1.2	1.0	1.0	0.0	1.0	0.944	0.000	0.01648	0.472	0.472	0.363	Pass	1/7/13
200.110 15'	1.5	2.0	2.0	1.5	1.0	1.2	0.965	0.017	0.02021	0.483	0.483	0.378	Pass	1/7/13
200.091 16'	1.0	1.7	0.0	0.0	0.0	1.2	0.977	0.000	0.02046	0.489	0.489	0.376	Pass	1/7/13

Comments: Pitot Tubes Required Only Minor Maintenance & Reconditioning

TYPE "S" PITOT TUBE CALIBRATION FORM														
Date: 1/7/13		Specifications:												
Calibrator: JJ		A.) Pitot tube assembly must be level.												
		B.) If pitot tube is damaged explain under comments section.												
		C.) $Z = A \sin g$ ( $<0.125$ ) and $W = A \sin q$ ( $<0.03125$ )												
		D.) $a < 10^\circ$ and $b < 5^\circ$												
Pitot Tubes Attached to Probes														
I.D. Length	a1°	a2°	b1°	b2°	g°	q°	A, in.	Z, in.	W, in.	PA, in.	PB, in.	Dt, in.	Pass/Fail	Cal. Date
Individual Pitot Tubes														
I.D. Length	a1°	a2°	b1°	b2°	y°	o°	A, in.	Z, in.	W, in.	PA, in.	PB, in.	Dt, in.	Pass/Fail	
200.304 3'	1.0	1.0	0.0	1.0	0.0	1.0	0.936	0.000	0.01634	0.468	0.468	0.380	Pass	1/7/13
200.305 3'	1.0	1.0	0.5	0.5	0.9	1.0	0.934	0.015	0.01630	0.467	0.467	0.383	Pass	1/7/13
200.704 7'	0.0	0.0	1.0	0.5	0.6	0.0	0.835	0.009	0.00000	0.418	0.418	0.385	Pass	1/7/13
200.708 3'	0.8	0.5	1.0	0.8	0.0	0.0	0.833	0.000	0.00000	0.417	0.417	0.384	Pass	1/7/13
200.706 3'	0.0	1.0	0.0	1.0	0.0	0.0	0.829	0.000	0.00000	0.415	0.415	0.381	Pass	1/7/13
200.255i	0.0	0.5	0.0	0.0	0.0	1.0	0.850	0.000	0.01483	0.425	0.425	0.382	Pass	1/7/13
200.711 5'	0.8	1.0	1.0	1.0	0.9	0.5	0.920	0.014	0.00803	0.460	0.460	0.384	Pass	1/7/13
200.712	1.0	0.5	0.0	0.0	1.0	1.0	0.931	0.016	0.01625	0.466	0.466	0.390	Pass	1/7/13
200.707	0.5	1.0	1.0	0.0	0.0	0.0	0.839	0.000	0.00000	0.420	0.420	0.381	Pass	1/7/13
s/n p 796	0.0	0.0	0.5	1.0	1.0	0.5	0.926	0.016	0.00808	0.463	0.463	0.388	Pass	1/7/13
Comments: Pitot Tubes Required Only Minor Maintenance & Reconditioning														



### Hotbox Thermocouple Temperature Calibration

Calibrated By: JJ      Date: 1/7/2013      Reference Thermometer: NIST      Tegan NIST Calibrator Serial No.:      Barometric Pressure, In. Hg. # 29.47

Asset Number	Id Letter	Ambient	Reference Ambient	Percent Difference	Passed	M.D. Temp.	Reference Temp.	Percent Difference	Passed	HIGH Temp.	Reference Temp.	Percent Difference	Passed
Hotbox	B	61	62	0.2%	Yes	208	208	0.0%	Yes	330	329	-0.1%	Yes
Hotbox	C	61	62	0.2%	Yes	202	208	0.2%	Yes	301	300	-0.1%	Yes
Hotbox	D	61	62	0.2%	Yes	205	206	0.2%	Yes	300	298	-0.3%	Yes
Hotbox	E	62	62	0.0%	Yes	219	218	-0.1%	Yes	308	309	0.1%	Yes
Hotbox	F	62	62	0.0%	Yes	208	206	-0.3%	Yes	317	316	-0.1%	Yes
Hotbox	G	61	62	0.2%	Yes	229	228	-0.1%	Yes	316	317	0.1%	Yes
Hotbox	H	61	62	0.2%	Yes	206	209	0.4%	Yes	354	353	-0.1%	Yes
Hotbox	I	65	65	0.0%	Yes	250	250	0.0%	Yes	320	325	0.6%	Yes
Hotbox	J	66	66	0.0%	Yes	251	250	-0.1%	Yes	319	325	0.8%	Yes
Hotbox	K	66	66	0.0%	Yes	254	250	-0.6%	Yes	327	325	-0.3%	Yes
Hotbox	L	67	67	0.0%	Yes	249	250	0.1%	Yes	321	325	0.5%	Yes
Hotbox	M	66	66	0.0%	Yes	238	240	0.3%	Yes	325	323	-0.3%	Yes
Hotbox	N	61	62	0.2%	Yes	217	218	0.1%	Yes	333	334	0.1%	Yes
Hotbox	O1	60	62	0.4%	Yes	208	206	-0.3%	Yes	321	322	0.1%	Yes
Hotbox	O2	62	62	0.0%	Yes								
Hotbox	B2	66	67	0.2%	Yes	249	250	0.1%	Yes	320	325	0.6%	Yes

Temperature Difference Calculation:  
 (Ref. Temp. Deg. F + 460) - (Test Temp. Deg. F + 460)  
 X 100 = <1.5%  
 Ref. Temp. Deg. F + 460



Environmental Supply Company, Inc.

Quality Source Sampling Systems & Accessories

## Wind Tunnel Pitot Calibration

S-type Pitot ID: **P-799** Date: **22-Jun-13**  
 Standard Pitot ID: **RE2-20** Personnel: **BR**  
 Cp(std): **0.99** Cp(actual): **0.765**  
 Part Number: **PPS12-Y-PM10** P(bar): **29.77**  
 Test Velocity (fps): **50** T(°F): **78**  
 Wind Tunnel Location: **Wake Forest, NC** Tunnel Size: **30" x 36"**

A-SIDE	$\Delta P_{ts}$ (in. H <sub>2</sub> O)	$\Delta P_s$ (in. H <sub>2</sub> O)	Cp(s)	Deviation*
	0.670	1.090	0.776	0.002
	0.657	1.120	0.758	-0.001
	0.650	1.100	0.761	0.000
	<b>AVERAGE</b>		<b>0.765</b>	0.001
		Std deviation	0.002	

### NOTES:

1. Pitot calibrated with an Environmental Supply Co. PM10 cyclone.
2. C<sub>p</sub> is only valid when used with PM10 cyclone.
3. C<sub>p</sub> is only valid with 1" spacing from PM10 cyclone.

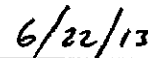
$$C_p(s) = C_p(std) \sqrt{\frac{\Delta P(std)}{\Delta P(s)}}$$

\*Deviation = {Cp(s) - AVG Cp(s)} {must be <0.010}

Standard deviation of the deviations must be less than 0.02 for both sides.

Pitot tube S/N P-799 was calibrated in accordance with the CFR 40, Part 60 Appendix A, Method 2, Section 10.

  
 Signature

  
 Date



Environmental Supply Company, Inc.

Quality Source Sampling Systems & Accessories

## Wind Tunnel Pitot Calibration

S-type Pitot ID: **P-753** Date: **26-Jul-12**  
 Standard Pitot ID: **RE2-20** Personnel: **BR**  
 Cp(std): **0.99** Cp(actual): **0.765**  
 Part Number: **PPS12-Y-PM10** P(bar): **29.58**  
 Test Velocity (fps): **50** T(°F): **89**  
 Wind Tunnel Location: **Wake Forest, NC** Tunnel Size: **30" x 36"**

A-SIDE	$\Delta P_{std}$	$\Delta P$	$C_p(s)$	Deviation*
	(in. H <sub>2</sub> O)	(in. H <sub>2</sub> O)		
	<b>0.563</b>	<b>0.940</b>	<b>0.766</b>	0.002
	<b>0.563</b>	<b>0.943</b>	<b>0.765</b>	-0.001
	<b>0.560</b>	<b>0.940</b>	<b>0.764</b>	0.000
		<b>AVERAGE</b>	<b>0.765</b>	0.001
			Std deviation	0.002

### NOTES:

1. Pitot calibrated with an Environmental Supply Co. PM10 cyclone.
2.  $C_p$  is only valid when used with PM10 cyclone.
3.  $C_p$  is only valid with 1" spacing from PM10 cyclone.

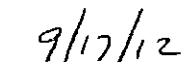
$$C_p(s) = C_p(std) \sqrt{\frac{\Delta P(std)}{\Delta P(s)}}$$

\*Deviation = {Cp(s) - AVG Cp(s)} {must be <0.010}

Standard deviation of the deviations must be less than 0.02 for both sides.

Pitot tube S/N P-753 was calibrated in accordance with the CFR 40, Part 60 Appendix A, Method 2, Section 10.

  
 Signature

  
 Date



## Precision Weighing

1949 Evans Road  
Cary, North Carolina 27513

Phone: (919) 678-0077 \* Fax: (919) 678-0078

Email: pweighing@aol.com

Client:  
CEC, Inc

Contact:  
Paul Jenkins

Department:  
Lab

Description: Thermometer  
Instrument ID: 1992  
Manufacturer: Erco  
Model: 30 to 214°F  
Calibration Interval: Annual

Calibration SOP: 2020 Rev. 1.0  
Serial Number: 1992  
Operating Range: 30 to 200 °F  
Instrument Range: 30 to 214 °F  
Calibration Tolerance: +/- 2 deg F

Calibration Notes: *Nominal Targets are 32, 110, 200 Degrees Fahrenheit*

*Calibration Data ("As left" data is identical to "As found" data, if "As left" is blank)*

Test Points	Units	Standard	As Found	Error	As Left	Error	Pass/Fail
30	° F	31.754	32.2	-0.446			Pass
110	° F	109.436	109.4	0.036			Pass
200	° F	199.786	199.2	0.588			Pass

Instrument Found in Tolerance? Yes  
Instrument Left in Tolerance? Yes

Calibration Date:	16-Jan-13	Calibration Due Date:	January 2014
-------------------	-----------	-----------------------	--------------

Test Standards:	Standard ID:	Expiration Date:
Digital Thermometer	111013846	November 13

Technicians Remarks: NA

Calibration Performed By:

STANLEY R. HALL

Approved Signature:



## Precision Weighing

1949 Evans Road  
Cary, North Carolina 27513  
Phone: (919) 678-0077 \* Fax: (919) 678-0078  
Email: pweighing@aol.com

Client:  
CEC, Inc

Contact:  
Paul Jenkins

Department:  
Lab

Description: Thermometer  
Instrument ID: 2206  
Manufacturer: Ertco  
Model: 0 to 200 °C  
Calibration Interval: Annual

Calibration SOP: 2020 Rev. 1.0  
Serial Number: 3082  
Operating Range: 0 to 200 °C  
Instrument Range: 0 to 200 °C  
Calibration Tolerance: +/- 1 deg C

Calibration Notes: *Nominal Targets are 0, 150, 200 Degrees Celcius*

*Calibration Data ("As left" data is identical to "As found" data, if "As left" is blank)*

Test Points	Units	Standard	As Found	Error	As Left	Error	Pass/Fail
0	°C	0.048	0.2	-0.152			Pass
150	°C	149.7	149.4	0.3			Pass
200	°C	199.2	199.0	0.2			Pass

Instrument Found in Tolerance? Yes  
Instrument Left in Tolerance? Yes

Calibration Date:	16-Jan-13	Calibration Due Date:	January 2014
-------------------	-----------	-----------------------	--------------

Test Standards:	Standard ID:	Expiration Date:
Digital Thermometer	111913848	November 2013
Glass Thermometer	5270241	January 2014

Technicians Remarks: NA

Calibration Performed By:

STANLEY R. HALL

Approved Signature:



**Precision Weighing**  
 1949 Evans Road  
 Cary, North Carolina 27513  
 Phone: (919) 678-0077 \* Fax: (919) 678-0078  
 Email: pweighing@aol.com

Client:  
CEC, Inc

Contact:  
Paul Jenkins

Department:  
Lab

Description: Thermometer  
 Instrument ID: 3062  
 Manufacturer: VWR  
 Model: 608-3S  
 Calibration Interval: Annual

Calibration SOP: 2020 Rev. 1.0  
 Serial Number: 3080  
 Operating Range: 0 to 110 °F  
 Instrument Range: -30 to 120 °F  
 Calibration Tolerance: +/- 2 deg F

Calibration Notes: *Nominal Targets are 32, 50, 110 Degrees Fahrenheit*

*Calibration Data ("As left" data is identical to "As found" data, if "As left" is blank)*

Test Points	Units	Standard	As Found	Error	As Left	Error	Pass/Fail
32	°F	31.754	32	-0.246			Pass
60	°F	60.092	60	0.092			Pass
110	°F	109.436	110	-0.664			Pass

Instrument Found in Tolerance? Yes  
 Instrument Left in Tolerance? Yes

Calibration Date:	16-Jan-13	Calibration Due Date:	January 2014
-------------------	-----------	-----------------------	--------------

Test Standards:	Standard ID:	Expiration Date:
Digital Thermometer	111913846	November 13

Technicians Remarks: NA

Calibration Performed By:

STANLEY R. HALL

Approved Signature:

\_\_\_\_\_



## Precision Weighing

1949 Evans Road  
 Cary, North Carolina 27513  
 Phone: (919) 678-0077 \* Fax: (919) 678-0078  
 Email: pweighthg@aol.com

Client:

Contact:

Department:  
Lab

Description: Thermometer  
 Instrument ID: 3080  
 Manufacturer: VWR  
 Model: 808-3S  
 Calibration Interval: Annual

Calibration SOP: 2020 Rev. 1.0  
 Serial Number: 3080  
 Operating Range: 0 to 110 °F  
 Instrument Range: -30 to 120 °F  
 Calibration Tolerance: +/- 2 deg F

Calibration Notes: *Nominal Targets are 32, 50, 110 Degrees Fahrenheit*

Calibration Data ("As Left" data is identical to "As found" data, if "As left" is blank)

Test Points	Units	Standard	As Found	Error	As Left	Error	Pass/Fail
32	°F	31.754	32	-0.246			Pass
50	°F	50.092	50	0.092			Pass
110	°F	109.436	109	0.436			Pass

Instrument Found in Tolerance? Yes  
 Instrument Left in Tolerance? Yes

Calibration Date:	16-Jan-13	Calibration Due Date:	January 2014
-------------------	-----------	-----------------------	--------------

Test Standards:	Standard ID:	Expiration Date:
Digital Thermometer	111913846	November 13

Technicians Remarks: NA

Calibration Performed By:

STANLEY R. HALL

Approved Signature:

\_\_\_\_\_



## Precision Weighing

1949 Evans Road  
Cary, North Carolina 27513  
Phone: (919) 678-0077 \* Fax: (919) 678-0078  
Email: pvcighing@aol.com

Client:  
CEC, Inc

Contact:  
Paul Jenkins

Department:  
Lab

Description: Thermometer  
Instrument ID: U38717  
Manufacturer: ERTCO  
Model: -5 to 400°C  
Calibration Interval: Annual

Calibration SOP: 2020 Rev. 1.0  
Serial Number: U38717  
Operating Range: 0 to 200 °C  
Instrument Range: -5 to 400 °C  
Calibration Tolerance: +/- 2 deg C

Calibration Notes: *Nominal Targets are 0, 50, 100 and 200 Degrees Celsius*

Calibration Data ("As left" data is identical to "As found" data, if "As left" is blank)

Test Points	Units	Standard	As Found	Error	As Left	Error	Pass/Fail
0	°C	0.048	0	0.048			Pass
50	°C	50.372	50	0.372			Pass
100	°C	100.222	99	1.222			Pass
200	°C	199.2	199	0.2			Pass

Instrument Found in Tolerance? Yes  
Instrument Left in Tolerance? Yes

Calibration Date:	16-Jan-13	Calibration Due Date:	January 2014
-------------------	-----------	-----------------------	--------------

Test Standards:	Standard ID:	Expiration Date:
Digital Thermometer	111813848	November 2013
Glass Thermometer	6270241	January 2014

Technicians Remarks: NA

Calibration Performed By:

Approved Signature:

Stanley R. Hall





Calibration  
Certificate No. 1750.01

Calibration complies with ISO/IEC  
17025, ANSI/NC SL Z540-1, and 9001



Cert. No.: 4000-4006344

Traceable® Certificate of Calibration for Digital Thermometer

Instrument Identification:

Model: 4000 S/N: 111913846 Manufacturer: Control Company

Standards/Equipment:

Description	Serial Number	Due Date	NIST Traceable Reference
Temperature Calibration Bath TC-275	A9A237		
Digital Thermometer	B16815	6/08/12	B1608038
PRT Temperature Probe	01641	5/28/12	B1526085
Digital Thermometer	111879346	10/21/12	4000-3872946
Temperature Calibration Bath TC-231	A79341		
Thermistor Module	A17118	1/24/12	1000291329
Temperature Probe	3039	2/01/12	6-BA02G-1-1

Certificate Information:

Technician: 68 Procedure: CAL-06 Cal Date: 11/08/11 Cal Due: 11/08/13  
Test Conditions: 24.0°C 46.0 %RH 1013 mBar

Calibration Data: (New Instrument)

Unit(s)	Nominal	As Found	In Tol	Nominal	As Left	In Tol	Min	Max	±U	TUR
°C		N.A.		0.001	-0.002	Y	-0.049	0.051	0.013	3.8:1
°C		N.A.		25.001	24.998	Y	24.951	25.051	0.014	3.6:1
°C		N.A.		60.001	59.998	Y	59.951	60.051	0.016	2.6:1
°C		N.A.		100.001	100.003	Y	99.951	100.051	0.018	2.8:1

This instrument was calibrated using instruments traceable to National Institute of Standards and Technology.

A Test Uncertainty Ratio of at least 4:1 is maintained unless otherwise stated and is calculated using the expanded measurement uncertainty. Uncertainty evaluation includes the instrument under test and is calculated in accordance with the ISO "Guide to the Expression of Uncertainty in Measurement" (GUM). The uncertainty represents an expanded uncertainty using a coverage factor k=2 to approximate a 95% confidence level. In tolerance conditions are based on test results falling within specified limits with no reduction by the uncertainty of the measurement. The results contained herein relate only to the item calibrated. This certificate shall not be reproduced except in full, without written approval of Control Company.

Nominal=Standard's Reading; As Left=Instrument's Reading; In Tol=In Tolerance; Min/Max=Acceptance Range; ±U=Expanded Measurement Uncertainty; TUR=Test Uncertainty Ratio; Accuracy=±(Max-Min)/2; Min = Nominal(Rounded) - Tolerance; Max = Nominal(Rounded) + Tolerance; Date=MM/DD/YY

*Nicol Rodriguez*  
Nicol Rodriguez, Quality Manager

*Wallace Barry*  
Wallace Barry, Technical Manager

Maintaining Accuracy:

In our opinion once calibrated your Digital Thermometer should maintain its accuracy. There is no exact way to determine how long calibration will be maintained. Digital Thermometers change little, if any at all, but can be affected by aging, temperature, shock, and contamination.

Recalibration:

For factory calibration and re-certification traceable to National Institute of Standards and Technology contact Control Company.

CONTROL COMPANY 4455 Rex Road Friendswood, TX 77546 USA  
Phone 281 482-1714 Fax 281 482-9448 service@control3.com www.control3.com

Control Company is an ISO 17025:2005 Calibration Laboratory Accredited by (A2LA) American Association for Laboratory Accreditation, Certificate No. 1750.01.  
Control Company is ISO 9001:2008 Quality Certified by (DNV) Det Norske Veritas, Certificate No. CERT-01805-2008-AQ-HOU-ANAB,  
International Laboratory Accreditation Cooperation (ILAC) - Multilateral Recognition Arrangement (MRA).



# Applied Technical Services Certificate of Calibration



Certificate #1050576

**Calibration Location:**

Applied Technical Services  
1049 Triad Court  
Marietta, GA 30062

**Customer:**

Precision Weighing  
111 Meece Bridge Road  
Taylors, SC 29687

**Instrument Information:**

Manufacturer: Fluke  
Model Number: 51  
Description: Thermometer, Thermocouple  
Asset Number: 6270241  
Serial Number: 5270241  
PO Number: STAN

**Calibration Information/Results:**

As Found Condition: In Tolerance  
Action Taken / As Left: In Tolerance - No Adjustment  
Temperature: 70° F  
Humidity: 26% RH  
Calibration Date: 01/08/2013  
Calibration Due Date: 01/08/2014  
Calibration Interval: 12 Months

**Calib. Procedure:** ATS-1005 Rev 2: Calibration of Thermocouple Thermometer Simulate

This instrument has been calibrated using primary or secondary standards whose calibration is traceable to the International System of Units (SI) through the National Institute of Standards and Technology (NIST) or applicable ASTM specification number for hardness testing equipment. Some measurements are traceable to natural, physical constants, consensus standards, or ratio type measurements.

The reported expanded measurement uncertainty is based on a standard uncertainty multiplied by a coverage factor of  $k=2$ , providing a confidence level of approximately 95%. The expanded measurement uncertainty is not considered when determining in-tolerance or out-of-tolerance conditions. No statement of compliance with specifications is made or implied on this certificate. Results are reviewed, if applicable, to establish where any measurement results exceeded the stated calibration tolerance and to communicate results by means of this certificate.

All calibrations are performed in accordance with the ATS Quality Manual QM1, Rev. 11, dated 10/22/12. Applied Technical Services, Inc.'s Quality System complies with the applicable requirements of ANSI/NCCL Z540-1, ISO 9001-2008, 10CFR50 Appendix B, 10CFR Part 21, and ISO/IEC 17025. The reported data is valid only at the time of the test and related only to the item calibrated. \*Calibration due dates appearing on this certificate and calibration label are determined by the client and do not imply continued conformance to specifications. This certificate shall not be reproduced except in full, without written permission of Applied Technical Services, Inc.

**Technical Remarks:**Calibrated By: *Tyler, Mike A*

Name

Technician

Title

**Calibration Equipment Utilized**

Standard I.D.	Mfg.	Model No.	Description	Serial	Cal. Date	Due Date
ATS-04528	Fluke	5522A	Calibrator, Multi-Function	1562801	05/04/2012	05/04/2013

Applied Technical Services

1049 Triad Court  
Marietta, GA 30062

Phone 770 423-1400 www.atslab.com

Issue date: 01/08/2013

Page 1 of 2

Batch Number: 939232

### Calibration Data

FUNCTION TESTED	Nominal Value	CALIBRATION TOLERANCE	As Found	As Left
Temperature K Type	-20.0 °C	-20.7 to -19.3 °C [EMU 0.19 °C]	-20.6	Same
	0.0 °C	-0.7 to 0.7 °C [EMU 0.19 °C]	-0.4	Same
	50.0 °C	49.3 to 50.7 °C [EMU 0.19 °C]	49.5	Same
	100.0 °C	99.2 to 100.8 °C [EMU 0.19 °C]	99.8	Same
	200.0 °C	199.1 to 200.9 °C [EMU 0.31 °C]	199.8	Same
Temperature J Type	400.0 °C	398.9 to 401.1 °C [EMU 0.31 °C]	399.6	Same
	-20.0 °C	-20.8 to -19.2 °C [EMU 0.17 °C]	-20.8	Same
	0.0 °C	-0.8 to 0.8 °C [EMU 0.17 °C]	-0.4	Same
	50.0 °C	49.2 to 50.8 °C [EMU 0.17 °C]	49.4	Same
	100.0 °C	99.1 to 100.9 °C [EMU 0.17 °C]	99.8	Same
	200.0 °C	199.0 to 201.0 °C [EMU 0.20 °C]	199.5	Same
	400.0 °C	398.8 to 401.2 °C [EMU 0.20 °C]	399.9	Same

End Of Report

Test Number: 1050576    Asset Number: 5270241    Desc: Fluke /51, Thermometer, Thermocouple

Page 2 of 2

Applied Technical Services  
1049 Triad Court  
Marietta, GA 30062  
Phone 770 423-1400    www.atslab.com  
Issue date: 01/08/2013

Batch Number: 939232



# Precision Weighing

1949 Evans Road  
Cary, North Carolina 27513  
Phone: (919) 678-0077 \* Fax: (919) 678-0075  
Email: pweighing@aol.com

## BALANCE CERTIFICATE OF CALIBRATION

Calibration Date: 16-Jan-13 Calibration Due Date: January 2014 SOP: 2000 rev. 1.3  
Balance ID #: N-A Type/Model: My Weigh I 1200 S/N: 600.044  
Dept: Lab Room Number: 1 Tolerance +/- : 0.1%

Weight set ID#	NIST Test Number	Cal Date	Cal Due
P 926	1951044	3-Jan-13	Jan 2014

Weight Standard (g)	Before Cal Readings (g)	Difference (g)	After Cal Readings (g)	Difference (g)	Tolerances +/- (g)
0	0.0	0.0	0.0	0.0	0.0
100	100.5	0.5	100.0	0.0	0.1
200	200.8	0.8	200.0	0.0	0.2
500	502.0	2.0	500.0	0.0	0.5
1000	1004.3	4.3	999.9	-0.1	1.0
1200	EEE	N-A	1199.7	-0.3	1.2

### Before Calibration Readings:

In Tolerance:   
Out of Tolerance:  X  
N-A:

### After Calibration Readings:

In Tolerance:  X  
Out of Tolerance:   
N-A:

### Comments:

This certifies that the balance listed above has been serviced and calibrated to manufacturer specifications and/or Precision Weighing Standard Operating Procedures with weights traceable to the National Institute of Standards and Technology (NIST).

*Stanley R. Hall*

Precision Weighing Technician

16-Jan-13

Date of Service

Customer Signature (Review)

Date of Review



# Precision Weighing

1949 Evans Road

Cary, North Carolina 27513

Phone: (919) 678-0077 \* Fax: (919) 678-0075

Email: pweighing@aol.com

## BALANCE CERTIFICATE OF CALIBRATION

Calibration Date: 16-Jan-13 Calibration Due Date: January 2014 SOP: 2000 rev. 1.3  
 Balance ID #: N-A Type/Model: Sartorius AY 1501 S/N: 27254925  
 Dept: Lab Room Number: 1 Tolerance +/-: 0.1%

Weight set ID#	NIST Test Number	Cal Date	Cal Due
P 926	1951044	3-Jan-13	Jan 2014

Weight Standard (g)	Before Cal Readings (g)	Difference (g)	After Cal Readings (g)	Difference (g)	Tolerances +/- (g)
0	0.0	0.0	0.0	0.0	0.0
200	200.0	0.0	200.0	0.0	0.2
500	499.9	-0.1	500.0	0.0	0.5
700	699.9	-0.1	700.0	0.0	0.7
1000	999.9	-0.1	1000.0	0.0	1.0
1500	1499.9	-0.1	1500.0	0.0	1.5

### Before Calibration Readings:

In Tolerance:   
 Out of Tolerance:  X  
 N-A:

### After Calibration Readings:

In Tolerance:  X  
 Out of Tolerance:   
 N-A:

### Comments:

This certifies that the balance listed above has been serviced and calibrated to manufacturer specifications and/or Precision Weighing Standard Operating Procedures with weights traceable to the National Institute of Standards and Technology (NIST).

*Stanley R. Hall*

Precision Weighing Technician

16-Jan-13

Date of Service

Customer Signature (Review)

Date of Review





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**APPENDIX E**  
**QSTI CERTIFICATIONS**

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# SOURCE EVALUATION SOCIETY



## Qualified Source Testing Individual


LET IT BE KNOWN THAT


### JOSHUA A. JONES

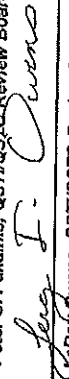
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### MANUAL GAS VOLUME MEASUREMENTS AND ISOKINETIC PARTICULATE SAMPLING METHODS

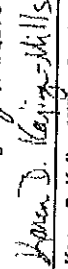
ISSUED THIS 22<sup>ND</sup> DAY OF FEBRUARY 2012 AND EFFECTIVE UNTIL FEBRUARY 21<sup>ST</sup>, 2017

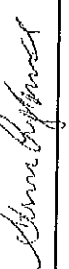
  
Peter R. Westlin, QSTI/QSTO Review Board

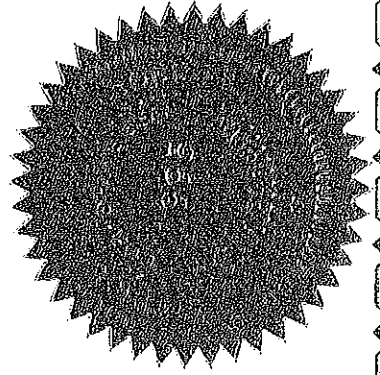
  
Peter S. Pakalnis, QSTI/QSTO Review Board

  
LeRoy Owens, QSTI/QSTO Review Board

  
C. David Bagweiff, QSTI/QSTO Review Board

  
Karen D. Kajiva-Mills, QSTI/QSTO Review Board

  
Glenn C. England, QSTI/QSTO Review Board



APPLICATION NO. 2012-621

# SOURCE EVALUATION SOCIETY



## Qualified Source Testing Individual


LET IT BE KNOWN THAT


### JOSHUA A. JONES

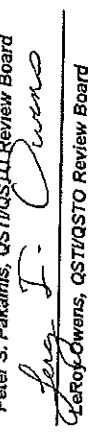
HAS SUCCESSFULLY PASSED A COMPREHENSIVE EXAMINATION AND SATISFIED EXPERIENCE REQUIREMENTS IN ACCORDANCE WITH THE GUIDELINES ISSUED BY THE SES QUALIFIED SOURCE TEST INDIVIDUAL REVIEW BOARD FOR


### MANUAL GASEOUS POLLUTANTS SOURCE SAMPLING METHODS

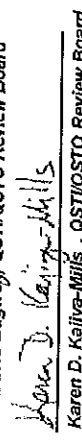
ISSUED THIS 22<sup>ND</sup> DAY OF FEBRUARY 2012 AND EFFECTIVE UNTIL FEBRUARY 21<sup>ST</sup>, 2017

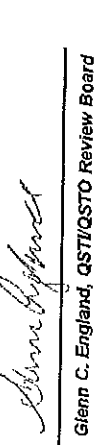
  
 Peter R. Westlin, QSTI/QSTO Review Board

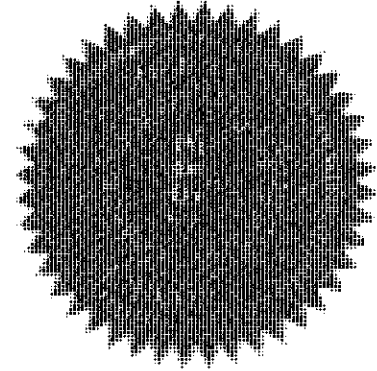
  
 Peter S. Pakalnis, QSTI/QSTO Review Board

  
 Leroy Owens, QSTI/QSTO Review Board

  
 C. David Bagwell, QSTI/QSTO Review Board

  
 Karen D. Kajiya-Mills, QSTI/QSTO Review Board

  
 Glenn C. England, QSTI/QSTO Review Board



# SOURCE EVALUATION SOCIETY



## Qualified Source Testing Individual

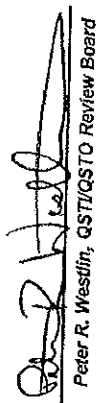
LET IT BE KNOWN THAT

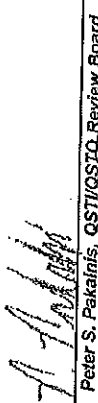
### JOSHUA A. JONES

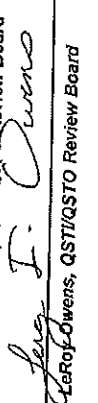
HAS SUCCESSFULLY PASSED A COMPREHENSIVE EXAMINATION AND SATISFIED EXPERIENCE REQUIREMENTS IN ACCORDANCE WITH THE GUIDELINES ISSUED BY THE SES QUALIFIED SOURCE TEST INDIVIDUAL REVIEW BOARD FOR

### HAZARDOUS METALS MEASUREMENT SAMPLING METHODS

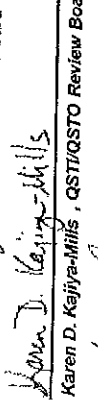
ISSUED THIS 22<sup>ND</sup> DAY OF FEBRUARY 2012 AND EFFECTIVE UNTIL FEBRUARY 21<sup>ST</sup>, 2017

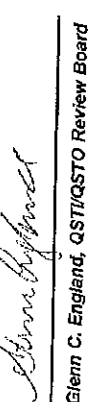
  
Peter R. Westlin, QSTI/QSTO Review Board

  
Peter S. Pakalnis, QSTI/QSTO Review Board

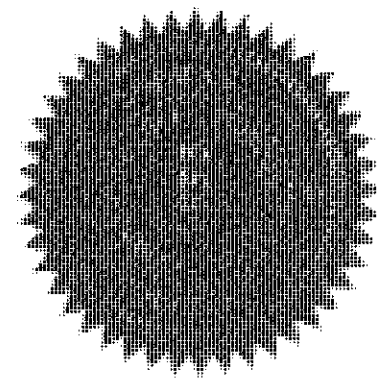
  
Leroy Owens, QSTI/QSTO Review Board

  
C. David Bagwell, QSTI/QSTO Review Board

  
Karen D. Kajjya-Mills, QSTI/QSTO Review Board

  
Glenn C. England, QSTI/QSTO Review Board

APPLICATION NO. 2012-621



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**APPENDIX F**

**PRODUCTION DATA DURING THE COMPLIANCE TEST**

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	Batch Code	Number of Batches	Pounds per Batch	Pounds Processed
Run #1	T4012WBV	51	719	36669
	AGC	1	700	700
	<b>Total Pounds Processed During the Run</b>			<b>37369</b>

Run #2	AGC	1	700	700
	Tread	11	700	7700
	G5036WCF	30	775.89	23276.7
	<b>Total Pounds Processed During the Run</b>			<b>31676.7</b>

Run #3	G5036WCF	6	775.89	4655.34
	T101JWAK	39	718.82	28033.98
	REMIL	3	700	2100
	<b>Total Pounds Processed During the Run</b>			<b>34789.32</b>

October 24<sup>th</sup> Run 1  
 9:55 am 4.0" of water  
 10:10 am 4.0" " "  
 10:25 am 4.0"  
 10:40 am 4.0"  
 10:55 am 4.0"  
 11:10 am 4.0"  
 11:25 am 4.0"  
 11:40 am 4.0"  
 11:55 am 4.0"  
 12:10 pm 4.0"

Boq house magnetic readings

Run 2  
 1:43 pm 4.0"  
 1:58 pm 4.0"  
 2:13 pm 4.0"  
 2:28 pm 4.0"  
 2:43 pm 4.0"  
 2:58 pm 4.0"  
 3:13 pm 4.0"  
 3:28 pm 4.0"  
 3:43 pm 4.0"

Run 3  
 4:30 pm 4.0"  
 4:45 pm /  
 5:00 pm 4.0"  
 5:15 pm 4.0"  
 5:30 pm 4.0"  
 5:45 pm /  
 6:00 pm 4.0"