

BRINE DISPOSAL WELL PERMIT APPLICATION BITTINGER #3

Bear Lake Properties, LLC

March 2015

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CLEAR SOLUTIONS"



March 24, 2015

S. Stephen Platt U.S. EPA Region III Ground Water & Enforcement Branch (3WP22) 1650 Arch Street Philadelphia, PA 19103

Subject: Application For Underground Injection Control Class II-D Brine Disposal Well Bear Lake Properties Bittinger #3 Well, Warren County, Pennsylvania

Dear Mr. Platt:

Enclosed please find two (2) copies of the Underground Injection Control Class II-D Brine Disposal Well permit application for the Bear Lake Properties, LLC (Bear Lake Properties) Bittinger #3 well located in Columbus Township, Warren County, Pennsylvania. As indicated in Section 10 "Necessary Resources", Bear Lake Properties will provide under separate cover the Certificate of Deposit to verify they have the necessary resources to properly plug and abandon the well.

Your prompt review of the application would be greatly appreciated. Please feel free to contact Karl Kimmich of Bear Lake Properties at (724) 444-7501 or me at (412) 921-4006 if you have questions or comments.

Sincerely, Tetra Tech, Inc.

Dale & Soof

Dale E. Skoff, P.G. Sr. Project Manager

cc: Dave Rectenwald – EPA Karl Kimmich – Bear Lake Properties John Holko – Bear Lake Properties

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Well Class and Type Codes

Class	I	Wells used to inject waste below the deepest underground source of drinking water.
Туре	"I" "M" "W" "X"	Nonhazardous industrial disposal well Nonhazardous municipal disposal well Hazardous waste disposal well injecting below USDWs Other Class I wells (not included in Type "I," [*] M," or "W")
Class	11	Oil and gas production and storage related injection wells.
Туре	"D" "R" "H" "X"	Produced fluid disposal well Enhanced recovery well Hydrocarbon storage well (excluding natural gas) Other Class II wells (not included in Type "D," "R," or "H")
Class	111	Special process injection wells.
Туре	"G" "S" "U" "X"	Solution mining well Sulfur mining well by Frasch process Uranium mining well (excluding solution mining of conventional mines) Other Class III wells (not included in Type "G," "S," or "U")
Other	Classe	S Wells not included in classes above.

Class V wells not included in classes above. Class V wells which may be permitted under §144.12. Wells not currently classified as Class I, II, III, or V.

Attachments to Permit Application

Class Attachments

I new well	A, B, C, D, F, H – S, U
existing	A, B, C, D, F, H – U
II new well	A, B, C, E, G, H, M, Q, R; optional – I, J, K, O, P, U
existing	A, E, G, H, M, Q, R, – U; optional – J, K, O, P, Q
III new well	A, B, C, D, F, H, I, J, K, M – S, U
existing	A, B, C, D, F, H, J, K, M – U
Other Classes	To be specified by the permitting authority

INSTRUCTIONS - Underground injection Control (UIC) Fermit Application

Paperwork Reduction Act: The public reporting and record keeping burden for this collection of information is estimated to average 224 hours for a Class I hazardous well application, 110 hours for a Class I non-hazardous well application, 67 hours for a Class II well application, and 132 hours for a Class III well application. Burden means the total time, effort, or financial resource expended by ersons to generate, maintain, retain, or disclose or provide information to or for a Federal Agency. This includes the time needed to review instructions; develop, acquire, install, and utilize technology and systems for the purposes of collecting, validating, and verifying information, processing and maintaining information, and disclosing and providing information; adjust the existing ways to comply with any previously applicable instructions and requirements; train personnel to be able to respond to the collection of information; search data sources; complete and review the collection of information; and, transmit or otherwise disclose the information. An agency may not conduct or sponsor, and a person is not required to respond to, a collection of information unless it displays a currently valid OMB control number. Send comments on the Agency's need for this information, the accuracy of the provided burden estimates, and any suggested methods for minimizing respondent burden, including the use of automated collection techniques to Director, Collection Strategies Division, U.S. Environmental Protection Agency (2822), 1200 Pennsylvania Ave., NW, Washington, DC 20460. Include the OMB control number in any correspondence. Do not send the completed forms to this address.

This form must be completed by all owners or operators of Class I, II, and III injection wells and others who may be directed to apply for permit by the Director.

- I. EPA I.D. NUMBER Fill in your EPA Identification Number. If you do not have a number, leave blank.
- II. OWNER NAME AND ADDRESS Name of well, well field or company and address.
- III. OPERATOR NAME AND ADDRESS Name and address of operator of well or well field.
- IV. COMMERCIAL FACILITY Mark the appropriate box to indicate the type of facility.
- V. OWNERSHIP Mark the appropriate box to indicate the type of ownership.
- VI. LEGAL CONTACT Mark the appropriate box.
- VII. SIC CODES List at least one and no more than four Standard Industrial Classification (SIC) Codes that best describe the nature of the business in order of priority.
- VIII. WELL STATUS Mark Box A if the well(s) were operating as injection wells on the effective date of the UIC Program for the State. Mark Box B if wells(s) existed on the effective date of the UIC Program for the State but were not utilized for injection. Box C should be marked if the application is for an underground injection project not constructed or not completed by the effective date of the UIC Program for the State.
- IX. TYPE OF PERMIT Mark "Individual" or "Area" to indicate the type of permit desired. Note that area permits are at the discretion of the Director and that wells covered by an area permit must be at one site, under the control of one person and do not inject hazardous waste. If an area permit is requested the number of wells to be included in the permit must be specified and the wells described and identified by location. If the area has a commonly used name, such as the "Jay Field," submit the name in the space provided. In the case of a project or field which crosses State lines, it may be possible to consider an area permit if EPA has jurisdiction in both States. Each such case will be considered individually, if the owner/operator elects to seek an area permit.
- X. CLASS AND TYPE OF WELL Enter in these two positions the Class and type of injection well for which a permit is requested. Use the most pertinent code selected from the list on the reverse side of the application. When selecting type X please explain in the space provided.
- XI. LOCATION OF WELL Enter the latitude and longitude of the existing or proposed well expressed in degrees, minutes, and seconds or the location by township, and range, and section, as required by 40 CFR Part 146. If an area permit is being requested, give the latitude and longitude of the approximate center of the area.
- XII. INDIAN LANDS Place an "X" in the box if any part of the facility is located on Indian lands.
- XIII. ATTACHMENTS Note that information requirements vary depending on the injection well class and status. Attachments for Class I, II, III are described on pages 4 and 5 of this document and listed by Class on page 2. Place EPA ID number in the upper right hand corner of each page of the Attachments.
- XIV. CERTIFICATION All permit applications (except Class II) must be signed by a responsible corporate officer for a corporation, by a general partner for a partnership, by the proprietor of a sole proprietorship, and by a principal executive or ranking elected official for a public agency. For Class II, the person described above should sign, or a representative duly authorized in writing.

For assistance in accessing the downent contact B3 UIC_Mailbox@epa.gov

Attachments to be submitted with permit application for Class I, II, III and other wells.

- A. AREA OF REVIEW METHODS Give the methods and, if appropriate, the calculations used to determine the size of the area of review (fixed radius or equation). The area of review shall be a fixed radius of 1/4 mile from the well bore unless the use of an equation is approved in advance by the Director.
- B. MAPS OF WELL/AREA AND AREA OF REVIEW Submit a topographic map, extending one mile beyond the property boundaries, showing the injection well(s) or project area for which a permit is sought and the applicable area of review. The map must show all intake and discharge structures and all hazardous waste treatment, storage, or disposal facilities. If the application is for an area permit, the map should show the distribution manifold (if applicable) applying injection fluid to all wells in the area, including all system monitoring points. Within the area of review, the map must show the following:

Class I

The number, or name, and location of all producing wells, injection wells, abandoned wells, dryholes, surface bodies of water, springs, mines (surface and subsurface), quarries, and other pertinent surface features, including residences and roads, and faults, if known or suspected. In addition, the map must identify those wells, springs, other surface water bodies, and drinking water wells located within one quarter mile of the facility property boundary. Only information of public record is required to be included in this map;

Class II

In addition to requirements for Class I, include pertinent information known to the applicant. This requirement does not apply to existing Class II wells;

Class III

In addition to requirements for Class I, include public water systems and pertinent information known to the applicant.

C. CORRECTIVE ACTION PLAN AND WELL DATA - Submit a tabulation of data reasonably available from public records or otherwise known to the applicant on all wells within the area of review, including those on the map required in B, which penetrate the proposed injection zone. Such data shall include the following:

Class I

Adescription of each well's types, construction, date drilled, location, depth, record of plugging and/or completion, and any additional information the Director may require. In the case of new injection wells, include the corrective action proposed to be taken by the applicant under 40 CFR 144.55.

Class II

In addition to requirement for Class I, in the case of Class II wells operating over the fracture pressure of the injection formation, all known wells within the area of review which penetrate formations affected by the increase in pressure. This requirement does not apply to existing Class II wells.

Class III

In addition to requirements for Class I, the corrective action proposed under 40 CFR 144.55 for all Class III wells.

D. MAPS AND CROSS SECTION OF USDWs - Submit maps and cross sections indicating the vertical limits of all underground sources of drinking water within the area of review (both vertical and lateral limits for Class I), their position relative to the injection formation and the direction of water movement, where known, in every underground source of drinking water which may be affected by the proposed injection. (Does not apply to Class II wells.)

EPA Form 7520-6

Page 4 of 6

- E. NAME AND DEPTHFOF DESTANCE (CEASSSING_this declass in the course of drinking water which may be affected by the injection.
- F. MAPS AND CROSS SECTIONS OF GEOLOGIC STRUCTURE OF AREA Submit maps and cross sections detailing the geologic structure of the local area (including the lithology of injection and confining intervals) and generalized maps and cross sections illustrating the regional geologic setting. (Does not apply to Class II wells.)
- G. GEOLOGICAL DATA ON INJECTION AND CONFINING ZONES (Class II) For Class II wells, submit appropriate geological data on the injection zone and confining zones including lithologic description, geological name, thickness, depth and fracture pressure.
- H. OPERATING DATA Submit the following proposed operating data for each well (including all those to be covered by area permits): (1) average and maximum daily rate and volume of the fluids to be injected; (2) average and maximum injection pressure; (3) nature of annulus fluid; (4) for Class I wells, source and analysis of the chemical, physical, radiological and biological characteristics, including density and corrosiveness, of injection fluids; (5) for Class II wells, source and analysis of the physical and chemical characteristics of the injection fluid; (6) for Class III wells, a qualitative analysis and ranges in concentrations of all constituents of injected fluids. If the information is proprietary, maximum concentrations only may be submitted, but all records must be retained.
- I. FORMATION TESTING PROGRAM Describe the proposed formation testing program. For Class I wells the program must be designed to obtain data on fluid pressure, temperature, fracture pressure, other physical, chemical, and radiological characteristics of the injection matrix and physical and chemical characteristics of the formation fluids.

For Class II wells the testing program must be designed to obtain data on fluid pressure, estimated fracture pressure, physical and chemical characteristics of the injection zone. (Does not apply to existing Class II wells or projects.)

For Class III wells the testing must be designed to obtain data on fluid pressure, fracture pressure, and physical and chemical characteristics of the formation fluids if the formation is naturally water bearing. Only fracture pressure is required if the program formation is not water bearing. (Does not apply to existing Class III wells or projects.)

- J. STIMULATION PROGRAM Outline any proposed stimulation program.
- K. INJECTION PROCEDURES Describe the proposed injection procedures including pump, surge, tank, etc.
- L. CONSTRUCTION PROCEDURES Discuss the construction procedures (according to §146.12 for Class I, §146.22 for Class II, and §146.32 for Class III) to be utilized. This should include details of the casing and cementing program, logging procedures, deviation checks, and the drilling, testing and coring program, and proposed annulus fluid. (Request and submission of justifying data must be made to use an alternative to packer for Class I.)
- M. CONSTRUCTION DETAILS Submit schematic or other appropriate drawings of the surface and subsurface construction details of the well.
- N. CHANGES IN INJECTED FLUID Discuss expected changes in pressure, native fluid displacement, and direction of movement of injection fluid. (Class III wells only.)
- O. PLANS FOR WELL FAILURES Outline contingency plans (proposed plans, if any, for Class II) to cope with all shut-ins or wells failures, so as to prevent migration of fluids into any USDW.
- P. MONITORING PROGRAM Discuss the planned monitoring program. This should be thorough, including maps showing the number and location of monitoring wells as appropriate and discussion of monitoring devices, sampling frequency, and parameters measured. If a manifold monitoring program is utilized, pursuant to §146.23(b)(5), describe the program and compare it to individual well monitoring.
- Q. PLUGGING AND ABANDONMENT PLAN Submit a plan for plugging and abandonment of the well including: (1) describe the type, number, and placement (including the elevation of the top and bottom) of plugs to be used; (2) describe the type, grade, and quantity of cement to be used; and (3) describe the method to be used to place plugs, including the method used to place the well in a state of static equilibrium prior to placement of the plugs. Also for a Class III well that underlies or is in an exempted aquifer, demonstrate adequate protection of USDWs. Submit this information on EPA Form 7520-14, Plugging and Abandonment Plan.

- R. NECESSARY RESOURCES^{sta}Stabilite construction and the well are available.
- S. AQUIFER EXEMPTIONS If an aquifer exemption is requested, submit data necessary to demonstrate that the aquifer meets the following criteria: (1) does not serve as a source of drinking water; (2) cannot now and will not in the future serve as a source of drinking water; and (3) the TDS content of the ground water is more than 3,000 and less than 10,000 mg/l and is not reasonably expected to supply a public water system. Data to demonstrate that the aquifer is expected to be mineral or hydrocarbon production, such as general description of the mining zone, analysis of the amenability of the mining zone to the proposed method, and time table for proposed development must also be included. For additional information on aquifer exemptions, see 40 CFR Sections 144.7 and 146.04.
- T. EXISTING EPA PERMITS List program and permit number of any existing EPA permits, for example, NPDES, PSD, RCRA, etc.
- U. DESCRIPTION OF BUSINESS Give a brief description of the nature of the business.

EPA Form 7520-6

Section 1 – Area of Review Methods/Calculations

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45610 Woodland Road, Suite 400, Sterling, VA 20166 703-444-7000 703-444-1685 (FAX)

TECHNICAL MEMORANDUM

- TO: Dale Skoff, Tetra Tech OGA
- FROM: Jeffrey Benegar

DATE: February 4, 2015

RE: Area of Review/Zone of Endangerment Analysis for Bittinger #3 and Smith-Ras #1 Wells – Bear Lake Properties

EXECUTIVE SUMMARY

This technical memorandum (TM) summarizes the analytical modeling we have performed for the area of review/zone of endangerment analysis for the Bittinger #3 and Smith-Ras #1 wells. The scenarios involved injecting simultaneously at existing Bear Lake Properties UIC Class IID brine disposal wells Bittinger #1, #4, and #2, all of which are located in Columbus Township, Warren County, Pennsylvania (the Bittinger #1 and Bittinger #4 wells received their final UIC Class IID (Commercial) well permits in November 2012 and Bittinger #2 in late 2014). The relevant parameters for our analysis were obtained from Bear Lake Properties, LLC or estimated in the absence of any information. Our analysis is described in more detail below.

OVERVIEW AND METHODOLOGY

There are several methods proposed for calculating the zone of endangerment of an injection well. The most simplistic method is the use of a fixed radius, based on the type of injection well being permitted. Other methods involve calculation of the radius based on well and formation properties. Most regulatory agencies require the use of calculations to determine the zone of endangerment. The method used here is the graphical method first used by US EPA Region 6. It involves the calculation of the increase of pressure in the formation due to injection, then converting that pressure into equivalent feet of head. The increase in head in the formation due to injection is then compared to the equivalent head of the lowest most underground source of drinking water (USDW). When plotted graphically, the intersection of those two curves at some distance, r, determines the radius of the zone of endangerment.

The increase in pressure in the formation due to injection depends on the properties of the injection fluid and the formation, the rate of fluid injection, and the length of time of injection. The most common mathematical expression to describe this increase in pressure was developed

by Matthews and Russell (1967). Matthews and Russell assume that, for a single well injecting into an infinite, homogeneous and isotropic, non-leaking formation, the increase in pressure (delta p) can be described as:

delta p = 162.6 Qµ / kh * [(log(kt / $\Phi\mu Cr^2$) – 3.23] where:

delta p = pressure change (psi) at radius, r and time, t

Q = injection rate (barrels/day)

 μ = injectate viscosity (centipoise)

k = formation permeability (millidarcies)

h = formation thickness (feet)

t = time since injection began (hours)

C = compressibility (total, sum of water and rock compressibility) (psi⁻¹)

r = radial distance from wellbore to point of investigation (feet)

 Φ = average formation porosity (decimal)

PARAMETERS USED IN THE ANALYSIS

The following parameters were used in the zone of endangerment analysis. For injection rate, we used the average daily rate based on the permitted monthly rate for the three existing permitted Bear Lake Properties UIC Class IID wells, which is 30,000 bbls/month for each well, which averages approximately 1,000 bbls/day per well. For permeability, we used a value of 50 md, which we feel is conservative based on the injection rate sustainable for existing disposal wells at the site and the substantial volume of natural gas produced from the reservoir, both of which indicate significant permeability. The initial pressure at the top of the injection formation was based upon measurements taken prior to injection at the Bittinger #4 well.

Bittinger #3 Medina Group Well

Q = 1000 barrels/day t = 10 years = 87,600 hours μ = 1 centipoise k = 50 md h = 61 feet C = 3.0e-06 psi⁻¹ Φ = 0.08 Specific gravity of injectate = 1.218 Surface elevation = 1638 feet Depth to injection formation = 4260 feet Base of lowest most USDW (MSL) = 1338 feet Initial pressure at top of injection formation = 128 psi

 $\frac{\text{Smith-Ras #1 Medina Group Well}}{Q = 1000 \text{ barrels/day}}$ t = 10 years = 87,600 hours μ = 1 centipoise

k = 50 md

h = 61 feet

 $C = 3.0e-06 \text{ psi}^{-1}$ $\Phi = 0.08$ Specific gravity of injectate = 1.218 Surface elevation = 1575 feet Depth to injection formation = 4222 feet Base of lowest most USDW (MSL) = 1275 feet Initial pressure at top of injection formation = 128 psi

Bittinger #2 Medina Group Well Q = 1000 barrels/day t = 10 years = 87,600 hours μ = 1 centipoise k = 50 md h = 61 feet C = 3.0e-06 psi⁻¹ Φ = 0.08 Specific gravity of injectate = 1.218 Surface elevation = 1621 feet Depth to injection formation = 4279 feet Base of lowest most USDW (MSL) = 1321 feet Initial pressure at top of injection formation = 128 psi

Bittinger #1 Medina Group Well

Q = 1000 barrels/day t = 10 years = 87,600 hours μ = 1 centipoise k = 50 md h = 61 feet C = 3.0e-06 psi⁻¹ Φ = 0.08 Specific gravity of injectate = 1.218 Surface elevation = 1518 feet Depth to injection formation = 4210 feet Base of lowest most USDW (MSL) = 1218 feet Initial pressure at top of injection formation = 128 psi

Bittinger #4 Medina Group Well Q = 1000 barrels/day t = 10 years = 87,600 hours μ = 1 centipoise k = 50 md h = 61 feet C = 3.0e-06 psi⁻¹ Φ = 0.08 Specific gravity of injectate = 1.218 Surface elevation = 1561 feet

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Depth to injection formation = 4285 feet Base of lowest most USDW (MSL) = 1261 feet Initial pressure at top of injection formation = 128 psi

RESULTS

The Matthews and Russell equation was solved for various distances from the wellbore based on the parameters listed above. The distance between each of the wells is:

Wells	Distance (ft)
Bittinger #3 to Bittinger #2	2,052
Bittinger #3 to Bittinger #4	3,566
Bittinger #3 to Bittinger #1	3,779
Smith-Ras #1 to Bittinger #2	1,714
Smith-Ras #1 to Bittinger #4	2,584
Smith-Ras #1 to Bittinger #1	2,180
Smith-Ras #1 to Bittinger #3	1,980
Bittinger #1 to Bittinger #4	1,300
Bittinger #1 to Bittinger #2	2,000
Bittinger #2 to Bittinger #4	1,600

The Matthews and Russell equation was used to calculate the increase in pressure in the formation with only one well injecting. This was done for all five wells. Then, the calculated pressures for each well were added together and this sum was added to the value of existing pressure in the injection formation to obtain the total pressure in the formation when all five wells are injecting.

These values were then converted to feet of head of formation brine. The values are plotted against distance from the wellbore and are shown in Figure 1 for the Bittinger #3 well and Figure 2 for the Smith-Ras #1 well. The plot shows the calculated pressure surface within the injection formation, measured as feet of head of formation brine above the top of the injection formation. Also shown is the head of the lowest most USDW. Where the two lines intersect, the radius of the zone of endangerment can be estimated. The results indicate that the increase in head in the formation due to injection will intersect the elevation of the lowestmost USDW at a distance of approximately 4 feet for the Bittinger #3 well and approximately 60 feet for the Smith-Ras #1 well. These distances are well within the ¹/₄ mile standard fixed radius for area of review/zone of endangerment.

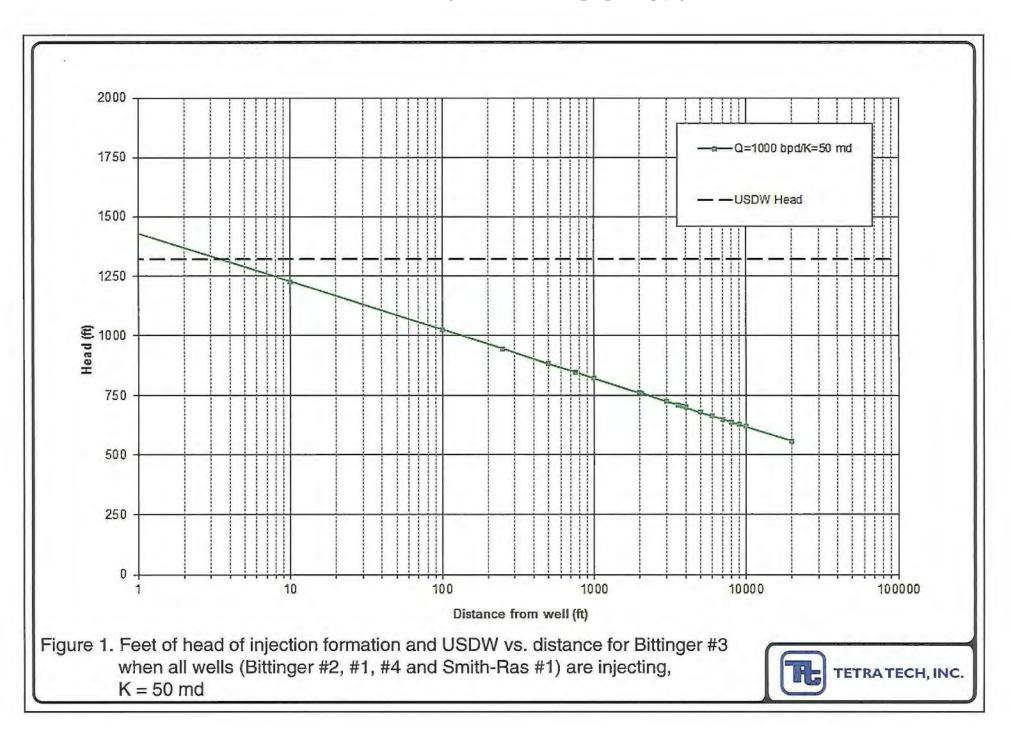
CONCLUSIONS

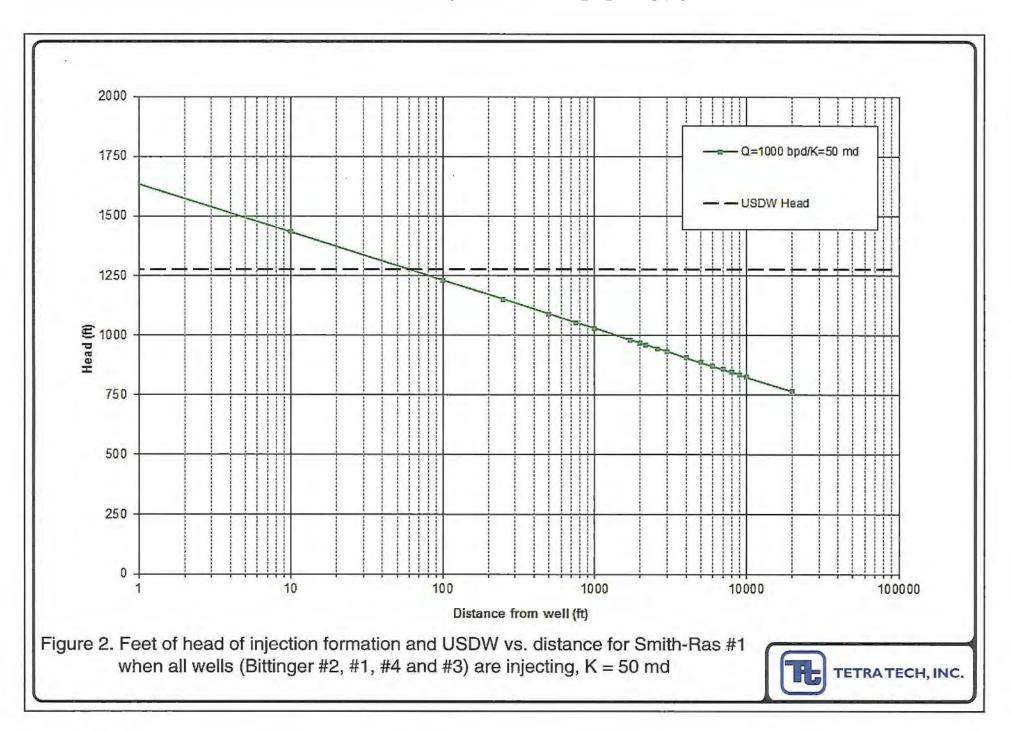
Our analysis of the area of review/zone of endangerment for the Bittinger #3 and Smith-Ras #1 wells (injecting together with the Bittinger #2, #4, and #1 wells) is based on a methodology typically used by US EPA. Based on the results, we believe the Bittinger #3 and Smith-Ras #1 wells are excellent candidates for use as brine disposal wells. The increase in head in the formation due to injection intersects the elevation of the lowestmost USDW well within ¼ mile

for each well. The standard fixed radius of ¹/₄ mile can be used for the area of review/zone of endangerment for the Bittinger #3 and Smith-Ras #1 wells.

REFERENCES

Matthews, C.S., Russell, D.G., (1967) Pressure Buildup and Flow Tests in Wells, SPE Monograph Series, Volume 1, New York.





Section 2 – Maps of Well Area and Area of Review

Section 2 – Maps of Well Area and Area of Review

According to publicly available records in the area, there are no intake or discharge structures, hazardous waste treatment, storage, or disposal facilities, mines, or quarries within one mile of the Bittinger #3 well. An intermittent unnamed tributary (UNT) to Tamarack Swamp is located approximately 1 mile southwest of the Bittinger #3 well. Tamarack Swamp is located approximately 1 mile southwest, Brokenstraw Creek is located approximately 1 mile northwest, and an UNT to Pine Valley Creek is located approximately 0.3 miles south of Bittinger #3.

The Pennsylvania Geologic Survey "Ground Water Inventory System" (GWIS) database was accessed to determine the sources of groundwater sources in the site area. The database search identified one well within the quarter mile AOR. It is noted that the well reporting requirement was established in 1968 is not considered to be a complete record of water wells and other wells may be present. (Pennsylvania Topographic and Geologic Survey, September 15, 2010). In addition to the one well on the PA GWIS database, eight additional water wells were identified with the AOR based on public input and a foot survey by Bear Lake Properties staff. Attached are a map showing the location of the above-referenced wells and a table summarizing information on the wells.

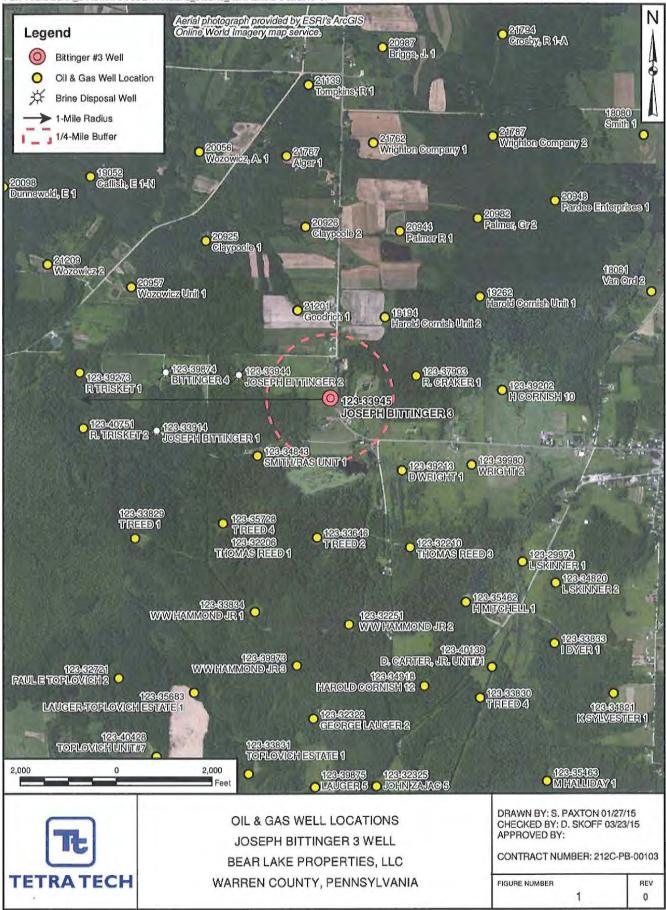
The names and addresses of residents located within 1/4 mile of the proposed injection well are provided in Appendix A.

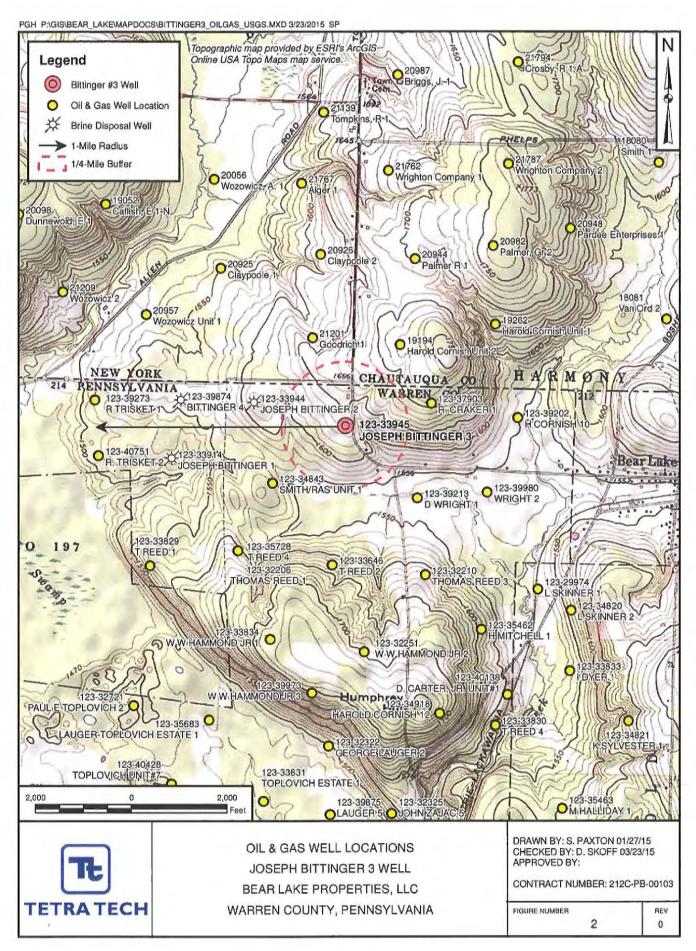
Wells Located Within the 1/4 Mile Radius Area of Review (AOR) For The Bittinger #3 Well

					Drilling			
Well Owner / Name	API #	Lat	Long	TD	Completed	Last Csg	Csg depth	Completion
		Oil ar	nd Gas and Pro	posed Injectio	n Wells			
Bear Lake Properties Bittinger #3 (Proposed								
InjectionWell)	123-33945	41.996022	-79.528068	4566 ft	10/19/1984	4.5 in	4508 ft	Perf'd and frac'd
			Wate	r Wells				
405218*		41.99812	-79.5288	86 ft	34304			
David Bemis #2	N/A	41.999667	-79.527733					
Casper Goodrich	N/A	41.998850	-79.528217					
Enos Miller	N/A	41.998267	-79.527367					
Lion/Bear Lake Property	N/A	41.998367	-79.528617					
Ted Smith	N/A	41.994867	-79.527767			_		
Ron Cracker	N/A	41.994767	-79.526617					
Charlie Wiliams	N/A	41.993583	-79.526300					
Jeff McRay	N/A	41.993650	-79.525033					

For assistance in accessing this document, contact R3_UIC_Mailbox@epa.gov

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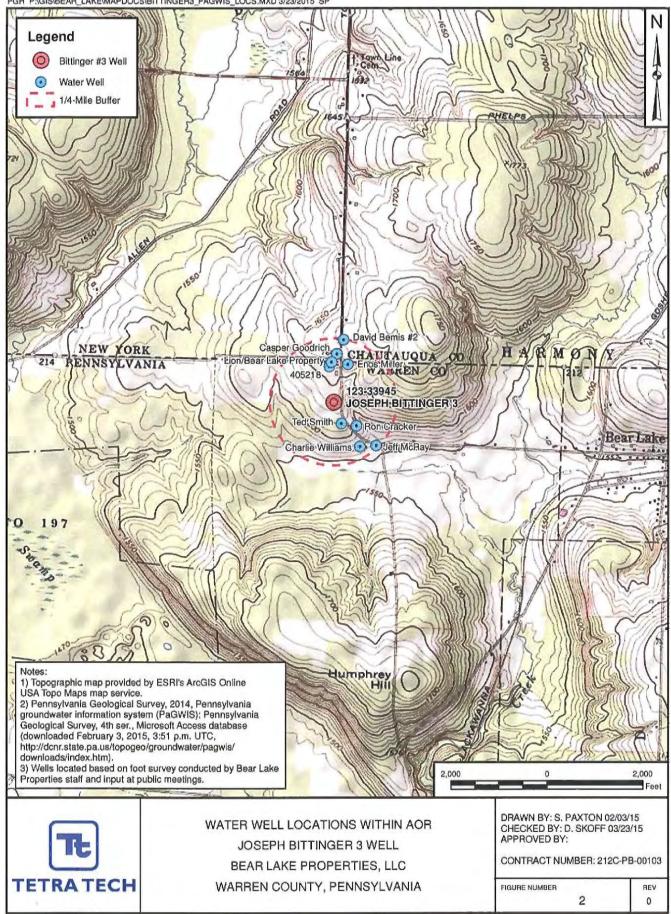




AREA OF REVIEW MAPS

GROUNDWATER WELLS

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Section 3 – Corrective Action Plan and Well Data

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Section 3 - Corrective Action Plan and Well Data

According to publicly available records of oil and gas wells and a survey conducted by foot, there are no existing, or plugged and abandoned wells within the ¼ mile radius AOR for the Bittinger # 3 well. The R. Craker #1 and D. Wright #1 wells will be used as monitoring wells. If the fluid level in either monitoring well is observed to rise up to within 100 feet of the base of the USDW, disposal operations in the Bittinger #3 well will be stopped immediately, EPA will be notified, and operating conditions will be evaluated in order to control the fluid levels.

Existing Oil and Gas Wells within the Area of Review

Well completion records are required to be submitted for all wells located within the AOR in order to evaluate the need for corrective action specific to each well. As indicated above, there are no oil and gas wells located within the AOR.

Plugged and Abandoned Wells

No plugged and abandoned wells have been identified within the 1/4 mile AOR for the Bittinger #3 well.

Section 4 – Name and Depth of USDWs

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Section 4 - Underground Sources of Drinking Water (USDW)

The site lies within the Glaciated Plateau section of the Appalachian Plateaus Physiographic province. Both unconsolidated glacial units and bedrock are used for potable water. The uppermost unit at the site is mapped as Wisconsin age glacial kame deposits. Kame deposits consist primarily of sand and gravel interbedded with minor amounts of silt and clay (Pennsylvania Topographic and Geologic Survey, 1959). The well log for Bittinger #3 indicates that unconsolidated gravel is present from the surface to a depth of 30 feet below ground surface.

The uppermost bedrock beneath the site is mapped as the Devonian age Venango formation. The Venango formation consists of interbedded pebble conglomerate, crossbedded sandstone, siltstone, and shale. This unit is up to 330 feet thick in Venango County; however, only a portion of the unit is present in the site area. This unit is used as an aquifer throughout Warren County. The well log for Bittinger #3 indicates that Devonian age shale is present from 30 ft to a depth of 2,816 ft below ground surface. This is believed to include the Venango Formation, the Chadokoin formation, and the underlying Bradford Group. Wells deeper than approximately 100 feet deep usually encounter salt water, which is supported by the generally shallow well depths in Columbus Township. (PADER, 1982, US Geologic Survey, 2007)

The Devonian age Chadakoin formation underlies Venango formation and consists of finegrained marine clastics (siltstone and shale) and includes a purplish pink sequence which is often used as a marker unit. This unit is up to 450 thick in Warren County.

The Pennsylvania Geologic Survey "Ground Water Inventory System" (GWIS) database was accessed to determine the sources of groundwater sources in the site area. The database search identified one well within the quarter mile AOR. It is noted that the well reporting requirement was established in 1968 is not considered to be a complete record of water wells and other wells may be present. (Pennsylvania Topographic and Geologic Survey, September 15, 2010). In addition to the one well on the PA GWIS database, eight additional water wells were identified within the AOR based on public input and a foot survey by Bear Lake Properties staff. Section 2 of this application includes a map showing the location of the above-referenced wells and a table summarizing information on the wells.

The New York Department of Environmental Conservation (DEC) "Water Well Program Information Search Wizard" website was utilized to determine if there were any water wells in New York State within the 1⁄4 mile AOR of the Bittinger #3 well. No water wells were identified within the AOR of the Bittinger #3 well.

Based on the available information, the glacial units and the top 100 feet of bedrock is considered the underground sources of drinking water in the site area. The well logs indicate that the glacial material is approximately 30 feet thick beneath the site. Freshwater is expected to be encountered to a depth of approximately 100 feet with increasing salinity beyond that depth. The Bittinger #3 well has 8 5/8 inch surface casing cemented to a depth of 405 feet below ground surface, providing a buffer of approximately 300 feet beyond the base of the underground sources of drinking water based on the well data in Columbus Township (maximum well depth of 130 feet) and the references indicating brine being encountered at depths over 100 feet within the bedrock units. In addition, production casing extends several thousands of feet below the drinking water source and is cemented approximately 900 feet above the injection interval. (Injection well construction is described in detail in the "Well Construction" section.)

In calculating the depth to the base of the lowermost USDW, the depth of the deepest well in the area 130 feet (it is believed that the generally shallow well depth in the area was related to water quality issues based on the available literature) was doubled and rounded upward to the nearest 100 feet, providing a conservative maximum depth estimate of the underground source of drinking water of 300 feet.

References:

New York Department of Environmental Conservation website "DEC Water Well Program Information Search Wizard": <u>http://www.dec.ny.gov/lands/33317.html</u>

Pennsylvania Topographic and Geologic Survey, 1959. "Glacial Geology of Northwestern, PA." Bulletin G 32.

Pennsylvania Topographic and Geologic Survey, 1981. "Atlas of Preliminary Quadrangle Maps of Pennsylvania, PA." Map 61.

PADER, 1982. "Engineering Characteristics of the Rocks of Pennsylvania". Environmental Geology Report 1.

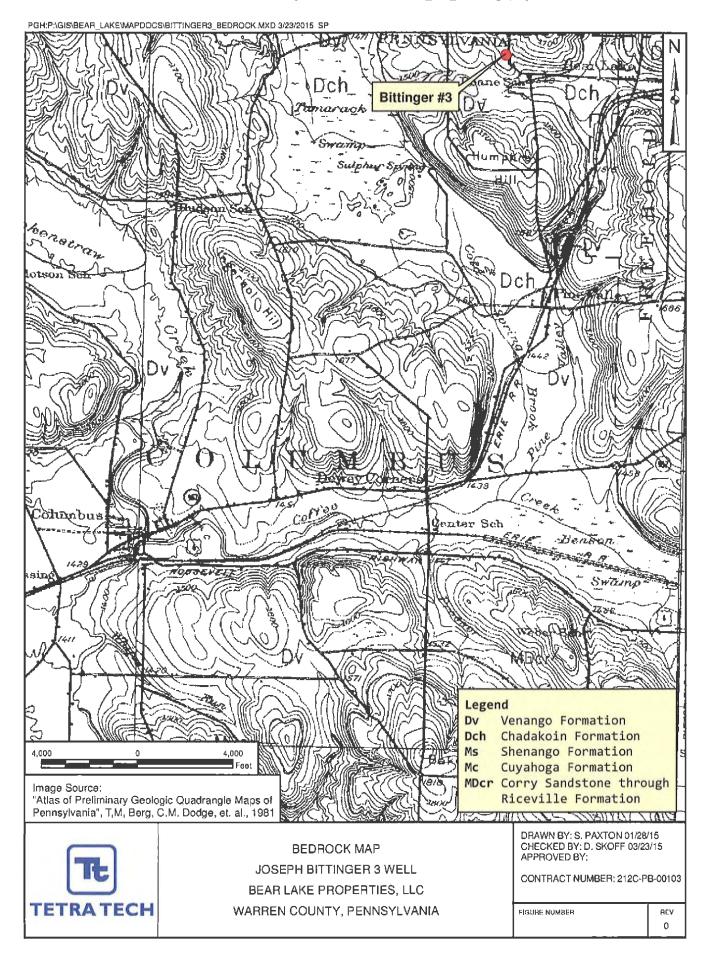
Pennsylvania Topographic and Geologic Survey, September 15/20, 2010. "Ground Water Inventory System". <u>www.dcnr.state.pa.us/topogeo/groundwater/PAGWIS</u>

US Geologic Survey, 2007. "Ground-Water Resources and the Hydrologic Effects of Petroleum Occurrence and Development, Warren County, Northwestern Pennsylvania." Scientific Investigations Report 2006-5263.

UNDERGROUND SOURCES OF DRINKING WATER

BEDROCK MAP

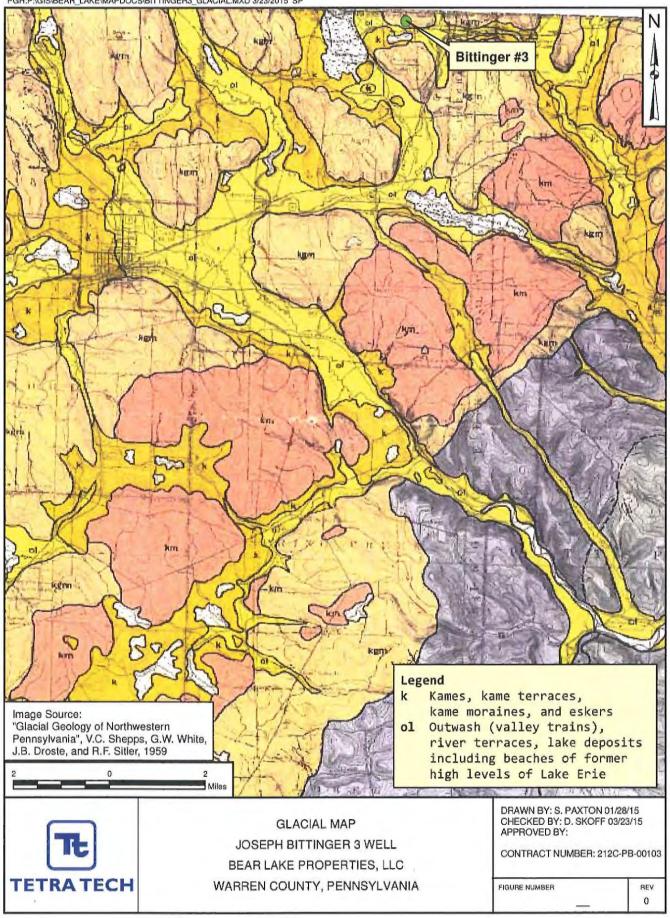
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UNDERGROUND SOURCES OF DRINKING WATER

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GLACIAL MAP



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Section 5 – Geologic Data on Injection and Confining Zones

Section 5 – Geologic Data on Injection and Confining Zones

The well is designed to inject into the Grimsby and Whirlpool sandstone units of the Medina Group which occurs at depths between 4,260 and 4,439 feet below grade in the Bittinger #3 well. The Medina is a depleted reservoir in this area.

As seen on the generalized stratigraphic column (attached), most of the geologic "groups" and "formations" overlying the Medina can be considered confining units totaling approximately 2,000 feet. Although many of these units are predominantly shale, they also contain reservoir rock and are shown with shading in confining unit column. Therefore, the Lockport and the Salina are seen as the most significant confining units and have a combined thickness of approximately 800 feet in the site area. As indicated, these units provide only a portion of the confining capacity and there are numerous other units that provide further protection.

The characteristics of the Medina Group formations including the Grimsby and Whirlpool are described in the attached report prepared by Billman Geologic Consultants entitled, "Geologic Review of the Bittinger Area, Planned SWD Site", dated August 2, 2010, and the cover letter dated April 5, 2014 discussing the Bittinger #2 well geologic characteristics. The subject report includes cross-sections in the vicinity of the Bittinger #3 well. As demonstrated by the cross-sections, the formation characteristics (lithology, thickness, porosity, etc.) of the Medina Group rocks in the Bittinger #3 well are very similar to those of the nearby wells including the three permitted brine disposal wells (Bittinger #1, #2 and #4 wells) operated by Bear Lake Properties.

Also attached are the following:

- Bittinger #3 completion record and geophysical log,
- Maximum Injection Pressure (MIP) calculations based on Instantaneous Shut-In Pressure (ISIP) data for the nearby Smith/Ras #1 well
- Smith/Ras #1 treatment reports.

Potential for Faults and Seismicity

As discussed in the attached Billman Geologic Consultants Report, geologic mapping performed at the Bear Lake Properties site as part of natural gas exploration and development in the Medina Group sandstone units has not identified evidence of significant faulting (e.g., duplicated intervals evident in log analysis, unusual thickening or thinning of intervals, etc.). Likewise the production of large volumes of natural gas from the Medina Group indicates the lack of significant faults which would allow for migration of the entrapped gas out of the Medina.

It is also noted that the Medina Group wells at the site are largely depleted resulting in lower than natural rock pressures. Production data for the Bittinger #3 are summarized on the attached table (referenced above) along with six other nearby wells. Cumulative gas production from the Bittinger #3 well is approximately 213 MMCF. Total production from all seven wells is over 1.75 BCF. The impact of removal of this large volume of gas is, as expected, a decrease in reservoir pressure. Injecting brine at or below the proposed maximum injection pressure would therefore not likely result in "overpressuring" faults (if any do exist in the area) and causing movement.

Finally, it is highly unlikely that injection at the site would engage any deep, Pre-Cambrian basement faults. According to the PA DCNR "Precambrian Basement Map of the Appalachian Basin and Piedmont Province in Pennsylvania" http://www.dcnr.state.pa.us/cs/groups/public/documents/document/dcnr 016250.pdf) the depth to

basement in the site vicinity is estimated at approximately 2,500 meters (or 8,200 feet) below sea level. The base of the Medina Group at the Bear Lake Properties site is approximately 2,800 ft. below sea level, or approximately a mile above Pre-Cambrian basement.

A review of the PA DCNR "Earthquake Epicenters in and Near Pennsylvania" (attached) indicates that there have been no recorded seismic events within 25 miles of the disposal project area since 1724, the start of the reporting period.

In summary, a detailed review of the zone of injection and data on geologic strata surrounding the zone of injection for the proposed brine disposal well, indicates the following supporting evidence that seismicity is highly unlikely: 1) The detailed geologic cross-sections (Appendix 2 of the Billman Geologic Consultants Report) and isopach and structural mapping completed by Billman Geologic Consultants show no evidence of faulting in the study area. 2) Historic production of over 1.75 billion cubic feet of gas among the Bittinger #1, #2, #3 and #4, Smith Ras #1 and Trisket #1 and #2 wells and unknown volumes of formation brine from the proposed zone of injection near the Bittinger #3 has depleted the zone of almost 90% of its original reservoir pressure. The disposal operations will re-fill this void space over the life of the project. 3) There have been no recorded seismic events within 25 miles of the disposal project area since 1724, the start of the reporting period referenced in the PA DCNR earthquake epicenters map.

GEOLOGIC DATA

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GENERALIZED STRATIGRAPHIC COLUMN

Generalized Stratigraphic Column Bittinger No 3 Warren County, PA

Age	Group	Formation	Predominant	Total Depth	Thick ness	Confining
			Rock Type	to Base(Feet)	Feet	Zone
Glacial Units				30	30	
Upper Devonian	Venango		Shale/sandstone			
Upper Devonian		Chadakoin	Shale			
Upper Devonian	Bradford		Shale			
Upper Devonian	Elk		Shale	2816	2786	
Upper Devonian		Java	Shale	2010	2700	
Upper Devonian		West Falls	Shale			
Upper Devonian		Sonyea	Shale			
Upper Devonian		Genesee	Shale			
Upper Devonian		Tully Limestone	Limestone	2926	110	
Upper Devonian	Hamilton	Mahantango	Shale, some sandstone	3097	171	
Upper Devonian	Hamilton	Marcellus Shale	Shale	3097	1/1	
Middle Devonian		Onondaga	Limestone	3256	159 ,	
		Unconformity Interval		3285	29	
Upper Silurian		Salina - including Akron-Berite, Camillus, Syracuse, Vernon	Evaporites/Dolomite	3900	615	
Upper Silurian		Lockport Dolomite	Dolomite	4108	208	
Lower Silurian	Clinton	Rochester Shale, Irondequoit-Reynales Dolomite	Sandstone	4260	122	
Lower Silurian		Medina, inlcuding the Grimsby and Whirlpool Sandstones	Sandstone/Shale	4439	179	

Notes



= Black shading Indicates that this unit is considered to be a confining zone

= Diagonal shading Indicates that this unit is a confining unit that also contains producing zones within it

= No shading indicates that this unit is a producing zone and is not considered to be a confining unit

GEOLOGIC DATA

BILLMAN GEOLOGIC CONSULTANTS REPORT

BILLMAN GEOLOGIC CONSULTANTS, INC.

то:	MR KARL KIMMICH, LION ENERGY COMPANY, LLC
FROM:	DAN A. BILLMAN, PG, CPG, BILLMAN GEOLOGIC CONSULTANTS, INC.
SUBJECT:	GEOLOGIC REVIEW OF THE BITTINGER #2, PROPOSED SWD WELL
DATE:	04/05/2014
CC:	

This memo is to be read in conjunction with the report entitled, "Geologic Review of the Bittinger Area, Planned SWD Site", dated 8/2/2010., Written by Dan A. Billman of Billman Geologic Consultants, Inc.

Billman Geologic Consultants, Inc. (BGC) was requested by Lion Energy Company, LLC to review the geology of a proposed SWD well at the Bittinger #2 (123-33944). The well is located in Columbus Township, Warren County, Pennsylvania. Specifically, the area is located in and around the Bittinger, Smith and Reed properties; collectively referred to as the "Bittinger SWD site". Figure 1 depicts the well base map of the Bittinger #2 area.

The Bittinger #2 (123-33944) was initially drilled by U.S. Energy Development and later acquired by Lion Energy, when Lion Energy acquired the field from Belden and Blake, Corp. The well was originally drilled to a total depth of 4,574', into the Queenston Shale Formation. The well was naturally completed in the Medina Sandstone and Whirlpool Sandstone. The well had a natural reported open flow 554 mcf/d and a reported natural rock pressure of 1,100 psi, recorded after a buildup of 72 hours (refer to completion reports included as Appendix 1 of this memo).

Geologic Analysis of Data Associated with the Bittinger SWD Site

The initial report of the Bittinger SWD area discusses the geology of both the Medina Sandstone and Whirlpool Sandstone. The Bittinger #2 well is located approximately 1,200' west of the Bittinger #4 and located approximately 1,500' northeast of the Bittinger #1. After review of the logs and completion reports (Appendix 1) of the Bittinger #2, both the Medina (Grimsby) and Whirlpool Sandstones are similar to the correlative formations within the Bittinger #1 and Bittinger #4 wells.

BGC completed a review of the logs associated with the Bittinger #2 (123-33944), as well as the Bittinger #1 (123-33914), #4 (123-39874) and other wells in the immediate area (Table 1 of the original report). The Medina Sandstone (Grimsby Sandstone) has 38' of formation equal or greater than 6% porosity, while the average for the area was

39.2'. Likewise, The Whirlpool Sandstone has 12' of formation equal or greater than 6% porosity, while the average for the area was 11.1'. For both sandstone formations, the characteristics are very typical for the area.

In the Bittinger #2, there is approximately 625' between the top of the Medina (Grimsby) Sandstone and the top of the Upper Silurian Salina Formation. The Salina Formation is a series of evaporates (including salt and anhydrite), shale and carbonate formations, which based on lithology should have low permeability and have characteristics of a good confining interval. Given the ductile nature of the salt and anhydrite, natural fractures tend not to propagate vertically up to and through the Salina Formation. Also, between the Medina (Grimsby) Sandstone and the Salina Formation are other potential confining intervals, including the Vernon and Rochester Shales and the Packer Shell (Irondequoit and Reynales Dolomites). Another shale interval, the Power Glen Shale (occasionally referred to as the Cabot Head Shale) lies between the Medina (Grimsby) Sandstone.

Conclusions

The Bittinger #2 (123-33944) appears to have a very porous Whirlpool Sandstone interval to allow for saltwater injection and storage. The formation was naturally completed and therefore, it is assumed to have sufficient natural (unstimulated) porosity and permeability development. The Bittinger #2 SWD site is located in an area of minimal tectonic influence (i.e. folding and faulting of the rock), other than the gentle dip of the formation to the southeast (refer to mapping included in the original report). Given the nature of the Salina Formation (i.e. bedded salts and anhydrites) above the SWD interval, minimal through-going, vertical fractures are expected to exist in the Bittinger #2 SWD site area.

BGC has not verified ownership of Lion's properties or completed a site visit as part of the geologic review of the area.

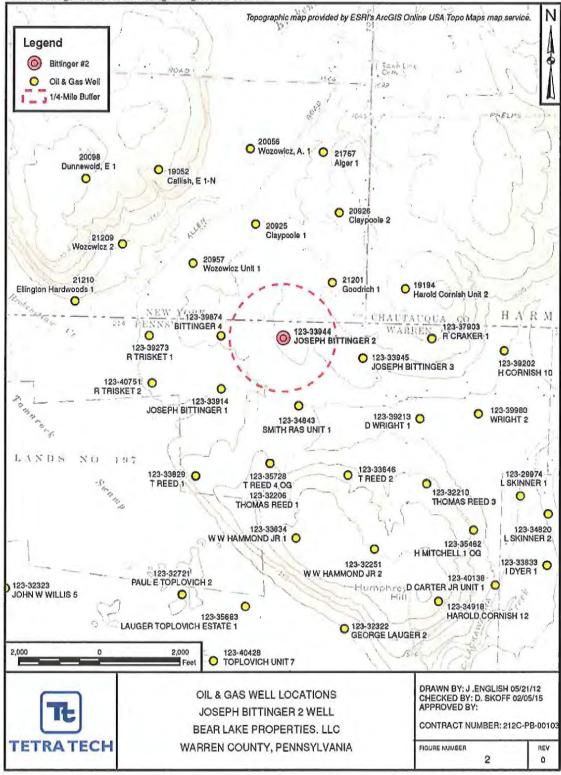
Respectfully submitted by:

Den a. Billow

Dan A. Billman, PG, CPG President, Billman Geologic Consultants, Inc.

DISCLAIMER

This document includes forward-looking statements as well as historical information. Forward-looking statements include, but are not limited to statements relating to geological and seismic data interpretations, prospect reserve estimates and prospect risk. Although BGC believes that its expectations reflected in these forward-looking statements are reasonable, such statements involve risks and uncertainties, and no assurance can be given that actual results will be consistent with these forward-looking statements. Investment in oli and gas exploration is high risk by its very nature. Important factors that could cause actual results to differ from these forward-looking statements include, but are not limited to: erroneous Interpretations of the seismic and geological data; the inability to acquire leases on identified prospects; mechanical problems while drilling and producing wells which prevent completion of a well or result in plugging of a well; dry holes; less reserves than originally estimated due to poor sand development or drainage by offsetting wells; non-commercial wells; and the variations in future gas pricing. BGC cannot and has not beyond normal due diligence care standards confirmed the accuracy and completeness of all the information we have reviewed in the course of this consulting engagement. Data for this review has been provided by Tetra Tech, NUS, Lion Energy, LLC or is publicly available and BGC, Inc. cannot be held responsible for errors in this provided data. Further, we express no opinion regarding any legal or securities issues. BGC shall assume no liability whatsoever for the use or reliance there upon by Tetra Tech, NUS, Lion Energy, LLC, their clients and/or their investors, of information, opinions and interpretation's provided by BGC. BGC reserves the right to adjust these findings and interpretations with the discovery of relevant data or future production data,

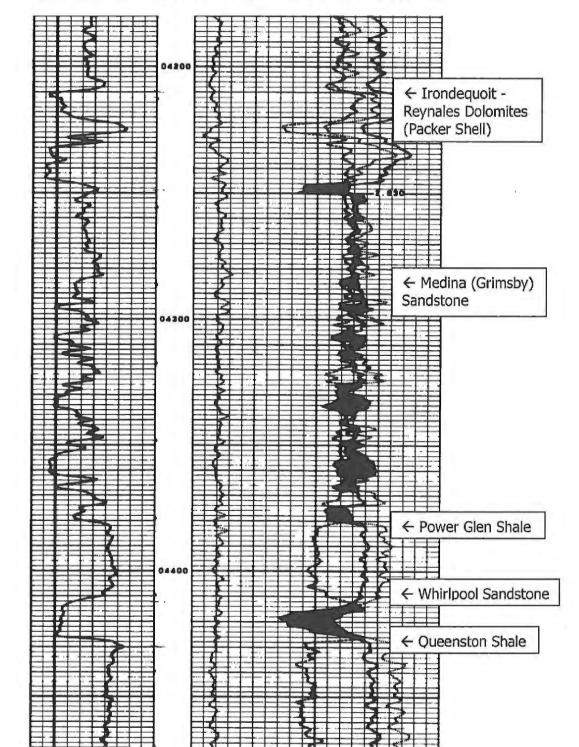


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Figure 1: Well location map of the Bittinger SWD Site. Well being permitted for SWD Bittinger #2 (123-33944) centered in map.

Appendix 1:

Log Data and Completion Reports for the Bittinger #2 (123-33944)



Gamma Ray, Density Neutron Log -- Bittinger #2 (123-33944)

Completion Report (page 1) -- Bittinger #2 (123-33944)

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Completion Report (page 2) -- Bittinger #2 (123-33944)

ER-02-4: 644, 2/30 (pg 2)

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APPROVED BY K. Walch

GEOPHYSICIST

TITLE

BILLMAN GEOLOGIC CONSULTANTS, INC.

TO:MR KARL KIMMICH, LION ENERGY COMPANY, LLCFROM:DAN A. BILLMAN, PG, CPG, BILLMAN GEOLOGIC CONSULTANTS, INC.SUBJECT:GEOLOGIC REVIEW OF THE BITTINGER AREA, PLANNED SWD SITEDATE:08/02/2010CC:CC:

Billman Geologic Consultants, Inc. (BGC) was requested by Lion Energy Company, LLC to review the geology of a planned salt water disposal (SWD) site in Columbus Township, Warren County, Pennsylvania. Specifically, the area is located in and around the Bittinger, Smith and Reed properties; collectively referred to as the "Bittinger SWD site". Figure 1 depicts the wellbase map of the Bittinger SWD site area. The wells being permitted include the 123-33914 (Bittinger #1) and the 123-39874 (Bittinger #4).

Both the Bittinger #1 and Bittinger #4 were initially drilled by U.S. Energy Development and later acquired by Lion Energy, when Lion Energy acquired the field from Belden and Blake, Corp. In both the Bittinger #1 and Bittinger #4, the perforated and hydraulically fracture treated interval includes both the Lower Silurian Medina Sandstone and Lower Silurian Whirlpool Sandstone. These formations have been produced, commingled, since 1983 and 1987, respectfully (refer to completion reports, Appendix 1).

Geologic Analysis of Data Associated with the Bittinger SWD Site

BGC completed an analysis of the logs in the Bittinger SWD site area and the porosity per foot data is included in Table 1. Within the Whirlpool Sandstone, the Bittinger #1 (123-33914) encountered 10' of sand greater or equal to 6% (log measured) porosity and 8' of sand greater or equal to 10% (log measured) porosity and 8' of sand greater or equal to 10% (log measured) porosity. Within the Medina Sandstone, the Bittinger #1 (123-33914) encountered 23' of sand greater or equal to 6% (log measured) porosity and 0' of sand greater or equal to 10% (log measured) porosity. Within the Whirlpool Sandstone, the Bittinger #4 (123-39874) encountered 11' of sand greater or equal to 6% (log measured) porosity and 7' of sand greater or equal to 10% (log measured) porosity. Within the Medina Sandstone, the Bittinger #4 (123-39874) encountered 38' of sand greater or equal to 6% (log measured) porosity.

The Whirlpool Sandstone across the producing Medina/Whirlpool trend is interpreted as a bar sand system and where it is present, it is often been a prolific hydrocarbon producer. Initial analysis of the Bittinger SWD site data indicates that the Whirlpool Sandstone is a consistently porous formation with a significant footage of porosity greater than 10% porosity. Gamma Ray, Density Neutron logs of the Medina/Whirlpool section of the Bittinger #1 and Bittinger #4 are included in Appendix 1. The Bittinger #1 has a peak, logged porosity of approximately 16% and the Bittinger #4 has a peak, logged porosity of approximately 18%. Cross-sections, oriented along regional strike (southwest – northeast) and regional dip (northwest – southeast) were constructed across the Bittinger SWD site and are included as an attachment to this report. The consistency of thickness and porosity of the Whirlpool Sandstone is evident in the cross-sections (Appendix 2).

The Medina Sandstone is interpreted as a braided channel system and therefore porous, reservoir quality Medina Sandstone typically is a very discontinuous across even short distances. As expected, within the logs of the Bittinger #1 and Bittinger #4 (Appendix 1) the Medina Sandstone is a series of interbedded sandstones, silts and shales and has a discontinuous nature from well to well. In the Bittinger #1 and Bittinger #4, porosities average 8% and lower, from sand body to sand body within the Medina interval in each well.

Both the Whirlpool and Medina Sandstones were mapped using footage at 8% porosity or greater cut-off. These maps are included, with this report, as Appendix 2.

Figure 2 depicts the structure on top of the Packer Shell (dolomites above the Medina Formation) in the Bittinger SWD site area. The structural mapping shows a very consistently dipping formation from the northeast to the southwest across the Bittinger SWD site. No obvious faulting or "deviations" from regional dip are evident on the structural top of the Packer Shell dolomites. Figure 3 depicts the structure on top of the Queenston Shale (Base of the Whirlpool Sandstone) in the Bittinger SWD site area. The structural mapping shows a very consistently dipping formation from the northeast to the southwest across the Bittinger SWD site. No obvious faulting or "deviations" from regional dip are evident on the structural top of the Queenston Shale. Both formations appear to show a fairly tectonically inactive situation exists in the Medina/Whirlpool interval at the Bittinger SWD site.

Approximately 850' above the top of the Medina Sandstone is the top of the Upper Silurian Salina Formation, a series of evaporates (including salt and anhydrite), shale and carbonate formations. The top of the Salina Salt (the evaporites within the Salina Formation) occurs approximately 650' above the top of the Medina Sandstone. Given the ductile nature of the salt and anhydrite, natural fractures tend not to propagate vertically up to and through the Salina Formation.

Conclusions

The Bittinger #1 and Bittinger #4 appear to have a very porous Whirlpool Sandstone interval to allow for saltwater injection and storage and was previously hydraulic fractured, allowing for increased permeability. The Bittinger SWD site is located in an area of minimal tectonic influence (i.e. folding and faulting of the rock), other than the gentle dip of the formation to the southeast (mapping included in Appendix 2). Given the nature of the Salina Formation above the SWD interval, minimal through-going, vertical fractures are expected to exist in the Bittinger SWD site area.

As a disclaimer, BGC has not had access to seismic data in and around the Bittinger SWD site and any observations or conclusions made are not made with the knowledge of seismic data. BGC has not verified ownership of Lion's properties or completed a site visit as part of the geologic review of the area.

Respectfully submitted by:

Dan a. pillaren

Dan A. Billman, PG, CPG President, Billman Geologic Consultants, Inc.

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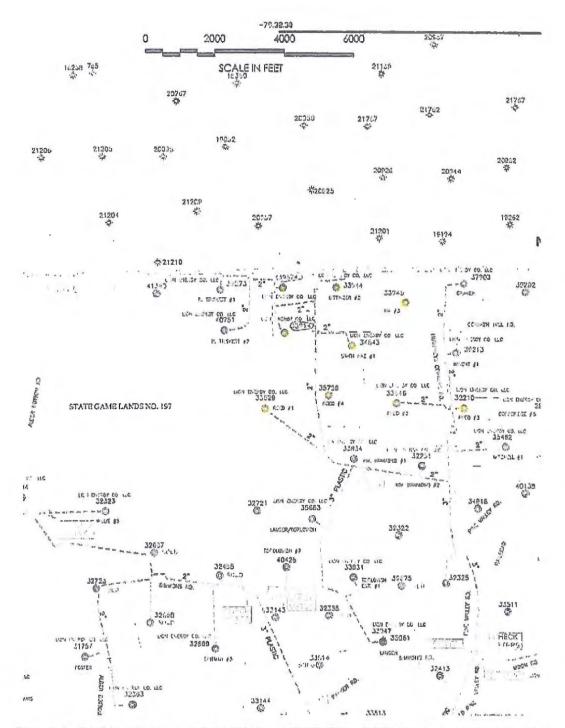


Figure 1: Well location map of the Bittinger SWD Site. Wells being permitted for SWD include the 123-33914 (Bittinger #1) and the 123-39874 (Bittinger #4).

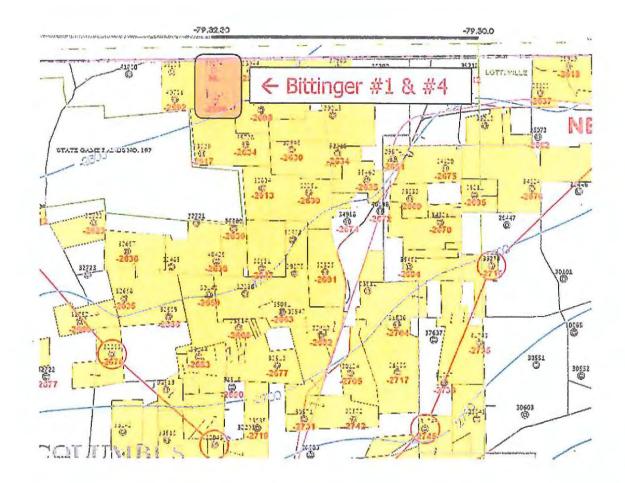


Figure 2: Map of the structure on top of the Packer Shell (above the Medina Sandstone). Structure on top of the Packer Shell is very consistently dipping to the southeast. The 123-33914 (Bittinger #1) and the 123-39874 (Bittinger #4) highlighted in orange.

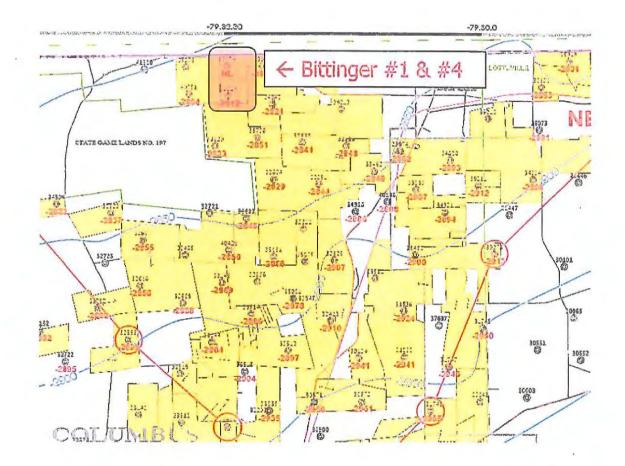


Figure 3: Map of the structure on top of the Queenston Shale (base of the Whirlpool Sandstone). Structure on top of the Queenston Shale is very consistently dipping to the southeast. The 123-33914 (Bittinger #1) and the 123-39874 (Bittinger #4) highlighted in orange.

API#	Whirlpool 6%	Whirlpool 8%	Whirlpool 10%	Medina 6%	Medina 8%	Medina 10%
123-33914	10	9	8	23	9	0
123-33944	12	10	9	38	7	0
123-33945	13	11	8	54	9	0
123-39874	11	10	7	38	6	0
123-34843	12	10	7	25	2	0
123-33829	11	9	8	42	7	0
123-35728	14	12	11	57	33	10
123-33646	8	5	3	47	10	1
123-32210	9	7	4	29	3	0

Table 1

Average: 11.1

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Average: 39.2

Appendix 1:

Log Data and Completion Reports for the Wells Being Permitted as Salt Water Disposal Wells

Gamma Ray, Density Neutron Log -- Bittinger #1 (123-33914)

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Completion Report (page 1) -- Bittinger #1 (123-33914)

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Completion Report (page 2) -- Bittinger #1 (123-33514)

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Unconsolidated Gravel	۵'	371			Fresh. @ 254	Drillar's record and geophysical
Devonian Shalo.	37 '	2679'				logs
"Tully" Le	2679'	2785"				
Hamilton Shales	2705'	2955'				
Onondaga	29551	31291				
Unconformity Interval	3129'	3145'				
Akron-Bertic	3145'	3220'			Salt @ 3935'	
Camillus .	3220'	32 98 '				
Syracuse	3298'	3525'				
Verhen Salt Zone	3525 3504	37841	44301		C.	
Lockport	3784	40091	4930.2	1	ana an an t	
Rochester	40091	4113'				}
Irondequoit-Reynales	4113'	4150'				· ·
Grimsby	4150'	42651		•		
Power Glan	4265'	4316'				
Whirlpool	4316'	4331,				
Queenston	4331'	тD		•		
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1984 <u>June</u> PATE Drugfin K Walch APPROVED BY Geophysicist THILE

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Gamma Ray, Density Neutron Log -- Bittinger #4 (123-39874)

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Completion Report (page 1) - Bittinger #4 (123-39874)

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11240'	W 79° 30'	004	W	ELL RECORD		6	10 17.70	274
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PEAM	T NO 17-123	-39074-00	PROJECT	NO DOS	1	TYPE OF W	BLL G	as
	DLumbu	S FIELD,	DEWE	Y CORN	ERS PO		DEU	
WELL OF	ERATOR Boergy Deve	alopment Corpor	ation		(7	TELEPHONE NO 16)856-9764		
ADDRESS	1	ra, Buffalo, NY		9990			21	P
FARM NA					FARM NO	SERIAL NO		ACRES
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DRILLIN	abus B COMMENCED		DRILLIN	D COMPLETED			_	
ELEVAT	3/33/87		QUADRA	NGIE	. 8/15			
DESTAT	J561'		Colum			DB 7%*	0	5'
222				AND TUBING				
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13 3/8'	30'	NA						8/11/87
8 5/8	506'	220		5	1			
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4 1/2"	1754.9'	265						11/5/87
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A WELL RECORD SHALL BE FILED WITHIN 30 DAYS OF CESSATION OF DRILLIND. IF THE WELL NE NOT COMPLETED WITHIN 30 DAYS OF CESSATION OF DRILLING, AN UPDATED WELL RECORD HUST BE SUBNITTED HODE COMPLETION OF THE WELL.

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Completion Report (page 2) -- Bidlinger #4 (123-39874)

ER-OG-41 Rav. 10/82 (pp 2)

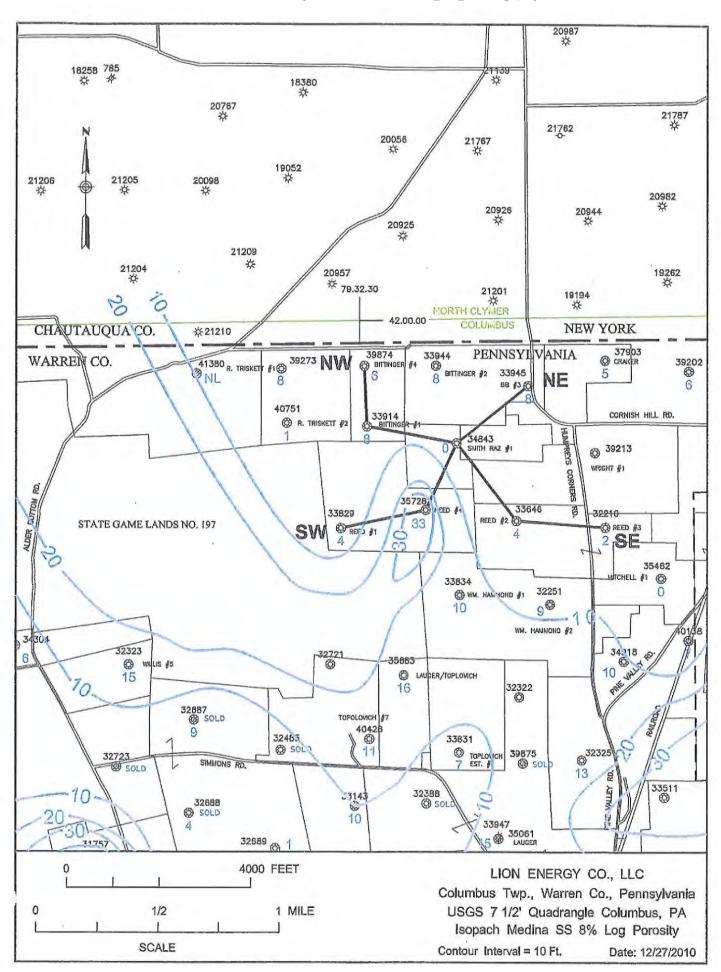
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		FORM	ATIONS		27-578/7	
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Unconsolidated Grave	0	18'				Driller's Record & Geophysical Logs
Devonian Shale	18'	2741'.				
Tully Limestone	2741	2040'	{		ļ	
Hamilton Shale	2848	3018'	ł			1
Onondaga Limestone	30181	3182'	Í	1		
Bois Blanc	31821	32111				
Akron Dol	32111	32921	!		1	
Camillus	3292'	3366'				
Syraouse	3366'	3547'				1
Salt	35471	3896'		1		
Lockport Dol	3896'	4067'			Salt water	
Rochester Shale	4067	4151'	l]	}
Parker Shell	41514	4189'	ſ		1	
Grimsby Sandstone	4189	4304'	Qas		i i	
Power Glen Shaia	4304	4350'				
Whirlpool Sandstone	43501	4367'	Gas	1		Î
Queenston Shale	4367'	4496'				
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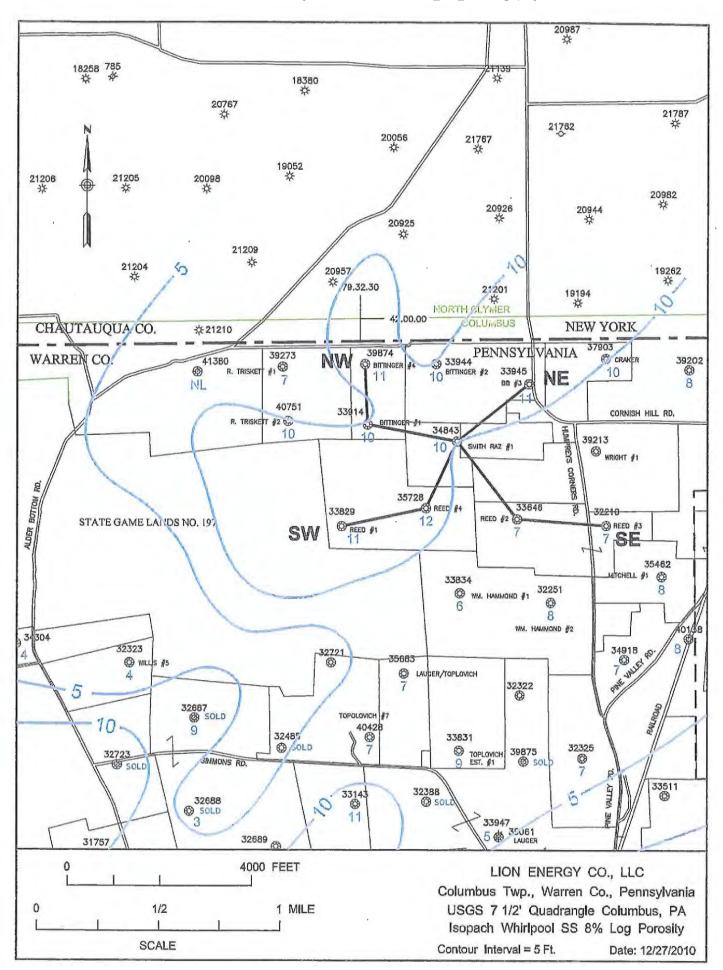
Appendix 2:

Cross-sections, Isopach and Structural Mapping Bittinger SWD Site

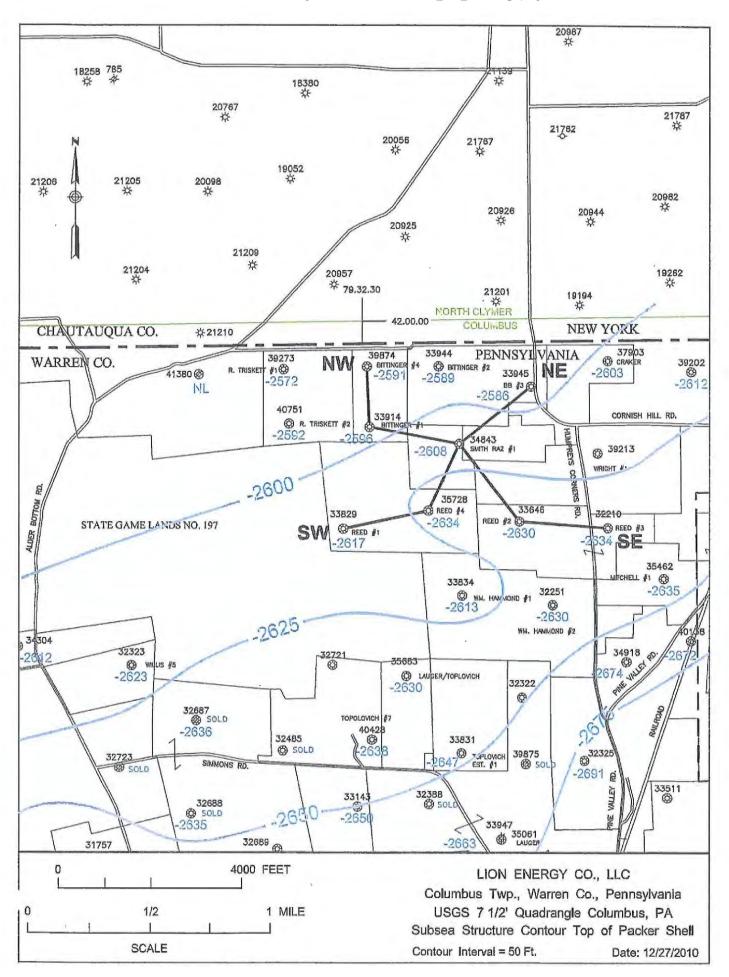
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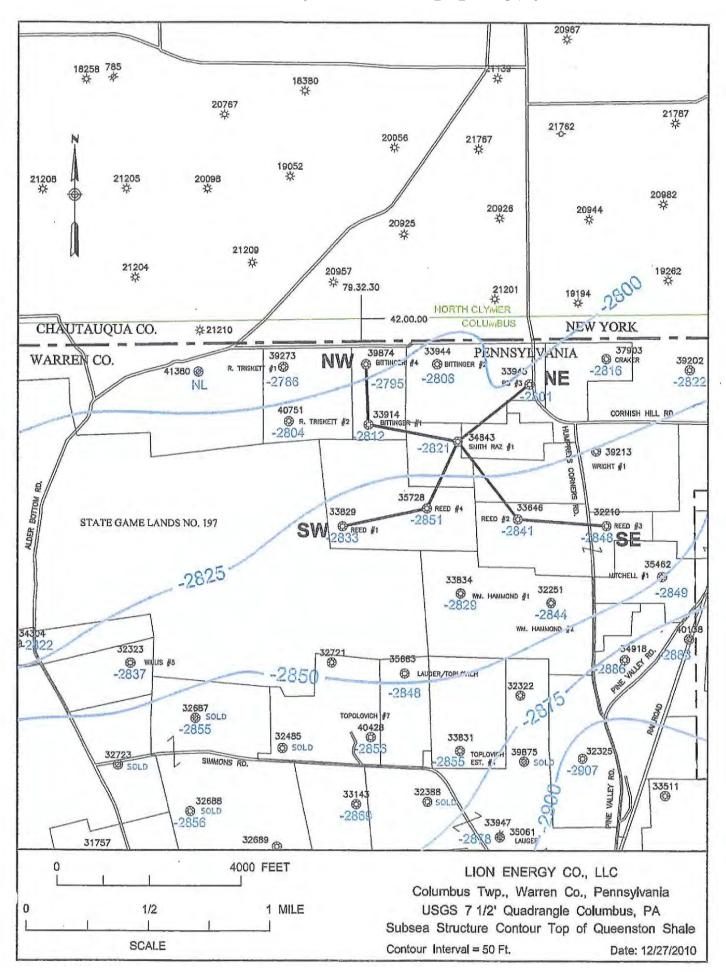
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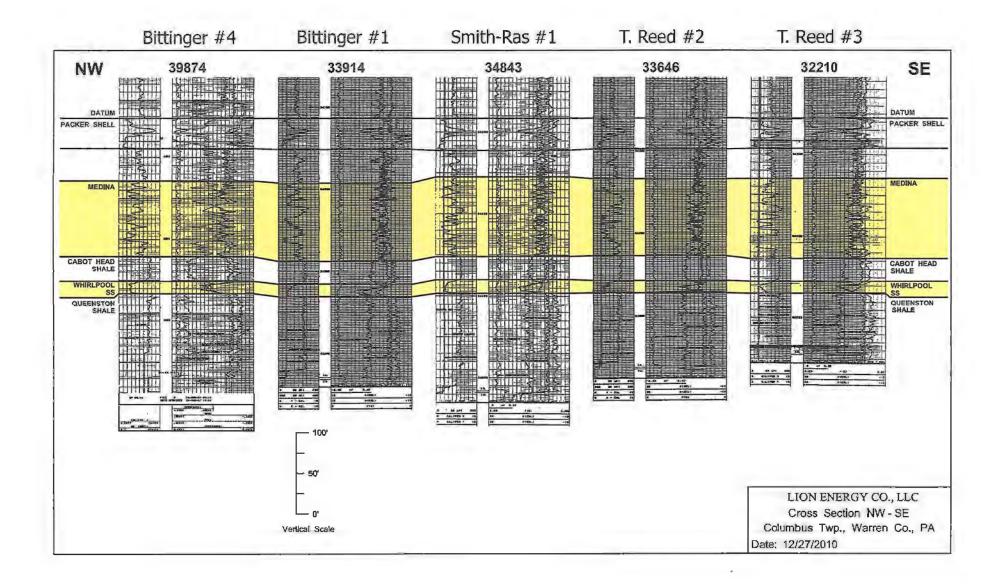


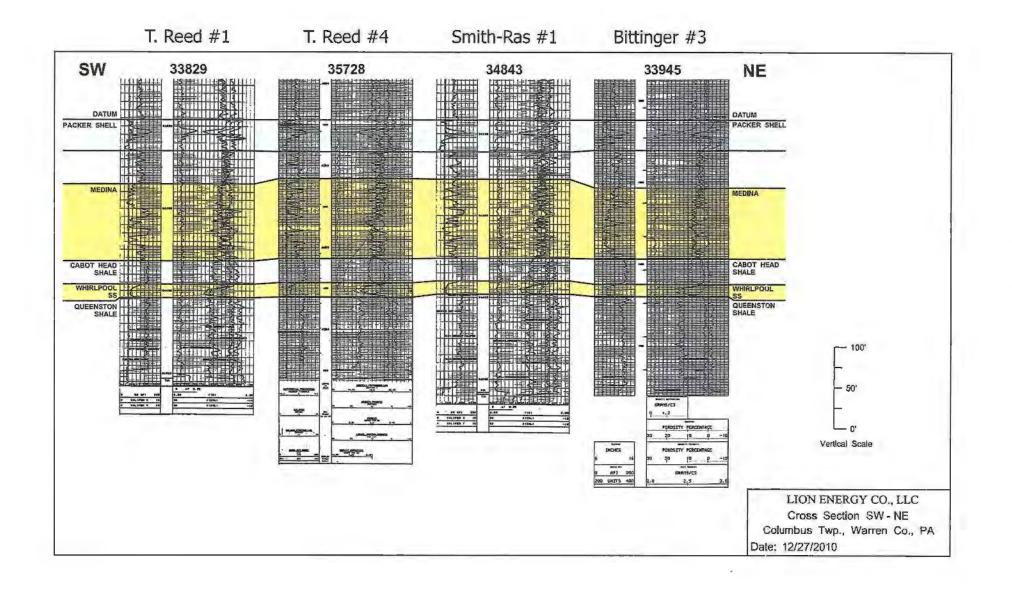
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GEOLOGIC DATA

BITTINGER #3 COMPLETION RECORD

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ADDRESS		U.S. Energy Deve	elopment Corporation	1	ELLPHONE NO	716-856-9	
FARMINA		670 Statler Buil	ding, Buffalo, N	EW YURK	SEALAL NO	_ Z(14202
TUANSIO		Bittinger	COUNTY	#3	1		160
CRILLING	CO IMENCED	Columbus	WATTER DRILLING COVPLETED				
ELEVATIO		10/16/84	10/19/84				
		1638' GL	Columbus		[X] 7½*	[] 1	5'
			CASING AND TUBING	PACION PAC	KFR		D4-E
IZE	AHOUNT IN	CEMENT (SKS)	GEL (SKS)	TYPE	SIZE	DEATH	DATE RUN
3 3/8"	381						10/16/84
8 5/8"	405*	200					10/17/34
4 1/2"	450 8'	225	-				10/20/94
		T.D. D.	D. D .P.I. (lass O G	Lease		
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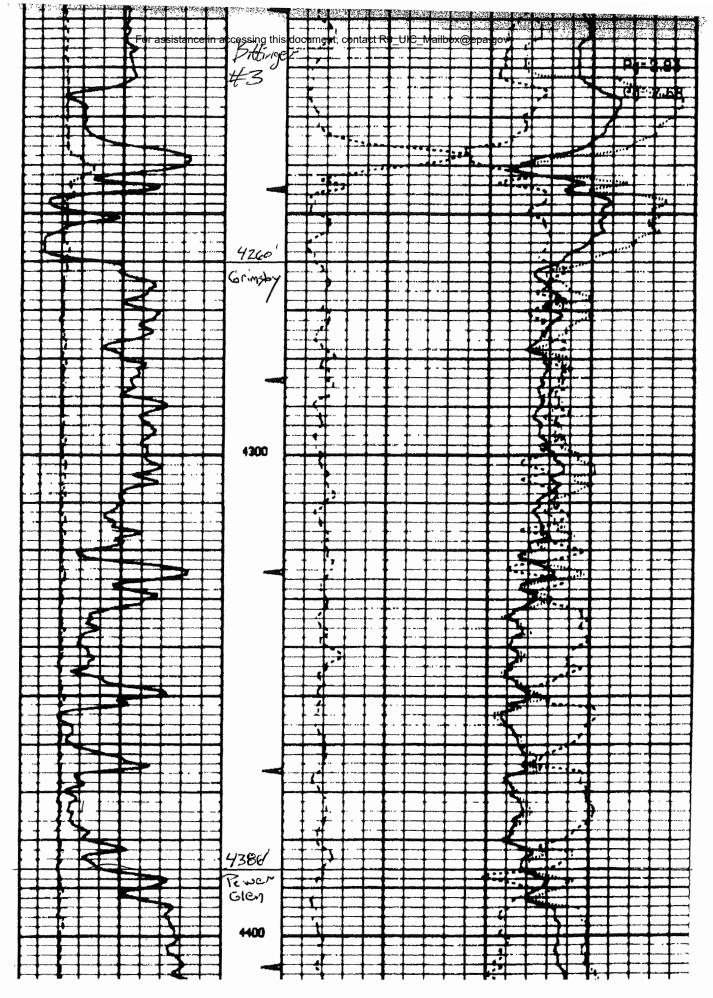
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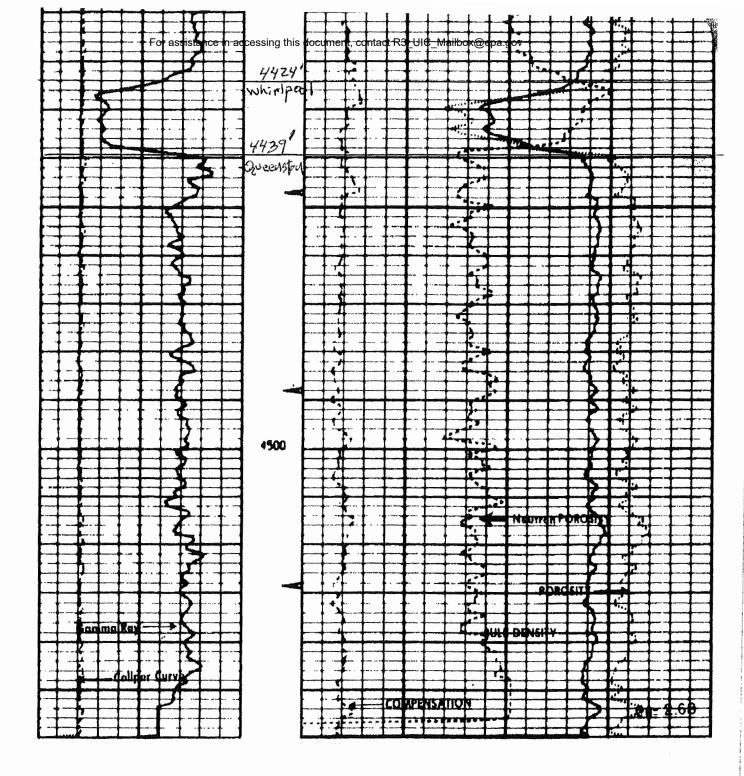
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NAME nconsolidated Gravel evonian Shales Tully" LS inition Shale hondaga nconformity Interval kron-Bertia amillus yracuse	то+ 0' 30' 2816' 2926' 3097' 3256' 3285' 3285' 3370' 3442'	воттом 30 * 2816 * 2926 * 3097 * 3256 * 3285 * 3370 * 3442 *	GAS AT	01L AT	WATER AT (FRESH OR SALT WATER) Fresh at 60'	SQUACE OF DAT Driller's records and geophysical logs
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evonian Shales [ully" LS amilton Shale noondaga noonformity Interval kron-Bertie amillus	30' 2816' 2926' 3097' 3256' 3285' 3285'	2816' 2926' 3097' 3256' 3285' 3370'				records and geophysical
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Page 14 of 2



Bensity Correction

PRAMP /PA

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GEOLOGIC DATA

MAXIMUM INJECTION PRESSURE CALCULATIONS

Maximum Injection Pressure (MIP) Calculations for Bear Lake Properties Bittinger #3 Well Warren County, PA

1) Frac Gradient (FG) Based on Nearby Smith- Ras #1 Well

FG = [ISIP + (.433 X SG X D)] /D Where: ISIP = 2200 psi SG = 1.0 (frac fluid) D = 4391

					Fracture
		Hydrostatic			Gradient
Well	ISIP (psi)	Factor (psi/ft)	SG	D (ft)	(psi/ft)
Smith/Ras #1	2200	0.433	1	4391	0.934

2) Maximum Injection Pressure (MIP) Calculation for Bittinger #3 Well Using FG from Smith-Ras #1 Frac

MIP = [FG - (.433XSG)] X D FG = 0.934 SG = 1.218 (brine)

Depth:

Medina Top 4260

					Fracture	
		Hydrostatic			Gradient	MIP
		Factor (psi/ft)	SG	D (ft)	(p s i/ft)	(Surface)
Bittinger #3	-	0.433	1.218	4260	0.934	1732

GEOLOGIC DATA

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SMITH - RAS #1 WELL DATA

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·	11.64	<u>,</u> , .	RTMENT OF ENVIRONMENT IVISION OF DIL AND GAS RE PITTSBURGH, PENNSYLVAN	GULATION	A . F	Office	Use Only
	<i>n</i>			:	· · · · · · · · · · · ·		
	- 900641 ⁴ - 917	1922 (315) 	WELL RECOR	D	·		· ··
RERM	TINO. WAR	34843	PROJECT NO.	· · · · · · · ·	TYPE OF W	ELC Gas	•
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WELL O	ERATOR		oment Corporation	1997 - 19	FELEPHONE NO.	(716)856-	9764
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FARM N	AMESSO	1. 1.11		FARM NO.	SERIAL NO.	· · · · ·	AORES
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DRILLIN	COMMENCED		WATTEN DRILLING COMPLETED	· · · · · · · · · · · · · · · · · · ·			
	5/21 DN	784	3/26/84				
	1575		Columbus		.1.		(b)
·			CASING AND TUBING				
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5/27/84 TURS ATURAL O	PEN FLOW MATTINENT OPEN FLOW	Standen Anutin II. stirt partin II. rushi	NATURAL ROCK PRESSU	Not Tak	I,	СЧ) (ТМ) - Н 2.5	HRS
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5/27/84 TURS ATURAL D	PEN FLOW MINING PEN FLOW N/AT ATMENT OPEN FL 5, 20 Dri J	анал'я П. ал. анал'я П. ал. ряг'я П. т. ал ряг'я П. т. ал сом ря ММСЕ	NATURAL ROCK PRESSU AFTEH TREATMENT ROC	Not Tak x pressure 1240_PS	I,	60 (DM 18 3)	HRS A
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5/27/84 TURS ATURAL O	PEN FLOW MINING PEN FLOW N/AT ATMENT OPEN FL 5, 20 Dri J	анон''н П., аб ряг''н П., аб ряг''н П., т. М. ряг''н П., т. М. сом 28 ММСЕ Ller's TD, 4525 '	NATURAL ROCK PRESSU AFTEH TREATMENT ROC	Not Tak x pressure 1240_PS	I;(FO (24));	01) (TN) -R 3.	DAY HRS 243
5/27/84 TURS ATURAL O	PEN FLOW MINING PEN FLOW N/AT ATMENT OPEN FL 5, 20 Dri J	анон''н П., аб ряг''н П., аб ряг''н П., т. М. ряг''н П., т. М. сом 28 ММСЕ Ller's TD, 4525 '	NATURAL ROCK PRESSU AFTEH TREATMENT ROC	Not Tak x pressure 1240_PS	I;(FO (24));		DAY HRS 243
ATURAL O	PEN FLOW MINING PEN FLOW N/AT ATMENT OPEN FL 5, 20 Dri J	анон''н П., аб ряг''н П., аб ряг''н П., т. М. ряг''н П., т. М. сом 28 ММСЕ Ller's TD, 4525 '	NATURAL ROCK PRESSU AFTEH TREATMENT ROC	Not Tak x pressure 1240_PS	I;(FO (24));		DAY HRS 243

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ER-OG-4: Rev. 2/80 (pg 2)

OIL AT	WATER AT (FRESH OR SALT WATER) Fresh @ 105'	SOURCE OF Drillers records a geophysic logs
	Fresh @ 105'	records a geophysic
		geophysic
		1095
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	Salt @ 3910'	
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K. Wilco APPROVED BY

, 19.84

Douglas K. Walch, Geophysicist

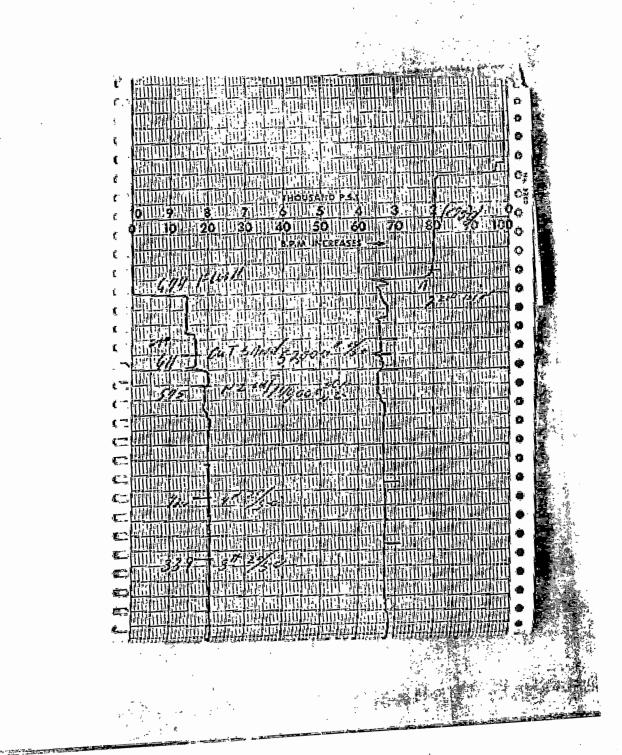
For assistance in accessing this document, contact R3 UIC Mailbox@epa.gov

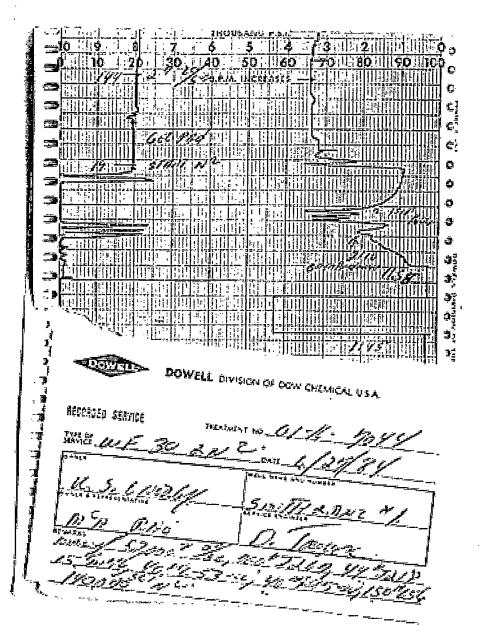
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Well Name & No. _____SHITU/RAS #1____ Loc. Co++ 100 In PA WARPTN TWP+: ____ 601,09805 Parmit No. PERFORATION RECORD Formation Moding Whisison Date 6/24/24 Cospany 31. ReCallough Pumped in 500 gel. acid and 500 gal. water, ran Garma Ray and collar log. PHTD LART It. Perf. as follows: shots w/_ shot: -4279 4316 ¥/ shots w/ ... <u>________</u> នាលាំដ 4318 w/_ -305 shots _₩*[*___ 4391 shols -----¥/ ------<u>4104</u> 4334. 1600 Total Shots 10 Size of shots _____ FRAC JOB Date 6/27/84 Company Develi Schlemberger Loaded hole. Broke formation @ 2100_# Back to _950 _#. Pumped in _500_gals. 152 KCL _ Acid Ø _20 _ BPN Ø _3300 Å, waited 5 min. A fraced as follows: SAND BFM Press. f Per Size BBLS./GEL. Čal. 3500 1. (-144 <u>975</u> ወልኩ 335D 21 2ϵ 20/502. 144-339 21 3250 20/50 38 з. <u>.936-420</u> 20/5020 3500 4. £₿ 470-411 14.5 <u>35(in)</u> 5. 613=675 <u>Flush</u> ---б. 7. 8. 9. 10. 11+ 12. F 13. ηų, 15. 16. 17, ٦Ė. 19, ŽŎ, ISIP 2200 5 MIN. 1950 # Job complete 12:36 P.6 Open to pit 1:26 P.M. Flowed back 24 hrs. Total water 675 bbls. 52,000 # 20/66 A ---- # 80/100. Avg. pump rate _21 BF4 0 _3369 # Press HHP used <u>1734</u>. Nitrogen used <u>140,000</u> REMARKS: At 340 BBLS cut N. Cov 10 high pressure - at 611 H345 cut sand due to high preasure - well servered off = 4 BBLS short of fluish to perfs. <u>///+1/14c/lec</u> EXECTIONER 7-6-84

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GEOLOGIC DATA

MEDINA GAS PRODUCTION SUMMARY

For assistance in accessing this document, contact R3_UIC_Mailbox@epa.gov

				-								
Permit Company	Year 1984	Product GAS	Quantity (MCF)	Brine		County	Municipality		Farm_Well_No	Field	Pool	Completion Date
123-33944 US ENERGY DEV CORP		(m. 14)	5,812		0	WARREN	COLUMBUS	JOSEPH BITTINGER	2		DEWEY CORNERS	29-Jan-84
123-33944 US ENERGY DEV CORP	1985	GAS	22,275		0	WARREN	COLUMBUS	JOSEPH BITTINGER	2		DEWEY CORNERS	29-Jan-84
123-33944 US ENERGY DEV CORP	1986	GAS	30,101		336	WARREN	COLUMBUS	JOSEPH BITTINGER	2		DEWEY CORNERS	29-Jan-84
123-33944 US ENERGY DEV CORP	1987	GAS	23,479		336	WARREN	COLUMBUS	JOSEPH BITTINGER	2		DEWEY CORNERS	29-Jan-84
123-33944 US ENERGY DEV CORP	1988	GAS	47,976		347	WARREN	COLUMBUS	JOSEPH BITTINGER	2		DEWEY CORNERS	29-Jan-84
123-33944 US ENERGY DEV CORP	1989	GAS	50,332		352	WARREN	COLUMBUS	JOSEPH BITTINGER	2		DEWEY CORNERS	29-Jan-84
123-33944 US ENERGY DEV CORP	1990	GAS	39,609		346		COLUMBUS	JOSEPH BITTINGER	2		DEWEY CORNERS	29-Jan-84
123-33944 US ENERGY DEV CORP	1991	GAS	21,121		347	WARREN	COLUMBUS	JOSEPH BITTINGER	2		DEWEY CORNERS	29-Jan-84
123-33944 US ENERGY DEV CORP	1992	GAS	6,351		323	WARREN	COLUMBUS	JOSEPH BITTINGER	2		DEWEY CORNERS	29-Jan-84
123-33944 US ENERGY DEV CORP	1993	GAS	3,039		339	WARREN	COLUMBUS	JOSEPH BITTINGER	2		DEWEY CORNERS	29-Jan-84
123-33944 US ENERGY DEV CORP	1994	BRINE		22.				JOSEPH BITTINGER	2		DEWEY CORNERS	29-Jan-84
123-33944 US ENERGY DEV CORP	1994	GAS	1,402		319	WARREN	COLUMBUS	JOSEPH BITTINGER	2		DEWEY CORNERS	29-Jan-84
123-33944 BELDEN & BLAKE CORP	2000	GAS	698		366	WARREN	COLUMBUS	JOSEPH BITTINGER	2		DEWEY CORNERS	29-Jan-84
123-33944 BELDEN & BLAKE CORP	2001	GAS	67		365	WARREN	COLUMBUS	JOSEPH BITTINGER	2		DEWEY CORNERS	29-Jan-84
123-33944 BELDEN & BLAKE CORP	2002	GAS	0		0	WARREN		JOSEPH BITTINGER	2		DEWEY CORNERS	29-Jan-84
123-33944 BELDEN & BLAKE CORP	2002	OIL	0		0			JOSEPH BITTINGER	2		DEWEY CORNERS	29-Jan-84
123-33944 RANGE RESOURCES APPALAC	and a complete second	GAS	5		31	WARREN	COLUMBUS	JOSEPH BITTINGER	2	COLUMBUS	DEWEY CORNERS	29-Jan-84
123-33944 RANGE RESOURCES APPALAC	HIA LLC 2003	GAS	701		334	WARREN	COLUMBUS	JOSEPH BITTINGER	2	COLUMBUS	DEWEY CORNERS	29-Jan-84
123-33944 RANGE RESOURCES APPALACI	HIA LLC 2004	GAS	718		365	WARREN	COLUMBUS	JOSEPH BITTINGER	2	COLUMBUS	DEWEY CORNERS	29-Jan-84
123-33944 RANGE RESOURCES APPALAC	HIA LLC 2005	GAS	670		334	WARREN	COLUMBUS	JOSEPH BITTINGER	2	COLUMBUS	DEWEY CORNERS	29-Jan-84
123-33944 RANGE RESOURCES APPALAC	HIA LLC 2006	GAS	374		334	WARREN	COLUMBUS	JOSEPH BITTINGER	2	COLUMBUS	DEWEY CORNERS	29-Jan-84
123-33944 TRINITY ENERGY CORP	2007	GAS	102		122	WARREN	COLUMBUS	JOSEPH BITTINGER	2	COLUMBUS	DEWEY CORNERS	29-Jan-84
123-33944 LION ENERGY CO LLC	2008	GAS	193		365	WARREN	COLUMBUS	JOSEPH BITTINGER	2	COLUMBUS	DEWEY CORNERS	29-Jan-84
123-33944 LION ENERGY CO LLC	2009	GAS	30		30	WARREN	COLUMBUS	JOSEPH BITTINGER	2	COLUMBUS	DEWEY CORNERS	29-Jan-84
		Total	255,055	22								
Permit Company	Year	Product	Quantity		Days	County	Municipality	Farm Name	Farm Well No	Field	Pool	Completion Date
123-33945 US ENERGY DEV CORP	1986	GAS	32,248		336	WARREN	COLUMBUS	JOSEPH BITTINGER	3	COLUMBUS	DEWEY CORNERS	19-Oct-84
123-33945 US ENERGY DEV CORP	1987	GAS	36,330		336	WARREN	COLUMBUS	JOSEPH BITTINGER	3		DEWEY CORNERS	19-Oct-84
123-33945 US ENERGY DEV CORP	1988	GAS	48,995		345	WARREN	COLUMBUS	JOSEPH BITTINGER	3		DEWEY CORNERS	19-Oct-84
123-33945 US ENERGY DEV CORP	1989	GAS	42,806		332	WARREN	COLUMBUS	JOSEPH BITTINGER	3		DEWEY CORNERS	19-Oct-84
123-33945 US ENERGY DEV CORP	1990	GAS	26,642		343	WARREN	COLUMBUS	JOSEPH BITTINGER	3		DEWEY CORNERS	19-Oct-84
123-33945 US ENERGY DEV CORP	1991	GAS	13,848		347	WARREN	COLUMBUS	JOSEPH BITTINGER	3		DEWEY CORNERS	19-Oct-84
123-33945 US ENERGY DEV CORP	1992	GAS	5.278		315	WARREN	COLUMBUS	JOSEPH BITTINGER	3	COLUMBUS	DEWEY CORNERS	19-Oct-84
123-33945 US ENERGY DEV CORP	1993	GAS	4,826		360	WARREN	COLUMBUS	JOSEPH BITTINGER	3		DEWEY CORNERS	19-Oct-84
123-33945 US ENERGY DEV CORP	1994	BRINE	,	73		WARREN		JOSEPH BITTINGER	3		DEWEY CORNERS	19-Oct-84
123-33945 US ENERGY DEV CORP	1994	GAS	1,B10		363	WARREN	COLUMBUS	JOSEPH BITTINGER	3		DEWEY CORNERS	19-Oct-84
123-33945 BELDEN & BLAKE CORP	2001	GAS	66		365	WARREN	COLUMBUS	JOSEPH BITTINGER	3		DEWEY CORNERS	19-Oct-84
123-33945 BELDEN & BLAKE CORP	2001	GAS	40		365	WARREN	COLUMBUS	JOSEPH BITTINGER	3		DEWEY CORNERS	19-Oct-84
123-33945 BELDEN & BLAKE CORP	2002	OIL	40		0	WARREN	COLUMBUS	JOSEPH BITTINGER	3		DEWEY CORNERS	19-Oct-84
123-33945 BELDEN & BLAKE CORP	2002	GAS	0		0	WARREN	COLUMBUS	JOSEPH BITTINGER	3		DEWEY CORNERS	19-Oct-84
123-33945 BELDEN & BLAKE CORP	2005	OIL	0		0	WARREN	COLUMBUS	JOSEPH BITTINGER	3		DEWEY CORNERS	19-Oct-84
123-33945 BELDEN & BLAKE CORP	2005	GAS	0		0	WARREN	COLUMBUS	JOSEPH BITTINGER	3	the second second second	DEWEY CORNERS	19-Oct-84
123-33945 BELDEN & BLAKE CORP	2006	OIL	0		0	WARREN	COLUMBUS	JOSEPH BITTINGER	3		DEWEY CORNERS	19-Oct-84
	2008	GAS	0		0			JOSEPH BITTINGER	3			
123-33945 BELDEN & BLAKE CORP		GAS	0		0	WARREN			-		DEWEY CORNERS	19-Oct-84
123-33945 BELDEN & BLAKE CORP	2008	Total	212,890	73	U	WARREN	COLUMBUS	JOSEPH BITTINGER	3	COLOIVIBUS	DEWEY CORNERS	19-Oct-84
Descrit Company		0	0		0	C	Read To Prov	-		Ph-1-1	Baral	Concellation Theorem
Permit Company	Year		Quantity		Days	County	Municipality	Farm_Name	Farm_Well_No	Field	Pool	Completion Date
123-39273 US ENERGY DEV CORP	1985	GAS	23,500		0	WARKEN	COLUMBUS	R TRISKET	1	COLUMBUS	DEWEY CORNERS	14-Dec-84

123-39273	US ENERGY DEV CORP	1986	GAS	29,581		308	WARREN	COLUMBUS	R TRISKET	1	COLUMBUS	DEWEY CORNERS	14-Dec-84
123-39273	US ENERGY DEV CORP	1987	GAS	26,012		322	WARREN	COLUMBUS	R TRISKET	1	COLUMBUS	DEWEY CORNERS	14-Dec-84
123-39273	US ENERGY DEV CORP	1988	GAS	34,866		307	WARREN	COLUMBUS	R TRISKET	1	COLUMBUS	DEWEY CORNERS	14-Dec-84
123-39273	US ENERGY DEV CORP	1989	GAS	60,104		352	WARREN	COLUMBUS	R TRISKET	1	COLUMBUS	DEWEY CORNERS	14-Dec-84
123-39273	US ENERGY DEV CORP	1990	GAS	29,211		335	WARREN	COLUMBUS	R TRISKET	1	COLUMBUS	DEWEY CORNERS	14-Dec-84
123-39273	US ENERGY DEV CORP	1991	GAS	6,338		293	WARREN	COLUMBUS	R TRISKET	1	COLUMBUS	DEWEY CORNERS	14-Dec-84
123-39273	US ENERGY DEV CORP	1992	GAS	3,309		321	WARREN	COLUMBUS	R TRISKET	1	COLUMBUS	DEWEY CORNERS	14-Dec-84
123-39273	US ENERGY DEV CORP	1993	GAS	1,474		165	WARREN	COLUMBUS	R TRISKET	1	COLUMBUS	DEWEY CORNERS	14-Dec-84
123-39273	US ENERGY DEV CORP	2000	GAS	519		240	WARREN	COLUMBUS	R TRISKET	1	COLUMBUS	DEWEY CORNERS	14-Dec-84
123-39273	US ENERGY DEV CORP	2001	GAS	1,165		365	WARREN	COLUMBUS	R TRISKET	1	COLUMBUS	DEWEY CORNERS	14-Dec-84
123-39273	BELDEN & BLAKE CORP	2001	GAS	15		365	WARREN	COLUMBUS	R TRISKET	1	COLUMBUS	DEWEY CORNERS	14-Dec-84
	US ENERGY DEV CORP	2002	GAS	684		365	WARREN	COLUMBUŞ	R TRISKET	1	COLUMBUS	DEWEY CORNERS	14-Dec-84
	US ENERGY DEV CORP	2003	GAS	527		365	WARREN	COLUMBUS	R TRISKET	1	COLUMBUS	DEWEY CORNERS	14-Dec-84
	US ENERGY DEV CORP	2004	GAS	1,073		365	WARREN	COLUMBUS	R TRISKET	1	COLUMBUS	DEWEY CORNERS	14-Dec-84
	US ENERGY DEV CORP	2005	GAS	1,485		365		COLUMBUS	R TRISKET	1		DEWEY CORNERS	14-Dec-84
	US ENERGY DEV CORP	2006	BRINE	.,	5				R TRISKET	1	COLUMBUS	DEWEY CORNERS	14-Dec-84
	US ENERGY DEV CORP	2006	GAS	1,068		365			RTRISKET	1		DEWEY CORNERS	14-Dec-84
	US ENERGY DEV CORP	2007	BRINE	_,	5		WARREN	COLUMBUS	R TRISKET	1		DEWEY CORNERS	14-Dec-84
	US ENERGY DEV CORP	2007	GAS	398	-	240			R TRISKET	1		DEWEY CORNERS	14-Dec-84
	LION ENERGY CO LLC	2008	GAS	201		365	WARREN	COLUMBUS	R TRISKET	1		DEWEY CORNERS	14-Dec-84
	LION ENERGY CO LLC	2009	GAS	596		365			R TRISKET	1		DEWEY CORNERS	14-Dec-84
123 332,3		2003	Total	222,127	10					-			
Permit	Company	Year	Product	Quantity		Davs	County	Municipality	Farm Name	Farm_Well_No	Field	Pool	Completion Date
	US ENERGY DEV CORP	1987	GAS	11,653		112	WARREN	COLUMBUS	BITTINGER	4		DEWEY CORNERS	20-Aug-87
	US ENERGY DEV CORP	1988	GAS	100,800		352	WARREN		BITTINGER	4		DEWEY CORNERS	20-Aug-87
	US ENERGY DEV CORP	1989	GAS	100,330		355	WARREN		BITTINGER	4		DEWEY CORNERS	20-Aug-87
	US ENERGY DEV CORP	1990	GAS	60,844		342	WARREN		BITTINGER	4	COLUMBUS		20-Aug-87
	US ENERGY DEV CORP	1991	GAS	35,401		324	WARREN		BITTINGER	4		DEWEY CORNERS	
	US ENERGY DEV CORP	1992	GAS	13,041		315	WARREN		BITTINGER	4		DEWEY CORNERS	0
	US ENERGY DEV CORP	1993	GAS	6,946		360			BITTINGER	4		DEWEY CORNERS	20-Aug-87
	US ENERGY DEV CORP	1994	BRINE	0,040	137	300	WARREN		BITTINGER	4	COLUMBUS	DEWEY CORNERS	20-Aug-87
	US ENERGY DEV CORP	1994	GAS	5,778	, 11	361	WARREN		BITTINGER	4		DEWEY CORNERS	20-Aug-87
	BELDEN & BLAKE CORP	2000	GAS	92		365	WARREN	COLUMBUS	BITTINGER	4	COLUMBUS		20-Aug-87
	BELDEN & BLAKE CORP	2000	GAS	21		365	WARREN		BITTINGER	4		DEWEY CORNERS	20-Aug-87
	BELDEN & BLAKE CORP	2001	GAS	551		273	WARREN	COLUMBUS	BITTINGER	4		DEWEY CORNERS	20-Aug-87 20-Aug-87
	BELDEN & BLAKE CORP	2002	OIL	0		0	WARREN		BITTINGER	4		DEWEY CORNERS	•
	RANGE RESOURCES APPALACHIA LLC	2002	GAS	5		62	WARREN		BITTINGER	4		DEWEY CORNERS	20-Aug-87
	RANGE RESOURCES APPACACHIA LLC	2003	GAS	79		242		COLUMBUS	BITTINGER	4		DEWEY CORNERS	
			GAS	308		214		COLUMBUS	BITTINGER	4		DEWEY CORNERS	0
	RANGE RESOURCES APPALACHIA LLC	2005							BITTINGER	4			-
	TRINITY ENERGY CORP	2007	GAS	32	20	122		COLUMBUS		4	COLUMBUS	DEWEY CORNERS	20-Aug-87
	LION ENERGY CO LLC	2008	BRINE	200	38				BITTINGER	4			20-Aug-87
	LION ENERGY CO LLC	2008	GAS	368		365	WARREN		BITTINGER	•	COLUMBUS	DEWEY CORNERS	20-Aug-87
123-39874	LION ENERGY CO LLC	2009	GAS	219	4.80	180	WARKEN	COLUMBUS	BITTINGER	4	COTOMBO2	DEWEY CORNERS	20-Aug-87
			Total	336,487	17S								
Designation	Company	Vera	Deaduct	Quantitu		Deve	Country	Municipality	Energy Manage	Enum Mail N-	Field	Page	Completion Data
Permit	Company	Year 1990	Product GAS			315	County	Municipality COLUMBUS	Farm_Name R. TRISKET	Farm_Well_No 2	Field	Pool DEWEY CORNERS	Completion Date 5-Jan-90
	US ENERGY EXPLORATION CORP			41,981		315		COLUMBUS	R. TRISKET	2		DEWEY CORNERS	5-Jan-90 5-Jan-90
	US ENERGY DEV CORP	1991	GAS	47,292			WARREN		R. TRISKET	2	COLUMBUS	DEWEY CORNERS	5-Jan-90 5-Jan-90
	US ENERGY DEV CORP	1992	GAS GAS	25,943		322			R. TRISKET	2		DEWEY CORNERS	
125-40751	US ENERGY DEV CORP	1993	GND	17,584		359	WARKEN	COLUMBUS	A THORE	4	COLONIBOS	DEWELCORNERO	3-190-20

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122 407E1 US ENERGY DD/ CORD	1994	BRINE		137			COLUMBUS	R. TRISKET	2	COLUMPLIC		5 1 00
123-40751 US ENERGY DEV CORP			10 177	137	363						DEWEY CORNERS	5-Jan-90
123-40751 US ENERGY DEV CORP	1994	GAS	19,177	-	303		COLUMBUS	R. TRISKET	2		DEWEY CORNERS	5-Jan-90
123-40751 BELDEN & 8LAKE CORP	2000	BRINE	C	5	D.C.C.		COLUMBUS	R. TRISKET	2		DEWEY CORNERS	5-Jan-90
123-40751 BELDEN & BLAKE CORP	2000	GAS	5,514		366		COLUMBUS	R. TRISKET	2			5-Jan-90
123-40751 BELDEN & BLAKE CORP	2001	BRINE		17			COLUMBUS	R, TRISKET	2		DEWEY CORNERS	5-Jan-90
123-40751 BELDEN & 8LAKE CORP	2001	GAS	4,531		365		COLUMBUS	R. TRISKET	2		DEWEY CORNERS	5-Jan-90
123-40751 BELDEN & BLAKE CORP	2002	GAS	2,340		273		COLUMBUS	R. TRISKET	2		DEWEY CORNERS	5-Jan-90
123-40751 BELDEN & BLAKE CORP	2002	OIL	0		0	WARREN	COLUMBUS	R. TRISKET	2	COLUMBUS	DEWEY CORNERS	5-Jan-90
123-40751 RANGE RESOURCES APPALACHIA LLC	2002	GAS	205		31	WARREN	COLUMBUS	R. TRISKET	2	COLUMBUS	DEWEY CORNERS	5-Jan-90
123-40751 RANGE RESOURCES APPALACHIA LLC	2003	BRINE		45	365	WARREN	COLUMBUS	R. TRISKET	2	COLUMBUS	DEWEY CORNERS	5-Jan-90
123-40751 RANGE RESOURCES APPALACHIA LLC	2003	GAS	1,594		365	WARREN	COLUMBUS	R. TRISKET	2	COLUMBUS	DEWEY CORNERS	5-Jan-90
123-40751 RANGE RESOURCES APPALACHIA LLC	2004	GAS	1,422		365	WARREN	COLUMBUS	R. TRISKET	2	COLUMBUS	DEWEY CORNERS	5-Jan-90
123-40751 RANGE RESOURCES APPALACHIA LLC	2005	GAS	1,554		365	WARREN	COLUMBUS	R. TRISKET	2	COLUMBUS	DEWEY CORNERS	5-Jan-90
123-40751 RANGE RESOURCES APPALACHIA LLC	2006	GAS	1,414		365	WARREN	COLUMBUS	R. TRISKET	2	COLUMBUS	DEWEY CORNERS	5-Jan-90
123-40751 TRINITY ENERGY CORP	2007	GAS	278		122	WARREN	COLUMBUS	R. TRISKET	2	COLUMBUS	DEWEY CORNERS	5-Jan-90
123-40751 LION ENERGY CO LLC	2008	GAS	869		365	WARREN	COLUMBUS	R, TRISKET	2	COLUMBUS	DEWEY CORNERS	5-Jan-90
123-40751 LION ENERGY CO LLC	2009	GAS	1,506		365	WARREN	COLUMBUS	R. TRISKET	2		DEWEY CORNERS	
		Total	173,205	204								
			A					100		P1.11		
Permit Company	Year	Product				County	Municipality		Farm_Well_No	Field	Pool	Completion Date
123-34843 US ENERGY DEV CORP	1985	GAS	17,683		0		COLUMBUS	SMITH- RAS	1		DEWEY CORNERS	26-Mar-84
123-34843 US ENERGY DEV CORP	1986	GAS	31,402		336		COLUMBUS	SMITH- RAS	1		DEWEY CORNERS	26-Mar-84
123-34843 US ENERGY DEV CORP	1987	GAS	29,357		322		COLUMBUS	SMITH- RAS	1		DEWEY CORNERS	26-Mar-84
123-34843 US ENERGY DEV CORP	1988	GAS	50,639		338		COLUMBUS	SMITH- RAS	1		DEWEY CORNERS	26-Mar-84
123-34843 US ENERGY DEV CORP	1989	GAS	52,016		344		COLUMBUS	SMITH- RAS	1		DEWEY CORNERS	26-Mar-84
123-34843 US ENERGY DEV CORP	1990	GAS	21,148		330		COLUMBUS	SMITH- RAS	1		DEWEY CORNERS	26-Mar-84
123-34843 US ENERGY DEV CORP	1991	GAS	8,423		327		COLUMBUS	SMITH- RAS	1		DEWEY CORNERS	26-Mar-84
123-34843 US ENERGY DEV CORP	1992	GAS	1,513		291		COLUMBUS	SMITH-RAS	1		DEWEY CORNERS	26-Mar-84
123-34843 US ENERGY DEV CORP	1993	GAS	2,088		268		COLUMBUS	SMITH- RAS	1		DEWEY CORNERS	26-Mar-84
123-34843 US ENERGY DEV CORP	1994	GAS	1,781		363		COLUMBUS	SMITH- RAS	1		DEWEY CORNERS	26-Mar-84
123-34843 LION ENERGY CO LLC	2008	GAS	270		365		COLUMBUS	SMITH-RAS	1	COLUMBUS	DEWEY CORNERS	26-Mar-84
123-34843 LION ENERGY CO LLC	2009	GAS	644		365	WARREN	COLUMBUS	SMITH- RAS	1	COLUMBUS	DEWEY CORNERS	26-Mar-84
		Total	216,965									
123-33914 US ENERGY DEV CORP	1984	GAS	5893		0	WARREN	COLUMBUS	JOSEPH BITTINGER	1	COLUMBUS	DEWEY CORNERS	29-Dec-83
123-33914 US ENERGY DEV CORP	1985	GAS	14431.49		0	WARREN	COLUMBUS	JOSEPH BITTINGER	1	COLUMBUS	DEWEY CORNERS	29-Dec-83
123-33914 US ENERGY DEV CORP	1986	GAS	44172.28		336	WARREN	COLUMBUS	JOSEPH BITTINGER	1	COLUMBUS	DEWEY CORNERS	29-Dec-83
123-33914 US ENERGY DEV CORP	1987	GAS	21594.73		336	WARREN	COLUMBUS	JOSEPH BITTINGER	1	COLUMBUS	DEWEY CORNERS	29-Dec-83
123-33914 US ENERGY DEV CORP	1988	GAS	51243.65		356	WARREN	COLUMBUS	JOSEPH BITTINGER	1	COLUMBUS	DEWEY CORNERS	29-Dec-83
123-33914 US ENERGY DEV CORP	1989	GAS	67741.18		364		COLUMBUS	JOSEPH BITTINGER	1		DEWEY CORNERS	29-Dec-83
123-33914 US ENERGY DEV CORP	1990	GAS	66748.67		352	WARREN	COLUMBUS	JOSEPH BITTINGER	1	COLUMBUS	DEWEY CORNERS	29-Dec-83
123-33914 US ENERGY DEV CORP	1991	GAS	38209		350		COLUMBUS	JOSEPH BITTINGER	1	-	DEWEY CORNERS	29-Dec-83
123-33914 US ENERGY DEV CORP	1992	GAS	13492		320		COLUMBUS		1		DEWEY CORNERS	29-Dec-83
123-33914 US ENERGY DEV CORP	1993	GAS	6206		352		COLUMBUS	JOSEPH BITTINGER			DEWEY CORNERS	29-Dec-83
123-33914 US ENERGY DEV CORP	1994	GAS	2570		341		COLUMBUS	JOSEPH BITTINGER	1		DEWEY CORNERS	29-Dec-83
123-33914 BELDEN & BLAKE CORP	2000	GAS	\$59		366		COLUMBUS	JOSEPH BITTINGER	1		DEWEY CORNERS	29-Dec-83
123-33914 BELDEN & BLAKE CORP	2001	GAS	438		365		COLUMBUS	JOSEPH BITTINGER	1		DEWEY CORNERS	29-Dec-83
123-33914 BELDEN & BLAKE CORP	2002	GAS	372		273		COLUMBUS		1		DEWEY CORNERS	29-Dec-83
123-33914 BELDEN & BLAKE CORP	2002	OIL	0		0		COLUMBUS	JOSEPH BITTINGER	1 .		DEWEY CORNERS	29-Dec-83
123-33914 RANGE RESOURCES APPALACHIA LLC	2002	GAS	46		31		COLUMBUS	JOSEPH BITTINGER	1		DEWEY CORNERS	29-Dec-83
123-33914 RANGE RESOURCES APPALACHIA LLC	2003	GAS	257.85		182		COLUMBUS	JOSEPH BITTINGER	—		DEWEY CORNERS	
									-			

123-33914 RANGE RESOURCES APPALACHIA LLC	2004	GAS	313.84		244	WARREN	COLUMBUS	JOSEPH BITTINGER	1	COLUMBUS DEWEY CORNERS 29-D	ec-83
123-33914 RANGE RESOURCES APPALACHIA LLC	2005	GAS	47.28		212	WARREN	COLUMBUS	JOSEPH BITTINGER	1	COLUMBUS DEWEY CORNERS 29-D	ec-83
123-33914 RANGE RESOURCES APPALACHIA LLC	2006	GAS	4.33		151	WARREN	COLUMBUS	JOSEPH BITTINGER	1	COLUMBUS DEWEY CORNERS 29-De	ec-83
123-33914 TRINITY ENERGY CORP	2007	GAS	64		365	WARREN	COLUMBUS	JOSEPH BITTINGER	1	COLUMBUS DEWEY CORNERS 29-D	ec-83
123-33914 LION ENERGY CO LLC	2008	BRINE		38		WARREN	COLUMBUS	JOSEPH BITTINGER	1	COLUMBUS DEWEY CORNERS 29-De	ec-83
123-33914 LION ENERGY CO LLC	2008	GAS	392		365	WARREN	COLUMBUS	JOSEPH BITTINGER	1	COLUMBUS DEWEY CORNERS 29-De	ec-83
123-33914 LION ENERGY CO LLC	2009	GAS	90		120	WARREN	COLUMBUS	JOSEPH BITTINGER	1	COLUMBUS DEWEY CORNERS 29-D	ec-83
		Total	334,886	38							

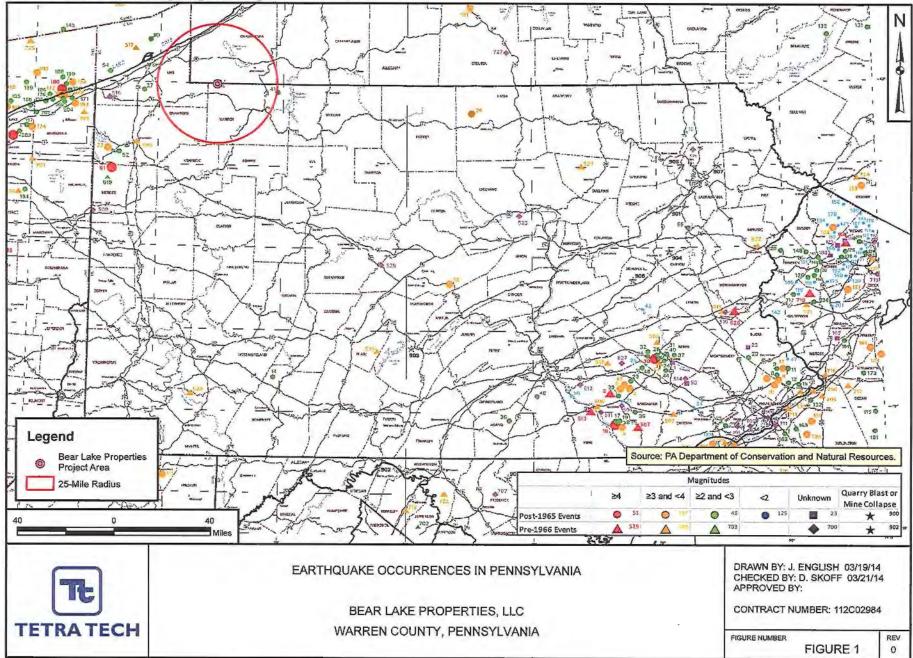
Total All 7 wells 1,751,614

GEOLOGIC DATA

EARTHQUAKE EPICENTERS MAP (PA DCNR)

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Section 6 – Operating Data

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Section 6 - Operating Data

The proposed commercial brine disposal well will primarily be utilized to inject produced and flowback water from wells completed in the Marcellus Shale, the Medina Group and other natural gas and oil producing formations. Other oil and gas related wastewaters associated with the production of oil and natural gas or natural gas storage operations, which are approved by EPA for injection under a UIC Class II D injection well, may also be injected. According to Title 40 Chapter I Sec. 144.6 (b)(1), such fluids include those "Which are brought to the surface in connection with natural gas storage operations, or conventional oil or natural gas production and may be commingled with waste waters from gas plants which are an integral part of production operations, unless those waters are classified as a hazardous waste at the time of injection."

Injection Rate

Injection rate and pressure data collected to date for the nearby Bittinger #4 permitted brine disposal well indicate the well is capable of a sustainable injection rate of approximately 1,000 bbls/day while operating within the maximum injection pressure permit limit. This is consistent with the permitted injection volume of 30,000 bbls/month for this well. (The 2014 Annual Disposal/Injection Well Monitoring Report for Bittinger #4 is attached.) Considering the proximity of the Bittinger #3 well to the Bittinger #4 well (which is located approximately 0.5 mile to the west) and the similarity in the injection rate while staying below the proposed MIP. (Please see the attached Billman Geologic Consultants report and included geologic cross-sections.) An injection rate of 30,000 bbls/month is therefore also proposed for the Bittinger #3 well.

Maximum Allowable Surface Injection Pressure (MASIP) and Average Surface Injection Pressure

MASIP calculations based on EPA approved equations are included in the "Geologic Data" section of this application. Based on these calculations, the proposed MASIP is 1732 psi. It is estimated that the average surface injection pressure will be approximately 1000 psi.

Laboratory Analysis of Injection Fluid Samples

Laboratory analytical results for samples representative of the types of brine which will be injected into the proposed injection well are attached. Samples were collected from produced water generated from gas wells in the vicinity of the injection well as well as Marcellus brine from a brine processing facility.

Monitoring of Injection Fluid Samples and Well

The following identifies the UIC Class II underground injection well regulatory requirements and operational procedures which will be conducted to meet the subject requirements:

- Monitoring of the nature of injected fluids at time intervals sufficiently frequent to yield data representative of their characteristics. An initial sample of fluid will be collected and analyzed from initial loads proposed for disposal from new disposal customers. In addition, samples will be collected for analysis from new types of sources (e.g., from different geologic formations, geographic regions, etc.) which would be expected to differ significantly from brine previously characterized for disposal at the facility. Samples will be analyzed for the following parameters at a minimum: specific gravity, total dissolved solids and pH.
- 2. Observation of injection pressure, flow rate, and cumulative volume at least weekly based on the regulatory requirements for produced fluid disposal operations. Injection pressures,

annular pressure, injection rate, and cumulative volume will be continuously monitored and recorded electronically.

- 3. A demonstration of mechanical integrity pursuant to 40 CFR Sec. 146.8 at least once every two years during the life of the injection well. A mechanical integrity test will be performed prior to initiating injection and at least once every two years.
- 4. **Maintenance of the results of all monitoring until the next permit review.** All monitoring records will be maintained throughout the life of the well.

Reporting requirements consist of the following:

An annual report will be submitted to EPA summarizing the results of the required monitoring, including monthly records of injected fluids, and any major changes in characteristics or sources of injected fluid.

Proposed Annulus Fluid

The proposed annulus fluid for the proposed injection well will consist of fresh water and a water soluble corrosion inhibitor. The corrosion inhibitor will be mixed in accordance with the manufacturer's recommendations then loaded into the well annulus prior to conducting injection operations. Product information for the type of corrosion inhibitor which will be utilized is attached. A similar type product may be used instead of the example product referenced.

Facility Layout and Operation

The attached drawing shows the following elements of the existing Bear Lake Properties brine disposal well facility including the recently permitted and constructed brine storage area. The brine storage facility was permitted as a residual waste transfer facility under PADEP residual waste regulations. The following key elements of the brine disposal facility are shown on the attached drawing:

- Existing permitted brine offloading facility located at the corner of State Route 4004 and State Line Road;
- The brine storage facility (located near the Bittinger #2 well) which is connected to the unloading area by underground double-walled piping; and,
- The three existing permitted UIC Class IID wells (Bittinger #1, #2 and #4) plus proposed UIC Class IID wells (Bittinger #3 and Smith-Ras Unit #1).

The brine storage facility has a capacity of 3,000 barrels and is anticipated to be operational during the First Quarter of 2015. A drawing showing details of the brine storage facility is attached.

Once the brine storage facility is operational, brine will be pumped from the offload station via the dual (secondary containment) pipeline to the storage tanks at the brine storage facility. The brine will then be pumped from the brine storage facility via high pressure dual (secondary containment) pipelines to the permitted brine disposal wells for injection.

The storage tanks in the brine storage area are located within a diked containment area with the containment area sized to account for the entire volume of the largest container, plus 10%. Automatic shut-off valves are incorporated into the tank design to prevent overflow during filling operations. The facility is surrounded by a fence having locking entrance and exit gates. A security camera is also strategically situated on the site.

OPERATING DATA

TYPICAL BRINE LABORATORY ANALYSIS

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Certificate Of Analysis Continued On Next Page

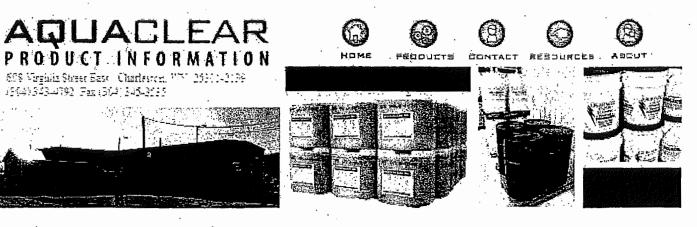
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Client Sample Results

Client: Bear Lake Properties, LLC Project/Site: Injection Well Permitting TestAmerica Job ID: 180-17986-1

ient Sample ID: CW 011013							Lab Sam	ple ID: 180-1	7986-1
ate Collected: 01/10/13 13:30								-	k: Water
ate Received: 01/11/13 09:30									
- Method: 200.8 - Metals (ICP/MS) -	Total Recove	rable							
Analyte		Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
Barium	5200000	В	5000	44	ug/L		01/16/13 09:44	01/16/13 18:31	5
Iron	1600	JB	5000	230	ug/L		01/12/13 12:22	01/14/13 21:03	100
Magnesium	2300000	в	10000	200	ug/L		01/12/13 12:22	01/14/13 21:03	100
Manganese	10000	В	500	3.7	ug/L		01/12/13 12:22	01/14/13 21:03	100
Sodium	32000000	в	1000D	270	ug/L		01/12/13 12:22	01/14/13 21:03	100
Conomi Chamistry									
General Chemistry Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
Chloride	130000		1000	200	mg/L			01/12/13 11:36	1000
Aikalinity	6.5	в	5.0	0.41	mg/L			01/14/13 08:05	1
Bicarbonate Alkalinity as CaCO3	6.5	_	5.0	0.41	mg/L			01/14/13 08:08	1
Carbonate Alkalinity as CaCO3	ND		5.0	D.41	mg/L		· · · · · ·	01/14/13 08:06	· · · · 1
Hardness	74000		2500	770	mg/L			01/14/13 09:05	500
Total Dissolved Solids	200000		1000	1000	mg/L			01/11/13 14:39	1
Total Organic Carbon - Duplicates	63		40	7.5	mg/L			01/21/13 11:02	40
Analyte	Result	Qualifier	RL	RL	Unit	D	Prepared	Analyzed	Dil Fac
рН	6.23	HF	0.100	0.100	SU			01/15/13 09:50	1
Specific Conductance	440000		1600	1600	umhos/cm			01/11/13 18:45	1600
Total Solids	220000		10	10	mg/L			01/15/13 15:50	1

CORROSION INHIBITOR STICKSTM: Oil and Gass Stalling Pradicessing Atlant adversing Atlant Contact R3_UIC_Mailbox@epa.gov



Corrosion Inhibitor SticksT

WHAT ARE CORROSION INHIBITOR STICKST?

Corrosion Inhibitor SticksT are water soluble or oil soluble sticks that contain a blend of Imidazolines which have excellent filming characteristics and low emulsion tendencies. This unique blend gives effective corrosion control for most oil field corrosion problems.

CORROSION INHIBITOR STICKTM USES

Corrosion Inhibitor Sticks ™ are primarily used to control common corrosion problems found in producing oil and gas well systems. They can be used to treat hard to reach 'dead' areas such as the annulus space above the packer, rat-hole, or the bottom of water supply tanks.

ADVANTAGES OF CORROSION INHIBITOR STICKST

Corrosion Inhibitor SticksT can provide corrosion control throughout the entire production system. Regular usage will help control corrosion at the point they begin - down-hole.

They are available in two different formulations (oil soluble and water dispersable) or (water soluble and oil dispersable). The oil soluble type is soluble in oil, condensate and wet gas and can slowly disperse inhibitor into the water phase. The water soluble type is soluble in water and can slowly disperse inhibitor into the oil phase.

Corrosion Inhibitor SticksT can effectively inhibit corrosion in wells that produce both water and distillate or oil phases. In this case, it may be desirable to treat the well with both types of sticks by first dropping water soluble sticks and allowing them to fall through the oil into the water, thus dissolving and releasing inhibitor in TREATMENT DETERMINATION The number of Corrosion Inhibitor SticksT used is based on the volume of total fluid produced (oil or condensate plus water). Field experience indicates that for most corrosive environments the best results are achieved by using a larger initial slug treatment (80 PPM daily) until the problem is under control then reduce to smaller periodic treatments (40 PPM daily) thereafter. EXAMPLE: An initial slug treatment of 80 PPM would require 0.64 lbs of Corrosion Inhibitor Stick™ per 24 BBL (1000 gallons) of total fluid produced.

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	TICKS PER BBL
	i per 58 bbls
	l per 40 bbls
	l per 29 bbls
	l per 18 bbls
MIDGET (5/8" x 15")	1 per 7 bbls

NOTE: To successfully control any corrosion problem, the inhibitor insertion into the fluid stream must be constant. For intermittent treatment or extreme corrosive environments increase the number of sticks accordingly.

THE MOST COMMON PROCEDURE for producing wells is to shut-in well and drop sticks through lubricator. Leave well shut until sticks fall to the bottom. The time in minutes for the sticks to fall to the bottom (assuming well is shut-in with fluid at surface) is equal to the depth divided by 100. (Time, min. = Depth, ft / 100).

EOR WATER INJECTION SYSTEMS drop the sticks into the water supply tank to inhibit more of the system.

the water column). Then drop the oil soluble sticks which will "FLOAT" at where the oil and water contact thus slowly dissolving and releasing inhibitor in the oil column.

The sticks are economical when compared to conventional corrosion control operations and therefore save investment in pumps, drums of chemical, and equipment maintenance.

Corrosion Inhibitor SticksT may be used in wells with bottom hole temperatures (BHT) of up to 375 degrees Fahrenheit. **PRODUCTION SPECIFICATIONS**

<u>OIL SOLUBLE</u>: The stick will dissolve in 20 to 120 minutes (in moving diesel) depending on temperature, salt content, and relative fluid motion. The stick will melt at 135 degrees Fahrenheit and the specific gravity is 0.95.

WATER SOLUBLE: The stick will dissolve in 12 to 24 hours (in 60,00 PPMmoving brine water) depending on temperature, salt content, and relative fluid motion. The stick will melt at 125 degrees Fahrenheit and the specific gravity is 1.10.

PRODUCT PACKAGING

SENIOR 1.55 lb/stick 24/case 31/pail 48/chest
JUNIOR(1) 1.20 lb/stick 36/case n/a 72/chest
JUNIOR(2) 0.76 lb/stick 36/case 52/pail 72/chest
THRIFTY 0.49 lb/stick 49/case 72/pail 98/chest
MIDGET 0.19 lb/stick 108/case 204/pail 216/chest

WHERE TO BUY

All good oll field supply stores carry Aqua-Clear, Inc. Corrosion inhibitor Sticks™, but you can also buy direct from us.

Ordering Information

Should you wish to speak to a sales representative about any of our products, you can call or email Tommy Halloran Jr., Ronald "Buster" Wilson, or Russell Cook directly:

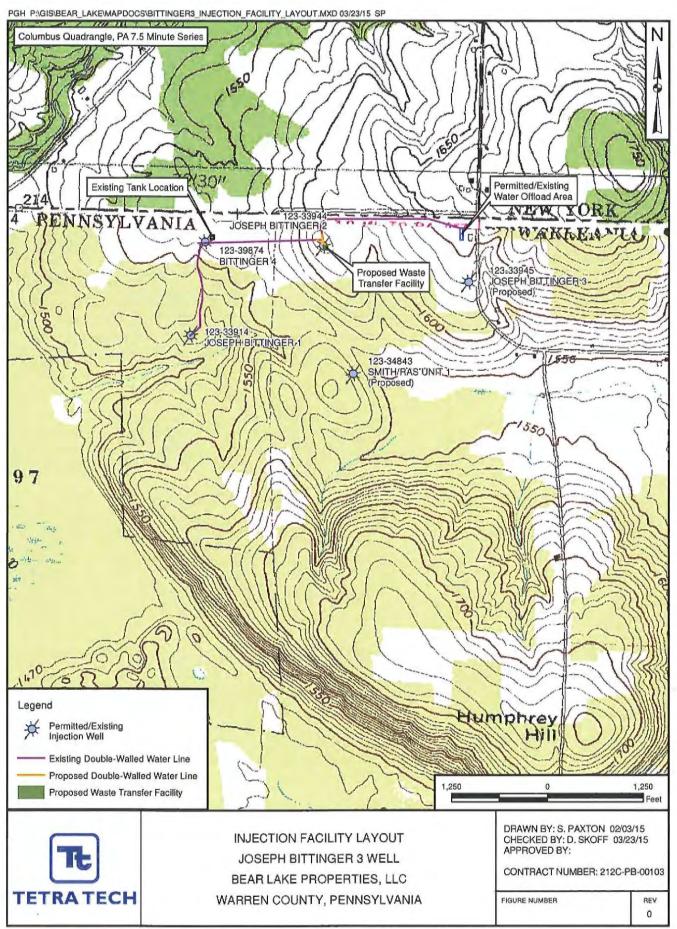
Tommy Halloran Jr. W 304-343-4792 H 304-345-5152 C 304-546-8526 tom@aquaclear-inc.com Ronald "Buster" Wilson W 304-546-8518 H 304-965-7996 Fax 304-965-2713 buster@acuaclear-inc.com Russell Cook W 304-546-2940 H 304-842-7050 Fax 304-842-7050 russell@aguaclear-inc.com

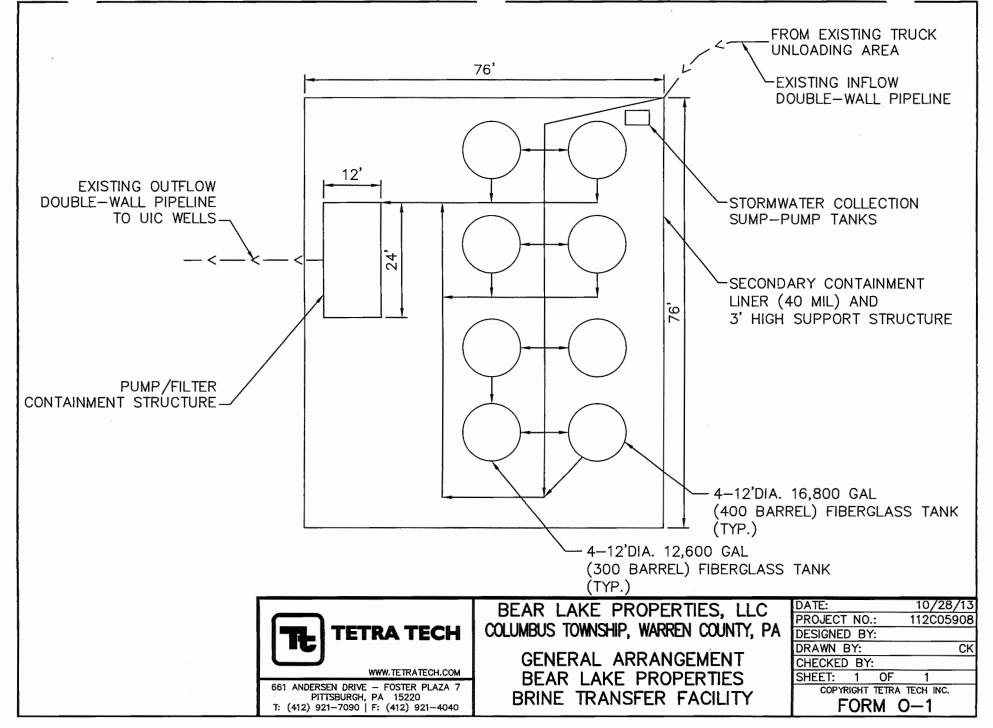
OPERATING DATA

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FACILITY LAYOUT SCHEMATIC

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OPERATING DATA

ANNUAL OPERATING DATA REPORTS

			generation of the second			C	DMB No. 2040-0042	Approv	al Expires 11	/30/2014		
United States Environmental Protection Agency Washington, DC 20460 ANNUAL DISPOSAL/INJECTION WELL MONITORING REPORT												
Name and Address of Ex					Name and Address of Surface Owner							
Bear Lake Properties, 3000 Village Run Roa		Miles Sampsel 82530 Pangan Rd., Erie, PA 16509										
				State Pennsylvania		County Warren			Permit Number PAS2D215 BWAR			
	i	Surface Location Description										
┝┽╍┝┽╸	╺┠┽╾┝╶┽╸	-	Locate well in two directions from nearest lines of quarter section and drilling unit									
┝┿╼┝┿╸		Line of quarter section										
w		E	WELL ACTIVITY TYPE OF PERMIT Image: State St									
┝╴┽╍┝╴┽╸	╺┠╸┽╺╸├╴┽╺	-										
Hydrocarbon Storage Number of Wells												
	╺┠╴┽╼┝╴┽╺	-	Lea	se Name	Bittinger			Well Nu	ımber 4]		
	s											
	INJECTION	PRESSURE			TOTAL VOLUME INJECTED				TUBING CASING ANNULUS PRESSURE (OPTIONAL MONITORING)			
MONTH YEAR	AVERAGE PSIG	MAXIMUM	PSIG	-	BL		MCF	MINIMU	JM PSIG	MAXIMUM PSIG		
January-2014	1100	1440		8995				0		540		
February-2014	960	1130		2716		1		0		0		
March-2014	0	0		1474				0		0		
April-2014	1200	1460		15395		I		0		120		
May-2014	1500	1600		14586	6			80		120		
June-2014	1550	1620		12803				80		100		
July-2014	1300	1400		17838		I		80		100		
August-2014	1380	1400		9316		[80		100		
September-2014	1540	1620		2434				50		150		
October-2014	1580	1620		12338		-		60		180		
November-2014	1580	1620		9840		Error of		80		200		
December-2014	1590	1620		8559		[80		200		
Certification I certify under the penalty of law that I have personally examined and am familiar with the information submitted in this document and all attachments and that, based on my inquiry of those individuals immediately responsible for obtaining the information, I believe that the information is true, accurate, and complete. I am aware that there are significant penalties for submitting false information, including the possiblility of fine and imprisonment. (Ref. 40 CFR 144.32)												
Name and Official Title (Please type or print)				gnature					1 5	ate Signed		
John C. Holko, Vice	President									01/29/15		

EPA Form 7520-11 (Rev. 12-11)

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OPERATING DATA

TYPICAL CORROSION INHIBITOR

CORROSION INHIBITOR STICKSTM: Oil for easiStathag Praductsing/Abisa Clearment, contact R3_UIC_Mailbox@epa.gov



Corrosion Inhibitor SticksT

WHAT ARE CORROSION INHIBITOR STICKST?

Corrosion Inhibitor SticksT are water soluble or oil soluble sticks that contain a blend of Imidazolines which have excellent filming characteristics and low emulsion tendencies. This unique blend gives effective corrosion control for most oil field corrosion problems.

CORROSION INHIBITOR STICK™ USES

Corrosion Inhibitor Sticks ™ are primarily used to control common corrosion problems found in producing oil and gas well systems. They can be used to treat hard to reach 'dead' areas such as the annulus space above the packer, rat-hole, or the bottom of water supply tanks.

ADVANTAGES OF CORROSION INHIBITOR STICKST

Corrosion Inhibitor SticksT can provide corrosion control throughout the entire production system. Regular usage will help control corrosion at the point they begin - down-hole.

They are available in two different formulations (oil soluble and water dispersable) or (water soluble and oil dispersable). The oil soluble type is soluble in oil, condensate and wet gas and can slowly disperse inhibitor into the water phase. The water soluble type is soluble in water and can slowly disperse inhibitor into the oil phase.

Corrosion inhibitor SticksT can effectively inhibit corrosion in wells that produce both water and distillate or oil phases. In this case, it may be desirable to treat the well with both types of sticks by first dropping water soluble sticks and allowing them to fall through the oil into the water, thus dissolving and releasing inhibitor in TREATMENT DETERMINATION The number of Corrosion Inhibitor SticksT used is based on the volume of total fluid produced (oil or condensate plus water). Field experience indicates that for most corrosive environments the best results are achieved by using a larger initial slug treatment (80 PPM daily) until the problem is under control then reduce to smaller periodic treatments (40 PPM daily) thereafter. EXAMPLE: An initial slug treatment of 80 PPM would require 0.64 lbs of Corrosion Inhibitor Stick™ per 24 BBL (1000 gallons) of total fluid produced.

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COR. INH. STICKT SIZES	STICKS PER BBL
SENIOR (1 5/8 " x 18")	1 per 58 bbls
JUNIOR (1.3/8 " x 16 ")	1 per 40 bbls
JUNIOR (1 1/4" x 15")	1 per 29 bbls
THRIFTY (1" x 15")	1 per 18 bbls
MIDGET (5/8" × 15")	1 per 7 bbls

NOTE: To successfully control any corrosion problem, the inhibitor insertion into the fluid stream must be constant. For intermittent treatment or extreme corrosive environments increase the number of sticks accordingly.

THE MOST COMMON PROCEDURE for producing wells is to shut-in well and drop sticks through lubricator. Leave well shut until sticks fall to the bottom. The time in minutes for the sticks to fall to the bottom (assuming well is shut-in with fluid at surface) is equal to the depth divided by 100. (Time, min. = Depth, ft / 100).

<u>FOR WATER INJECTION SYSTEMS</u> drop the sticks into the water supply tank to inhibit more of the system.

the water column). Then drop the oil soluble sticks which will "FLOAT" at where the oil and water contact thus slowly dissolving and releasing inhibitor in the oil column.

The sticks are economical when compared to conventional corrosion control operations and therefore save investment in pumps, drums of chemical, and equipment maintenance.

Corrosion Inhibitor SticksT may be used in wells with bottom hole temperatures (BHT) of up to 375 degrees Fahrenheit. **PRODUCTION SPECIFICATIONS**

<u>OIL SOLUBLE</u>: The stick will dissolve in 20 to 120 minutes (in moving diesel) depending on temperature, salt content, and relative fluid motion. The stick will melt at 135 degrees Fahrenheit and the specific gravity is 0.95.

WATER SOLUBLE: The stick will dissolve in 12 to 24 hours (in 60,00 PPMmoving brine water) depending on temperature, salt content, and relative fluid motion. The stick will melt at 125 degrees Fahrenheit and the specific gravity is 1.10.

PRODUCT PACKAGING

	SENIOR 1.55 lb/stick 24/case 31/pail 48/chest	
	IUNIOR(1) 1.20 lb/stick 36/case n/a 72/chest	
:	IUNIOR(2) 0.76 lb/stick 36/case 52/pail 72/chest	
	THRIFTY 0.49 lb/stick 49/case 72/pail 98/chest	
	MIDGET 0.19 (b/stick 108/case 204/pail 216/ches	ŧ

WHERE TO BUY

All good oil field supply stores carry Aqua-Clear, Inc. Corrosion Inhibitor Sticks™, but you can also buy direct from us.

Ordering Information

Should you wish to speak to a sales representative about any of our products, you can call or email Tommy Halloran Jr., Ronald "Buster" Wilson, or Russell Cook directly:

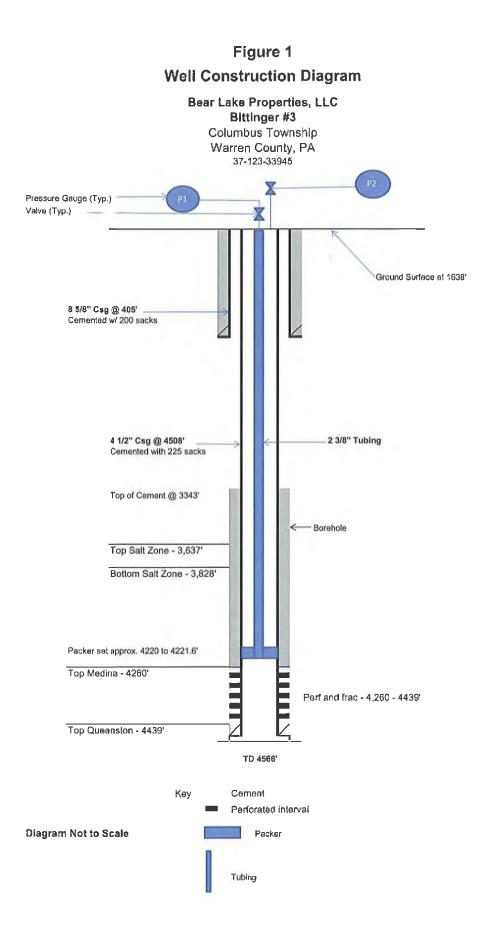
Tommy Halloran Jr. W 304-343-4792 H 304-345-5152 C 304-546-8526 tom@aquaclear-inc.com Ronald "Buster" Wilson W 304-546-8518 H 304-965-7996 Fax 304-965-2713 buster@acuaclear-inc.com

Russell Cook W 304-546-2940 H 304-842-7050 Fax 304-842-7050 russell@aguaclear-inc.com Section – 7 Well Construction Details

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WELL CONSTRUCTION

INJECTION WELL CONFIGURATION



Bittinger #3 Surface cement calculation:

Surface hole size: 12-1/4"* Suface cement volume: 200 sx Class A* Surface casing: 405ft. of 8-5/8"

Class A cement yield: 1.18 cu. ft. per sack Annular volume between 12-1/4" O.H. and 8-5/8" casing: 0.4127 cu. ft. per ft.

Cement volume required: 405 ft. x 0.4127 cu. ft. per ft. = **167.1 cu. ft.**

Cement volume pumped: 200 sx class A x 1.18 cu. ft./sk = **236 cu. ft.**

*surface casing hole size and cement type based upon detail offset well surface cement ticket of the Smith-Ras #1 well – cement ticket attached in this section. This offset well was drilled by the same operator in the same approximate time period as the Bittinger #3.

All " " . OIL FIELD SERVICES For assistance in accessing this document contact the Mailbox per story services DOWELL SERVICE LOCATION NAME AND NUMBER REMITTANCE COPRESECNDENCE WELL SERVICE OFDER, P.O. BOX 100344 HOUSTON, TEXAS 77212 PO BOX 4378 CEIFT, AND INVOICE NO CORRY HOUSTON, TEXAS 77210 11-120 TYPE SERVICE CODE CUSTOMER NUMBER CUSTOMER P.O NUMBER BUSINESS CODES -16-6292 VERBAL 792186 275 API OR IC NUMBER WORKOVER NEW WELL OTHER ISTOMER'S U.S. ENERGY ME OTHER SIDE FOR TERMS & CONDITIONS DDRESS 680 STATLER BLD. BUFFALO, N.Y. 14202 ARRIVE MO DAY $\tilde{2}\tilde{2}$ LOCATION TY, STATE AND SERVICE ORDER I authorize work to begin > CODE vice instructions in accordance with terms and (ditions printed on the reverse side of this form DOWELL shall furnish and Customer shall purchase materials and services required in the represent that I have authority to accept and sign performance of the following SERVICE INSTRUCTIONS or DOWELL INDUSTRIAL SERVICE CONTRACT NO. 01-16-6292 CEMENT 394 OF 8518 CASING INTO 419 OF OPEN HOLE USING 150 SKS OF CLASS "A" WITH 3% CACL order. CUSTOMER AUTHORIZED AGENT Michael The JOB 24 COMPLETION AND JOLB OF D46. ADD SOLB OF D29 WHILE SERVICE RECEIPT I certify that the materials MIXING SLURRY. services listed were received and all services formed in a workmanlike manner. CODE COUNTY / PARISH CODE CITY CUSTOMER AUTHORIZED AGENT PA. Midleal 123 BEAR LAKE TWP. WARREN 11-60 م تيني -NAME AND NUMBER & JOE SITE ... LOCATION AND POOL / PLANT ADDRESS SHIPPED VIA SMITH KAZZ #10 DOWELL BEAR LAKE ITEM/PRICE REF. NO. MATERIAL, EQUIPMENT AND SERVICES USED UNIT QUANTITY UNIT PRICE S AMOUNT CLASS "A" CEMENT 4,76 714,00 10 823-121 SKS. 150 182,00 \$7005-100 S-1 DOWFLAKE 400 ,27 LB D46 ANTIFOAM AGENT 102-050 2,50 30 75,00 1B 44003-025 D29 CELLOFLAKE 1,22 50 61,00 LB 8518 WOOD PLUG 60.00 6702-085 60,00 ÉÁ 6008-085 190,00 190,00 85/8 GUIDE SHOE EA 8-18 180.00 BASKET EA 53,00 6011-088 8 5/8 106,00 CENTRALIZER EÅ 190.00 11 1003-044 412 FLAPPER FLOAT SHOE ĔΑ 190.00 3004-045 442 LATCH IN RECEP E4 265,00 6008-044 105.00 412 BASKET 105,00 EA 4031-044 205.00 41/2 CENTRALIZER 5 41.00 EA 9800-001 MILEAGE ON PUMPER 21,50 10 2,15 MI 01104-005 Equipment CHARGE ADDITIONAL DEPTH DERVICE CHARGE 440,00 440,00 EA FT 01104-100 ,44 CUIFT 153,52 49100-000 162. 196 HAULING CHARGE T.2 X MI 19102-000 4,75 131 51.75 T.M. 9102-SUB TOTAL 29日 LICENSE/REIMBURSEMENT FEE LICENSE/REIMBURSEMENT FEE STATEME ARKS: % TAX ON S COUNTY % TAX ON S HANKS FOR USING DOWELL CITY S TAX ON S DOWELL REPRESENTATIVE TOTAL 79DA Eg MADWICH

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WELL CONSTRUCTION

BITTINGER #3 COMPLETION RECORD

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ER-OG-4: Rev. 2/60

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"Tully" LS	2816'	2926'				geophysical logs	
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Unconformity Interval	3256'	3285'					
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Camillus	3,370'	3442'	· ·				
Syracuse	3442'	3641'					
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Section 8 – Monitoring Program

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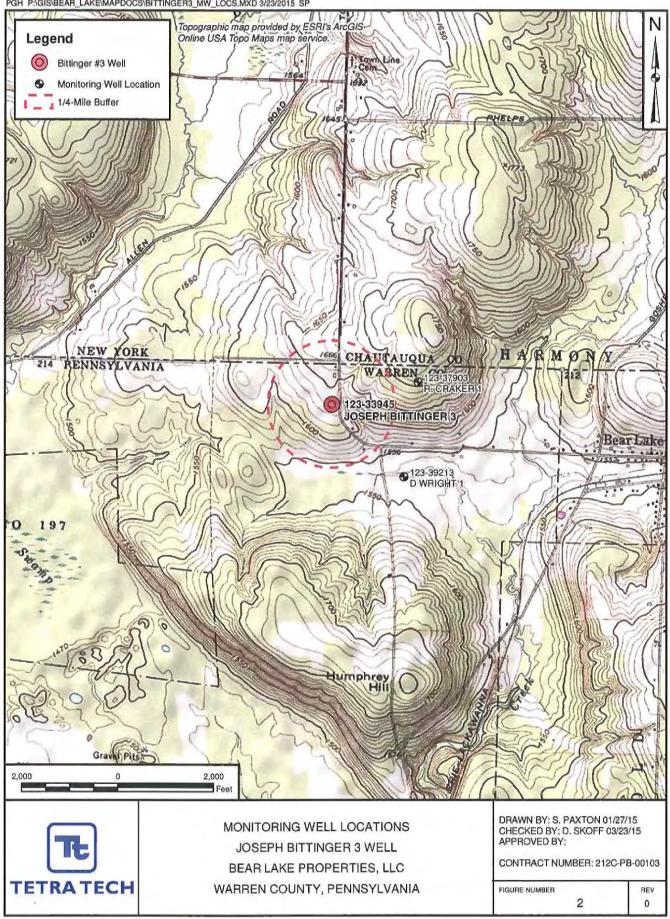
Section 8 - Monitoring Program

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The fluid levels in the following nearby depleted Medina natural gas wells will be measured and recorded semi-annually, at a minimum. The monitoring well locations are shown on the attached figure.

Injection Well	Monitoring Well	Approximate Distance and Direction From Injection Well
Bittinger #3	R. Craker #1	1,900 ft to the northeast
	D. Wright #1	2,000 ft to the southeast

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PGH P:\GIS\BEAR_LAKE\MAPDOCS\BITTINGER3_MW_LOCS.MXD 3/23/2015 SP

Section 9 – Plugging and Abandonment Plan

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Section 9 - Plugging and Abandonment Plan

At the point when the well is no longer used, the well will be abandoned in accordance with EPA and PADEP regulations. With regard to PADEP regulations, this currently includes providing a "Notice of Intent to Plug a Well" no less than 3 days and no more than 30 days prior to abandoning the well, to allow a PADEP inspector to be present during the plugging procedure. The PADEP may waive the notification period. The notification will include well location plat, well logs, production logs, injection logs, construction details, and proposed abandonment method. After receiving approval from PADEP to proceed, the well will be abandoned and the abandonment procedures will be documented on a "Certificate of Plugging".

The USEPA will be notified of the plugging activity at least 45 days prior to commencing activities. This notification will include USEPA Form No. 7514-20. A proposed plugging plan (Form 7514-20) is attached based on the current PADEP and USEPA regulations. However, this may be modified prior to plugging in order to meet the requirements at the time of the plugging activity. A contractor cost estimate to perform plugging and abandonment according to the proposed plugging plan is attached. The contractor estimate is approximately \$24,000 for these services.

PLUGGING AND ABANDONMENT PLAN

PLUGGING AND ABANDONMENT ESTIMATED COSTS



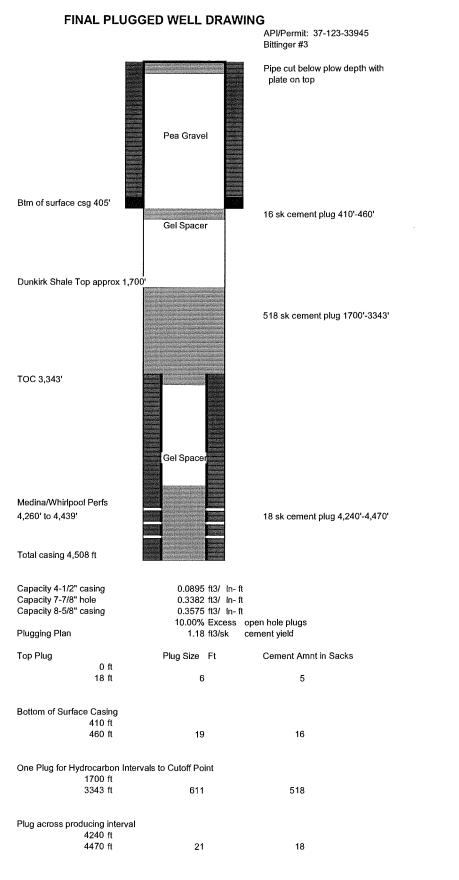
DLH Energy Service, LLC PO Box 40 5296 Bly Hill Road Ashville, NY 14710 Phone: 716-410-0204 or 716-410-0028 Fax: 716-526-4080 www.dlhenergyservice.com

03/18/2014		
Re: Plugging Estimate for the Bittinger 3 Well Columbus Twp PA		
Dear Sirs,		
The following is an estimate for the plugging to abandon the above mention	ned well.	
Rig Time: Two twelve hour days rig at \$215/hour, crew truck \$100/day, 4 th man 8 hou for laying down casing,	rs \$40/hr	\$5,680.00
Wire line servic <mark>e:</mark> Jet Cut 4 ½ casing:		\$2,500.00
Cement and pumping service: Up to 500 sacks cement and up to 140 bbls. Gel.		\$9,948.00
Water Hauling and Disposal: Delivery of fresh water and removal of returned fluid		\$855.00
Rentals: 500 bbl. Water tank and open top returns tank 5 day minimum		\$500.00
Support equipment: Dozer at 2 days		\$500.00
Trucking: mob and de mob dozer, excavator, water tank, open top, casing and tangibles (20 hrs)		\$1,900.00
Remedial Work Pea stone plug back with delivery, tank cleaning, excavating and cutting off surface casing, welding cap and monument, reclamation and seeding.	:	\$1,500.00
r	otal	\$23,383.00
If you have any questions, please feel free to contact me at (716) 410-1543	i,	
Best Regards, . <i>Bill Weaver</i>		
вill Weaver Operations Supervisor DLH Energy Service		

PLUGGING AND ABANDONMENT PLAN

EPA FORM 7520-14

<u>o</u> Ei	DA			Unite		nvironm shingto		Protection 2 20460	Agency						
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Section 10 – Necessary Resources

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Section 10 - Necessary Resources

Bear Lake Properties, LLC will establish the financial resources for the plugging and abandonment of the well prior to EPA's issuance of the public notice, draft permit and statement of basis for the well. A Certificate of Deposit will be filed under separate cover in the amount of \$24,000.

Section 11 – Plan for Well Failures

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Section 11: Plans for Well Failure

<u>General system design and monitoring</u>: The system being utilized for monitoring and control will function with the use of pressure switch gauges with adjustable limit switches and motor valves. The gauges provide a sensing device for changes in pressure conditions and if the limit switches are reached, they will send responses to activate motor valves controlling injection flow and pressure relief. In addition to the automated portion of the system, the manual operation of all pumping equipment as well as the continual inspections of the pumping and monitoring equipment provide additional safeguards for appropriate actions necessary in case of well failures.

<u>Injection Pressure Limit Monitoring:</u> The primary safeguard to prevent over pressuring is the automated shutdown on the pumping equipment at which the maximum operating pressure can be set as a limit at which all pumping will cease.

Additional switch gauges and motor valves will be utilized at the wellhead to monitor pressure changes that would be caused by tubing or casing failures and the appropriate valve will be activated to cease injection.

<u>Tubing and Packer Monitoring:</u> With the monitoring switch gauge connected to the tubing, we will have a secondary system to prevent over pressuring of the tubing. When the maximum pressure is sensed, a response is sent to a motor valve which will stop additional injection into the tubing.

<u>Tubing to Casing Annulus Monitoring:</u> This annular space will be monitored for both increase and decreases in pressure. The switch gauge will have both a low and high shutdown tab limit. When either of the limits is reached, the sensor will send a response to a motor valve shutting down flow. The lower limit will be used to monitor damage to the casing which allows fluid to leave the casing, and the high limit will sense a pressure increase in the casing that may be caused by communication with the tubing or flow into the annular space. Both of these limits when reached will send responses shutting down the injection cycle.

<u>8-5/8" Annular Monitoring:</u> The PADEP requires the annular valve on the 8-5/8" casing head to remain open to the atmosphere at all times. We will connect this point to a storage tank capable of collecting any fluid and allowing visual monitoring of any fluid flow. The valve and associated gauge will be monitored and inspected visually for changes or fluid flow. If such is detected, the system will be shut down and the remaining equipment associated with the system will be inspected to evaluate the cause of the changes.

Under the monitoring provided above, well failures will either be identified by the automated equipment and switch gauges or by visual inspection during injection operations or at other times. Should any failure occur, all injections will cease and proper notifications to EPA will be made. Analysis of the failure will take place and the

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necessary repairs to be implemented along with any equipment replacement will be coordinated with the EPA.

APPENDIX A

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SURROUNDING LANDOWNER INFORMATION

Landowners Within 1/4 Mile of the Bittinger #3 Well

	Pennsylvania Landowners								
PARCEL #	OWNER	ADDRESS							
2341	Bear Lake Properties, LLC	3010 Village Run, Suite 103, Wexford, PA 15090							
2361	Enos and Nettie Miller	1892 Cornish Hill Road, Bear Lake, PA 16402							
2382	Theodore G & Eloise R Smith	1655 Cornish Hill Rd, Bear Lake, PA 16402							
2633	John C. & Annaliese Wright	50 Long Branch Lane, Stafford, VA 22336							
3147	Ronald Craker et ux	1608 Cornish Hill Rd, Bear Lake, PA 16402							
3156	Jeffrey and Elizabeth McCray	1493 Cornish Hill Rd, Bear lake, PA 16402							
3198	Dennis G & Gail R Wright	1165 Cornish Hill Rd, Bear Lake, PA 16402							
23691	Theodore G and Eloise Smith	1655 Cornish Hill Rd, Bear Lake, PA 16402							
31752	Charlie H and Jenifer E Williams, Jr	1529 Cornish Hill Rd, Bear Lake, PA 16402							
31753	Jeffrey and Elizabeth McCray	1493 Cornish Hill Rd, Bear lake, PA 16402							
31763	Jeffrey and Elizabeth McCray	1494 Cornish Hill Rd , Bear lake, PA 16402							

New York Landowners							
PARCEL #	OWNER	ADDRESS					
448.00-1-24	Casper Goodrich	5 Weeks Rd Panama NY 14767					
448.00-1-25	Casper Goodrich	5 Weeks Rd Panama NY 14767					
449.00-1-5	Jackson Bemis	46 Weeks Rd Panama NY 14767					

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